PART I. A STUDY OF THE VELOCITY STRUCTURE OF THE EARTH BY THE USE OF CORE PHASES

PART II. THE 1971 SAN FERNANDO EARTHQUAKE SERIES FOCAL MECHANISMS AND TECTONICS

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ABSTRACT

The initial objective of Part I was to determine the nature of upper mantle discontinuities, the average velocities through the mantle, and differences between mantle structure under continents and oceans by the use of P'dP', the seismic core phase P'P' (PKPPKP) that reflects at depth d in the mantle. In order to accomplish this, it was found necessary to also investigate core phases themselves and their inferences on core structure. P'dP' at both single stations and at the LASA array in Montana indicates that the following zones are candidates for discontinuities with varying degrees of confidence: 800-950 km, weak; 630-670 km, strongest; 500-600 km, strong but interpretation in doubt; 350-415 km, fair; 280-300 km, strong, varying in depth; 100-200 km, strong, varying in depth, may be the bottom of the low-velocity zone. It is estimated that a single station cannot easily discriminate between asymmetric P'P' and P'dP' for lead times of about 30 sec from the main P'P' phase, but the LASA array reduces this uncertainty range to less than 10 sec. The problems of scatter of P'P' main-phase times, mainly due to asymmetric P'P', incorrect identification of the branch, and lack of the proper velocity structure at the velocity point, are avoided and the analysis shows that one-way travel of P waves through oceanic mantle is delayed by 0.65 to 0.95 sec relative to United States mid-continental mantle.

A new P-wave velocity core model is constructed from observed

times, dt/d\(^1\)s, and relative amplitudes of P'; the observed times of SKS, SKKS, and PKiKP; and a new mantle-velocity determination by Jordan and Anderson. The new core model is smooth except for a discontinuity at the inner-core boundary determined to be at a radius of 1215 km. Short-period amplitude data do not require the inner core Q to be significantly lower than that of the outer core. Several lines of evidence show that most, if not all, of the arrivals preceding the DF branch of P' at distances shorter than 143° are due to scattering as proposed by Haddon and not due to spherically symmetric discontinuities just above the inner core as previously believed. Calculation of the travel-time distribution of scattered phases and comparison with published data show that the strongest scattering takes place at or near the core-mantle boundary close to the seismic station.

In Part II, the largest events in the San Fernando earthquake series, initiated by the main shock at 14 00 41.8 GMT on February 9, 1971, were chosen for analysis from the first three months of activity, 87 events in all. The initial rupture location coincides with the lower, northernmost edge of the main north-dipping thrust fault and the aftershock distribution. The best focal mechanism fit to the main shock P-wave first motions constrains the fault plane parameters to: strike, N 67° (\pm 6°) W; dip, 52° (\pm 3°) NE; rake, 72° (67°-95°) left lateral. Focal mechanisms of the aftershocks clearly outline a downstep of the western edge of the main thrust fault surface along a northeast-trending flexure. Faulting on this

downstep is left-lateral strike-slip and dominates the strain release of the aftershock series, which indicates that the downstep limited the main event rupture on the west. The main thrust fault surface dips at about 35° to the northeast at shallow depths and probably steepens to 50° below a depth of 8 km. This steep dip at depth is a characteristic of other thrust faults in the Transverse Ranges and indicates the presence at depth of laterally-varying vertical forces that are probably due to buckling or overriding that causes some upward redirection of a dominant north-south horizontal compression. Two sets of events exhibit normal dip-slip motion with shallow hypocenters and correlate with areas of ground subsidence deduced from gravity data. Several lines of evidence indicate that a horizontal compressional stress in a north or north-northwest direction was added to the stresses in the aftershock area 12 days after the main shock. After this change, events were contained in bursts along the downstep and sequencing within the bursts provides evidence for an earthquake-triggering phenomenon that propagates with speeds of 5 to 15 km/day. Seismicity before the San Fernando series and the mapped structure of the area suggest that the downstep of the main fault surface is not a localized discontinuity but is part of a zone of weakness extending from Point Dume, near Malibu, to Palmdale on the San Andreas fault. This zone is interpreted as a decoupling boundary between crustal blocks that permits them to deform separately in the prevalent crustal-shortening mode of the Transverse Ranges region.

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PART I.

A STUDY OF THE VELOCITY STRUCTURE OF THE EARTH
BY THE USE OF CORE PHASES

1. INTRODUCTION

- 1.1 Development of the Study. Initially, the primary objective of this study was to determine the nature of upper mantle discontinuities, the average velocities through the mantle, and differences between mantle structure under continents and oceans by the use of the P'P' (PKPPKP) seismic core phase recorded at both single seismic stations and large-aperture arrays. It soon became apparent that the definition of the core phases was not sufficient to adequately accomplish the above goals. Thus, as an auxiliary to the study of the upper mantle, an investigation was made of core phases themselves and their determination of core velocity structure.
- 1.2 Motivation. The explosive increase of seismological data and research as a result of the VELA program during the last decade and the resulting jump in our knowledge of the earth's interior (as well as of seismic discrimination, the major goal of the program) is well documented. The establishment of a worldwide standard seismic station net (WWSS) and improvement of other seismic station nets has enabled the broad-frequency-band study of seismic phases from a single event over wide epicentral distance ranges; this has led to meaningful improvements in our definition of those phases. One of the most significant new techniques for seismological research that is a direct result of the VELA program is the use of large-aperture seismic arrays

to increase the signal-to-noise ratio and band-pass filter coherent energy in the wave-number domain. These developments have already led to a point in several areas of earth investigation too numerous to mention where improvement of earth-structure models can be confidently made over the classic investigations of Gutenberg, Richter, Jeffreys, Bullen, and Birch, which have withstood the test of time so well.

In the upper mantle, use of refracted body phases, surface waves, and normal modes of the earth to outline inhomogeneous velocity and density increases with depth has stimulated interest in investigation of the sharpness of these discontinuities. Reflections of seismic body waves, which have not been extensively used in the mantle, are well-suited to the study of sharp discontinuities because their steep incidence to the plane of the discontinuity gives them maximum sensitivity to the reflector depth and their mere existence puts fairly stringent limits on the reflector thickness. Possible reflections from the top of upper-mantle discontinuities were studied by Hoffman et al. (1961), Whitcomb and Anderson (1968), and Niazi (1969). A major difficulty with this type of phase is identification of a relatively low-amplitude reflection signal from other phases arriving after the first P wave on the seismogram. A convenient way around this problem is to use reflections from the underside of mantle discontinuities of the phase P'P' (PKPPKP); the deeper reflections arrive before the main surface reflection in a quiet part of the short-period

seismogram. This technique was first suggested by Gutenberg (1960) who noted arrivals up to 30 sec before P'P' and was later applied by Adams (1968), Whitcomb and Anderson (1968), Engdahl and Flinn (1969a), Whitcomb and Anderson (1970), and others. However, as with any newly discovered seismic phase, the uniqueness of its interpretation must be well-established and a possible source of misinterpretation was pointed out by Engdahl and Flinn (1969b) in their examples of the strong SKKKP phase as confirmed by Whitcomb and Anderson (1970). Another difficult challenge to uniqueness is posed by the maximum—time nature of the P'P' phase, which allows asymmetric reflections from the surface of the earth to arrive before the symmetric phase. It is therefore important to estimate the likelihood that asymmetric P'P' be misinterpreted as a deeper reflection.

Although the potential of P'P' as an accurate measure of earthquake depths and average velocity through the earth has long been
recognized (Gutenberg and Richter, 1934), scatter of the P'P' readings
has discouraged previous investigators from using the times for
anything more than an approximate check on results. However, once
the problem of core-phase branch identification and asymmetric P'P'
are resolved, the major source of scatter can be attributed to
multiple reflections from the ocean bottom and surface, and a meaningful
analysis of P'P' times can be done.

Study of the upper-mantle velocity discontinuities, their nature and depths, is an important tool for inferring the chemical and physical

state of materials at those inaccessible depths (for example, Anderson, 1967). Lateral variations, or their absence, of both the discontinuity depths and average velocities in the upper mantle have direct application to the problems of the chemical and thermal state of the mantle and the dynamic configuration of convection in the mantle which is required by the observed gain (at oceanic rises) and loss (at trenches) of the oceanic lithosphere. However, lateral variations, especially in oceanic areas, are a difficult seismological problem because almost all stations are located on continental structures and the few island stations tend to have high noise levels. P'P' phases are one of the few seismological data types that can remotely sample under oceanic areas with continental stations.

The core has been subjected to more variable interpretations than perhaps any other region of the earth's interior. The reasons for this lie mostly in the inaccessibility of the core not only in terms of physical location but in terms of seismic observability due to the sharp and profound drop in seismic velocity as one passes from the mantle into the core. Complications that arise from looking through this extremely distorting "lens" have only recently begun to be unraveled through the improved observation capabilities of worldwide station nets and the large-aperature seismic arrays. As a result, models of core structure are now beginning to converge to a point where their details may shed some light on the physical properties of materials in the core and, thus, the composition,

physical state, and dynamics of those materials. In particular, details that are emerging from core studies are the high velocity gradient in the outermost core, the low gradient just above the inner-core boundary, the small velocity jump at the inner-core boundary, and high gradient at the top of the inner core. In addition, certain core phases suggest that there are strong lateral variations in material properties near the core-mantle boundary.

One might fairly inquire as to the potential usefulness of our improved knowledge of core phases and core structure other than the obvious desirability of increasing our general knowledge of this remote portion of the earth. Three relevant areas that are at the forefront of current scientific investigation are immediate candidates. One is related to the basic origins of our earth. The investigation of lunar mineral samples has led to theories involving the composition of the primary solar-system material, formation of the planetary bodies, including the earth, and finally to specific predictions that can be tested about the nature and composition of materials of the core as they relate to this process (for example, Anderson and Hanks, 1972). Second is the phenomenon of periodic reversal of the earth's magnetic field. This process is almost certainly related to dynamics within the outer core, and the velocity gradients in this region may be crucial parameters in discovering the mechanism and critical conditions necessary for reversal. The third

is related to the burgeoning field of plate tectonics and a recent proposal that narrow plumes extending from the core-mantle boundary to the surface of the earth are at least a partial driving mechanism and configuration control for lithospheric plates, which dominate the location and rate of major earthquake occurrence. The latter two, involving magnetic reversals and major earthquake occurrence, have clear social implications dealing with the quality of life on the earth's surface.

1.3 Scope. Chapter 2 is essentially a review and minor revision of the Whitcomb and Anderson (1970) study of the P'P' phase and its precursors at single stations for reflections under the Atlantic-Indian rise south of the tip of Africa and the Ninety-East ridge in the Indian Ocean; a new set of data is included for reflections under the rift zone of Southeast Africa. The revision of the previous paper takes into account the developments of core structure that culminate in Chapter 6. Conclusions from Chapter 2 are delayed in favor of the more complete investigation of P'P' in Chapter 3.

Chapter 3 investigates the $dt/d\Delta$ of the P'P' phase and its precursors for ten events recorded at the LASA array in Montana. The reflection areas are under the East Indian ocean, ocean areas near the Atlantic-Indian rise and East Indian rise (classic spreading

centers), and the Antarctic continent. The depth variation, continuity, strength, and an approximate limit on the thickness of the discontinuities are discussed.

Chapter 4 estimates the likelihood that asymmetric P'P' phases that reflect from dipping interfaces near the surface of the earth are misinterpreted at P'P' reflecting at depth.

Chapter 5 investigates the causes of the large scatter observed for the main P'P' phase and resolves the scatter by using relative amplitudes, bathymetry data, the ocean-surface reflection, and the results of Chapter 6. The results are analyzed with respect to ocean bottom reflectivity, the effect of P tables on hypocentral locations and calculated P'P' times, and the implications of the observed P'P' times on average mantle velocities under continents and oceans.

Chapter 6 makes a new determination of core structure using recent advancements in identification of core-phase branches with large-aperture arrays, the Jordan and Anderson (1973) B1 mantle model which has a different velocity structure and core radius than those previously used, and improved knowledge of core-phase amplitudes. The inversion takes observations of times, $dt/d\Delta$, and amplitudes of core phases and constructs a consistent $dt/d\Delta$ data set as a function of distance for the core phases P^{\dagger} , SKS, and SKKS. The times of PmKP, where m is 2 or greater, are not used for the inversion because of the phase's maximum-time nature. The mantle times and distances

are stripped away using PcP and ScS (reflections from the core-mantle boundary) from the B1 model to get a dt/d\(\) curve corresponding to the surface of the core. The classic Wiechert-Herglotz integration method is applied to the curve to obtain P-wave velocity with depth in the core and the resulting velocity model is then checked and modified by P' and PKiKP absolute times. Finally, oceanic and continental mantle velocity differences, Q structure of the core, and scattering of core phases are discussed in relation to the final core velocity model and observed data.

2. P'dP' OBSERVED AT SINGLE STATIONS

2.1 Introduction. Recent models of the structure of the upper mantle, such as those of Anderson and Toksöz (1963), Niazi and Anderson (1965), Archambeau et al. (1969), Johnson (1967), Ibrahim and Nuttli (1967), Green and Hales (1968), Julian and Anderson (1968), Anderson and Julian (1969), and Jordan and Anderson (1973) include regions of high velocity gradient in the upper mantle. The sharpness of these discontinuities has led to new interest in looking for reflections of seismic waves from structures in the upper mantle. Hoffman et al. (1961), Whitcomb and Anderson (1968), and Niazi (1969) studied possible reflections from the upper surfaces of discontinuities in the upper mantle.

Another reflection of interest is the reflection of P'P' (PKPPKP) from the underneath surface of discontinuities as shown in Figure 2.1. This reflection has the decided advantage of being in a quiet part of the seismic record before the main P'P' phase. Gutenberg (1960) noted arrivals up to 30 sec before P'P' and Adams (1968) interpreted P'P' precursors as reflections arriving up to 70 sec before the main phase. Because Adams was using isolated stations for reading the precursors, he could not recognize that some of his readings for the deep earthquakes were probably SKKKP which has a different $dt/d\Delta$ as noted by Engdahl and Flinn (1969b). The remaining

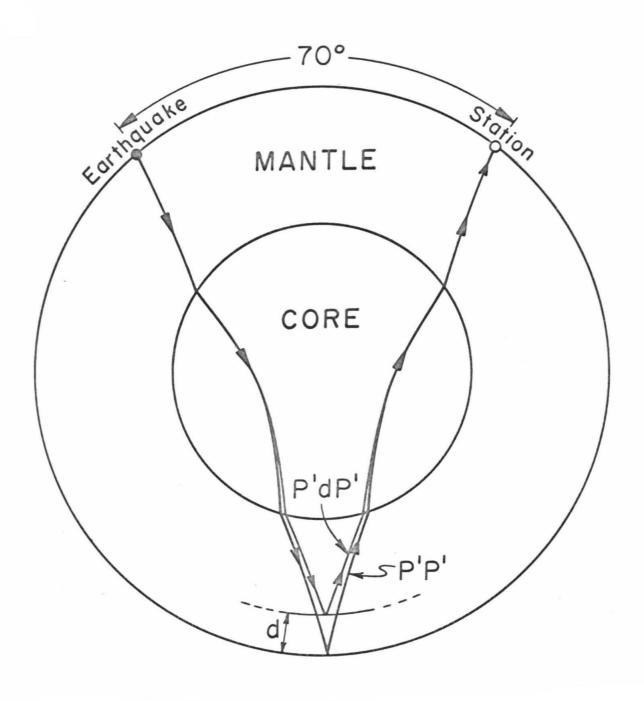


Figure 2.1

A schematic diagram of the P'P' and P'dP' phase ray paths through the earth.

readings of Adams indicated discontinuities near 65 to 70 km and 160 to 180 km in depth. However, as discussed in Chapter 4, all phases with lead times less than 30 sec from the main P'P' phase (an equivalent reflection depth of about 120 km) have an alternative explanation as asymmetric P'P' if only individual stations are used. Whitcomb and Anderson (1968) and Engdahl and Flinn (1969a) found a strong precursor with the proper dt/d\Delta that they interpreted as P'P' reflecting at a depth near 650 km. These phases are called P'dP', as defined by Whitcomb and Anderson (1970), and indicate a reflection of the P'P' phase at a depth d in kilometers. Thus, a reflection at 650 km would be P'650P', and P'0P' is equivalent to P'P'. In this and succeeding chapters, all core-phase branch nomenclature and calculations are based on the development of core structure in Chapter 6.

Whitcomb and Anderson (1970) systematically searched seismic records of individual stations for P'P' precursors up to five minutes before the main phase, estimated depths and strengths of reflectors in the upper mantle, and discussed their correlation with possible phase changes. They investigated two geographic regions of reflection: one near the Atlantic-Indian rise south of the tip of Africa, and the second near the Ninety-East ridge in the Indian Ocean shown in Figure 2.2. This chapter reviews and somewhat modifies their P'dP' results to account for recent advances in the knowledge of

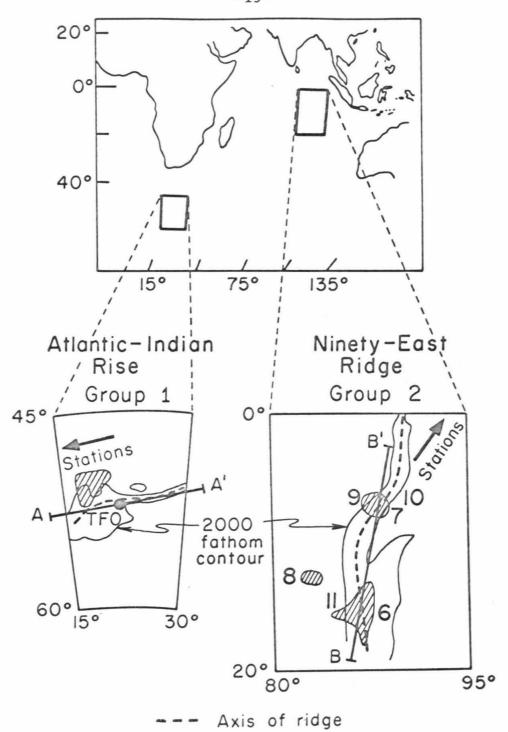


Figure 2.2

The regions of reflection of P'P' at the Atlantic-Indian rise and the Ninety-East ridge for the single-station data.

Areas of P'P' reflection

core structure that are developed in later chapters. The P'dP' single-station analysis is extended in this chapter to a new "continental" reflection area under the rift zone of Southeast Africa which allows us to compare results from oceanic mantle to continental mantle. Conclusions from the results of this chapter are deferred until they can be compared with the more complete analysis of P'dP' in the next chapter.

2.2 <u>Data</u>. The data were collected from short-period vertical seismometers located mainly at stations in Southern California as described in Whitcomb and Anderson (1970); some data were used from Central California and Arizona stations. Earthquakes from the Hokkaido region of the Japanese arc, reflecting under the Atlantic-Indian rise, and from South America, reflecting under the Ninety-East ridge, were used as seen in Figure 2.2; both areas are between 55° and 75° from Pasadena near the P'P' caustic where largest amplitudes are expected. The new events have reflection points under Southeast Africa for Southern California stations and are located at the northern Tonga trench. Table 2.1 shows the parameters for all events (from the USCGS bulletins) used for P'P' studies in this and succeeding chapters. The P-wave residuals at Southern California stations are less than one second.

The periods of the P'P' arrivals and precursors are generally

Table 2.1

Events used for P'P' studies.

146		Origin			Epicenter			
No.	Date	-	Time	Dep	th	Lat.	Long.	Mag.
1	05/31/64	0h	40m 36.	4s 48	km	43.5°	146.8°	6.3
2	06/23/64	1h	26m 37.	0s 77	km	43.3°	146.1°	6.2
3	06/11/65	3h	33m 44.	9s 47	km	44.7°	148.7°	6.0
4	10/25/65	22h	34m 24.	3s 180	km	44.2°	145.3°	6.2
5	01/29/68	10h	19m 5.	6s 40	km	43.6°	146.7°	7.0
6	11/03/65	1h	39m 2.	5s 583	km	-9.1°	-71.4°	6.2
7	05/11/67	15h	5m 16.	8s 67	km	-20.3°	-68.5°	6.1
8	09/03/67	21h	7m 30.	8s 38	km	-10.6°	-79.8°	6.5
9	12/21/67	2h	25m 21.	6s 33	km	-21.8°	-70.0°	6.3
10	12/27/67	9h	17m 55.	7s 135	km	-21.2°	-68.3°	6.4
11	06/19/68	8h	13m 35.	0s 28	km	-5.6°	-77.2°	6.6
12	05/16/68	10h	39m 1.	5s 3 3	km	41.5°	142.7°	7.0
14	11/09/63	21h	15m 30.	4s 600	km	-9.0°	-71.5°	7.2
15	11/07/68	10h	2m 5.	2s 0	km	73.4°	54.9°	6.0
16	10/14/69	7h	Om 6.	2s 0	km	73.4°	54.8°	6.1
18	02/28/69	4h	25m 36.	9s 33	km	36.2°	-10.5°	5.7
22	08/12/69	5h	3m 26.	9s 33	km	43.6°	148.0°	6.5
23	10/09/67	17h	21m 49.	5s 654	km	-21.1°	-179.3°	7.0

Table 2.1 (continued)

No.	Date	Origin Time	Depth	Epice Lat.	Long.	Mag.
24	02/17/67	10h 10m 51.5s	19 km	-23.7°	-179.3°	7.0
25	01/19/67	12h 40m 12.6s	18 km	-14.8°	-178.8°	6.7
26	05/21/62	21h 15m 30.0s	342 km	-19.8°	-177.4°	7.0
27	04/14/57	19h 18m 2.0s	32 km	-15.4°	-173.4°	7.5
28	09/15/54	17h 56m 9.0s	542 km	-17.8°	-178.6°	7.0

in the 1.5 to 3.0 sec range on the Benioff short-period vertical seismometers. Waves with periods as short as one second and as long as five seconds are seen, however. No systematic difference in period is noted between the main branches of P'P' and the early arrivals, and all arrivals from the same earthquake tend to have similar periods in this distance range; this is discussed in more detail later.

Records from the various stations were read independently without reference to each other or to a travel-time scale, and all of the readings were made by the authors in an effort to be completely systematic. The readings of P'P' and precursors were read to the nearest second and were graded according to the following confidence scale:

- 3 High; sharp pulse or a wave train with a sharp beginning.
- 2 Medium; emergent beginning but a definite signal, usually a wave train.
- 1 Low; small wave train with an emergent beginning; character (difference in period or amplitude) distinguishes it from the prevailing noise level.

Examples of seismograms with readings are shown in Figure 2.3.

In order to compare the P'P' data from different earthquakes, corrections were made for the earth's ellipticity and the focal depth of the earthquake in order to put the origin at the surface

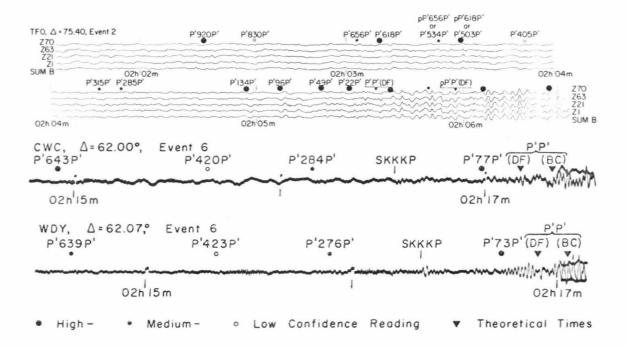


Figure 2.3

Short-period vertical records of P'P' and precursors from Events 2 (Tonto Forest Array) and 6 (stations CWC and WDY) with coded readings and theoretical main branch times.

of a standard spherical earth. The epicentral depth correction depends on which branch of P'P' is being considered because each branch has a different apparent slowness. Whitcomb and Anderson (1970) used the determination of the largest-relative-amplitude branch (the largest-amplitude branch on a single seismogram) from Adams and Randall (1964) as a function of distance. Subsequent investigations in Whitcomb (1971) and Chapters 5 and 6 have modified some conclusions about the relative amplitudes of the P' phases; and analysis of the original P'dP' data of Whitcomb and Anderson (1970), which is dependent on the relative amplitudes, will be altered slightly. They reasoned, as did Adams (1968), that the P'dP' phase observed on a single seismogram would be the same branch as the largest-relative-amplitude phase of P'P' for an equivalent core path. This assumption is based on the large and consistent amplitude differences observed for the branches of P' and P'P' (Adams and Randall, 1964; Whitcomb and Anderson, 1970; and Whitcomb, 1971) and is confirmed by the analysis of P'dP' using LASA in Chapter 3.

Once the determination of the proper branch for a reading is made, calculations can be done to correct the times and distances to a surface focus and calculate the depth d of the P'dP' phases as in Whitcomb and Anderson (1970). Due to the systematic reading of all phases on the record, it is necessary to identify as many

as possible of the phases other than P'P' and P'dP' and eliminate them from analysis. SKKKP, a phase identification by Engdahl and Flinn (1969b), is prominent in the recordings of Event 6 (Figure 2.2), and its $dt/d\Delta$ of 4.4 sec/deg easily separates it from the P'P' and precursor readings. pP'P', the near-source surface reflection of P'P', is seen and eliminated in a number of cases, and these are, except for Event 2, significantly smaller than the main phase P'P'. In Event 2 (a sample record is shown in Figure 2.2), the phase pP'P' is large with respect to the P'P' phase, and this leads to an ambiguity in identifying a precursor as pP'dP' or P'dP'. If both occur as reflections from a given depth, then the time difference between the pP'P' and P'P' phases should be the same as between pP'dP' and this possibility arises in Event 2. The Event 2 precursors in Figure 2.2 designated with a depth of 534 and 503 km could be the pP'P' reflections from 656 and 618 km which are seen approximately 23 sec earlier, the proper P'P'-pP'P' time interval for 77 km focal depth. This ambiguity is discussed later. Another phase that can be misinterpreted as P'dP' is asymmetric P'P' which, as discussed in Chapter 4, casts doubt on the interpretation of precursors less than 30 sec before the main phase for single-station analysis. Analysis of data in the 0 to 30 sec range is avoided in this chapter.

2.3 Ninety-East Ridge and Atlantic-Indian Rise Reflectors.

The Atlantic-Indian rise is a classical ocean-floor-spreading structure and is the continuation of the Mid-Atlantic rise into the Indian Ocean where it connects with the Mid-Indian rise. Study of the Ninety-East ridge (Francis and Raitt, 1967, and Le Pichon and Heirtzler, 1968) indicates that it is not a source of ocean-floor spreading but that it is some type of compressional feature with a thickening of the crust under the ridge. Distribution of the P'P' reflection points extends about 3° north of the Atlantic-Indian rise and about 5° west of the Ninety-East ridge as seen in Figure 2.2

Figure 2.4 from Whitcomb and Anderson (1970) shows the original zones of reflection proposed for the P'dP' data compared to velocity structures derived from various assumptions of mantle composition and phase changes. The revised interpretation of these data with the use of new core-phase information as developed in later chapters is represented in the histograms of Figure 2.5. The histogram is constructed by summing the weights of the readings at 20 km intervals and can be compared directly with the histograms in Whitcomb and Anderson (Figure 6, p. 5722). No significant change is made in the depths of the zones or their strengths as represented by the size of the sums. However, the data for the Ninety-East ridge have a somewhat larger scatter; also, the 20 km difference in depth originally proposed for reflection zones below 500 km and shown

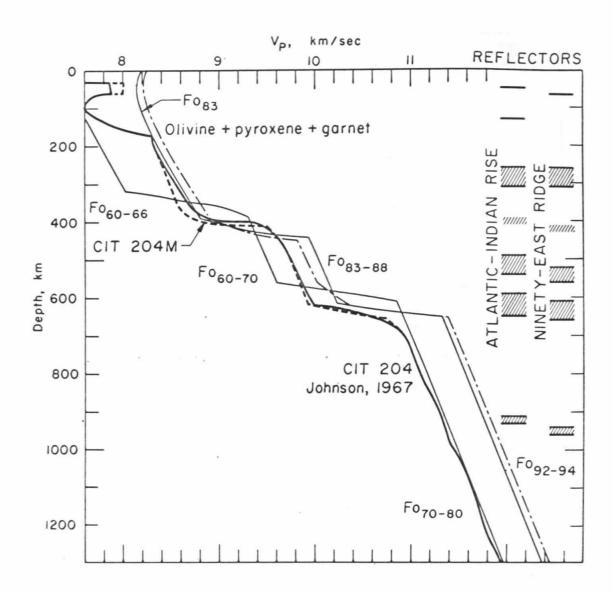
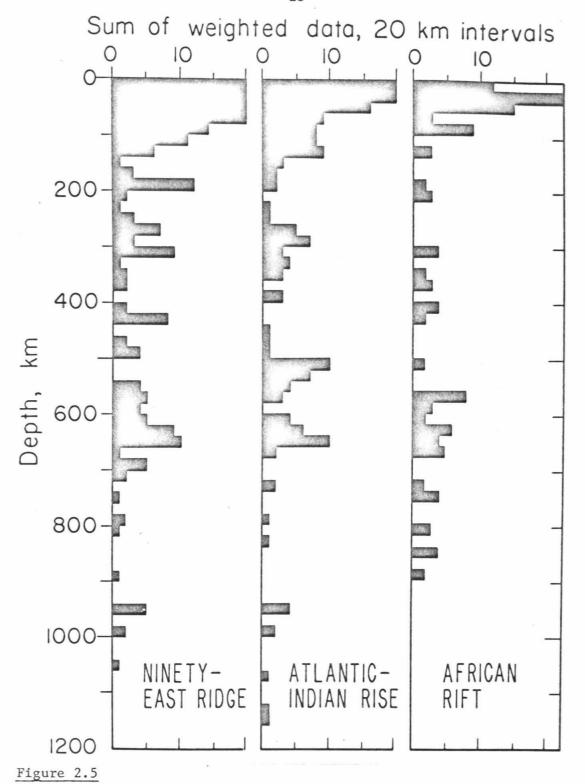


Figure 2.4

Comparison of reflecting zones with P-wave velocity models (CIT 204M and Johnson, 1967) and with calculated velocities of various mantle compositions (from Whitcomb and Anderson, 1970).



Histograms of the P'P' precursors interpreted as P'dP' as a function of depth for the Ninety-East ridge, Atlantic-Indian rise, and the African rift reflection areas. The summation interval is 20 km and the data are weighted by their confidence ratings as discussed in the text.

in Figure 2.4 is not as clear in the new data reduction of Figure 2.5. Figures 2.6 and 2.7 show the calculated depths of the precursor readings as a function of distance from the Atlantic-Indian rise and Ninety-East ridge (in Figure 2.2, perpendicular distance from lines A-A' and B-B', respectively). The Ninety-East ridge data extend over a greater distance and the reflectors appear to deepen to the west, especially in the depth ranges near 650 and 150 km. However, it is difficult to form any firm conclusions about the depth variation of these data in light of the possibility of asymmetric P'P' (Chapter 4). The possibility of depth differences is better evaluated in the following chapter where the use of array beam-forming methods resolves some of the uncertainties due to asymmetric phases.

The basic results from the Ninety-East ridge and Atlantic-Indian rise data are that arrivals strong enough to be read on single-station seismograms tend to group at specific depth zones when interpreted as P'dP'; the zones are near 950, 640, 520, and 820 km with marginal indications at 410 km as in Whitcomb and Anderson. The 630 zone is by far the strongest in terms of the number and strength of the phases. These zones have a one-to-one correspondence between the two areas which is significant when we consider that 1) the data are sampled from a narrow (Atlantic-Indian rise) and broad (Ninety-East ridge) range of epicentral distances, 2) the focal depths of the events vary widely, and 3) the P'P' phases for

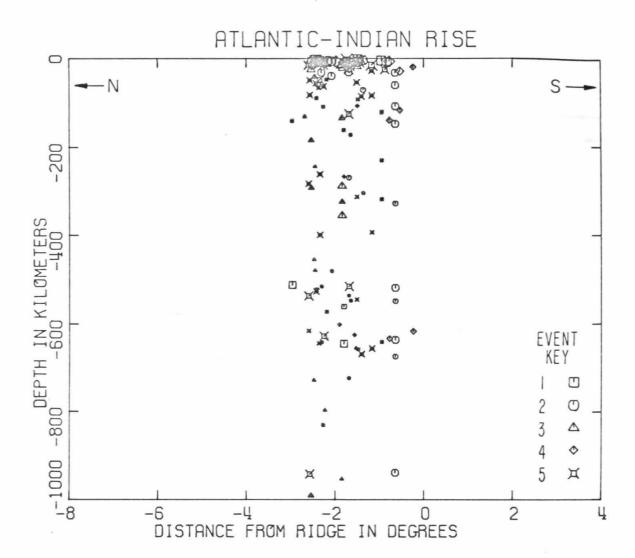


Figure 2.6

Atlantic-Indian rise P'dP' data plotted as a function of depth and distance from the rise (line A-A' in Figure 2.2). The size of the symbol indicates its confidence rating and the type of symbol indicates the event.

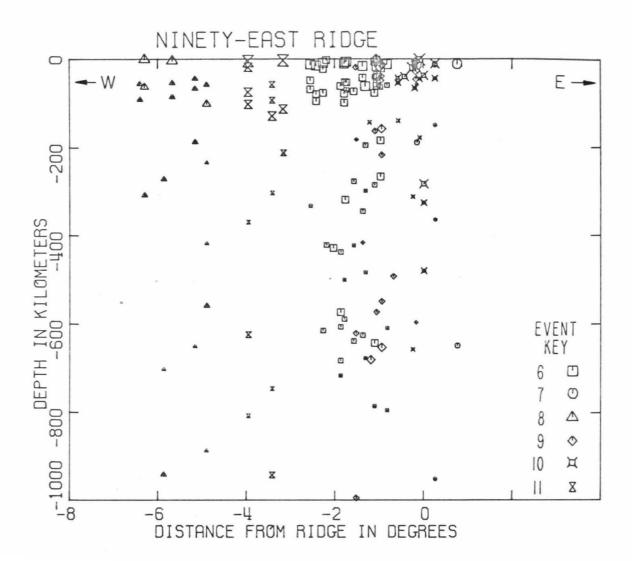


Figure 2.7

Ninety-East ridge P'dP' data plotted as a function of depth and distance from the ridge (line B-B' in Figure 2.2). The size of the symbol indicates its confidence rating and the type of symbol indicates the event.

each group reflect at widely separated locations on the earth. As mentioned previously, the interpretation of data corresponding to the 520 km zone is clouded by possibilities of their being reflections of secondary phases, such as pP'P', from the very large 640 km discontinuity. This problem has not been resolved as yet and may require another data type such as reflections from the top for a satisfactory answer. An outstanding exception to direct correspondence between the data of the two areas is the large histogram bar at about 190 km in the Ninety-East ridge data of Figure 2.5. It has no analogue in the Atlantic-Indian rise data and the difference may be significant in light of the results of Chapter 3.

2.4 <u>Southeast Africa Reflectors</u>. Figure 2.8 shows the Southeast-Africa reflection area for P'P' from events at the northern trench. The epicenters of earthquakes in the African continent, shown for the time 1961-1969 (Anonymous, 1970), outline the African rift system, a broad and not too well defined seismic feature in the area of the reflections. Figure 2.5 shows the data interpreted as P'dP' in histogram form as a function of depth. The outstanding zone is again in the 630 km range as for the previous two areas shown in the same figure. There are some readings between 300 and 410 km that stand out principally because of the lack of data just above and below this range. Data deeper than 700 km are spread

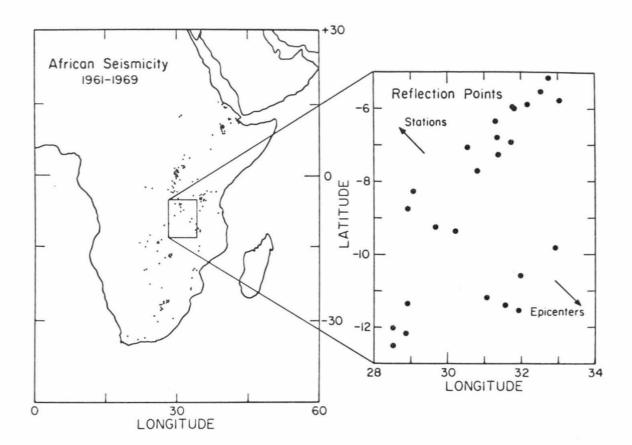


Figure 2.8

The regions of reflection of P'P' at the African rift zone in Southeast Africa for the single-station data.

between 720 and 900 km but no deeper points are seen similar to the 950 km zone of the previous data set. Readings also concentrate in the depths between 500 and 600 km but the same difficulties of interpretation are present as discussed previously. However, the depth distribution in this range is more like the Ninety-East ridge data than that of the Atlantic-Indian rise, an important consideration if the 520 km reflector can be shown to exist. Thus, the African rift data set, although it has fewer readings than the Atlantic-Indian rise or the Ninety-East ridge data sets, is more like the latter in its depth distribution.

- 3. P'dP' OBSERVED AT THE LASA ARRAY: REFLECTOR CONTINUITY AND SHARPNESS
- 3.1 Introduction. The previous studies of P'dP' (Adams, 1968; Whitcomb and Anderson, 1968; Engdahl and Flinn, 1969a; and Whitcomb and Anderson, 1970; and others) point out the need for direct and accurate dt√d∆ measurement of the phases with a large-aperture array such as LASA in Montana. Use of a large array enables one to greatly improve the signal-to-noise ratio of coherent arrivals by beamforming and also to identify the proper branch of the arrival; the latter is an important consideration when calculating the depth d of P'dP'. Further, the observation of coherency across the array, which has an aperture of about 200 km, is some measure of continuity of the reflecting zones and this property is useful both here and in Chapter 6.

This chapter investigates the $dt/d\Delta$ of P'dP' phases from ten events recorded at LASA that pertain to the mantle under a wide range of surface-structure types. Four reflect under deep-oceanic structure near the Ninety-East ridge in the East Indian ocean; four reflect under oceanic structure that is near classic crustal-spreading rises; and two reflect under the Antarctic continent. The results confirm that the dominant P'dP' energy is from one branch which is the largest-amplitude P'dP' branch as assumed in Adams (1968),

Whitcomb and Anderson (1968 and 1970), and Chapter 2. The lateral continuity and strengths of the reflectors are estimated along with some approximate limits on their structures.

3.2 P'dP' Recorded at LASA. Figure 3.1 shows the P'dP' reflection areas with event numbers (parameters are given in Table 2.1) and symbols used in succeeding plots in this chapter. Events 5, 12, and 22 are 800 km south of the Atlantic-Indian rise (indicated by earthquake seismicity from Barazangi and Dorman, 1969) and Event 18 is in a corresponding position just 300 km south of the East Indian rise. Events 8, 9, 10, and 11 are all to the east of the Ninety-East ridge in the East Indian ocean which is an area of deepoceanic structure. Events 15 and 16, which are from Novaya Zemlya explosions, reflect under the Antarctic continent.

The processing of the P'dP' phases at LASA is schematically illustrated in Figure 3.2. The P'dP' phase arrives at the array from a direction opposite from that of the event epicenter. The time series from the seismometers are filtered and summed for the direction of arrival at different slownesses or $dt/d\Delta$'s (the inverse of apparent velocity) to form beams. Each beam corresponds to a given value of $dt/d\Delta$. The power of each beam is then averaged over discrete time intervals (a one-second interval is used here) and the contours of equal power are constructed from several beams

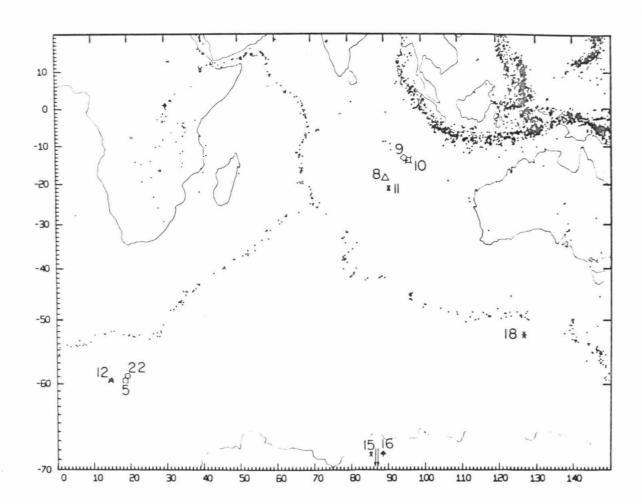


Figure 3.1

P'dP' reflection areas studied with the LASA array. Event numbers correspond to the event data in Table 2.1 and the associated symbols are used in succeeding plots in this chapter.

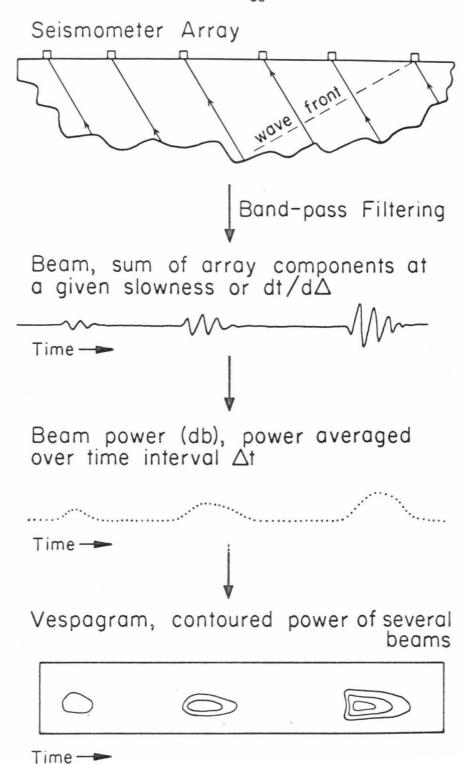
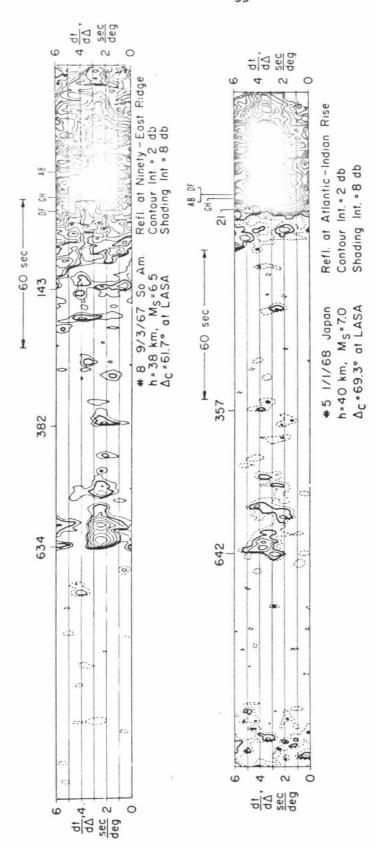


Figure 3.2

A schematic representation of the array processing involved in construction of a vespagram.

placed side by side. The result is a contour plot of coherent seismic-phase power as a function of dt/d\(^\Delta\) and time for a given azimuth of arrival; the procedure is termed a "vespa" process (velocity spectrum analysis) and the diagrams are called "vespagrams". Descriptions of the process and interpretations of vespagrams are in Kelly et al. (1968) and Davies et al. (1971). The problems of complex travel-time anomalies at the LASA sub-arrays have essentially been circumvented for beam-forming at the periods used here (about 1 to 3 sec) by extensive calibration of the relative sub-array travel-time anomalies such as the work of Engdahl and Felix (1971). Further, the results of Chapter 6 indicate that, except for arrivals from the south, calibration of LASA is quite adequate for core phases.

Figure 3.3 shows two examples of vespagrams for Events 8 and 5. Time increases to the right and dt/dΔ increases upwards. The power contours are at 2 db intervals with shading changes every 8 db or 4 contours. The heavy contour is a subjective judgment of the first contour above the noise level which is based on the early, quiet portion of the record; thus, power at or above the heavy contour level is considered to be signal of some type. The predicted times of the main P'P' phases are shown to the right above the vespagrams and the maximum power approximately corresponds to these times as expected. Event 8 is at an epicentral distance of 61.7° which predicts that the first branch should be DF at about 1.7 sec/deg, then the largest



Theoretical main branch times Vespagrams for Events 8 and 5.

Figure 3.3

and depths d of the P'dP' readings are shown.

branch BC at 2.7 sec/deg, and finally AB at 4.1 sec/deg as seen for the main phases in the travel time chart in Figure 3.4. These are all seen in the vespagram at their proper $dt/d\Delta$'s. Event 5 is at 69.3 where all three branches arrive within a few seconds of each other. Here the the dominant amplitude is that of the AB branch with its $dt/d\Delta$ near 3.5 sec/deg.

The outstanding phase at times earlier than the main P'P' phases stands out clearly for both events in Figure 3.3 about 2.5 min before the main phase. This is the P'640P' phase as interpreted by Whitcomb and Anderson (1968), Engdahl and Flinn (1969), Whitcomb and Anderson (1970), and others. It clearly has the most power of all the P'dP' phases studied thus far. The branch of the P'640P' phase is completely predictable on the basis of the maximum-amplitude ranges defined in Chapter 6. In Event 8, for example, only the BC branch of P'640P' is seen even though both the AB and DF branches are seen in the main P'P' phase. This is, of course, not precisely the case at distances where the maximum-amplitude change takes place from one branch to another but it is a good approximation between almost the entire range of 55° to 85° used in the interpretation of single-station data in Chapter 2. The $dt/d\Delta$ and, thus, bottoming depth in the core of a P'dP' phase is not the same as that of the main P'P' phase at a given station. However, for most cases they are nearly the same so that the branch with the maximum main phase amplitude is the branch with the maximum P'dP' amplitude with nearly the same dt/dA. Thus,

to pick the P'dP' phases usually means simply to follow the $dt/d\Delta$ of the maximum-amplitude main phase backwards in time until significant power peaks are seen.

Picks of the onset of peaks read in the above manner are shown in the travel-time plot of Figure 3.4. The symbols represent events used and are keyed in Figure 3.1 and Table 2.1. The symbol size represents the confidence of the reading as in Chapter 2, and the slopes through the data points indicate the measured dt/d\(\Delta \). The readings of P'dP' at a given station are all uniformly from a single branch with the exception of two readings near 76° that have dt/d\(\Delta \)'s more like that of the AB branch than that of the DF branch used for calculations in this range. This duality is a result of being on the border where the largest-amplitude branch is switched as discussed above. These two points were not used for depth calculations. The time range approximately 30 sec before the P'640P' phase is avoided in the readings due to the problems of identification mentioned in Chapter 2. Significant arrivals are noted here but their interpretation is difficult at present.

The depths of the P'dP' phases are calculated as in Chapter 2 and are shown in Figure 3.5 for the ten events. The P'640P' zone is the most consistent in terms of depth of onset and strength. Only two readings are deeper than this level. A reading near P'640P' was not picked for Event 10 (crossed-square symbol) but a second more objective

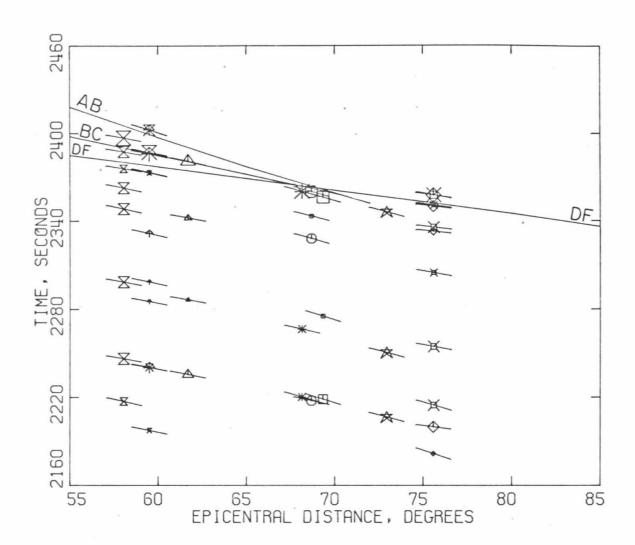


Figure 3.4

Travel-time plot of vespagram P'dP' readings with sloping lines to indicate measured $dt/d\Delta$. The size of the symbol indicates its assigned confidence rating. The theoretical main P'P' times are shown for reference.

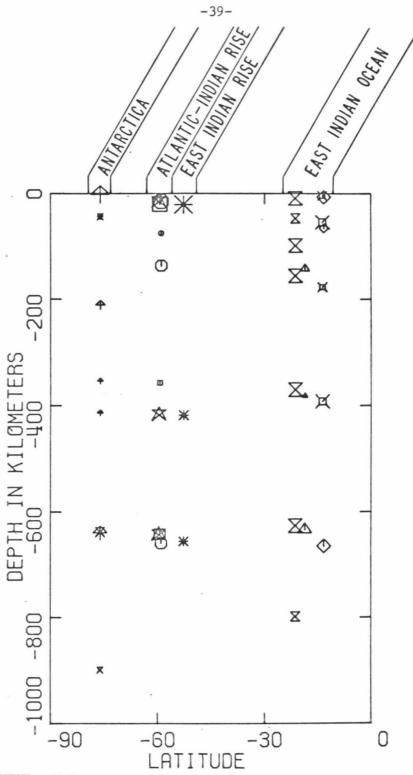


Figure 3.5

Calculated depths of the LASA-vespagram P'dP' readings from Figure 3.4 as a function of latitude (see the map of Figure 3.1). method of phase identification outlined later does pick a phase in this zone. The onset of the P'640P' reflection is at 640 km for the two events reflecting under Antarctica, between 640 and 660 km for the four reflections near oceanic rises, and between 630 and 670 km for the four reflections under the East Indian ocean. All readings are omitted between the 640 km zone and about 500 km due to the problems of interpretation as discussed above. The next shallower level of readings is a zone between 360 and 410 km; under Antarctica and the rises, the readings are at the extreme depth ranges of this zone, and under the East Indian ocean they are in the middle of the range. Above 360 km, no readings are seen until about 200 km under Antarctica, 140 km near the Atlantic-Indian rise, and 140 to 180 km under the East Indian ocean.

Because of the subjective manner in which the significance of the power peaks is determined, a second method of picking phases is used. It was noted that all of the obviously significant arrivals have very sharp onsets, that is, the time derivative or onset slope of the proper power beam (see Figure 3.2) is large. Therefore, a criterion was developed whereby all onsets with a power slope or time derivative that exceeds a certain value are picked; the critical value was determined by the characteristics of the noise. Figure 3.6 shows the data points picked with this method plotted as a function of depth in the same manner as in Figure 3.5. The length

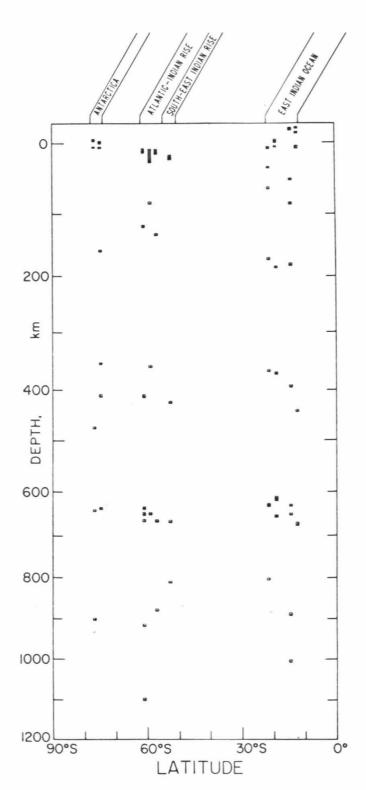


Figure 3.6

Calculated depths of the LASA-vespagram P'dP' phases read by the power-slope method described in the text. The event numbers are, from left to right; 15, 16, 12, 5, 22, 18, 11, 8, 10, and 9.

of the points is a measure of the time that the slope exceeds the critical value. Use of this method does not significantly alter the data for the 640 zone but adds a reading for Event 10 that was not picked with the previous method. The onset of the P'640P' reflection is at about 640 km for the two reflections under Antarctica, between 640 and 670 km for the four reflections near rises, and between 635 and 675 km for the four reflections under the East Indian ocean. The previous readings between the 360 and 410 km range are essentially unchanged but two new points are added for Events 15 and 9 near 470 and 450 km, respectively. Above 360 km, the depths of the readings are changed somewhat to about 160 km under Antarctica, 130 km near the Atlantic-Indian rise, and 180 km under the East Indian ocean; the rise points are still shallower than the other two areas. One significant difference in Figure 3.6 from the previous method of reading of Figure 3.5 is that more points are picked below the 640 km zone. All but two are approximately between 800 and 900 km deep.

3.3 Sharpness of the 640 km Discontinuity. The work of Richards (1971) and others have shown that a reflection amplitude more than about 3% requires a material property change that takes place over a distance that is less than one-half of a wavelength. Thus, the mere observation of a reflection with amplitudes larger

than 3% of the incident wave from a velocity discontinuity implies that the discontinuity is limited in thickness to less than onehalf wavelength. Figure 3.7 shows an example of a P'601P' phase from the BC branch and the corresponding main phase. Both phases have a period very close to one second and the amplitude of the precursor is about 10% of the main phase, which is similar to the ratios reported by Engdahl and Flinn (1969), Whitcomb and Anderson (1970), and others. Although, amplitude comparisons with the main phase are difficult to interpret due to the generally unknown complexities of near-surface structure and asymmetric P'P' as discussed in Chapters 4 and 5, it is clear that the reflection from the P'640P' zone is larger than 3% of the incident wave. Thus, this single example implies that a velocity-density discontinuity of the order of 8% is required over a depth interval less than 5 km (for calculations, see Whitcomb and Anderson, 1970). A smaller jump in material properties would be required if the discontinuity were a series of alternating layers that caused constructive interference of the reflecting wave. However, this type of reflector would be strongly frequency dependent. Figure 3.8 shows power spectra of a LASA beam of the BC branch of P'P' and P'630P' from Event 8. The phases have a dominant period of about 2 sec and no significant difference is seen between the two between periods of 1 to 2 sec (1 to 0.5 hz). This result effectively rules out the constructive

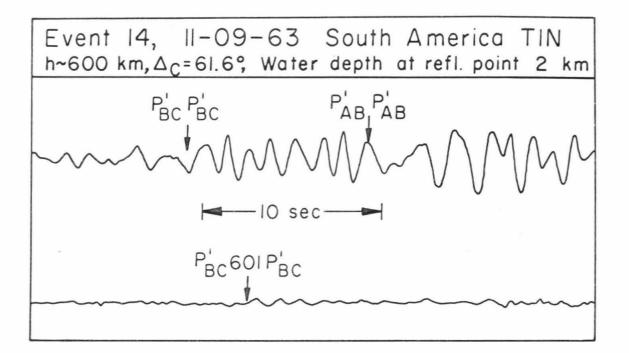


Figure 3.7

Comparison of the main P'P' phase with P'601P' at a single station. Both have nearly identical periods (about 1 sec) and the P'601P' amplitude is about 10% of that of the main phase.

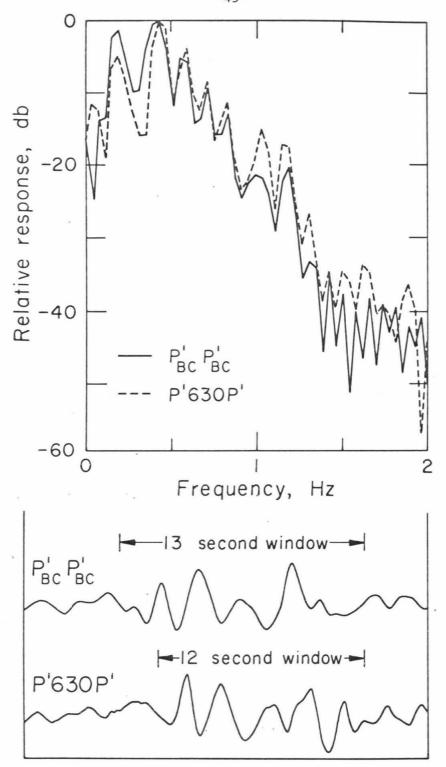


Figure 3.8

Comparison of the power spectrum of the main P'P' phase with that of P'630P' at LASA for Event 8. The dominant energy is at 2 sec (0.5 hz) and there is essentially no difference in relative spectral content between periods of 1 and 2 sec.

interference hypothesis because no difference is seen in reflectivity for a continuous range of wavelengths from 10 to 20 km.

3.4 <u>Conclusions</u>. Possible mantle discontinuities that reflect short-period seismic energy and produce P'dP' phases are reviewed in the order that they appear on the seismogram; that is, from the deepest to the shallowest zones.

800 to 950 km. Only scattered readings are present below 700 km and these tend to concentrate in the 800 to 950 km range. Single station data favor 950 km and the vespagram data interpreted by the power-slope method described above range between 800 and 900 km.

both single stations and in array beams and the reflection is present at every site studied thus far including normal deep oceans, oceanic and continental spreading centers, and continents. Evidence from comparison of the spectral contents of the reflection and the main P'P' phase from the same branch leads to the conclusion that the discontinuity must be a monotonic change in material properties of the order of 8% that occur over a depth range of 5 km or less. The maximum depth range of the onset (bottom edge) of the reflector is about 630 to 670 km as measured by the vespa process; this method is least susceptible to problems of asymmetric P'P' as discussed in Chapter 4. This 40 km depth range corresponds to a time range of 8 sec on the seismogram.

Reflections under the Antarctic appear to be 20 km shallower than those under the oceanic rise areas. The maximum scatter of depths is seen in the East Indian ocean region from vespagram data and this is supported by the scatter of data for the same region from single station data in Chapter 2 (Figures 2.5 and 2.7). Although the depth differences appear to be consistent at the different areas, it is probably premature to rule out the likelihood that the discontinuity is at the same depth everywhere and the ± 20 km (± 4 sec) variation is due to a combination of reading errors, lower-mantle velocity variations, and source complexity. The contribution due to reading errors should be no more than ± 1 sec and that due to different lower mantle velocities should be also no more than ± 1 sec.

500 to 600 km. A strong grouping of arrivals equivalent to P'dP' for this depth range is present in both the single station data for the Atlantic-Indian rise at 520 km in Chapter 2 (Figures 2.5 and 2.6). However, it is difficult to interpret these data as P'dP' because it is possible that the arrivals represent delayed near-source-related phases that are reflections from the strong 640 km discontinuity. The problem is not resolved here and its solution must be reserved for later investigations.

350 to 415 km. Data for this zone are more consistent in the vespagram analysis of this chapter than from the single station readings in Chapter 2. This may be evidence that the reflecting

discontinuities in this range are very close to horizontal but their reflection coefficients are small. Thus, their P'dP' phases across a large array such as LASA are very coherent which allows the beamforming process to fully utilize its signal-to-noise improvement capabilities and bring out arrivals that are too weak to be regularly observed in the noise level of a single station.

280 to 300 km. Evidence for a discontinuity at this level comes solely from the single-station data of Chapter 2; a fact that somewhat weakens confidence in its existence. However, its absence in the vespagram readings may indicate that, although it is strong enough to give reflections, the discontinuity is not horizontal and varies in depth so that its P'dP' reflections are not coherent across a large array. Indeed, evidence for precisely this effect is seen in the vespagram for Event 8 in Figure 3.3. For times later than the indicated 382 km reading, energy peaks appear to diverge from the proper dt/dΔ for P'dP' (about 2.5 sec/deg) towards both higher and lower values of dt/dΔ. This energy may represent asymmetric P'dP' phases reflecting from non-horizontal discontinuities and suggests that spherical symmetry is absent above a depth of about 350 km.

100 to 200 km. Further evidence for lack of spherical symmetry in the mantle above 350 km comes from depth variations of reflections in the range of 100 to 200 km, especially from the vespagram data which have no readings from 350 km until this level. East Indian Ocean and Atlantic-Indian rise data indicate strong reflections

at 190 km and 130 km, respectively, in both the single-station readings (Figure 2.5) and the vespagram readings (Figures 3.5 and 3.6). The Antarctic continent data show a reflection from 160 to 200 km depending on the method of reading the vespagrams. these reflections are from the same discontinuity, a conclusion that has some support from the observation that they are the first vespagram readings above 350 km, then a strong candidate for the cause of the discontinuity is the bottom of the low-velocity zone. Anderson and Sammis (1970) have shown that partial melting is the most likely cause of the low-velocity zone and this puts some limitations on conditions between 100 and 200 km for the different areas by the nature of the discontinuity depth variation. depth of the lower boundary of partial melting is strongly dependent on both rock temperature and content of volatiles such as water; both an increase of temperature or an increase of volatile content will increase the depth of the lower partial-melt boundary. The boundary appears shallowest near oceanic rise areas which, if the temperature hypothesis were adopted, would imply that temperatures near 150 km are colder beneath rises than elsewhere. A model that produces this situation is unlikely, especially in the framework of plate tectonics concepts. Thus, the most attractive hypothesis is that volatiles are depleted in the upper-most mantle near the Atlantic-Indian rise relative to that under continental or older oceanic crustal areas. An alternative explanation for a

discontinuity depth that is shallower near oceanic spreading centers is a solid-solid phase change. If the phase-change depth dependence is entirely due to temperature differences and temperatures under the rise are higher, then a negative-phase-equilibrium slope is required.

4. ASYMMETRIC P'P'

4.1 Introduction. Precursors up to 30 seconds before P'P'
(PKPPKP) were first noted by Gutenberg (1960) and were interpreted
as sub-surface reflections. Later authors including Adams (1968),
Engdahl and Flinn (1969a), Whitcomb and Anderson (1970), Whitcomb
(1971), Adams (1971), and Richards (1972) have made studies of
these and earlier precursors based on the same interpretation that
they are reflections within the upper mantle, i.e., P'dP' (as defined
by Whitcomb and Anderson, 1970) where d is the depth of reflection.

This new data type is important because it can give details of upper mantle structure heretofore unavailable, and provides one of the few means at hand for comparison of mantle structure under different lithospheric regions such as continents and oceans. However, as with any newly discovered seismic phase, the uniqueness of its interpretation must be well established. A violation of this uniqueness was pointed out by Engdahl and Flinn (1969b), who showed that the phase SKKKP for deep earthquakes occurs in the same part of the travel-time curve and could be mistaken for P'dP'. This problem is eliminated by avoiding readings at the time of SKKKP at a single station, or by using the difference in dt/dA between SKKKP and P'dP' at an array of stations.

A much more difficult problem is posed by the maximum-time nature

of P'P' phases discussed by Jeffreys and Lapwood (1957) and later by Richards (1972) and Wright (1972). Asymmetric P'P' phases reflecting from dipping interfaces at or near the earth's surface would arrive earlier than the main phase for all branches except for a special path of the AB branch. This chapter deals with the estimation of asymmetric P'P' amplitudes and, therefore, the likelihood that these phases be misinterpreted as P'dP'.

4.2 Asymmetric Reflections of P'P'. P'P' is a true maximumtime phase with the exception of the receding AB branch. Specifically,
if P'P' reflects from any non-horizontal surface of the earth at
a non-symmetrical point, it will arrive earlier than its symmetrical
counterpart. This is not true for the receding AB branch reflecting
on the station-epicenter great circle; the AB branch is thus a
"mini-max" phase (in the reverse sense of the phase PP for which
symmetric reflections on the great circle arrive earlier). It will
be seen, however, that asymmetric reflections off the great circle
are most important and for our purposes the AB branch is effectively
a maximum-time phase.

For convenience of calculation, asymmetric P'P' reflections are divided into two types as shown in Figure 4.1: those in the great circle plane and those out of the great circle plane reflecting at points on a line that is perpendicular to the great circle and passes through the symmetrical reflection point. Of course, any

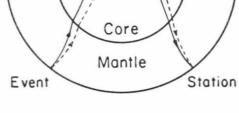
P'P' Asymmetric Reflection Types
In Great Circle Plane (full view)

Out of Great Circle Plane (side view)

Mantle

Core

Event Station



— Symmetric Ray ---- Asymmetric Ray

Figure 4.1

Asymmetric reflection types: in the great circle plane, and out of the great circle plane. Symmetric rays are shown for reference.

combination of these two types is permitted. The symmetric ray is shown in each case in Figure 4.1. In all of the calculations, the non-horizontal reflector is assumed to be at or very near the earth's surface where the largest reflection amplitudes are expected. The reflectivity coefficient of the Moho (Mohorovičić discontinuity) is about 0.14 (Whitcomb and Anderson, 1970). This reduces the amplitude almost to the 10% cutoff used below and the asymmetric reflection from this interface is probably not important. The most likely candidates for asymmetric reflectors are a non-horizontal ocean bottom or land surface; the former's reflectivity can be as high as 0.8 and the latter's is 1.0. Therefore, no reduction in amplitude is made for asymmetric phase reflectivity coefficients because they may be equal to that of the symmetric phase.

Another possibility for the generation of asymmetric P'P' phases lies in the distortions of $dt/d\Delta$ produced by inhomogeneities in the upper mantle. A good example is a cold lithospheric slab sinking into the mantle attrench areas. However, the calculations of Julian (1970, Figure 4.2) show that, for such a complex structure, the anisotropy scatters the rays too severely to reflect from the surface a second core phase of significant amplitude. Broader anisotropic structures in the upper mantle might be more effective in evenly distorting a large cone of P'P' energy, but calculations of this effect must await a better understanding of broad lateral variations

in upper mantle structure.

4.3 Observed Amplitudes. Figure 4.2 shows schematic traveltime curves of the branches of P'P' and P'dP. The relative amplitudes (amplitudes relative to the DF branch) of the P' branches have been calculated from the results of Chapter 6 with a mantle Q of 2000 and a core Q of 2200 and are shown in Figure 4.3. The actual amplitude data scatter by as much as ± 50% from these curves. However, the P' amplitudes contrast so markedly as a function of distance and the branch, that useful predictions can be made of relative amplitudes (that is, amplitude ratios on the same seismogram) of specified rays.

The P'P' precursor amplitudes are 30% to 50% of the main P'P' phase at lead times of 0 to 30 seconds and 10% to 20% of the main phase at lead times greater than 30 seconds (Whitcomb and Anderson, 1970). We initially assume, and later justify, that only the 0- to 30-second precursors are candidates for asymmetric P'P'. Therefore, we can define a likelihood criterion as follows: when the asymmetric P'P' amplitudes fall below 10% of the theoretical symmetric phase, they are too small to be identified as readings. That is, when the calculated asymmetric P'P' amplitudes fall below one-third of the smallest actual readings in that time-window, we conclude that the readings are not asymmetric P'P'.

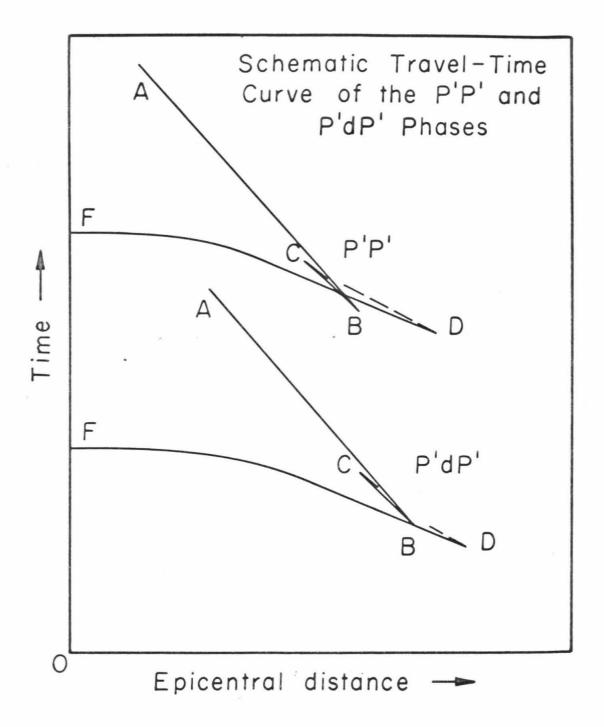


Figure 4.2

Schematic travel-time curves of the branches of P'P' and P'dP'.

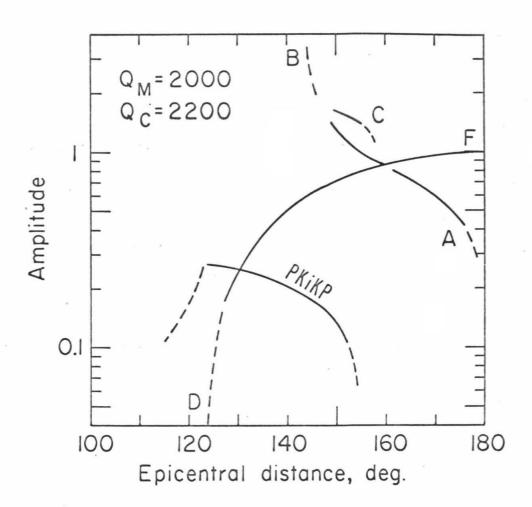


Figure 4.3.

Amplitudes of the branches of P' calculated from the model of Chapter 6 and normalized by the DF branch at 180° epicentral distance. A Q of 2000 was used for the mantle and 2200 for the core.

4.4 Theoretical Amplitudes of Symmetric P'P'. Because the amplitudes of P'P' are not as well known as those of P', we translate P' into symmetric P'P' amplitudes for use as comparisons. From Bullen (1963, p. 127), the energy density due to geometrical spreading of a seismic ray at the earth's surface can be written in the form

$$E(\Delta) = \frac{Bf}{\sin \Delta} \left| \frac{d^2T(\Delta)}{d\Delta^2} \right|$$
 (4.1)

where B is a constant, f is a function depending mainly on emergence angle, T is the travel time, and Δ is epicentral distance.

Suppose now that $T_1(\Delta)$ corresponds to P' of the DF branch; for a surface focus $T_{11}(2\Delta)$ corresponds to P'P' of the same branch. From symmetry we can write

$$T_{11}(2\Delta) = 2T_1(\Delta) \tag{4.2}$$

or, defining $\Delta' = 2\Delta$, (2) becomes

$$T_{11}(\Delta') = 2T_1(\Delta)$$
 (4.3)

Then, differentiating twice with respect to Δ ', we have

$$\left| \frac{d^2 T_{11}(\Delta')}{d(\Delta')^2} \right| = \frac{1}{2} \left| \frac{d^2 T_1(\Delta)}{d\Delta^2} \right| \tag{4.4}$$

The energies for the P' and P'P' phases, DF branch, are then, from equation (4.1),

$$E_{1}(\Delta) = \frac{B_{1}f_{1}}{\sin \Delta} \left| \frac{d^{2}T_{1}(\Delta)}{d\Delta^{2}} \right|$$
 (4.5)

and

$$E_{11}(\Delta') = \frac{B_1 f_{11}}{\sin (2\Delta)} \frac{1}{2} \left| \frac{d^2 T_1(\Delta)}{d\Delta^2} \right|$$
 (4.6)

respectively; where again Δ corresponds to the P' epicentral distance and Δ ' to the P'P' distance for the same part of the branch.

The energy expression (4.5) and (4.6) can be related to amplitude by (Bullen, 1963, p. 128)

$$E = \frac{2\pi^2 \rho \lambda a^2}{\tau^2} \tag{4.7}$$

where ρ is density of the medium, λ is wave-length, τ is wave period, and a is amplitude. All of our observations are in the period range 1 to 2 seconds so that, for our purposes, amplitude is directly proportional to the square root of energy. Thus, from (4.5), (4.6), and (4.7) we can form amplitude functions for P' and P'P'

$$a_1(\Delta) = \frac{BF_1(\Delta)}{\sqrt{\sin \Delta}}$$
 (4.8)

$$a_{11}(\Delta') = \frac{BF_1(\Delta)}{\sqrt{2 \sin (2\Delta)}}$$
 (4.9)

where B is a new constant, and $F_1(\Delta)$ is a ray parameter containing emergence angle and some spreading information. Now we can see that the ratio of the symmetric P'P' amplitude to the corresponding P' amplitude from (4.8) and (4.9) is

$$\frac{a_{11}(\Delta')}{a_{1}(\Delta)} = \sqrt{\frac{\sin (\Delta)}{2 \sin (2\Delta)}}$$

$$= \frac{1}{\sqrt{4 \cos \Delta}}$$
(4.10)

This function is shown in Figure 4.4.

We can now transform the amplitude data for P' in Figure 4.3 to amplitudes of P'P' using equation (4.10), which involves only geometrical spreading. Figure 4.5 shows the P'P' amplitudes from this calculation with the amplitudes normalized by that of the DF branch at 0° epicentral distance.

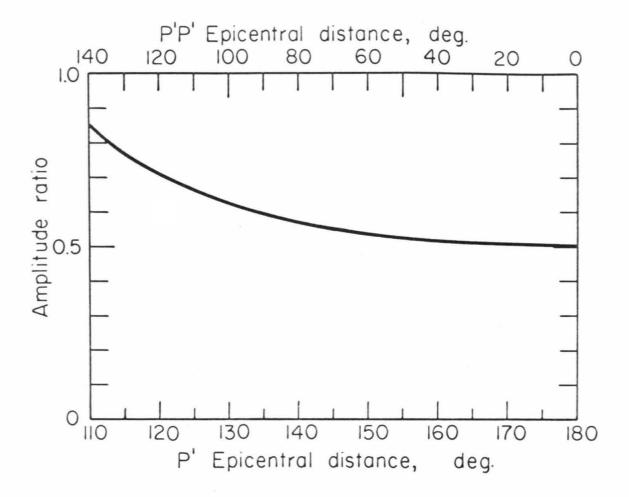


Figure 4.4

Amplitude ratio of P'P'/P' from geometrical spreading.

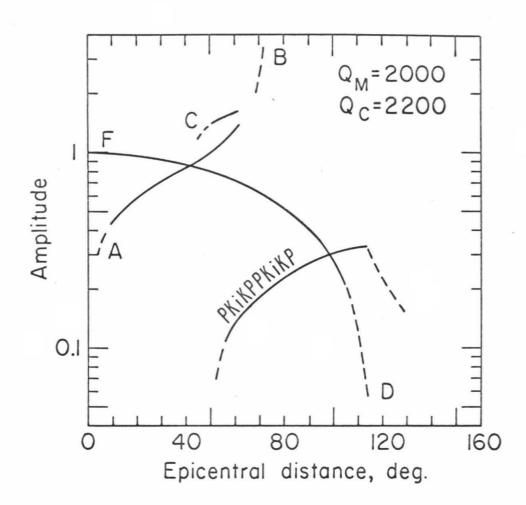


Figure 4.5

Amplitudes of the branches of symmetric P'P' calculated from the P' amplitudes of Figure 4.3. Amplitudes are normalized by the amplitude of DF at 0° epicentral distance.

4.5 Estimated Amplitudes of Asymmetric P'P' from Extensive Dipping Reflectors. In this section, we assume that the reflecting surface is large enough so that a small change in its size does not change the reflection amplitude. The geometrical spreading of an asymmetric P'P' phase is a function of the particular P' branch travelled on each leg and is also a strong function of the reflecting surface shape, which may focus or defocus the energy. The latter phenomenon is not easily resolvable and, for now, we assume that neither focusing nor defocusing takes place at the reflecting point. Spreading due to the particular P' branch is easily handled because the equivalent distance for each leg of an asymmetric P'P' phase can be calculated and the corresponding rays and relative amplitudes for each of those distances are known. Each P' leg travelled can be used to estimate the asymmetric P'P' amplitude. But because we are trying to set an upper limit on the amplitudes, we will simply use the largest-amplitude P' leg for our calculations unless one of the legs falls below 1% of the largest-amplitude symmetric phase. Use of the largest-amplitude P' leg will compensate somewhat for any focusing effects.

The 'P'dP' studies have been done in the epicentral distance range of 55° to 80° with the largest-amplitude branches being BC between 55° and 62.5°, AB between 62.5° and 73°, and DF between 73° and 80° (Whitcomb, 1971). We want to calculate for each of

these distance ranges the earliest precursor time for an asymmetric P'P' reflection with an amplitude that is 10% of the largest-amplitude phase. For time calculations, the velocity model developed in Chapter 6 was used.

First we direct our attention to reflections in the great circle plane as shown in Figure 4.1. Table 4.1 shows the asymmetric phases that give the earliest 10%-amplitude arrivals. The lead time shown is calculated from the time of the largest-amplitude symmetric P'P' branch at that distance. The dip of the reflector for all of the reflections in the great circle plane is less than 2°. The earliest lead times of 41.9 and 32.5 sec are at distances where BC or AB is the largest-amplitude branch and one leg of asymmetric P'P' is P'DF at 120°. Although the amplitude criterion that was established is satisfied by these phases, their amplitudes should never be significantly above the 10% cutoff due to the P'DF leg near 120°, and they are not as important at these distances as phases out of the great circle plane as seen below. The remaining asymmetric phases in the great circle plane have lead times less than 21 sec.

Next we calculate the times of asymmetric P'P' out of the great circle plane reflecting on a line that is perpendicular to the great circle and which intersects the symmetrical reflection point as seen in Figure 4.1. Table 4.1 shows that the asymmetric phases out of the great circle plane with each leg composed of the same branch are significantly earlier than the phases in the preceding

Table 4.1

Earliest Asymmetric P'P' Phases

with 10% Amplitudes at a Single Station

Azimuth Deviation at Station	я	0	0	0	0	0	0	0
Lead Time (sec)		2.9	32.5	21.0	11.8	41.9	19.9	13.5
Reflector Dip		< 5°	< 2°	< 5°	< 5°	< 2 °	< 2°	. < 2°
2nd P' Leg Branch-∆		BC 143.5°	DF 120°	BC 143.5°	BC 143.5°	DF 120°	BC 143.5°	DF 120°
lst P' Leg Branch-∆	*	BC 155°	DF 177.5°	DF 161.5°	BC 154°	DF 177.5°	DF 154.0°	DF 167°
4	cle Plane	61.5°	62.5	55°	62.5°	62.5°	62.5°	73°
Largest Amplitude Branch of P'P'	In Great Circle	BC (55°-62.5°)			AB (62.5°-73°)			DF (73°-80°)

Table 4.1 (continued)

Azimuth Deviation at Station	÷.	°05	. 35°	63°
Lead Time (sec)		48.8	39.5	89.1
Reflector Dip		5.1°	5.2°	3.0°
2nd P' Leg Branch-∆		BC 143.5°	AB 143.5°	DF 120°
lst P' Leg Branch-∆	lane	BC 143.5°	AB 143.5°	DF 120°
⊲	Circle I	55°	62.5°	73°
Largest Amplitude Branch of P'P'	Out of Great Circle Plane	BC (55°-62.5°)	AB (62.5°-73°)	DF (73-80°)

paragraph: up to 48.8 seconds in the BC range, 39.5 seconds in the AB range, and 89.1 seconds in the DF range. The reflector dips range from 3° to 5.2°. The DF branch is left out of the BC and AB range calculations due to the same amplitude arguments put forth in the preceding paragraph. Because the asymmetric P'P' out of the great circle plane can be constructed of nearly the same rays as the symmetric P'P', the asymmetric amplitudes are relatively large. Thus, P'P' out of the great circle plane is the most likely asymmetric phase to be seen as a precursor to the main phase at lead times greater than a few seconds.

4.6 Effect of the Finite Size of the Reflecting Surface. The previous calculations assumed an extensive, nearly plane reflecting surface. Because the boundaries of major physical property changes in the earth are, or have been controlled in a rough sense by equal pressure and temperature surfaces that are approximately spherically symmetric, the boundaries themselves tend to be spherically symmetric or "horizontal". Deviations from spherical symmetry are readily observed, especially at major boundaries at or near the earth's surface: the land-surface, ocean-bottom, and Moho discontinuity for example. But, because we need nearly plane surfaces with which to reflect P'P' waves, it is important to observe that the more a typical boundary deviates from spherical symmetry, the less extensive are its nearly planar surfaces; that is, it is rougher. For example, the

ocean surface is horizontal over extensive areas, whereas steep slopes of mountains have almost no planar surfaces of dimensions larger than a few kilometers. We must therefore estimate what surface extent is adequate for appreciable reflection of P'P' energy. This can be approximated by a calculation of the Fresnel diffraction pattern of a wave that is reflected from a semi-infinite plane with a straight edge (Born and Wolf, 1965, p. 433). A wavelength of 10 km and an observer distance of 12,000 km are used. The calculated amplitude at the observer begins to be affected appreciably when the reflector edge is within 170 km of the optical reflection point. Thus, for reflection surfaces of radii less than 170 km or diameters less than 340 km, the amplitude will begin to be reduced because of the size of the reflection surface, and reflections from surfaces significantly smaller, say 100 km in dimension, will probably not be seen.

The results of Table 4.1 show that the earliest asymmetric P'P' phases, based on a 10% amplitude cut-off, reflect from surfaces dipping from 3° to 5.2°. It is a difficult task to find a 3°-dipping surface at the ocean bottom or land surface that is nearly planar over dimensions of 100 km. Thus the cases in Table 1 are too extreme because of the finiteness of the asymmetric P'P' reflector, and the earliest lead times for the rays out of the great circle plane are probably too large. If the reflector dip were set at an upper limit of 3°, then the phases travelling out of the great circle

plane would be limited to lead times of 30 seconds or less for the GH and AB branches and 80 seconds for the DF branch. If a more reasonable dip limit of 2° is set, then all branches would have asymmetric P'P' lead times less than about 20 seconds.

4.7 Effect of Array Processing. Seismic arrays, through beamforming, have the ability to band-pass filter coherent energy in both $dt/d\Delta$ and azimuth. When this is done, considerable improvement over recording at a single station can be made by elimination of the undesired asymmetric P'P' phases. Bandpass of a particular dt/dA eliminates all asymmetric P'P' phases whose last P' leg has a different $dt/d\Delta$ than the largest-amplitude branch for that epicentral-distance range. More importantly, bandpass of arrivals from a certain azimuth eliminates those asymmetric phases travelling out of the great circle plane, which are the most bothersome type. However, because the bandpass is not a delta function and has some width, arrivals that deviate only a little from the desired azimuth will be passed. A typical beam azimuth response is shown in Figure 4.6 for the LASA array in Montana for the outer three rings: D, E, and F. A dt/d∆ of 2.0 sec/ deg. and frequency of 1.0 hz was used. The curve shows that the amplitude response falls to 10% at an azimuth of 16° off the great circle path. If this 16° azimuth limit is used for the phases in Table 4.1, then all of the asymmetric P'P' phases are limited to lead times less than 10 seconds.

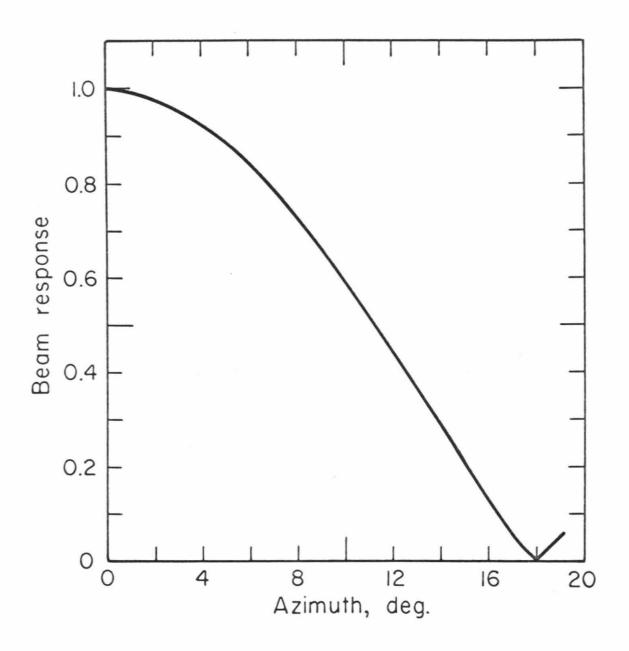


Figure 4.6

LASA beam azimuth response for rings D, E, and F. A dt/d Δ of 2.0 seconds/degree and frequency of 1.0 hz was used.

4.8 <u>Conclusions and Summary</u>. The possible ranges where asymmetric P'P' might be observed are summarized in Figure 4.7. The ranges are relative to the largest-amplitude symmetric P'P' branches that are used for the study of P'dP' phases. Three ranges corresponding to recording at a single station with 2° and 3° reflector dips and recording at a LASA-type array are shown. The calculations have been considerably simplified on the conservative side and should represent lead-time maximums that include consideration of the relative amplitudes of P' phases, the finiteness of the reflecting surfaces of dipping interfaces, and the beam-forming capabilities of a seismic array.

From Figure 4.7, we conclude that for lead times much less than 30 seconds, equivalent to a P'dP' with d at about 110 km, a single station cannot easily discriminate between asymmetric P'P' and P'dP'. The DF range between 75° and 85° may be worse depending on the reflector dip. However, use of a beam-forming array such as LASA in Montana reduces the possible asymmetric P'P' lead times to less than 10 seconds.

Examination of P'P' precursors at single stations in both the seismic recordings and data summaries in Whitcomb and Anderson (1970), Whitcomb (1971), and Chapter 2 reveals that there is a significant build-up of energy starting at around 30 seconds lead time. The vespagram of the array data shown in Chapter 3 further indicates that much of this energy within a 30-second lead time is arriving at $dt/d\Delta$'s different from those of the largest-amplitude branch and

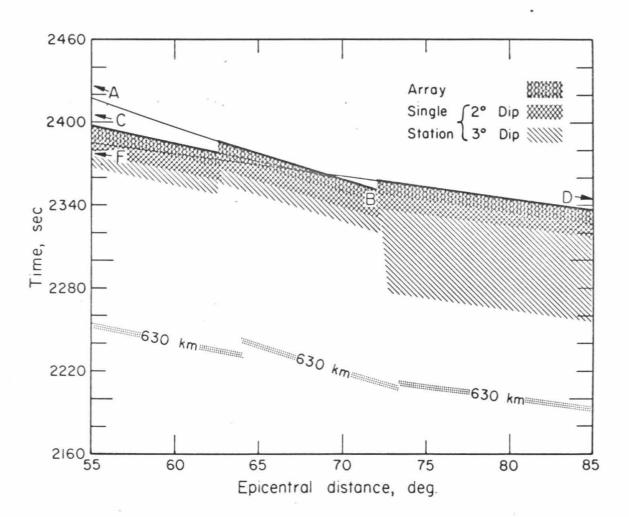


Figure 4.7

A schematic summary of possible asymmetric P'P'-phase lead times recorded at a single station with 2° and 3° reflector dips and at a LASA-type array. The largest-amplitude branches are indicated by heavy lines and the time of a P'63OP' phase is shown for reference.

other symmetric branches. This would imply that asymmetric P'P' is indeed present. However, there are arrivals in the same figure with lead times between 10 and 30 seconds recorded at LASA with the proper dt/d\(^1\) that indicate the presence of P'dP' phases. Thus, we must conclude that both asymmetric P'P' and P'dP' are seen on the seismic record from 0 to 30 seconds lead time. The interpretation of these phases as solely P'dP' by studies such as Gutenberg (1960), Adams (1968), Whitcomb and Anderson (1968), Engdahl and Flinn (1969a), Whitcomb (1971), and Adams (1971) is therefore in question because single stations were used for interpretation. Precursors with 0-to 30-second lead times should be studied using seismic arrays.

Deeper reflections, such as the strong P'640P' phase, can also show leading, emergent arrivals of asymmetric phases if the reflection is strong enough. This is indeed seen on good single-station recordings of the deep reflector such as the excellent example of Adams (1971, Figure 6), but the emergent arrivals are not seen in array-formed beams such as those in Chapter 3.

A further effect that is apparent from the analysis of asymmetric P'P' is that the geographical reflection point of a P'P' phase is poorly determined. An example of this is seen in the first entry in Table 4.1. An asymmetric surface reflection 6° away from the symmetric reflection point differs in time from the symmetric reflection by only 3.0 seconds. It is apparent that, unless the

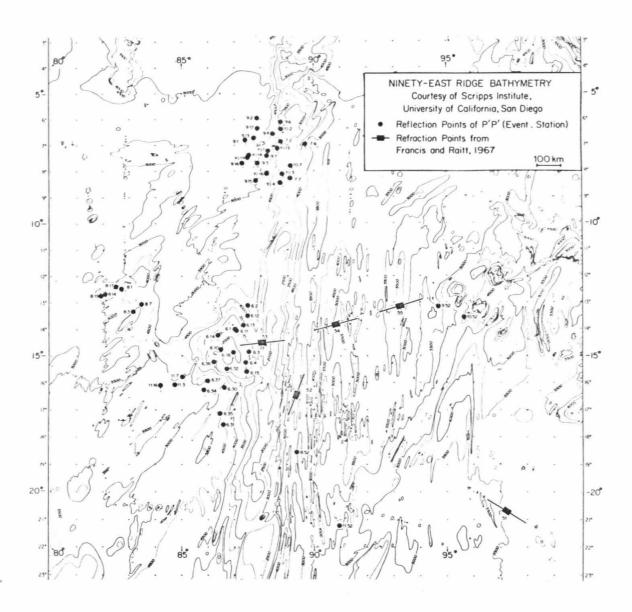
orientation of the reflector is known, one can determine the reflection point of a P'P'-type phase to within only a few degrees.

- 5. THE TIMES AND LARGEST RELATIVE AMPLITUDES OF P'P' AND AVERAGE
 MANTLE VELOCITIES UNDER CONTINENTS AND OCEANS
- 5.1 Introduction. Gutenberg and Richter (1934), upon their discovery of the P'P' phase, recognized its potential for accurate measurement of travel-time through the earth and the resulting benefits to hypocentral-depth location and earth-velocity determination. However, scatter of the P'P' readings has discouraged investigators from using the main P'P' phase for anything but an approximate check on times (for example, Gutenberg, 1951; Subiza and Båth, 1964; Engdahl, 1968; Whitcomb and Anderson, 1970; and others). A partial explanation for the scatter is asymmetric P'P' which arrives earlier than the symmetrically reflected phases as discussed in Chapter 4 and in Whitcomb (1973). But, at least some of the difficulty lies in assignment of the incorrect P'P' branch to a reading and in assumption of the incorrect velocity structure at the reflection point. Before a meaningful analysis of P'P' times can be performed, these problems must be resolved, and that is the objective of this chapter.

The problems of asymmetric P'P' are avoided by isolation of the P'P' reflection from the ocean surface, which is perfectly horizontal for purposes here. The identification of the proper P'P' branch is done using the LASA array in Montana to measure the $dt/d\Delta$ of a phase and by the determination of the largest-relative-amplitude branch

of P'P' at a given distance. This is shown to be very consistent and is an important aid in identification of a P'P' branch at single stations which provide most of the data used here. The bathymetry and crustal structure is well-known at most of the oceanic reflection points studied and, when the data are analyzed as a function of their crustal structure, the ocean-bottom and ocean-surface reflections and their times are easily identified. The reflections are then analyzed with respect to ocean-bottom reflectivity, the effect of P tables on hypocentral locations and calculated P'P' times, and the implications of the observed P'P' times on average mantle velocities under continents and oceans.

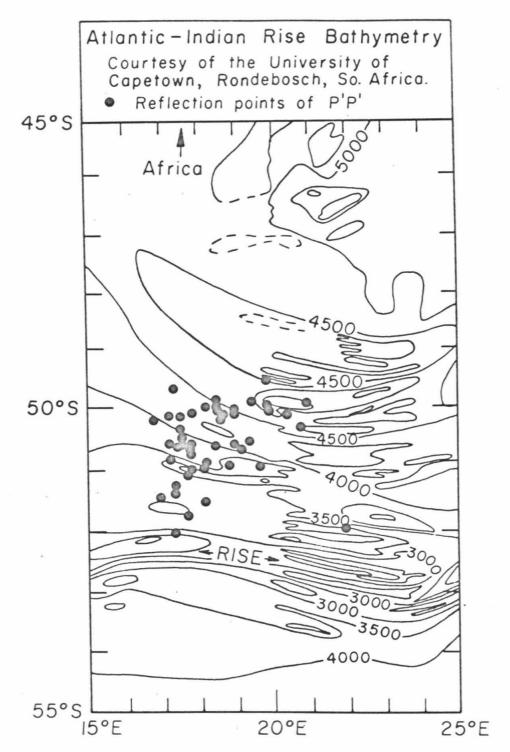
5.2 <u>Data</u>. Earthquakes from the northern part of the Japanese Arc and South America are used (except for one event, they are the same as those used in Chapter 2) and their parameters are given in Table 2.1. The corresponding oceanic reflection areas are near the Ninety-East Ridge, Indian Ocean, and the Atlantic-Indian Rise, south of Cape Good Hope shown in Figures 5.1 and 5.2, respectively. Seismic recordings were used from several stations in California and from the Tonto Forest Array in Arizona (in one case). In addition, the dt/dΔ or apparent wave slowness of some of the phases was determined using the LASA installation in Montana as a beam-forming array as in Chapter 3. An example of P'P' on a vespagram plot is shown for two events in Figure 5.3. However, the majority of the data was



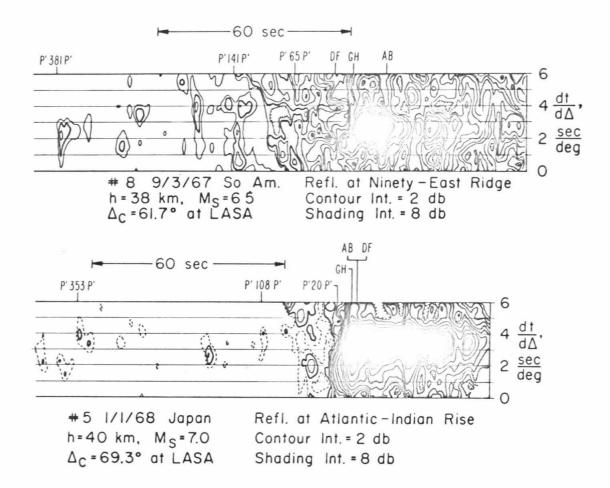
Map of the reflection points at the Ninety-East ridge, events 6,8,11 (southern group) and events, 7,9,10 (northern group).

Bathymetry was provided by the University of California, San Diego.

Contour interval is 500 meters.



Map of the reflection points at the Atlantic-Indian rise, events 1,2,3,4,5,12. Bathymetry is from unpublished data of E.S.W. Simpson and Erica Forder, University of Capetown, Rondebosch, South Africa. Contour interval is 500 meters.



Vespagrams (velocity spectra) or contour plots of beam signal power in db as a function of time and $dt/d\Delta$ for Events 8 and 5. Depths of reflection and theoretical main branch times are shown; main branch times are from Chapter 6. Note the double arrival at the $dt/d\Delta$ for the BC branch in Event 8. The first is interpreted as the ocean-bottom reflection and the second is the ocean-surface reflection.

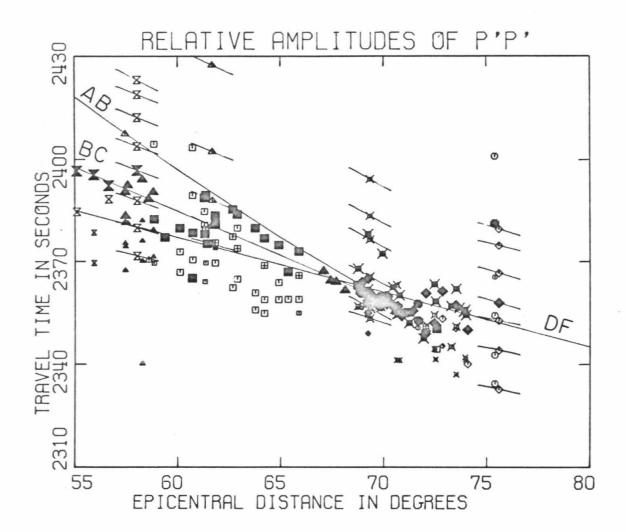
picked as signal onsets on individual seismograms as in Chapter 2.

The times were read to the nearest second and were graded according to the following scale:

- 4 Beginning of the largest-amplitude P'P' phase on the record.
- 3 Sharp pulse or a wave train with a sharp beginning.
- 2 Emergent beginning but a definite signal, usually a wave train.
- 1 Small wave train with an emergent beginning; character (difference in period or amplitudes) distinguishes it from the prevailing noise level.

The data were reduced to surface-focus on a spherically symmetric earth in the same manner as in Chapter 2.

Knowledge of the largest-amplitude branch at a given distance is useful because 1) it is unambiguous, 2) it is nearly independent of amplitude variations caused by local structure from station to station, 3) it is a constraint on core velocity structure (as seen in Chapter 6), and 4) it is a simple way to identify the branch of the largest-amplitude P'P' phase on the record. The latter property is most helpful when direct measurement of $dt/d\Delta$ is not possible such as at a single station. P'P' largest amplitudes are shown as solid points in the travel-time plot of Figure 5.4. In all of the time plots, the solid points represent grade 4, and the open points represent grade 3 (largest points) through grade 1 (smallest points).



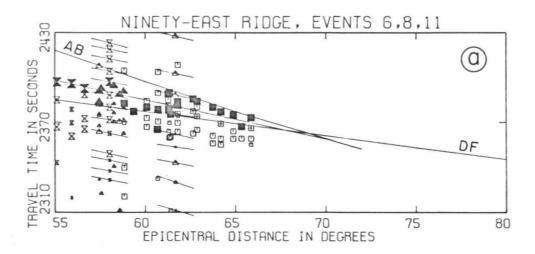
Main P'P' phase travel times and largest amplitudes (shown as solid points) as a function of epicentral distance. Sloping lines through points indicate the $dt/d\Delta$ measured at LASA. Largest amplitude branches are BC between 55° and 62.5°, AB between 62.5° and 72°, and DF between 72° and 80°. Points close to a branch which is not the largest-amplitude branch are not used as P'dP' data. The symbols are the same as those in Figures 2.6 and 2.7.

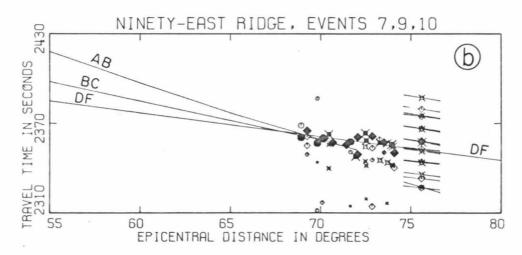
The type of symbol identifies the event for which the key is given in Table 5.1. Several stations were used for each event so that the same symbol is seen at different distances. Adams and Randall (1964) stated that the largest-amplitude P'P' branches are $P'_{DF}P'_{DF}$ at distances greater than 70°, $P'_{GH}P'_{GH}$ between 70° and 54°, and $P_{AB}^{\dagger}P_{AB}^{\dagger}$ at distances less than 54°. As discussed in Chapter 6, the P'_{GH} phase between P'_{AB} and P'_{DF} is identified as P'_{BC} . However, the phase and its $dt/d\Delta$ are well-determined and the analysis here is independent of the terminology. For consistency with Chapter 6, it will always be called P'RC in the remainder of this chapter. Figure 5.4 indicates that Adams and Randall's largest-amplitude determinations are correct except in the range of 62.5° to 72°. In this range, it is apparent that the largest amplitudes follow the AB branch from 62.5° to the end of the B caustic at about 72°. Measurement of dt/d Δ from LASA are indicated by sloping lines through the data and they show that the largest amplitude branch is BC at 58° and 62°, AB at 69°, and DF at 76° as predicted.

5.3 Analysis and Discussion. The predicted times of P'P' arrivals shown in Figure 5.4 are based on P' studies by Adams and Randall (1964), Bolt (1968), and Cleary and Hales (1971) as discussed in Chapter 6. It can be seen that the largest amplitudes sometimes miss the predicted times for that branch by several seconds, such as

the LASA data at 58°, 69°, and 76° (points pierced by short lines indicating dt/d∆). Figure 5.5 shows the same data divided into three groups based on their reflection location: Ninety-East Ridge, Events 6, 8, 11 (southern group in Figure 5.1); Ninety-East Ridge, Events 7, 9, 10 (northern group in Figure 5.1); and the Atlantic-Indian Rise (Figure 5.2). In order to compare all largest-amplitude P'P' data with each other, irrespective of the branch they represent, all of the times are reduced by subtracting the predicted time of the largest-amplitude P'P' branch at the distance (BC between 55° and 62.5°, AB between 62.5° and 72°, and DF between 72° and 80°). It is to be remembered that these predicted times correspond to continents, since that is where most of the P' data is gathered.

If one initially assumes that the average mantle velocities seen by P' phases do not vary, then the main variation of the reduced P'P' times will be due to differences at the reflection point of crustal structure, water depth, and of course depth and dip of the reflector. Three crustal velocity models shown in Figure 5.6 that differ only in the upper 56 km are used to estimate the time variations. The model used for continental crust is from the CIT 208 model of Johnson (1969). For oceanic models, two types of crust were chosen based on seismic refraction work done by Francis and Raitt (1967) in the deep ocean (5.3 km water depth) and on the Ninety-East Ridge (2.0 km water depth), here called models Oc and 90°E, respectively. Since, as





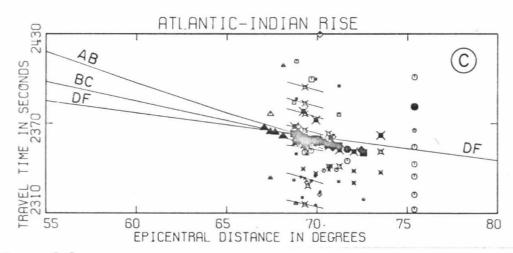


Figure 5.5

Travel times as a function of spicentral distance for each reflection area. Points with a cross in the center and points with the wrong $dt/d\Delta$ compared to the largest-amplitude branch for that range are not used. The symbols are the same as those used in Figures 2.6 and 2.7.

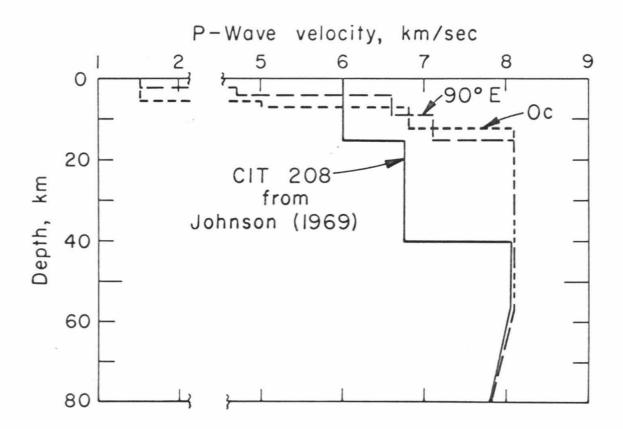
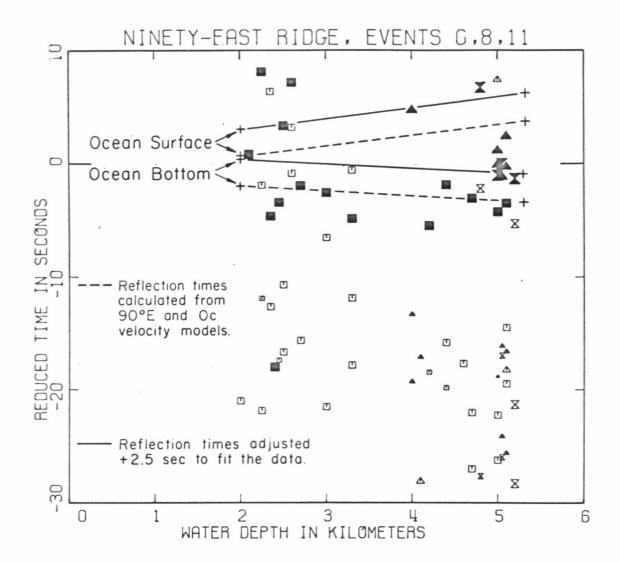


Figure 5.6

P-wave crustal-velocity models CIT208 [from Johnson, 1969], $\underline{\text{Oc}}$, $\underline{\text{90}^{\circ}\text{E}}$.

stated above, the P'P' branch times used to reduce the P'P' observations are based on continentally-observed P', then a reduced time of zero corresponds to a reflection of P'P' from the surface of the continental crust of Figure 5.6. Because the lowest velocity in the models is that of the ocean water, variations of ocean depth dominate the variations of time for surface reflections of the models and the data are best presented as a function of water depth at the reflection point.

Bathymetry charts for the reflection areas vary in coverage (Figures 5.1 and 5.2). The best data are from the Ninety-East Ridge, Events 6, 8, and 11, and Figure 5.7 shows the reduced times as a function of water depth (again, zero time corresponds to a surface reflection under a continent). The dashed lines in Figure 5.7 indicate interpolated times calculated for a reflection from the ocean surface and ocean bottom between model Oc, with a 5.3 km water depth and model 90°E with a 2 km depth. A fairly good fit of largest amplitude arrivals can be made to surface and bottom reflection times if the predicted times are increased by 2.5 sec. This fit, shown as the solid lines in Figure 5.7, is made mainly on the basis of ocean surface reflections, which should have the least scatter. The implications of this time shift are evaluated later. The three late points near 2 km ocean depth are probably due to using the wrong branch to reduce their times; they are near the right time for AB but are at a distance less than 62.5° so that the BC branch was used for reduction. With the adjustment of 2.5

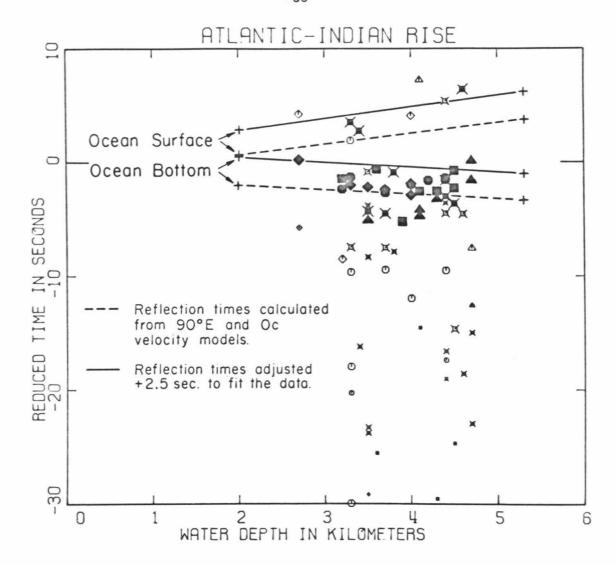


Reduced times as a function of water depth for Ninety-East ridge, Events 6, 8, 11 data. The dashed lines represent times for ocean-surface and ocean-bottom reflections which are extrapolated between velocity models 90°E (2.0 km water depth) and 0c (5.3 km water depth). The solid lines represent the same times adjusted to fit the data. The symbols are the same as those used in Figure 2.7.

sec to fit the water surface reflection times, it is seen that most of the largest-amplitude data are earlier than the ocean bottom time; some are close to the ocean surface time. But, most importantly, there is a gap between the ocean-bottom and ocean-surface times as would be expected; that is, no reflection should occur within the water.

Reduced-time data from Events 7, 9, and 10 on the Ninety-East Ridge (not shown) show no systematic distribution, probably because the reflections are too closely spaced (Figures 5.1 and 5.5) and the bathymetry data in that area are too sparse to provide a useful comparison of reduced times with water depth.

The Atlantic-Indian Rise plot of reduced time as a function of water depth is shown in Figure 5.8. The dashed lines again correspond to predicted times from the <u>Oc</u> and <u>90°E</u> velocity models (Figure 5.6), and the solid lines correspond to the adjusted times just as in Figure 5.7. The largest-amplitude data do not fit the slope of the calculated ocean surface reflection as well. However, the bathymetry data are based on very few ship tracks and the shallower water depths can be systematically plotted too deep, since any smoothing caused by lack of data will wipe out the high bottom features. Thus, shallow water points would tend to be displaced towards too great a water depth, as they appear in Figure 5.8. Nonetheless, the important trend of a widening gap with deeper water is easily seen in the data



Reduced times as a function of water depth for Atlantic-Indian rise data. The dashed lines represent times for ocean-surface and ocean-bottom reflections which are extrapolated between velocity models 90°E (2.0 km water depth) and Oc (5.3 km water depth). The solid lines represent the same times adjusted to fit the data. The symbols are the same as those used in Figure 2.6.

and the 2.5 sec time shift is again required to agree with the surface reflection for the deep-ocean points.

In both Figures 5.7 and 5.8, the largest-amplitude points tend to scatter to earlier times than that predicted for the ocean-bottom reflection. This effect can be explained by two possible phenomena. Due to the technique for reading the phases as described in a previous section, it is expected that if two signals arrive within one or two periods of each other (for P'P' this is within about three seconds) then they are read as one arrival with the earlier arrival time. The second arrival may be missed even if it is larger because both phases may appear as a single emergent wave train. This effect is important but presently unavoidable when calculating the time of the largest-amplitude P'P' phase. Thus, if there is a strong reflector in the crust as much as 20 km deeper than the largest-amplitude reflector, the two phases may merge and the deeper interface will be erroneously designated as the strongest reflector. The second possibility is an earlier arrival of asymmetric P'P' as discussed in Chapter 4. The combination of these two effects predicts that reflections from the earth-air or earth-water interface will always tend to be scattered between the predicted time and earlier times. But the reflection from the water-air interface of an ocean, because it is horizontal (for our purposes), does not suffer the asymmetric P'P' complication. Neither is there an intermediate reflection between the times of the ocean-bottom and ocean-surface reflection,

as the data of Figure 5.7 and 5.8 clearly indicate.

The data of Figures 5.7 and 5.8 show that the largest-amplitude reflector can be associated with either the ocean-bottom or oceansurface reflection. Simple reflectivity calculations indicate that, if there is a fairly hard ocean bottom with P-wave velocity greater than about 3.5 km/sec (density about 1.8 gm/cc), the bottom reflection will be larger than the ocean-surface reflection. Conversely, the amplitude of the bottom reflection is easily reduced below that from the surface reflection by an appreciable sediment layer; sediment velocities are usually much less than 3.5 km/sec. Interference effects can also be effective in reducing the ocean-bottom reflection amplitude. For example, a sediment layer that is one-fourth wavelength thick, about 0.2 to 0.5 km, overlying a crystalline-rock strata will cause destructive interference of the ocean-bottom reflection. The detailed sediment data needed to test this hypothesis are not available. However, studies of Ewing et al. (1969) show that sediment thicknesses in the Ninety-East Ridge's northern group area can be up to 0.5 km thick adjacent to the ridge, and in the southern group up to 0.3 km adjacent to the ridge. Sediment thicknesses in the vicinity of the Atlantic-Indian Rise can be up to 0.5 km. A further and perhaps very effective mode of reducing the amplitude of ocean-bottom reflections is scattering due to large bathymetric relief. A non-horizontal reflecting surface

changes the dt/d\(\text{of} \) an incoming ray and prevents the ray from continuing on its second P' leg through the same level of the earth's core. This effect, discussed in Chapter 4, tends to scatter the reflecting energy. Thus, the ocean-bottom character may be expected to have a large effect on reflection amplitudes. Relative to the ocean-surface reflection, reduced ocean-bottom-reflection amplitudes can be expected with thick sediments, sediments of one-quarter wave length (about 0.2 to 0.5 km thick), or strong bottom relief. For bottoms that are flat with thin sediment cover, the ocean-bottom reflection should be the largest-amplitude P'P' phase. Most of the data of Figures 5.7 and 5.8 fall into the latter category.

It is important to assess the validity of the 2.5 sec time shift required to fit P'P' observed times because of the implications to average mantle velocities under continents, from which the predicted times were derived, and under oceans, from which a large part of the observed times were derived. Because the predicted P'P' times are based on tables of P' for a surface focus, the assumptions that go into the development of P' tables are of prime importance. A typical study of the times of P' generally avoids the uncertainties of focal-depth and origin-time determinations by adjusting the origin time until the P residuals are minimized at epicentral distances near 90°. The adjustment is based on the assumption that near-source time anomalies for P' will be approximately the same as those for P at

its steepest emergent angle, and effectively makes the total traveltime of P' dependent on the P table used to locate the earthquake.

Of course, when the origin time and focal depth of an event are
accurately resolved, such as for explosions, dependence on a P table
is not necessary. However, most of the P' studies are of the former
type.

It is clear that one must estimate the effects of the dependence of P' time on P tables for the calculation of predicted P'P' times. From the discussion above, the measurement of P' times is effectively the differential time of the P' phase relative to P at 90°, $[t_{p'}(\Delta') - t_{p}(90°)], \text{ to which the P-table time at 90°, } t_{p}^{M}(90°), \text{ is added to construct the P' table:}$

$$t_{p'}^{M}(\Delta') = [t_{p'}(\Delta') - t_{p}(90^{\circ})] + t_{p}^{M}(90^{\circ})$$
 (5.1)

In all of these calculations, a superscript denotes reference to a particular table and lack of a superscript denotes actual (and generally unknown) travel times for a surface focus. Calculation of P'P' times from (5.1) is then simply a matter of doubling the time and distance:

$$t_{p'p'}^{C}(2\Delta') = 2 t_{p'}^{M}(\Delta')$$

$$= 2 t_{p'}(\Delta') + 2 [t_{p}^{M}(90^{\circ}) - t_{p}(90^{\circ})]$$

$$= t_{p'p'}(2\Delta') + 2 [t_{p}^{M}(90^{\circ}) - t_{p}(90^{\circ})]$$
(5.2)

or

$$t_{p'p'}^{C}(\Delta) = t_{p'p'}(\Delta) + 2 [t_{p}^{M}(90^{\circ}) - t_{p}(90^{\circ})]$$
 (5.3)

where $\Delta = 360^{\circ} - 2\Delta'$.

Direct observations of P'P' times are similarly tied to focal depths and origin times, and differential times are also used to avoid their uncertainties. But, because the distances for P and P'P' coincide, the differential times can be measured directly at the same station, which avoids some problems of station anomalies. Thus, the total travel time of the observed P'P' phase is

$$t_{p'p'}^{0}(\Delta) = [t_{p'p'}(\Delta) - t_{p}(\Delta)] - t_{p}^{M}(\Delta)$$

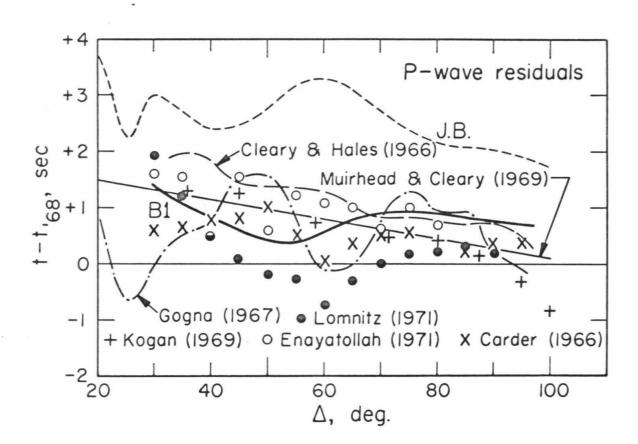
$$= t_{p'p'}(\Delta) + [t_{p}^{M}(\Delta) - t_{p}(\Delta)] \qquad (5.4)$$

The difference between observed and calculated P'P' that is due to assumptions of a P table is therefore

$$\delta t = t_{p'p'}^{0^{*}}(\Delta) - t_{p'p'}^{C}(\Delta)$$

$$= [t_{p}^{M}(\Delta) - t_{p}(\Delta)] - 2 [t_{p}^{M}(90^{\circ}) - t_{p}(90^{\circ})]$$
(5.5)

The size of the model-related terms in equation (5.5) depend on how well the P-wave model represents the "real" earth. Unfortunately, the "real" earth velocities can only be estimated and one must choose what he feels is the best approximation. Figure 5.9 (from Jordan and Anderson, 1973) shows that recent P tables are generally bracketed by the B1 model of Jordan and Anderson and the 1968 tables in the epicentral distances range of 65° to 90°, the range of applicability Therefore the "real" earth values, that is the $t_p(\Delta)$ and $t_p(90^\circ)$ terms in equation (5.5), are assumed to fall somewhere between these two tables. All of the events used for P'P' readings were located with Jeffreys-Bullen tables and all of the P' tables have been correspondingly normalized to the same tables, which are then used for the $t_p^M(\Delta)$ and $t_p^M(90^\circ)$ terms in equation (5.5). If we let Δ = 70°, a typical distance for P'P', and use the time differences in Figure 5.9 of the B1 and 1968 tables from the Jeffreys-Bullen values, then δt in equation (5.5) is between -0.6 and -1.2 sec. This correction reduces the previous required adjustment of 2.5 sec in Figures 5.7 and 5.8 to between 1.9 and 1.3 sec, with the observed times still later than those predicted.



Comparison of P-wave travel times relative to the 1968 P tables as a function of epicentral distance for several investigators (from Jordan and Anderson, 1973).

Because differential times were used, near-source and nearstation time anomalies should be minimal and the 1.3 to 1.9 sec adjustment is undoubtedly from lateral differences in mantle velocity structure. The nature of the mantle at the two source regions is unclear; both sets of events are associated with trench structures which represent the down-going lithospheric slab in plate tectonic theory. However, anomalous times from these regions are generally believed to be early (for example see Davies and MacKenzie, 1969) which is in the opposite direction of our anomaly. The mantle at the stations is continental and should correspond to the P' tables used to derive predicted P'P' times. Therefore the mantle under the oceanic reflection points is the remaining candidate for an average mantle velocity that will delay times relative to those predicted. Because P'P' traverses the mantle under the reflection twice, the anomaly corresponds to a one-way delay of 0.65 to 0.95 sec (the uncertainty due to reading arrivals to the nearest second is ± 0.25 sec). This is not a large delay and is of the same size as station delays observed in the Basin and Range Province relative to the Central United States (Cleary and Hales, 1966). There appears to be no difference between the time anomaly under a typical oceanic basin, that near the Ninety-East Ridge which is not considered a spreading center, and the time anomaly under a classic spreading center. the Atlantic-Indian Rise.

Although P'P' reflections from the surface of continents is not as dependable because a horizontal surface is not assured there as with the ocean surface, it is interesting to note that the LASA largest amplitudes from Antarctic reflections in Chapter 3 are within a second of zero reduced time as seen in Figure 5.10. This supports the assumption that zero reduced time corresponds to a P'P' reflection under a continent, but there is always the possibility that the arrivals are too early by a few seconds due to asymmetric P'P'. The largest-amplitude reflections are clearly at the ocean bottom for the LASA data near the rises and at the ocean surface for that in the East Indian ocean; the ocean-bottom to ocean-surface 8 sec gap shows up nicely in the latter case. As can be seen in Figure 3.2, the reflection points near -60° latitude are on somewhat younger and sediment-isolated ocean floors compared to the East-Indian ocean points. Thus, varying sediment thickness is an attractive explanation for the largest-amplitude reflection seen from the ocean bottom near the rises (thinner sediments) and from the ocean surface in the East Indian ocean (thicker sediments that reduce the ocean bottom reflection).

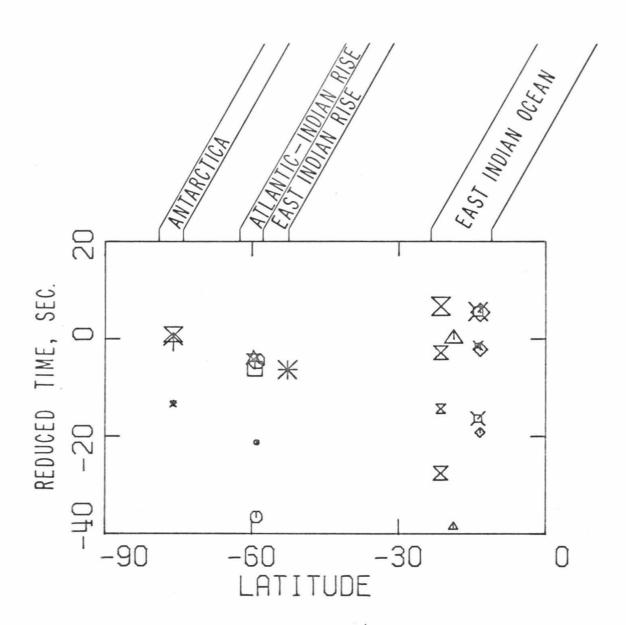


Figure 5.10

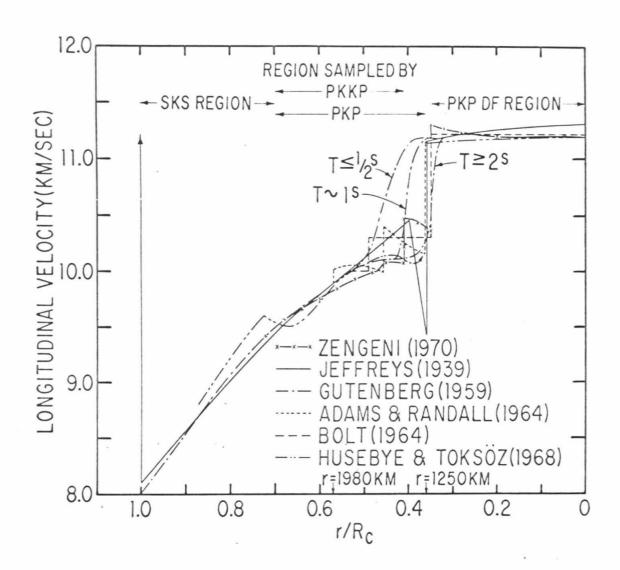
Reduced times of the LASA data from Chapter 3. The symbols are the same as those in Figure 3.1.

5.4 Summary. The times of the P'P' phase have previously been thought to scatter too severely to be useful for investigation of earth structure. The problems appear to be due to asymmetric P'P', incorrect identification of the branch, and lack of the proper velocity structure at the reflection point. They are solved by use of the horizontal ocean surface as a reflector, use of the LASA array and largest-relative amplitudes as branch identification tools, and use of detailed bathymetry maps at the reflection points of P'P'. The ocean-bottom reflection is generally the largest-amplitude phase of P'P' but occasionally the ocean-surface reflection is seen to be larger; calculations show that reasonable variations of oceanbottom type permit either case. The ocean-surface reflection is easily identifiable by its strong time dependence on water depth. When corrected by recent determinations of P velocity in the mantle and core, the predicted times of P'P' agree with observations only if they are delayed by 1.3 to 1.9 sec. This time anomaly is attributed to a delay in the oceanic mantle under the reflection points relative to continental mantle on which the predicted times are based. The anomaly corresponds to a one-way time delay of 0.65 to 0.95 sec which is not exceedingly large. It corresponds in size to time delays observed at stations in the Basin and Range Province relative to the Central United States.

6. CORE STRUCTURE

6.1 Introduction. A multitude of compressional-wave velocity models for the earth's core exist in the literature. Some of these are shown in Figure 6.1 taken from Kovach (1971), who gives a review of core studies. The problems in determining core velocity lie in three main observational difficulties of core phases: 1) structure in different parts of the core must be gleaned from widely different types of core phases, some of which are easier to observe than others; 2) all core phases are observed through the "lens" of the mantle whose effects, which are only partially known, must be removed from the data; and 3) simple identification of certain core phases and their end points has often proved difficult.

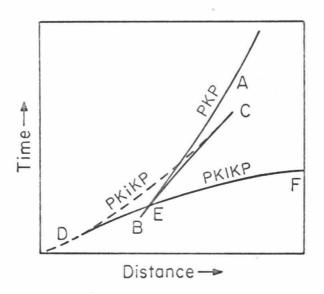
The motivation for making a new determination of the core velocity structure arises from some major improvements in core data in the areas outlined above. Use of large seismic arrays enables the direct measurement of dt/d\(\Delta \) or wave slowness of core phases which, in addition to being a new independent data set, greatly aids in the identification of core phases. A major modification in the mantle "lens" through which we see the core has been made by Jordan (1972) and Jordan and Anderson (1973); their favored mantle model, called the Bl model in the remainder of this chapter, is significantly different in velocity structure and core radius from those previously used for core studies. Finally, amplitudes of the PKP branches



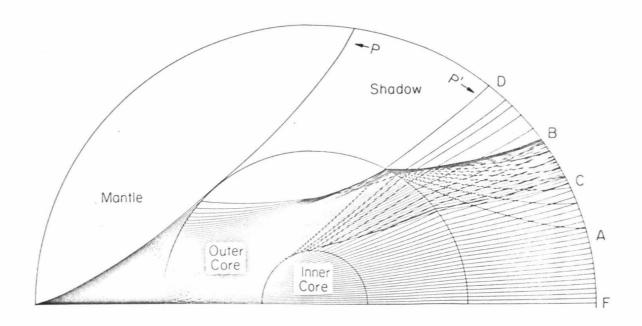
A sample of compressional-wave velocity models of the earth's core from Kovach (1971).

are better known and provide additional constraints on core models.

The nomenclature of core phases has a rather complicated history largely due to the problems of phase identification. The notation of PKP, SKS, PKS, etc., is well established. P or S denotes ray travel in the mantle and K is the ray segment in the core; P' is the accepted shorthand for PKP. Discovery of the inner core by Lehmann (1936) led to the definitions PKIKP and PKiKP (Jeffreys, 1939a) where travel through the inner core is denoted by I and reflection from the inner core boundary by i, respectively. In anticipation of the results of this paper, the labeling of the end-points of the PKP or P' branches by Jeffreys (1939b) is adopted as shown in Figure 6.2. With the use of these end-points and the notation of Adams and Randall (1964), the abbreviated form is adopted where P' $_{\Delta R}$ identifies the branch of the P' curve from points A to point B and P'_{DF} is used in place of PKIKP. P'_{CD} is the same as the reflection PKiKP but since the inner core reflection exists at distances shorter than point D, the notation PKiKP is retained. Figure 6.3 shows the ray paths followed by the P' phases of Figure 6.2; each ray is emitted from the surface source at take-off angles spaced by 0.2° intervals. For the ray tracing, the P-wave velocities in model B1 are used for the mantle and the final velocity model of this paper is used for the core. The shallowest ray to enter the core defines point A and steeper rays follow the P' curve of Figure 6.2 through



P' branches and end-point designations after Jeffreys (1939).



P' ray tracing from a surface source at take-off angles spaced by 0.2 deg intervals. The Jordan (1972) model is used for the mantle and the final model of this paper is used for the core.

points B, C, D, and finally F, which is the ray that points straight down from the source.

The plan of this study is to use observations of times, dt/d\(\), and amplitudes of core phases to construct a consistent dt/d\(\) data set as a function of distance for the core phases, P', SKS, and SKKS. The times of PmKP, where m is 2 or greater, are not used for the inversion because of the phase's maximum time nature. The mantle times and distances are stripped away using PcP and ScS (reflections from the core-mantle boundary) from the Bl model to get a dt/d\(\) curve corresponding to the surface of the core. The classic Wiechert-Herglotz integration method is applied to the curve to obtain P-wave velocity with depth in the core and the resulting velocity model is then checked and modified by P' and PKiKP absolute times. Finally, oceanic and continental mantle velocity differences, Q structure of the core, and scattering of core phases are discussed in relation to the final core velocity model and observed data.

6.2 Method. P' is easily observed on short-period instruments and is in a relatively clear part of the travel-time chart. It therefore has the best-determined times, $dt/d\Delta$'s, and amplitudes of the core phases and it would be desirable to use this phase for determining velocity throughout the core. Unfortunately, the outer

part of the core is a low-velocity zone for P' because of the highvelocity mantle which prevents those rays from bottoming above a radius of 2400 km. P', therefore, can be used only to obtain an average velocity above that level. The phases SKS and SKKS, while not as well-determined as P' due to their long-period character and the fact that earlier arrivals may obscure their beginnings, do bottom in the outer core and are the best phases available for velocity inversion at those levels. In order to strip away the effects of the mantle from the different core phases and put them on a common basis, the classic method developed by Wadati and Masuda (1934) is employed. It consists of the use of PcP or ScS data with a specified $dt/d\Delta$ and subtraction of the time and distance from the corresponding core phase with the same dt/dA. This process effectively removes the times and distances of the P legs from PKP and the S legs from SKS and SKKS to leave only the time and distance traveled in the core, denoted $t_{_{\rm K}}$ and $\Delta_{_{\rm K}},$ respectively. The $dt/d\Delta$ for a given ray is left unchanged in the process. At this point, all the different types of core data are reduced to a common base, that is, the core-mantle boundary, and analysis can proceed as if the mantle were absent.

With Δ_K and $dt/d\Delta$ data for a family of rays that start and end at the core-mantle boundary, the standard Wiechert-Herglotz

method can be applied to obtain the radial velocity distribution in the core (Bullen, 1963). Inherent in the Wiechert-Herglotz method is the assumption that the ratio r/v, where r is radius and v is P-wave velocity, is a continuously decreasing or constant function as r decreases. If this requirement is not fulfilled, then a level exists where rays do not bottom which is defined as a "low-velocity zone". Note that v may drop with decreasing r without a low-velocity zone being present as defined above as long as r/v is constant or decreasing at the same time. Proof of the existence or absence of a low-velocity zone is one of the most difficult tasks in seismological inversion, but in this study, all of the data are found to be satisfied with no low-velocity zone in the core.

6.3 <u>Data</u>. The gathering and reduction of core phase data, including corrections for ellipticity for possible errors in source locations and origin times, is a significant undertaking. Because of this, most core studies tend to concentrate on specific phases or branches. One of the major problems in attempting to combine several sets of core data is to account for the varying assumptions and models that are implicit in the data reduction process; these are generally referred to in the literature as baseline corrections. There are two general types of baseline corrections: those that use a certain time table or velocity model as a reference, termed

here as a model baseline, and those that use a specific group of stations as a reference, termed here a station baseline. Combinations of these types are often used. In this study, when a data set includes the model baseline correction, the correction is adjusted to correspond to the mantle model Bl which is the reference mantle used throughout. When a data set includes the station baseline correction, which uses a group of stations as a reference, no adjustment is made to the data. However, we should recognize that, if there is a difference between oceanic and continental mantle, the data are biased towards the continents which are the base for almost all stations. Some of the results of this paper bear on the station baseline problem.

Model B1 satisfies a large number of normal mode and differential travel time data, in addition to the mass and moment of inertia of the earth. Because of the averaging nature of this data, the model more nearly represents a earth-wide average of the mantle velocities than earlier determinations. Jordan and Anderson (1973) made an estimate of the core radius using differential times of PcP-P and obtained a value of 3485 km. This is somewhat larger than that attributed to Jeffreys (1939c) of 3473 km and Taggert and Engdahl (1968) of 3477 km. However, the recent results of Hales and Roberts (1970b) and Engdahl and Johnson (1972) support the larger value.

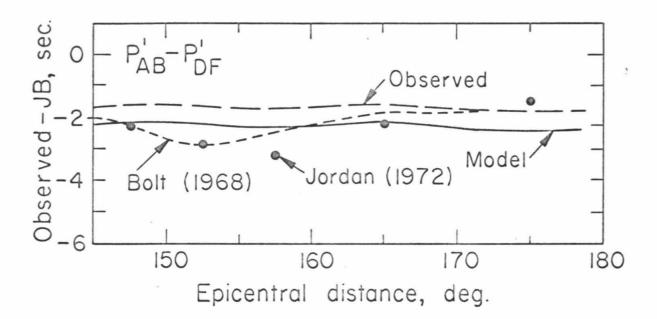
The $P'_{\ DF}$ times used here are those of Cleary and Hales (1971) who estimated the times, station anomalies and source anomalies for

18 events over the entire range of the phase, 110° to 180°. Cleary and Hales adjusted their data to a model baseline by making the times relative to their P travel-time curve between 94° and 100°. Thus, the times for P'DF depend on the times for P at 100° and they are not the same for other models. In order to make their data set compatible with the Bl mantle, 0.4 sec was added. Cleary and Hales also adjusted their data to a station baseline by specifying that stations in shield areas have anomalies of about -1.0 sec and stations in the Basin and Range Province of the United States have anomalies of about +1.0 sec. Because of the ease with which P'DF is observed, it is considered the most dependable of the core-phase data sets and no further modifications are made to the Cleary and Hales data. However, the results of this paper do suggest some minor changes near point D of the branch.

Theory requires that P' $_{\mathrm{DF}}$ be concave downward along its entire length while PKiKP, the reflection from the inner core, is concave upward; the two phases are tangent to each other at point D. As Cleary and Hales point out, their fit of an eighth-order polynomial to the data has an upward curvature near 110°. The reversal of curvature occurs at 121°, although they believe that the reversal is not significant and that a straight line can be just as readily fit to the data between 110° and 135°. Upward curvature or at least a stright-line fit between 110° and 135° has been found in

previous studies of the P' $_{
m DF}$ branch (Gogna, 1968; and Bolt, 1968) and indicates that we are not forced to bring the point D to as short a distance as 110°, as done by Jeffreys (1939a). At distances shorter than point D, PKiKP is a partial reflection. Therefore, we expect a sharp dropoff in amplitude of the P' $_{
m DF}$ -PKiKP arrival as the observer passes through D towards shorter distances (see, for example, the calculations of Buchbinder, 1971). Use of this criterion with the P' $_{
m DF}$ amplitude studies of Denson (1952, Figure 8), Hai (1963, Figures 15 and 16), and Buchbinder (1971, Figures 6-10) places the point D in the range of 120° to 125°. Point F is of course at 180° with a dt/d Δ of zero.

The times for the branch P'_{AB} are constructed initially from P'_{AB}-P'_{DF} differential times, a measurement which requires no assumption of baselines, which are then added to the P'_{DF} times already tabulated. The P'_{AB}-P'_{DF} differential times are taken from the tables of Bolt (1968) and are in substantial agreement (except for a difference of 1.0 sec near 158°) with those measured by Jordan (1972) as seen in Figure 6.4. Point B is a caustic which results from the outer core appearing as a low velocity zone to the P' phase. There is no equivalent caustic for the phases of the type SKS. Diffraction from the ray theoretical position of the caustic by one-second-period energy should be limited to less than 3° according to calculations by Jeffreys (1939b). As discussed below,



 $P'_{AB}-P'_{DF}$ differential times of Bolt (1968) and Jordan (1972) relative to the Jeffreys-Bullen tables. The observed data for model inversion and the final model are also shown.

evidence suggests that asymmetries of the earth cause arrival of scattered energy at much shorter distances, but this should not greatly affect the location of the caustic because the amplitudes at point B dominate all other P' energy. Shahidi (1968) gives a good review of efforts to locate the B caustic and, by fitting his amplitude data to the expected distribution calculated from the Airy integral, he places the ray theoretical caustic at 144.2°, the initial value used here. The point A is difficult to fix precisely from available data. The curvature of the ${\rm P\,}^{1}_{\ AB}$ travel-time curve becomes small towards A which requires that the amplitudes also become small. This effect, combined with diffraction into the shadow zone beyond A by finite-wave-length energy (discussed by Richards, 1973, and others) means that A is not marked by a sharp dropoff in amplitudes. Bolt (1968) measured what he believed to be weak P'_{AB} phases at 185° and the P' records of Jordan (1972, Figures 4.7 and 4.8) show $P'_{\Lambda R}$ to be clear arrivals at 176°. The position of A is not as sensitive to core velocity structure as it is to the velocity at the base of the mantle (as pointed out by Buchbinder, 1972) and deviations from spherical symmetry at the core mantle boundary. Thus, because its precise position does not greatly affect derivation of the core model, point A is loosely constrained to be between 175° and 185°.

Gutenberg (1957, 1958, and 1959) reported short period arrivals

preceding P'_{DF} in the range 110° to 143° which he attributed to a dispersive layer in the earth just above the inner core. Bolt (1962), Adams and Randall (1964), Ergin (1967), Engdahl (1968), Zengeni (1970), Buchbinder (1971) and others explained these arrivals as due to one or more separate branches of P' that derive from spherically symmetric discontinuities just above the inner core. The scattered nature of these arrivals has more recently led Haddon (1972) to postulate that they are due to irregularities on or near the coremantle boundary, not to structure deep within the core. Supporting Haddon's hypothesis, Müller (1973) computed theoretical seismograms from the Bolt (1964) core model and found that the phases predicted by the model's discontinuity just above the inner core were not observed on long-period seismograms. The recent measurements of Doornbos and Husebye (1972) at the NORSAR array in Norway suggest that the P' $_{\text{DF}}$ precursors have dt/d∆'s near 3.3 sec/deg in the range 136° to 143°, just before the B caustic. But, no energy with $dt/d\Delta$ near that of P' $_{\rm CH}$ of the Bolt (1968) tables is seen. This agrees with the scattering hypothesis as discussed below, but it does not rule out the P'_{TT} branch hypothesis of Adams and Randall (1964).

If the P' $_{
m DF}$ precursors are indeed P' branches from spherically symmetric discontinuities within the core, they should have coherency equivalent to that of P' $_{
m DF}$. Their amplitudes on short-period seismograms have been shown by Buchbinder (1971, Figures 6-10) to be

largest near 140°, just before the B caustic, where they are approximately equal to the amplitudes of P'DF. Beam-forming at the LASA array in Montana has demonstrated that the main core phases are coherent across that array (Whitcomb, 1971; and Davies et al., 1971) which is about twice the aperture of the NORSAR array. Therefore, the branches in question should always be seen at the proper $dt/d\Delta$ in the range near 140° just as the other core phases are always seen at their respective $dt/d\Delta$'s and distances. Davies et al. (1971) investigated P' phases for one event at distances shorter than the B caustic at 143.2° and found no coherent energy other than that for the P'DF phase. The same results were seen by Whitcomb (1971) for the P'P' phase of two events at 75.6° and 75.8°; these distances are equivalent to P' at 142.2° and 142.1°, respectively. In order to confirm these results, beam-forming was performed at LASA for 4 events in the distance range 130° to 142°. Figure 6.5 shows two examples of the resulting vespagrams (contour plots of beam power as a function of time and $dt/d\Delta$ in the direction of the event) for events near 135.4° and 139.5°. No coherent energy is seen at the $dt/d\Delta\,{}^{\prime}s$ other than that of P $^{\prime}_{\,\,{\rm DF}}$ in the two examples shown or in the remaining two events, which are at distances of 137.8° and 140.1°. Thus, the precursors to P'_{DF} are definitely not coherent across an array that is the size of LASA as the established P' and P'P' branches have proven to be. This conclusion strongly supports

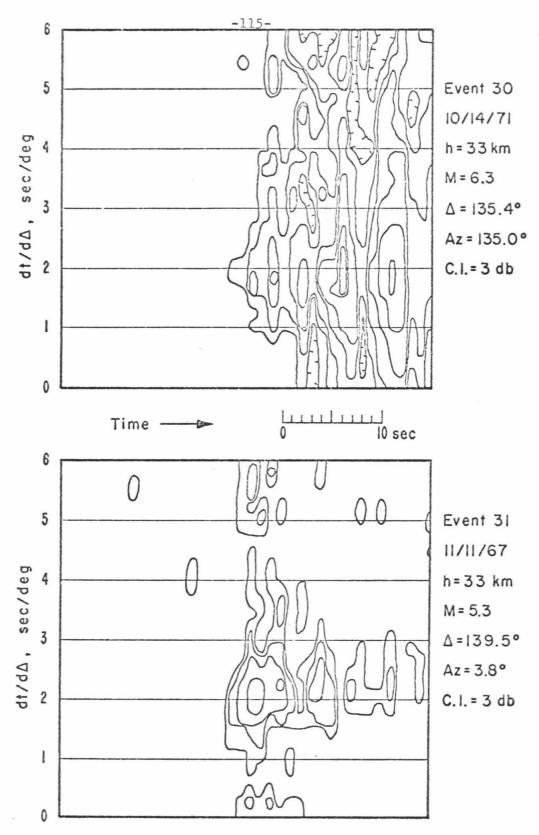


Figure 6.5. Vespagrams (contour plots of beam power as a function of time and $dt/d\Delta$ in the direction of the event) of P' in the epicentral distance ranges 135.4° and 139.5°.

Table 6.1

dt/d∆ Measured at LASA

ace- Azimuth Equiv. dt/d\(of P' (sec/deg) Phase (deg) (deg)	330.2 149.2 4.3 P'P'	149.2 2.6 P'P'	149.2 1.7 P'P'	150.4 2.5 P'640P'	325.5 142.2 1.8 P'P'	143.1 1.8 P'640P'		323.7 142.1 2.0 P'P'	144.1 3.6 P'640P'	
Origin Time Surface- at. Long. Focus epth Magn. $\Delta(\deg)$	7 30.8 61.7	N 8.8 W	6.5		5 21.6 75.6	S 70.0 W	6.3	7 55.7 75.6	21.2 S 61.3 W	
Origi Date Lat. Depth	09/03/67 21 07	10.6 s	. 38		12/21/67 02 25	21.8 S	33	12/27/67 09 17	21.2	
vent No.	œ				6			07		

Table 6.1 (continued)

Phase	P'P' .	P'P'	P'P' .	P'640P'	P'P'	P'640P'		P'P'	P'P'		P'P'	P'640P'	
dt/d∆ (sec/deg)	4.3	2.3	1.5	2.3	3.4	3.8		3.3	2.0		3.5	2.7	
Equiv. P' Δ(deg)	151.0	151.0	151.0	152.2	145.3	147.4		143.5	143.5		145.7	147.0	
Azimuth of Arrival (deg)	325.3				132.1			132.9			131.4		
Surface- Focus A(deg)	58.0				69.3			72.9			.68.7		
Time Long. Magn.	35.0	77.2 W	9.9	æ	9.50	146.7 E	7.0	01.5	142.7 E	6.5	26.9	148.0 E	6.5
Origin Time Lat. Long Depth Magn	08 13	5.6 S	28		10 19	43.6 N 146.7 E	40	10 39	41.5 N 142.7 E	33	05 03	43.6 N 148.0 E	33
Date	06/19/68				01/29/68		ř,	05/16/68			08/12/69		
Event No.	11				2			12			22		

Table 6.1 (continued)

Phase	P'P'	P'P'	P'P'	P'640P'	P'P'	P'P'	P'P'	P'640P'	P'P'	P'640P'	
dt/d∆ (sec/deg)	4.1*	2.7*	1.6*	2.6*	4.1*	2.7*	1.6*	2.4*	3.1	3.2	
Equiv. P' Δ(deg)	150.3	150.3	150.3	151.5	150.3	150.3	150.3	151.5	145.9	148.0	
Azimuth of Arrival (deg)	186.2				186.2				240.1		
Surface- Focus A(deg)	59.5				59.5				68.2		
Time Long. Magn.	05.2	54.9 E	0.9		06.2	54.8 E	6.1		36.9	10.5 W	5.7
Origin Time Lat. Long Depth Magn	10 02	73.4 N	0		00 40	73.4 N	0		04 25	36.2 N	33
Date	11/07/68		*		10/14/69	æ y			02/28/69		
Event No.	15				16				18		

Table 6.1 (continued)

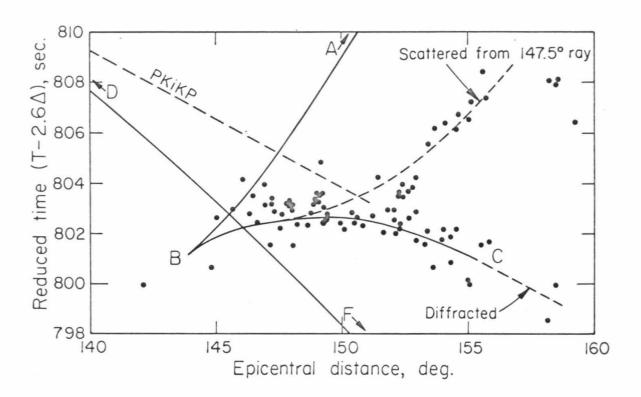
Phase	P.	P. "
dt/d∆ (sec/deg)	1.6	2.0
Equiv. P' A(deg)	135,4	139.5
Azimuth of Arrival (deg)	135.0	3.8
Surface- Focus A(deg)	135.4	139.5
Time Long. Magn.	22 36 28.6 54.3 S 1.8 E 33 6.3	10.3 71.3 E 53.3
Origin Time Lat. Long. Dept. Magn.	22 36 54.3 S	15 05 6.1 S 33
Date	10/14/71	11/11/67
Event No.	30	31

*0.6 sec/day added

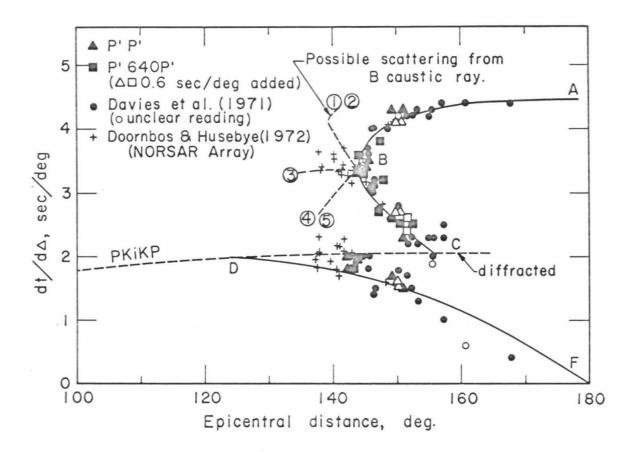
the hypothesis that these phases are not normal P' branches but are scattered energy due to asymmetries somewhere in the earth.

A strong P' arrival is present in the distance range 146° to about 155° at times between the P'_{AB} and P'_{DF} phases. The simplest explanation of this phase is a continuation from the caustic B to point C as shown in Figure 6.2. Adams and Randall (1964) made a special study of arrivals between P'_{AB} and P'_{DF} and their data are shown in Figure 6.6 in the form of a reduced time plot (reduced by 2.6 sec/deg). Adams and Randall did not adjust their data to a model baseline but instead used several explosions and deep earthquakes for which the hypocenters were specially studied. Their data, reduced to a surface focus, are somewhat dependent on the Jeffreys-Bullen tables used for locating the events, but they did not specifically use a model baseline and no baseline adjustments were made. The P' branches shown in Figure 6.6 are discussed below.

The dt/d∆'s for P' have been measured directly using the LASA seismic array. Data from Whitcomb (1971) with some new measurements for P', P'P', and P'640P' (the P'P' phase reflecting at 640 km) are given in Table 6.1. Distances in the table for the latter two wave types are for the corresponding P' phase distance for ease of comparison. These data plus data for P' from Davies et al. (1971) measured at LASA and Doornbos and Husebye (1972) measured at NORSAR are plotted as a function of epicentral distance in Figure 6.7. As



Arrivals between P'_{AB} and P'_{DF} shown in a reduced time plot (reduced by 2.6 sec/deg) from Adams and Randall (1964). The branches P'_{AB} , P'_{DF} , and the final fit of P'_{BC} to the data are shown.



 $dt/d\Delta$ measured at LASA as a function of distance for P', P'P', and P'640P' phases; distances for the latter two phases have been adjusted to the corresponding P' phase distance.

can be seen, the A-B-C part of P' is very well defined by the $dt/d\Delta$ data. ${\rm P\,}^{\prime}_{\,\,{\rm DF}}$ is not as well defined, partly because there are few data beyond 155° and because most of the data are in a distance the same time (see Figure 6.2). The data from NORSAR between 3 and 4 sec/deg at distances shorter than B will be discussed later. There is no obvious dependence in Figure 6.7 on azimuth of arrival for most of the LASA data, which is a measure of how well the individual station anomalies within the array are determined. There is an exception however in Events 15 and 16 in Table 1, which arrive from the south at an azimuth of 186.2°. Three different branches are present on the vespagrams for both events and their data fit that of Figures 6.7 only if 0.6 sec/deg is added to the measured $dt/d\Delta$'s. The points, which have been adjusted by this amount, are marked with parentheses in Table 6.1 and as open triangles and squares in Figure 6.7. These events indicate that the LASA station anomalies need revision for steeply incident arrivals from the south.

Amplitudes at a given distance are required by ray theory to be proportional to $\sqrt{|d^2t/d\Delta^2|}$ ignoring Q effects (Bullen, 1963). Thus, the amplitudes are a function of the slope of the $dt/d\Delta$ curve or the curvature of the travel-time curve. In practice, measured amplitudes scatter considerably (see for example Buchbinder, 1971; Figures 6-10; and Jordan, 1972, Figures 4.7 and 4.8). However,

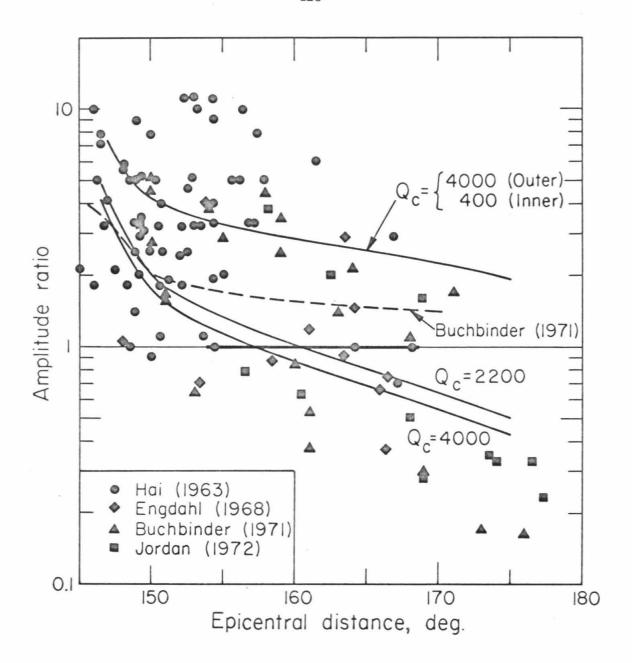
for multiple core phases arriving at the same distance, Adams and Randall (1964), Whitcomb and Anderson (1970) and Whitcomb (1971) have shown that one phase is usually the largest and this simple information over the P' range is found to be an extremely useful constraint when used in conjunction with the independently determined times and $dt/d\Delta$'s. Table 6.2 summarizes the approximate ranges and corresponding largest relative amplitudes for the P' phases. The ranges from 154° to 180° where the largest amplitudes are either P'_{AB} or P'_{DE} are determined from data of Hai (1963), Engdahl (1968), Buchbinder (1971), and Jordan (1972) that are shown as P'_{AB}/P'_{DF} amplitude ratios in Figure 6.8. A large amount of scatter allows only an approximate estimation of the distance where P'_{AB}/P'_{DE} drops below one, taken as 61° ± 7° epicentral distance. The large scatter of P'_{AB}/P'_{DF} may be an indication of lower mantle or core asymmetries; for example small corrugations of the core-mantle boundary cause large variations of the P' $_{\mbox{\scriptsize AB}}$ and P' $_{\mbox{\scriptsize DF}}$ amplitudes as illustrated by the simplified calculation of Jordan (1972, Figure 4.10).

The amplitudes and $dt/d\Delta$'s are especially useful in determining the travel-time curve of P'_{BC} , which has been subjected to the most variable interpretation in the past because of interference in the region of the B caustic. The determination procedure began with an

Ranges of the Largest-Relative-Amplitude P' Phases

Table 6.2

Epicentral Distance	P' Branch
< 143.8°	P' _{DF} or PKiKP
143.8° - 148.7°	P'AB
148.7° - 153.5°	P' _{BC}
153.5° - 161° (±7°)	P' _{AB}
161° (±7°) - 180°	P'DF



Observed and calculated amplitude ratios of P'_{AB}/P'_{DF} . Various Q structures are used with the final model and periods of one second for the calculations. The result of Buchbinder (1971) is also shown.

initial fit of a curve to the travel-time data of Figure 6.6. Point C was initially set at 154° because both the travel-time data of Figure 6.6 and the $dt/d\Delta$ data of Figure 6.7 appear to scatter beyond that distance. The scatter is taken as an indication of amplitude drop due to entry into the ray shadow, and arrivals at greater distances would therefore be diffracted around the inner core. The expected diffracted phase is shown in Figures 6.6 and 6.7. An initial $dt/d\Delta$ curve was derived from a curve fit to the time data of Figure 6.6. The $dt/d\Delta$ curve was then adjusted to agree with the $dt/d\Delta$ data of Figure 6.7 while maintaining constant the quantity

$$\int_{B}^{C} \left(\frac{dt}{d\Delta}\right) d\Delta \tag{6.1}$$

which is equivalent to fixing the ends of the travel-time curve at points B and C. The same procedure of combining time and $dt/d\Delta$ data was applied to constructing a $dt/d\Delta$ curve for P'_{AB} . A $dt/d\Delta$ curve for P'_{DF} was calculated directly from the times without further modification because of the paucity and scatter of $dt/d\Delta$ data as seen in Figure 6.4, and the assumed dependability of the time readings due to the clarity of that phase. At this point, the maximum relative amplitude determinations were used by requiring that $|d^2t/d\Delta^2|$, or the derivative of the calculated $dt/d\Delta$ curves, be largest for the

largest amplitude phase in each range defined in Table 6.2. During the adjustments, the integral properties of the time and $dt/d\Delta$ curves defined by quantities similar to (6.1) and

$$\int_{R}^{C} \left(\frac{d^2t}{d\Delta^2}\right) d\Delta \tag{6.2}$$

were maintained constant, which effectively fixes the ends of the curves. $d^2t/d\Delta^2$ was smoothed on all data sets. As a result of the $dt/d\Delta$ and amplitude adjustments, the original times for P' $_{\rm RC}$ that were determiend from the data of Figure 6.6 were shifted by no more than 0.3 sec. However, P' $_{\Delta \rm B}$ times were shifted by + 1.2 sec in the region near 152°. This was mainly due to the large values of dt/dA between about 148° and 155° seen in Figure 6.7. Possible reasons for this are discussed later. The $dt/d\Delta$ of point C is fixed at 4.50 sec/deg by the P-wave velocity and depth at the base of the mantle model used. At point B, it was initially fixed at 3.30 sec/deg from the travel-time data and partly from comparison with the data in Figure 6.7; the final model has 3.36 sec/deg. The $dt/d\Delta$ at point C is important because the difference between it and the $dt/d\Delta$ at point D, which is well determined at 1.98 sec/deg (1.95-1.99), determine the velocity jump at the inner core boundary. Unfortunately, the scatter of both the time data of Figure 6.6 and the $dt/d\Delta$ data

of Figure 6.7 allow only loose limits to be put on the $dt/d\Delta$ of C, 2.0 to 2.3 sec/deg. Thus, the time and $dt/d\Delta$ data appear to loosely constrain the velocity jump at the inner core boundary to be between 0.11 and 1.49 km/sec. However, as discussed below, the introduction of PKiKP data provides additional constraints that allow a better determination of the velocity jump.

The initial data for SKS and SKKS were taken from Hales and Roberts (1970 and 1971) who fit polynomials to their data after calculating station anomalies and source anomalies. They adjusted the times to a station baseline which would give stations in the central United States a zero station anomaly. Their data for SKS range from 85° to 126° and those for SKKS range from 90° to 126°, and are given by the polynomials

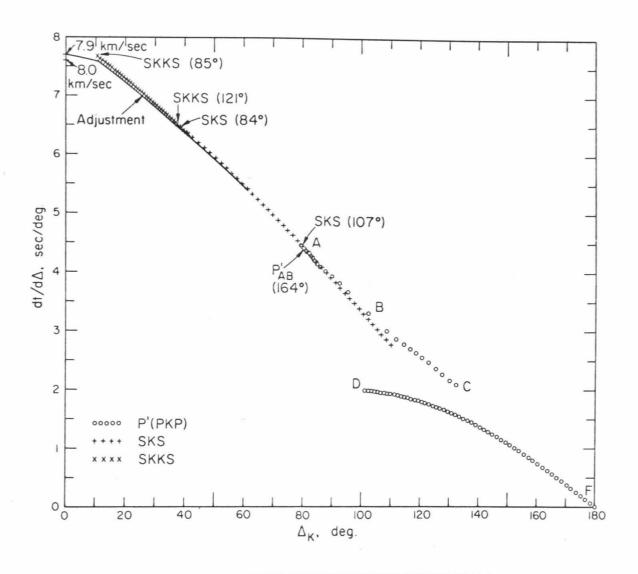
$$t_{SKS} = 1493.96 + 4.61 (\Delta - 105.0) - 0.0440 (\Delta - 105.0)^2$$
 (6.3)

$$t_{SKS} = 1539.18 + 7.02 (\Delta - 105.0) - 0.0161 (\Delta - 105.0)^2$$
 . (6.4)

6.4 Inversion and Discussion of Results. Appendix 1 gives Δ , t and dt/d Δ data for the core phases P', SKS, and SKKS in one-degree intervals of Δ along with the corresponding Δ_k and t $_k$ values obtained by stripping the Bl mantle from the data. The resulting dt/d Δ data as a function of Δ_k used for the initial Wiechert-Herglotz inversion

are shown in Figure 6.9. The separation of the points in the figure corresponds to one degree spacing of the indicated phase on the earth's surface. As can be seen, rays arriving in a one degree interval at the earth's surface near the B caustic of P' sample a broad depth range of the core, whereas rays in a one-degree interval near point A sample an extremely narrow depth range of the core. This effectively constrains the shape of the P' $_{AB}$ travel-time curve near point A much more than near point B, and also implies that changing the Δ of point A a few degrees will affect the velocity in only a small region of the core.

Because the parameters of the P', SKS, and SKKS phases are measured independently, the agreement of $dt/d\Delta$ where they overlap in Figure 6.9 is a measure of the consistency of the data. It is seen that SKS and SKKS agree where they overlap (as noted by Hales and Roberts, 1971), and that SKS agrees with the $dt/d\Delta$ of P' at point A. However, SKS increasingly deviates from P' at greater Δ_k ranges and the deviation reaches a significant amount past the data from point B of P'. The P' $dt/d\Delta$'s are believed to be more reliable in this range because they were derived both from direct measurements and observed times, whereas those for SKS were obtained from a second-order polynomial fit to the data; the polynomial-fitting process allows the largest errors of the first derivative near the ends of the fit. The connecting points of the $dt/d\Delta$ data for P', SKS, and



 $dt/d\Delta$ as a function of Δ_k for the core phases used in the Wiechert-Herglotz inversion. The ranges where the different phases were joined are indicated. An adjustment was made to the SKS and SKKS data as shown for the final model.

SKKS are shown in Figure 6.9. It is seen from the figure that coverage is still not complete in the first 10° of Δ_k , which corresponds to about the outermost 24 km of the core. Velocities in this interval will have little effect on the average velocity through the core, but they are important for an initial starting value in the Wiechert-Herglotz inversion. Once the radius of the core is fixed, the velocity at the surface of the core is determined by the $\mathrm{d}t/\mathrm{d}\Delta$ value at $\Delta_k = 0^\circ$. It will be seen that, although $\mathrm{d}t/\mathrm{d}\Delta$ and therefore velocities in this range must be assumed, an upper limit of 8.0 km/sec can be put on the velocity at the surface of the core if a low velocity zone is not present.

When an initial inversion of the $dt/d\Delta$ data is done, with an assumption of the starting velocity at the core surface, it is readily apparent that the data set thus far developed is relatively insensitive to the radius of the inner core. Without a precise determination of the inner core radius several other variations in the model are permitted involving tradeoffs between the velocity jump at the inner core, the positions of the points C and D of P † . and the relative times of the P † branches. The radius of the inner core boundary is most sensitive to the times of the phase PKiKP at short epicentral distances (0° to 50°), and this phase has been identified for explosions and earthquakes by Engdahl et al. (1970) and others. A one second shift in the time of PKiKP (or in the

travel time through the outer core) gives only a 5 km shift of the inner core radius. But, to shift the time of P'_DF by one second with a change in radius would take an adjustment of more than 100 km. The final inversion produces an inner core radius of 1215 km when constrained to fit the PKiKP data to within 0.2 sec. The value is essentially the same as the 1216 km found by Engdahl et al. and exactly the same as the 1215 km found by Jordan and Anderson (1973) from the same data, which illustrates the insensitivity of the determination to different mantle and outer core velocity models. This radius is not too different from the results of Bolt (1964) who proposed a "mean radius" of 1220 km but is considerably less than the 1257 km of Jeffreys (1939a).

For the velocity model to be compatible with an inner core radius of 1215 km, the dt/d Δ data of P'BC, and the requirement that point C be at a Δ less than 155° as determined above, the velocity at the base of the outer core must be 10.27 km/sec or greater, which requires that the dt/d Δ at point C must be about 2.07 sec/deg or less. At point D, 1.98 sec/deg is the value adopted for the dt/d Δ and that gives a velocity at the top of the inner core of 10.73 km/sec; values between 1.95 and 1.99 sec/deg are possible, however, which would give a velocity range of 10.68 to 10.89 km/sec. Thus, the velocity jump at the inner core boundary is calculated from short-period data to be 0.46 km/sec with an uncertainty range of 0.41 to 0.62 km/sec.

The jump is small but is in agreement with the recent determinations of 0.58 km/sec by Buchbinder (1971) and 0.6 to 0.7 km/sec by Müller (1973) who used long-period amplitude data. 0.46 km/sec is in agreement with Müller's jump because the final velocity model has a rapid velocity increase just below the inner core boundary which would cause the velocity jump to appear larger to long-period energy. The above parameters for rays grazing the inner core boundary result in placement of point C at 155.4° and point D at 123.6° epicentral distance.

The velocity model derived from the original $dt/d\Delta$ data and determination of the inner core boundary parameters produces absolute P'_{DF} times that are late by about 2 sec, even when the $dt/d\Delta$ at $t_k=0$ is assumed to be its minimum possible value (the value of the first SKKS data point; see Figure 6.9). In order to fit the absolute times, the velocity in the outer core must be increased. Based on the previous judgment that P' data are the most accurate, an adjustment is made to SKS and SKKS $dt/d\Delta$ values in the ranges that are used for the inversion. The values are reduced by adding the cosine-taper function

$$\delta = (-0.78 \text{ sec/deg}) \quad \cos \left[\frac{\pi}{2} \frac{(\Delta'_k - \Delta_k)}{(\Delta'_k - \Delta''_k)} \right]$$
 (6.5)

where Δ_k^{\prime} = 79.9° and $\Delta_k^{\prime\prime}$ = 10.7°. This adjustment retains the smoothness of the dt/d Δ curve and keeps the maximum change of the observed

dt/d Δ data to less than 0.8% for SKS and 0.9% for SKKS (accounting for the derivation of SKKS from SKKS-SKS times). This is a minor dt/d Δ change which translates into time shifts of the SKS and SKKS curves of about a second. The adjustment is shown in Figure 6.9. The dt/d Δ assumed at Δ_k = 0° is 7.70 sec/deg and gives a velocity at the top of the core of 7.90 km/sec. The lowest dt/d Δ possible without a low velocity zone at the top of the core is 7.60 sec/deg which results in a velocity of 8.00 km/sec; this velocity is considered an upper bound for the top of the core. The seismological data do not provide a reasonable lower bound; it will have to be determined from new data or from physical principles. This range of velocities agrees with the recent determinations of Hales and Roberts (1971) of 7.91 km/sec from the same SKS and SKKS data as used here and of Jordan and Anderson (1973) of 8.02 km/sec from normal mode and differential travel-time data.

The final P-wave velocity model for the core is tabulated in Table 6.3 and shown in Figure 6.10. The core models of Jeffreys (1939a), Gutenberg (1958, $T \ge 2$ sec), Bolt (1964), and Hales and Roberts (1971) are shown for comparison. The outstanding characteristic of the Jeffreys model is the sharp low velocity zone just above the inner core. This derived mainly from his locations of points C and D of the P' curve. Gutenberg's model is smooth but has different radii for the inner core as a function of seismic-wave frequency in an attempt

Table 6.3
P-wave velocity model of the core.

R(km)	d(km)	V(km/sec)
0		6371	11.17
100		6271	11.17
200		6171	11.17
300		6071	11.17
400		5971	11.17
500		5871	11.17
600		5771	11.16
700		5671	11.16
800		5571	11.15
900		5471	11.14
1000		5371	11.11
1100		5271	11.05
1215		5156	10.73
1215		5156	10.27
1300		5071	10.25
1400	-,	4971	10.22
1500		4871	10.18
1600		4771	10.15
1700		4671	10.09
1800		4571	10.01

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Table 6.3 (continued)

R(km)	d(km)	V(km/sec)
1900	4471	9.93
2000	4371	9.84
2100	4271	9.75
2200	4171	9.67
2300	4071	9.57
2400	3971	9.47
2500	3871	9.37
2600	3771	9.27
2700	3671	9.16
2800	3571	9.05
2900	3471	8.94
3000	3371	8.81
3100	3271	8.68
3200	3171	8.52
3300	3071	8.34
3400	2971	8.11
3485	2886	7.90

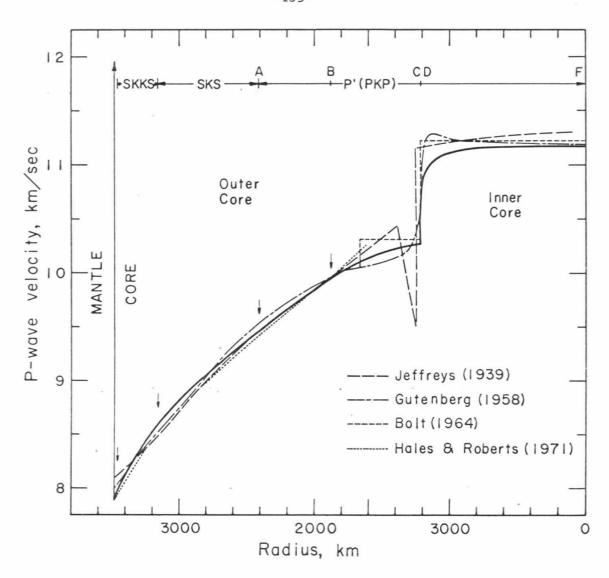


Figure 6.10

The final P-wave velocity model (heavy line). The ranges corresponding to the core phases used for velocity inversion at that depth are indicated at the top of the figure and marked with arrows along the velocity profile. Some earlier core models are shown for comparison.

to explain precursors to the P'_DF phase; only the smallest radius corresponding to T \geq 2 sec is shown which would be the model if no precursors were present. The Bolt model, which is the same as that of Jeffreys except just above and within the inner core, is an example of the class of models with discontinuities that generate extra branches to explain the P'_DF precursors. The model of Hales and Roberts relates only to the outer core because it was derived only from the SKS and SKKS data. Their data were used here for radii of 2411 to 3461 km and the differences between their curve and that of this paper for the same range is due to a different core radius and mantle S-velocity structure, and a minor adjustment of their $\mathrm{dt}/\mathrm{d}\Delta^{*}\mathrm{s}$.

The core model of Jordan and Anderson (1973), which was derived from the normal mode and differential travel-time data, is dependent on the starting model of the inversion in that the initial model is perturbed until all data are satisfied within specified limits. When comparing models, the important factors are the sensitivity of the data to velocity at specific levels in the core and the direction of perturbation from the starting model. Figure 6.11 shows both the model of Table 3 and the B1 core model; the starting velocities have been subtracted from both models. The direction of perturbation of the B1 model is in the direction of the Table 6.3 model at the

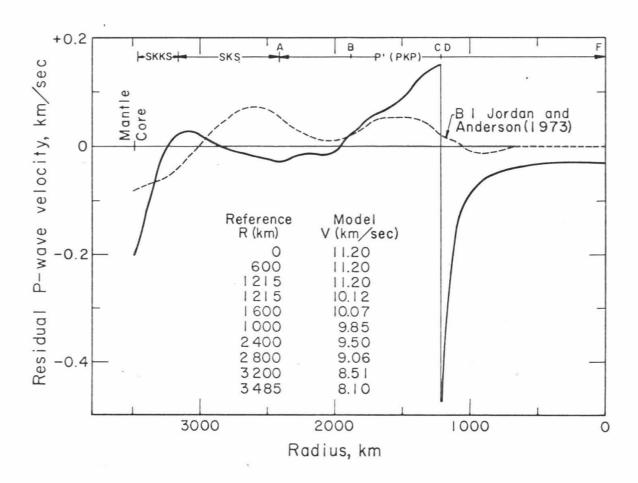


Figure 6.11

The final P-wave velocity model compared with the Bl model of Jordan (1972). The models have been reduced by the subtraction of Jordan's starting model tabulated in the figure. The ranges corresponding to the core phases used for velocity inversion at that depth are indicated at the top of the figure.

mantle-core boundary, the region above the inner core, and within the inner core except that no perturbation is made below a radius of 700 km. The large difference at the inner core boundary is due to the larger velocity jump used by Jordan and Anderson and the remainder of the inner core is not significantly different. The outstanding discrepancy between the two models is in the outer core at a radius of about 2600 km. The Bl perturbation is relatively large (0.07 km/sec) and positive whereas the velocities of Table 6.3 are somewhat less than the starting model. This discrepancy occurs mainly in the SKKS depth range which cannot be considered as well-determined as that of P', but the averaging kernels published by Jordan (1973) for this region are quite broad with side lobes extending into other depth ranges. Therefore, it is difficult to say at the present which model is most reliable. Resolution of the discrepancy will be reserved for future work.

The fit of the model of Table 6.3 to the $dt/d\Delta$ data of P' is shown in Figure 6.7. The $dt/d\Delta$ data plot to the inside of the model curve at the B caustic because the P'_AB and P'_BC phases arrive at almost the same time (see Figure 6.6). Thus, the beam power peaks of the vespagram merge to a single peak with the center point at some intermediate value between the $dt/d\Delta$'s for the separate phases. A similar effect can be expected at distances shorter than 144° where P'_DF and PKiKP arrive at nearly the same time. The fit of

the model to Adams and Randall (1964) time data between P'_AB and P'_DF is shown in Figure 6.6. P'_BC follows quite well the curvature of the main branch of data and plots about 0.3 sec behind the leading edge of the points, which have a scatter of about 1.0 sec. A dashed line is continued from point C to indicate the expected time of arrival of a high frequency phase that has been diffracted around the inner core. The two points observed near 158° may be related to this phase.

Table 6.4 shows the fit of the model to the observed time data set for the core phases as modified above by $\mathrm{d}t/\mathrm{d}\Delta$ and amplitude data. The times are listed in 5° intervals and the endpoints calculated from the model of Table 6.3 are also given. The residuals (observed - calculated) are positive for P'_{AB} and are less than 0.3 sec. The residuals for P'_{DF} are negative and their magnitudes are less than 0.4 sec. Calculated PKiKP times fit the curve of Engdahl <u>et al</u>. (1970) to within 0.2 sec.

It is interesting to note that the P' $_{AB}$ -P' $_{DF}$ differential times of the final model shown in Figure 6.4 generally parallel the Jeffreys-Bullen times and approximately average the Bolt (1964) and Jordan (1972) values. However, the differential time observed-model residuals given in Table 6.4 are + 0.6 sec. The observed times are different from the Bolt values mainly due to the high $dt/d\Delta$ of P' $_{AB}$ in the distance range of 145° to 165°. The differential times for the model cannot be greatly modified by changing the parameters

Table 6.4

Fit of the Model to Observed Times

Phase	<u>A</u>	Observed	Model Model	<u>0-M</u>
P'(PKP) (surface focus)	A 178.2		1322.0	
	175	$(1308.1)^{1}$	1307.8	0.3
	170	(1285.8)	1285.6	0.2
	165	1263.7	1263.5	0.2
	160	1241.8	1241.6	0.2
	155	1220.2	1220.0	0.2
	150	1199.2	1199.0	0.2
	145	1179.4	1179.3	0.1
·	В 143.8	1175.1	1175.1	0.0
	145	1178.9	1178.8	0.1
b	150	1192.6	1192.6	0.0
	C 155.4	1205.0	1204.9	0.1
	D 123.6	1139.92	1140.3	-0.4
	125	1142.7	1143.0	-0.3
	130	1152.5	1152.9	-0.4
	135	1162.0	1162.4	-0.4
	140	1171.2	1171.5	-0.4
	145	1179.9	1180.3	-0.4
	150	1188.0	1188.3	-0.3

-141Table 6.4 (continued)

Phase	Δ	Observed	<u>Model</u>	<u>0-M</u>
P'(PKP) (surface focus)	155	1195.2	1195.6	-0.4
	160	1201.5	1201.9	-0.4
	165	1206.6	1207.0	-0.4
	170	1210.4	1210.8	-0.4
	175	1212.8	1213.1	-0.3
	F 180	1213.6	1213.9	-0.3
PKiKP	150		1193.9	
	140		1173.3	
	130		1153.0	
	120		1133.2	
	110	1113.83	1114.0	-0.2
	100	1095.5	1095.6	-0.1
	90	1078.2	1078.3	-0.1
	80	1062.2	1062.1	0.1
*	70	1047.4	1047.3	0.1
	60	1034.2	1034.2	0.0
	50	1022.8	1022.7	0.1
	40	1013.2	1013.1	0.1
	30	1005.7	1005.5	0.2
	20	1000.1	1000.0	0.1
	10	996.9	996.7	0.2
	0	995.8	995.6	0.2

Table 6.4 (continued)

		(001102111		
Phase	Δ	Observed	Model	<u>O-M</u>
P'AB-P'DF	145	-0.5	-1.0	0.5
	150	11.2	10.7	0.5
	155	25.0	24.4	0.6
	160	40.3	39.7	0.6
	165	57.1	56.5	0.6
	170	75.4	74.8	0.6
	175	95.3	94.7	0.6
SKS	85	1384.14	1387.9	-3.8
	90	1414.9	1418.2	-3.3
	95	1443.4	1446.3	-2.9
	100	1469.8	1472.5	-2.7
	105	1494.0	1496.6	-2.6
	110	(1515.9)	1518.5	-2.6
	115	(1535.7)	1538.4	-2.7
	120	(1553.2)	1556.6	-3.4
	125	(1568.6)	1572.8	-4.2
SKKS	85	1392.34	1394.9	-2.6
	90	1430.3	1432.6	-2.3
	95	1467.4	1469.4	-2.0
	100	1503.7	1505.4	-1.7
	105	1539.2	1540.6	-1.4

Table 6.4 (continued)

Phase	Δ	Observed	Mode1	<u>0-M</u>
SKKS	110	1573.9	1575.1	-1.2
	115	1607.8	1608.8	-1.0
	120	1640.9	1641.6	-0.7
	125	(1673.1)	1673.8	-0.7
		,		
SKKS-SKS	85	8.24	7.0	1.2
	90	15.4	14.4	1.0
	95	24.0	23.1	0.9
	100	33.9	32.9	1.0
	105	45.2	44.0	1.2
	110	(58.0)	56.6	1.4
A	115	(72.1)	70.4	1.7
	120	(57.7)	85.0	2.7
·	125	(104.5)	101.0	3.5

 $^{^{1}{\}rm Bracketed\ times\ not\ used\ in\ inversion}$

 $^{^{2}}$ Cleary and Hales (1970)

³Engdahl <u>et al</u>. (1970)

 $^{^4}$ Hales and Roberts (1970 and 1971)

at the inner core boundary. In order to reduce the observed-model residual, we must either decrease the velocity in the outer core or increase the velocity in the inner core. As discussed below, a reduction of the outer core velocities is undesirable because of residuals of the P4KP phase and the preferred solution would be an increase in the inner core by an average of about 0.03 km/sec, which would then agree with the model Bl value of 11.20 km/sec. The velocity increase would require minor decreases of the P' $_{\text{NP}}$ $\,dt/d\Delta$ curve of the order of 0.03 sec/deg near point D, and a corresponding shift of the branch times reaching a maximum of -0.6 sec at D. A further implication of this velocity change and reduction of the residual would be to confirm the disagreement approaching 1.5 sec with the Bolt and Jordan $P'_{AR}-P'_{DF}$ differential times near 150° to 155° as seen in Figure 6.3. However, this apparent conflict may be explained by a scattered phase arriving in this range just before P_{AB} as discussed below.

The residuals of SKS (observed-model) are between -2.6 and -4.2 sec as seen in Table 6.4. Gutenberg and Richter (1939, p. 99) pointed out that possible errors in reading S-type waves may derive from conversions to or from P-wave energy either near the source or near the receiver, resulting in times a few seconds too early. Observations confirming the phenomenon of S-to-P conversion at the base of the crust in Fennoscandia have been published by Båth and Stefansson (1966),

Whitcomb (1969), and others and are readily observed in seismograms from many stations in the United States (author, unpublished data). Further, the recent trend of observed S travel-time curves towards later times (for example, the results of Hales and Roberts, 1970) compared to the Jeffreys-Bullen tables indicate that the older S-wave tables may have been affected by converted phases. However, this affect must be kept separate from the previously mentioned problem of station baselines and associated implications of differences in average mantle velocities under continents and oceans. The SKS phase should be the least affected by conversions near the earth's crust because of its steep angle of incidence. Thus, the final model residuals of SKS are mainly due to 1) the S station baseline assumed, 2) the mantle model used to derive the $dt/d\Delta$ versus $\Delta_{l_{k}}$ curve, and 3) the P' station baseline to which all of the absolute core phase times have been anchored. Adjustment of the baseline of the SKS times observed by Hales and Roberts (1970) by + 3.4 sec would bring the observed times within 0.8 sec of the final model (see Table 6.4), which is considered a satisfactory fit. Assuming that the Bl model is a good worldwide average of mantle S-wave velocities, and that P^{\dagger}_{DF} station baselines are the same for continents and oceans, we would conclude that S waves arrive at continental stations about 3.4 sec earlier than a hypothetical worldwide average arrival time. However,

difference between P'DF station baselines between oceanic and continental mantle structures is made in Chapter 5 from P'P' phases reflecting under oceans. P waves travelling through continental mantle arrive about 0.7 to 1.0 sec earlier than those through oceanic mantle (a P'P' anomaly of 1.3 to 1.9 sec). Using the surface areas of continents and oceans to average this value over the earth produces about a 0.6 (0.5 to 0.7) sec difference between the P' $_{\mbox{\scriptsize DF}}$ world-average and continental station baselines. Adjustment for this P-wave station baseline determines that S waves arrive at continental stations about 4.0 sec earlier than a hypothetical worldwide average arrival time. This station baseline correction would considerably reduce the large differences (-3.0 to -7.5 sec) between the Bl model S times and the observations of Hales and Roberts (1970) to be between + 1.0 and -3.5 sec. The difference between S station baselines for continents and oceans is predicted to be 5.7 sec. with the oceanic mantle slower.

Multiple core reflections of the type PmKP have been studied by Engdahl (1968), Buchbinder (1971 and 1972), Adams (1972) and others. Comparison of the P4KP times from the model of Table 6.3 with those from Adams, who made ellipticity and first-order station corrections to Novaya Zemlya explosion data, shows that the model is apparently too late by 3.4 sec, or 0.85 sec per K leg. An increase of the velocity in the outer core to remove the disagreement would

cause the P' $_{\Delta R}$ residuals to be about + 0.85 sec in Table 6.4, which is a relatively large residual for that phase. However, the time of the PmKP phase is not only sensitive to velocity in the core, but it is very sensitive to the radius of the core. To agree with the P4KP times would require only a 4 km decrease of the core radius, that is, the inner reflecting surface of the core. Because the radius was fixed by reflection from the upper surface of PcP, the PmKP discrepancy raises the possibility that the core-mantle boundary is a transition region of the order of 4 km thick. Thus, short period reflections from the upper surface would effectively reflect from a boundary slightly shallower than reflections from underneath. An alternative to a transition region is provided by recent evidence such as that of Mitchell and Helmberger (1973) that there is a 0.3 to 0.5 km/sec high-velocity zone up to 70 km thick immediately above the core-mantle boundary. Adjustment for this zone to fit PcP-P data would decrease the core radius by up to 2.5 km, which would remove most of the discrepancy between P' and PmKP. However, conclusions based on the use of PmKP times, where m is 2 or larger, are seriously compromised by their maximum time nature (Jeffreys and Lapwood, 1957). Reflections from non-spherically symmetric surfaces give rise to phases arriving earlier than the calculated symmetric-phase time. The effect is greatest for reflections out of the great circle plane (Whitcomb, 1973). Thus, if the PcP-determined core radius and the

 P'_{AB} times are correct, the PmKP data indicate either that the coremantle boundary is a transition region approximately 4 km thick or that the boundary is not spherically symmetric.

Up to this point, no account for Q structure in the core has been made. It is clear that the Q in the outer core is relatively high from the studies of the PmKP phase such as those of Buchbinder (1971), who determined a Q of 4000, and Adams (1972), who put a lower limit on Q of 2200. The Q of the inner core through which P' $_{\mbox{\scriptsize DF}}$ travels is a much more difficult determination. No phase with multiple travel paths bottoming at the same depth, such as PmKP, is available. Amplitudes of P'_{DF} between 123° and 143° affect only the outer 134 km of the core and are difficult to separate from the PKiKP phase which arrives just after P' $_{
m DF}$. Thus, P' $_{
m DF}$ beyond 146° is the best candidate for determining the inner-core Q. It is well known that short-period amplitudes of core phases scatter by an order of magnitude. Attempts to reduce this scatter by taking the amplitude ratio $P_{AB}^{\dagger}/P_{DE}^{\dagger}$ to remove near-station effects do not significantly reduce this scatter as seen in the data of Figure 6.8. Buchbinder (1971) found that his velocity model required a Q of 400 in the inner core to agree with the relative amplitudes of P $^{\text{\tiny I}}_{AB}$ and P $^{\text{\tiny I}}_{DF}.$ His calculation of ${\rm P\, '}_{\rm AB}/{\rm P\, '}_{\rm DF}$ is shown in Figure 6.8. The Q model of Buchbinder was applied to the model of Table 6.3 and the resulting amplitude ratio calculated from ray theory is shown in the figure. All calculations

are done at a frequency of 1 hz with a mantle Q of 2000. The P'AB/P'DF values are above one out to at least 170°, which is also a characteristic of Buchbinder's curve. However, the observed ratios, even though scattered, seem to require a drop below one at least by distances of 170° because no data point beyond 172° is above 0.4. The amplitude ratio is now calculated for the model in Table 6.3 using a constant Q in the core of 4000 and shown in the figure. This curve is more satisfactory at the larger distances and is well within the data scatter elsewhere. The same calculation shown for a constant Q of 2200 appears to be a slightly, but not significantly, better fit. While the data scatter prevents us from ruling out the possibility of a low Q in the inner core, the calculations show that there is certainly no requirement from short-period P' data that the inner core Q be significantly lower than that of the outer core.

A conclusion was reached earlier that the precursors to P'_{DF} at distances shorter than 143° are due to scattering either at the core-mantle boundary or within the core. Scattering is most likely from rays in or near point B because the P'_{DF} precursors appear to converge at that point, and the amplitudes of P' are largest there. Times and distances for point scattering of up to \pm 20° from the point B ray is calculated at five regions in the earth as shown in Figure 6.12. Regions 1 and 2 are just above and below the core-mantle

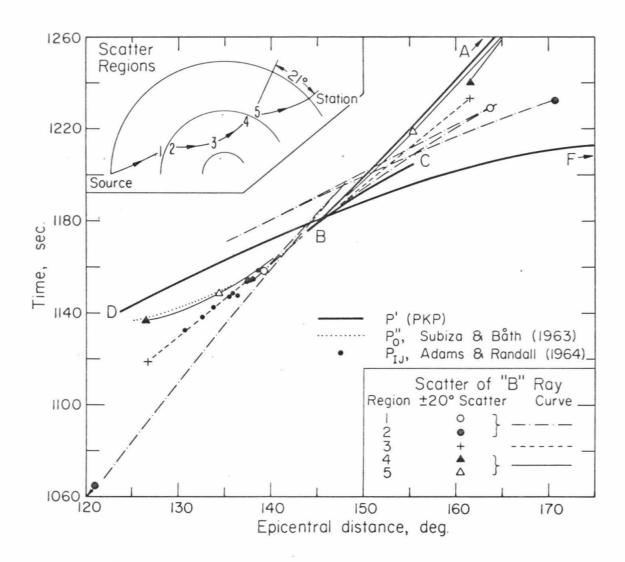


Figure 6.12

Scattering travel-time curves from the point B ray of P'. Five point scatterers are located along the ray as shown in the inset and the symbols indicate a maximum scatter angle of \pm 20°. P' from the final model and some observed data are also shown.

boundary near the source; Region 3 is at the bottoming point of the ray; and Regions 4 and 5 are just below and above the core-mantle boundary near the station. The travel-time curves for scattered energy from each region are shown in the figure with symbols indicating maximum (20°) scatter. The curves for Regions 1 and 2 near the source and those of Regions 4 and 5 near the station coincide except that their 20° scatter points are at different distances. The 20° scatter points clearly illustrate that scattering just below the boundary in the low-velocity media is much more effective (Regions 2 and 4) than just above (Regions 1 and 5). In order to produce the same scatter distances as those for Regions 2 and 4 by a dipping core-mantle boundary, dips of at least the same order as the scattering angles are required.

For distances shorter than about 140° in Figure 6.12, the times and $dt/d\Delta$'s of the scattered arrivals vary markedly with the scatter location. Subiza and Båth (1964) made a comprehensive study of the P'_{DF} precursor times and periods and found that the first arrivals fit a curve that was strongly concave upwards, which they labeled P''_{o} . Their determination of P''_{o} is shown in Figure 6.12 and it agrees remarkably well with the scatter curve from the near-station coremantle boundary (Regions 4 and 5). The later arrivals of Subiza and Båth, called P''_{1} (not shown), would easily fit scattering from the same region of rays near point B. The periods of P''_{o} and P''_{1} are between 0.5 and 1.0 sec. The phase "X" of Hai (1963) closely agrees

with the $P_0^{"}$ phase. Arrivals earlier than $P_0^{"}$ were read by Adams and Randall (1964) and were interpreted as an extra branch labeled P'_{I,I}; their readings for distances shorter than 139° are shown in Figure 6.12. These readings could be explained by either scattering within the core (which is not significantly different from Adams and Randall's proposed discontinuity) or scattering of another ray near point B from the core boundary near the source. However, only six readings of Adams and Randall precede the Region 4 and 5 curve by more than 3 sec which weakens any conclusions about the data's origin. The travel-time data of the P^{*}_{DF} precursors from Buchbinder (1971, Figure 3) scatter between the Adams and Randall and Subiza and Båth values, but the data show a clear concave upwards curvature as indicated by the curve fit to the data by Buchbinder. Doornbos and Husebye (1972), who analyzed the P' $_{DF}$ precursor times and dt/d $\!\Delta\!$'s at the NORSAR array in Norway, did not cover epicentral distances shorter than 136°. As seen in Figure 6.12, the Regions 3 and 4 scatter curves are not well-separated beyond 136° but the measurements of dt/dD of 3.3 to 3.6 sec/deg at 138° by Doornbos and Husebye tend to favor the curve of Regions 1 and 2 or that of Region 3. However, as Doornbos and Husebye state, strong corrections to their data were necessary and the calibration of the array is not complete, which makes their dt/dA data subject to future revision.

The scatter curves in Figure 6.12 beyond 145° fall in the time space between the P' $_{AB}$ and P' $_{BC}$ branches. Their dt/d $_{A}$'s are quite different and this characteristic may be useful in determining the origin of scattered energy in this distance range. The Adams and Randall (1964) arrivals after P' $_{BC}$ shown in Figure 6.6 were the basis of their extension of P' $_{IJ}$ beyond 145°. The points later than P' $_{BC}$ at distances between 153° and 156° appear to have a slope or dt/d $_{A}$ larger than that proposed for P' $_{IJ}$ in this range (see also, Adams and Randall, 1964, Figure 5). The scattered phase that fits these points best is from the ray of P' $_{BC}$ at 147.5° scattered from the core boundary near the station; the phase is shown in Figure 6.6.

Scatter of the point B ray from core boundary near the station precedes the P'AB branch by 1 to 3 sec between 150° and 165° as seen in Figure 6.12. As the scatter curve approaches 165°, the scatter angle increases and the likelihood of scattering decreases. This mechanism gives an attractive explanation of the apparent discrepancy between the observed P'AB-P'DF differential times and the values of Bolt (1968) and Jordan (1972) centered at about 150° to 155° as seen in Figure 6.4. Increased use of short-period high-gain instruments since the publication of the Jeffreys-Bullen table may have led to a more frequent reading of the scattered phases whose periods are generally shorter than a second. Thus, more recent readings of P'AB tend to be the earlier scattered phase instead, resulting in a dip of

the P' $_{AB}$ -P' $_{DF}$ curve relative to the Jeffreys-Bullen values near 150° to 155°. Extension of the Bolt and Jordan values at 175°, where the earlier scattered phase is absent, backwards and in parallel with the Jeffreys-Bullen values would coincide with the observed curve in Figure 6.4, which was constructed with times, $dt/d\Delta$'s, and relative amplitudes.

Comparison of the observations to the scatter curves leads to the conclusion that the strongest scattering of P' appears to take place near the core-mantle boundary closest to the observing station. The angular distance from the station of the scattering point on the boundary is about 21° as shown in Figure 6.12. Inspection of the ray plot of Figure 6.3 supports this conclusion because adjacent rays are more concentrated at this location on the core-mantle boundary than at any other; in fact, all rays of ${\rm P}^{\, 1}_{\ \Delta {\rm R}}$ must pass through an internal caustic as seen in the figure. The most effective scattering location that agrees with the data is just below the core-mantle boundary near the station. Scattering of up to 20° is required for the $P'_{\ \ DF}$ precursors and a much larger angle is needed if the scattering takes place above the boundary. The $P'_{\tau\tau}$ times of Adams and Randall (1964) at distances shorter than 143° and the dt/dA data of Doornbos and Husebye (1972) may be evidence for scattering within the core or at the core-mantle boundary near the source. However, the data do not permit a more definite conclusion about scattering from these regions at present.

6.5 Summary. A core P-wave velocity model is constructed from observed times, dt/da's, and relative amplitudes of P'; the observed times of SKS, SKKS, and PKiKP; and a new mantle-velocity determination model B1 by Jordan and Anderson (1973) which represents a sphericallysymmetric average over the earth. The resultant velocity structure fits the P' absolute times to within 0.4 sec and the P' $_{AB}$ -P' $_{DF}$ differential times to within 0.6 sec. These residuals could be reduced to less than 0.1 sec by a small velocity increase in the inner core if some adjustment were made to the $P^{\dagger}_{\ DF}$ curve of Cleary and Hales (1971) near point D up to a maximum of 0.6 sec. The $dt/d\Delta$'s observed at the LASA array in Montana and the maximum-relative amplitudes of the P'-type phases provide important constraints on the data used for inversion and the final velocity model, especially the P'_{AB} and P'_{BC} branches. The PKiKP times of Engdahl <u>et al</u>. (1970) are fit to within 0.2 sec which results in an inner core radius of 1215 km; this is essentially the same as the 1216 km derived by Engdahl et al. The model's ray-theoretical end-points of the P' refraction branches for a surface focus are at 123.6° for D, 155.4° for C, 143.8° for B, and 178.2° for A; all of these values are within observational limits.

Care is taken in the use of the time data to keep assumptions of a model baseline and a station baseline separate. The final core velocity model is mainly dependent on the $dt/d\Delta$'s of the core phases,

the absolute times of the P' branch, and the absolute PKiKP times. The absolute SKS time residuals are then a function of the P station baseline and the mantle S-velocity structure that is stripped from the observed times. After correction for the oceanic P baseline from Chapter 5, the SKS continental station baseline is calculated to be 4.0 sec earlier than that for the earth average. The model's baseline-adjusted SKS and SKKS residuals are within 0.8 sec and 2.7 sec, respectively, of Hales and Roberts' (1970 and 1971) observations. Use of this same baseline reduces the disagreement between the S times of Jordan and Anderson (1973) and those of Hales and Roberts (1970) to between + 1.0 and - 3.5 sec. The agreement suggests that contamination of the Hales and Roberts' S readings with earlier converted phases from near the station is not much greater than about 3 sec from that of SKS, and contamination of the latter should be small due to its steep angle of emergence. The baseline analysis leads to the conclusion that mantle velocities, presumably in the upper mantle, are slower under oceans that those under continents. The travel-time differences are of the order of 0.8 sec for P waves and 5.7 sec for S waves.

The core velocity model is smooth except for a discontinuity at the inner-core boundary. The velocity jump at the inner-core boundary is determined to be between 0.41 and 0.62 km/sec from the inner-core

boundary radius (fixed by PKiKP times), the dt/d\(\text{at point D of P',} \) and constraints on the position of point C of P'. Velocity at the top of the core has an upper bound of 8.0 km/sec. Very steep velocity gradients are required by SKKS data in the outer 400 km of the core and the gradient smoothly decreases to a low, but not negative, value just above the inner-core boundary. The velocity gradient is again very steep at the top of the inner core but rapidly levels out to between 11.17 and 11.20 km/sec over most of the inner core.

Q in the outer core has been shown to be high, 2200 to 4000, from PmKP studies of previous investigators (Buchbinder, 1971; Adams, 1972; and others). However, because no similar phase has been observed for the inner core, the Q at that depth is much more difficult to estimate. The determination of an inner-core Q of 400 by Buchbinder (1971) is not required by the highly scattered short-period P' amplitude data, and an improved fit can be easily made with Q constant in the core.

Most, if not all, of the arrivals preceding P' $_{
m DF}$ at distances shorter than 143° appear to be due to scattering as proposed by Haddon (1972) and not due to spherically symmetric discontinuities just above the inner core. Doornbos and Husebye (1972) measured a dt/d $_{
m A}$ of about 3.3 sec/deg for the precursors between 136° and 143° at the NORSAR array in Norway. This is the same dt/d $_{
m A}$ as that of the B caustic and effectively rules out the P' $_{
m CH}$ branch of Bolt (1964), but

the P'_{IJ} branch of Adams and Randall (1964) does not disagree with this measurement. However, investigation of the precursors just short of the B caustic at the LASA array in Montana, a larger array, shows no coherent energy other than P'_{DF} even though the amplitudes of the precursors should be maximum and nearly the same as P'_{DF} at this range. The precursors clearly do not have the coherency of the P' main branches which is a finding that strongly supports the scattering hypothesis.

Calculation of the travel-time distribution of scattered phases and comparison with published data show that the strongest scattering takes place at or near the core-mantle boundary close to the receiving station. Scattering is from rays of, or near, the B caustic, of P'. The scattering angles are up to at least 20° for energy of 0.5 to 1.0 sec periods and scattering at a given angle is more effective just below the core-mantle boundary than above. Arrivals previously identified as P'_{IJ} beyond 145° and possible early readings of the P'_{AB} branch between about 150° and 160° can also be attributed to scattering from this region. Placement of the scatterer close to core-mantle boundary near the station is the most reasonable location because adjacent rays leaving the source are more concentrated at this point on the core-mantle boundary than at any other, thus providing the maximum energy density available for scattering. There are a few observed arrivals that cannot be explained by scattering from the

core-mantle boundary near the station and, if the readings are actually core-phase energy, they must be interpreted as scattering either within the core or close to the core-mantle boundary near the source. Until more complete evidence is available, the latter explanation is preferred because only one scattering level is required.

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APPENDICES

1. Δ , t, dt/d Δ , Δ_k , and t $_k$ for the core phases used in the initial Wiechert-Herglotz inversion.

PHASE	DELTA	T (SEC)	DT/DD (SEC/DEG)	DELTA(K) (DEG)	T(K)
P*(F)	180 179 178 177	1213.56 1213.53 1213.43 1213.27	0.0 0.065 C.130 0.190	180.00 178.33 176.65 175.03	702.76 702.71 702.54 702.28
	176 175	1213.05	C.250 0.310	173.41 171.78	701.92
	174 173	1212.43	0.370	170.15 168.42	700.92 700.21
	172 171	1211.55	0.500	166.80	699.45
	170 169	1210.43	0.615	163.59	697.66
	168	1209.09		160.38	695.49
	167 166 165	1206.53	0.845	157.15	692.95
	164 163	1205.72	0.955	153.97	690.10
	162	1203.71	1.055		688.59 687.00 685.39
	160 159	1201.51	1.145	147.91	683.72 681.91
	158 157	1199.12	1.240	144.86	680.08
	156 155	1196.56	1.320	141.97	676.38
	154 153	1193.84	1.360	139.07	674.43
	152 151	1190.96	1.440		670.36
	150 149	1187.95	1.505	134.87 133.47	666.33
	148	1186.39	1.575	132.06	662.01
	146	1183.19	1.625	129.48 128.13	657.88 655.66
	145	1179.88	1.680	126.84	653.50
	143 142 141	1176.48 1174.74 1172.98	1.725 1.750 1.770	124.30 123.01 121.77	649.20 646.94 644.77
	A T A .	-115010	1.110	467011	04401

	· ×,				
	DELTA	T	DT/DD	DELTA(K)	T(K)
PHASE	(DEG)	(SEC)	(SEC/DEG)	(DEG)	(SEC)
*	140	1171.20	1.790	120.54	642.56
	139	1169.40	1.810	119.29	640.32
	138	.1167.58	1.825	118.11	638.18
	137	1165.75	1.840	116.92	
	136	1163.90	1.860	115.69	633.71
	135	1162.03	1.875	114.51	631.51
	134	1160.15	1.885	113.38	629.39
	133	1158.26	1.900	112.20	627.16
	132		1.915	111.10	624.89
	131	1154.43	1.925	109.89	622.74
	130	1152.50	1.935	108.71	620.58
	129	1150.56	1.940	107.71	618.51
	128	1148.60	1.945	106.64	616.43
	127	1146.65	1.955	105.52	614.24
	126	1144.69	1.965	104.40	612.04
	125	1142.72	1.975	103.27	609.82
	124	1140.74	1.980	102.21	607.72
	123	1138.76	1.985	101.16	605.63
	122	1136.78	1.989	100.09	603.52
P'(D)	121	1134.79	1.990	99.09	603.52
P (C)	155	1204.12	2.070	132.44	
, ,,,,	154	1202.01	2.150	130.06	664.54
	153	1199.81	2.253	127.72	659.40
	152	1197.51	2.357	125.32	653.87
	151	1195.10	2.458	122.94	648.14
	150	1192.59	2.549	120.66	642.42
	149	1190.00	2.625	118.55	636.99
	148	1187.34	2.694	116.53	631.58
	147	1184.61	2.771	114.37	625.68
	146	1181.80	2.865	111.89	618.69
	145	1178.88	3.000	108.68	609.30
P (B)	144		3.300	102.27	589.14
,	145	1179.38	3.664	95.30	564.93
	146	1183.12	3.807	92.51	554.52
	147	1186.99	3.929	89.91	544.45
	148	1190.97	4.017	87.80	536.09
	149	1195.03	4.090	85.97	528.65
	150	1199.15	4.138	84.91	524.46
	151	1203.30	4.171	84.35	521.96
	152	12(7.49	4.200	83.92	520.18
	172	17 (104)	7.200	03.72	720.10

PHASE	DELTA (DEG)	T (SEC)	DT/CD (SEC/DEG)	DELTA(K) (DEG)	T(K)
	153		4.226	83.51	518.43
	154	1211.70 1215.94	4.249	83.20	517.15
	155	1220.20	4.269	82.98	516.CC
	156	1224.48	4.288	82.71	515.03
	157	1228.78	4.307	82.34	513.46
	158	1233.10	4.326	81.94	511.73
	159	1237.43	4.344	81.41	509.41
	160	1241.79	4.359	81.00	507.64
14.5	161	1246.15	4.370	80.87	507.09
	162	1250.53	4.380	80.76	506.61
	163	1254.91	4.390	80.56	505.71
	164	1259.31	4.399	80.21	504.19
	165	1263.71	4.406		
	166	1268.13	4.413		
	167	1272.55	4.420		
P * (A)	168	1276.98	4.425	70 01	400 03
SKS	107	1503.00	4.435	79.86	
	106	1498.52	4.525	78.16	492.39
	105 104	1493.95 1489.29	4.615	76.53	484.75
	103	1484.55	4.700 4.785	74.88 73.22	477.08 469.23
	102	1479.72	4.875	71.52	461.00
	101	1474.80	4.965	69.81	452.61
	100	1469.79	5.055	68.09	443.95
	99	1464.69	5.140	66.39	435.31
	98	1459.51	5.225	64.69	426.47
	97	1454.24	5.315	62.93	417.20
	96	1488.88	5.405	61.15	407.69
	95	1443.43	5.495	59.37	397.95
	94	1437.89	5.580	57.61	388.20
	93	1432.27	5.665	55.84	378.26
	92	1426.56	5.755	54.00	367.80
	91	1420.76	5.845	52.15	357.04
	90	1414.87	5.930	50.32	346.26
	89	1408.90	6.015	48.48	335.29
	88	1402.84	6.105	46.57	323.72
	87	1396.69	6.195	44.64	311.84
	86	1390.45	6.285	42.68	299.61
SKS	85 84	1384.12	6.375 6.460	40.69 38.74	287.02 274.48
3//3	04	1311.10	0.400	30.14	214.40

PHASE	DELTA	(SEC)	DT/CD (SEC/DEG)		T(K)
SKKS	121	1647.38	6.505	37.61	270.38
	120	1640.86	6.535	36.94	265.99
	119	1634.30	6.565	36.26	261.54
	118	1627.72	6.600	35.55	256.89
	117 116	1621.10	6.635 6.665	34.83 34.15	252.51 247.64
	115	1607.77	6.695	33.47	243.05
	114	1601.06	6.730	32.75	238.23
	113	1594.31	6.765	32.03	233.33
	112	1587.53	6.795	31.33	228.66
	111	1580.72	6.825	30.64	223.90
	110	1573.88	6.860	29.91	218.93
	109	1567.00	6.895	29.27	213.87
	108	1560.09	6.925	28.47	209.02
	107	1553.15	6.955	27.76	204.09
	106	1546.18	6.985	27.06	199.18
	105	1539.18	7.020	26.31	193.92
	104	1532.14	7.055	25.55	188.60
	103	1525.07	7.085	24.83	183.55
	102	1517.97	7.115	24.11	178.39
	101	1510.84	7.145	23.39	173.25
	100	1503.68	7.180	22.62	167.72
	99	1496.48	7.215	21.85	162.16
	98	1489.25	7.245	21.10	156.82
	97	1481.99	7.275	20.36	151.41
	96 95	1474.70 1467.37	7.310	19.58	145.69
	94	1460.01	7.345 7.375	18.78	139.84
	93	1452.62		17.26	128.64
	92	1445.20	7.405 7.435	16.49	122.92
	91	1437.75	7.470	15.66	116.84
	90	1430.26	7.505	14.84	110.63
	89	1422.74	7.535	14.05	104.68
	88	1415.19	7.565	13.25	98.65
	87	1407.60	7.600	12.40	92.23
	86	1399.99	7.635	11.54	85.64
SKKS	85	1392.34	7.665	10.72	79.35
ASSUMED	0	0.0	7.700	0.0	0.0

PART II.

THE 1971 SAN FERNANDO EARTHQUAKE SERIES FOCAL MECHANISMS AND TECTONICS

1. INTRODUCTION

The main shock of the San Fernando earthquake series occurred on February 9, 1971, in the tectonically active Transverse Ranges structural province of Southern California. Immediately following the main shock, the aftershock region was inundated with portable instrumentation from many agencies including the California Institute of Technology (CIT) to make this the most extensively monitored aftershock sequence to date and provide a unique data set for aftershock studies. Allen et al. (1972) assigned the main shock parameter as: 34° 24.7' N, 118° 24.0 W, h = 8.4 km, and M_{T} = 6.4. The main fault motion, as inferred from observed surface faulting (Kamb et al., 1971, and U. S. Geological Survey Staff, 1971), static displacement of the ground surface (Jungels and Anderson, 1971; Jungels and Frazier, 1973; and Alewine and Jordan, 1973), and from the initial focal mechanisms (Division of Geological and Planetary Sciences, California Institute of Technology, 1971; Whitcomb, 1971; Wesson et al., 1971; Dillinger and Espinosa, 1971, and Canitez and Toksoz, 1972), was of the thrust type on a north-northeast-dipping fault plane with some left-lateral strike slip. The general type and orientation of the main fault plane agree with mapped north-dipping thrust faults which bound many of the southern edges of the Transverse Ranges.

From the lunate-shaped distribution of the M_L = 3.0 or larger aftershock epicenters shown in Figure 1 and the relatively low seismicity near the surface break (Allen et al., 1971; Hanks et al.,

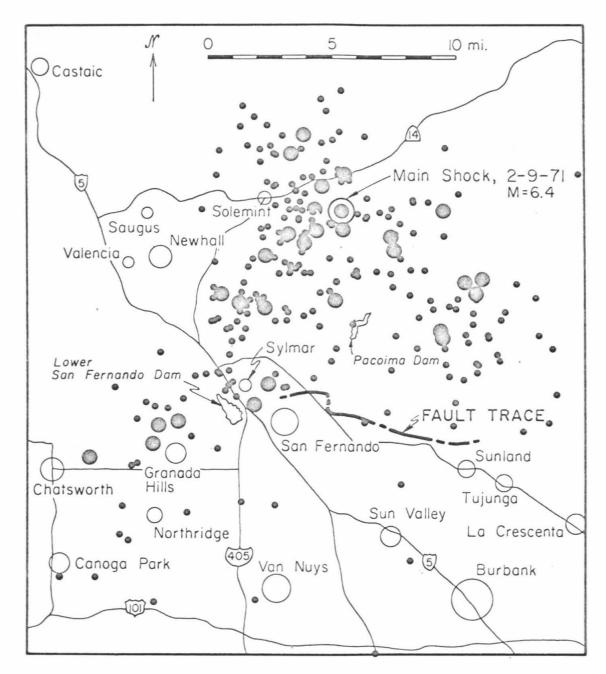


Figure 1.

Epicentral locations of the main San Fernando event of February 9, 1971, and aftershocks through December 31, 1971. All events of $\rm M_L=3.0$ or larger, including those not specially studied, are shown. The larger points indicate events of $\rm M_L=4.0$ or larger.

1971; Wesson et al., 1971; and Allen et al., 1972), it appears that the stresses were completely relieved on the main fault surface and the larger aftershocks were mainly limited to the edges where stress was concentrated. However, Whitcomb (1971), using focal mechanisms, showed that the apparent lunate symmetry is misleading in that the tectonic pattern along each limb of the distribution is totally different.

Allen et al. (1972) used the largest aftershocks, mainly those with M_T = 4.0 or greater, to formulate a tectonic model of the associated faulting. The focal mechanisms which substantiate that development are presented first with a review of the model's construction. We then investigate a more extensive set of 87 aftershocks chosen in a uniform manner from the three months between the onset of the series and May 7, 1971. The cutoff date is the time when many of the CIT portable seismometer trailers were removed and the aftershock rate had decreased to less than one per four days. This second set confirms the general features of the fault surface model. Some of the individual focal mechanisms and their locations are obviously not compatible with the model, but this might have been predicted for a region with such large tectonic movement of up to two meters (see for example Burford et al., 1971), and complex geological structure and seismicity (Wentworth et al., 1971). The deviations of the focal mechanisms from the model-predicted norm are shown to provide additional insight into the time and spatial

variations of the tectonics in the aftershock region. We then investigate isolated bursts of activity occurring later in the series which suggest a propagating phenomenon that triggers events. Last, we relate the pre-1971 seismicity and the mapped structure in the region to the tectonic features of the San Fernando earthquake series.

2. DATA SET

A major goal of aftershock studies is to outline the associated tectonics of the region. It is therefore desirable to chose the set of aftershocks that is most representative of the major tectonic stress release. This means that the aftershock set must contain the largest events. A practical limit is set at the lower end of the magnitude scale due to a limit on the size of the data set and the signal strengths that the stations record. From this reasoning, the aftershock set that is most representative of the regional tectonic activity includes all events above a certain size.

Two definitions of cutoff size are used. The first set is defined as all aftershocks of $M_L = 4.0$ or larger. P-wave first motions that are immersed in the coda of previous shocks are not used, and this unfortunately precludes the use of events during the first hour of the aftershock series. But the set is complete after the first hour, giving a total of 20 events. A histogram of all aftershocks of $M_L = 4.0$ or larger is shown in Figure 2a. The dark portions

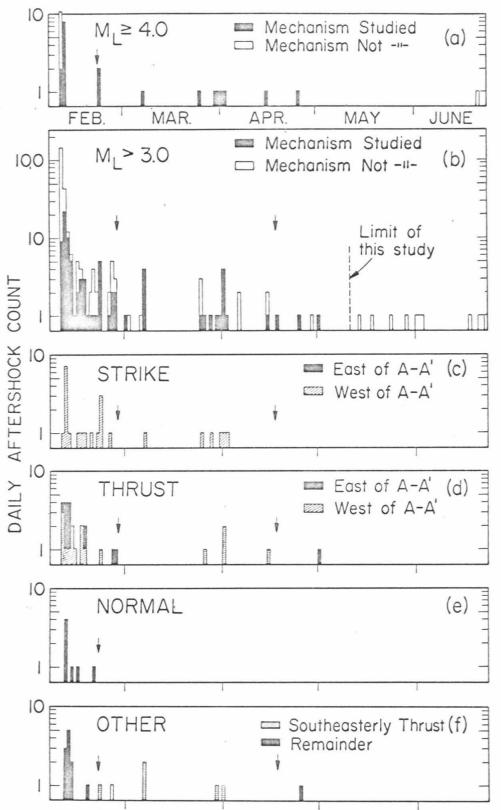


Figure 2. Histograms of the aftershock groups: (a) M $_L$ of 4.0 or greater, (b) M $_L$ greater than 3.0, (c) strike-slip events that fit the model, (d) thrust events that fit the model, (c) events with normal dip slip, (f) others.

indicate the events in the first set.

The second set is defined as those shocks whose P-wave first motions are clear on most of the CIT permanent stations, most of which are between 90 and 300 km from the epicenters. The rationale for this definition is that the data from the more distant stations are much less sensitive to hypocentral location and velocity errors than the close-in portable stations when their first motions are mapped onto the focal hemisphere. Again, the homogeneity of the aftershock set is compromised by the occasional immersion of first motions in the coda of a previous shock. This occurs most often during the first few hours of the aftershock series, and its effect on the conclusions cannot be estimated. One can only assume that the masking is distributed randomly with aftershock type, and that the stress release during the first few hours is not basically different except in rate from the remainder of the series. Some of the conclusions reached below deal with the latter assumption. A histogram of the aftershocks with ${\rm M}_{\!_{\rm T}}{}^{\rm t}{\rm s}$ larger than 3.0 is shown in Figure 2b. The dark portions indicate the events included in the second set.

Table 1 lists all of the events of the second set, which of course includes the first set, along with M_{L} , location, location quality, focal mechanism quality, and number of stations used for first motion determinations (most of these parameters are discussed below). The smallest shock that fulfills the criterion of first-motion

First	Motion	101	7	12	12	12	10	12	13	15	11	17	18	19	20	16	12	13
Focal	Mechanism Quality	В	O	В	O	В	В	В	O	A	В	В	А	C	O	A	A	O
	Location	B*	C@	C@	B*	* 0	C@	C@	C@	C@	C@	ce	B*	B*	B*	C@	C@	C@
	Depth	8.4	80	8	0.6	-1.	8	. 80	8	8	8	· &	8.0	4.7	5.8	8	8	. 8
enter	118°W Lon.	24.0'	24.7	28.0	20,10	25.62	29.5	26.8	28.9	23.7	21.3	32.0	18.12	19.76	24.85	17.8	19.5	27.0
Epic	34°N 118 Lat. Lon	24.7	24.8	24.4	22,46	27,44	22.2	24.7	23.7	26.1	18.5	19,3	22.20	24.67	25,55	21.6	24.4	23.7
	M _L	6.4	3.9	3.9	4.8	4.2	3.9	3.6	3.8	3.4	3.7	3.9	4.0	4.3	4.5	3.7	3.4	3.4
	Time (h:m)	14:00	15:10	15:38	15:58	16:19	17:03	17:19	18:29	20:53	20:56	01:38	03:12	90:50	05:18	05:41	06:24	06:54
	Date	2/09										/10						
	No.	Main	П	2	3	4	2	9	7	8	6	10	11	12	13	14	15	16

Table 1 (continued)

First Motion Stations	, 14	18	17	16	19	20	20	20	. 18	21	22	20	21	21	22	24	25
Focal Mechanism Quality	Α	A	O	A	В	В	A	А	A	æ	A	В	В	A	O	В	В
Location Quality	ce	C@	C@	C@	C@	C@	B*	C@	C@	A*	A*	A*	A*	В	В	B+	A
Depth		8	8	8	8	8	0.9	8	8	6.7	4.4	6.2	4.2	11.3	8.1	5.0	8.0
Epicenter 34°N 118°W Lat. Lon.	18.5	26.5	26.1	15.2	27.7	25.6	27.30	28.5	16.9	25.12	29.20	21,98	26.16	18.07	21,41	16.63	26.32
Epic 34°N Lat.	18.1	21.4	24.1	9.61	26.8	27.2	23.06	23.4	20.7	23.94	21.69	23.74	26.75	22,51	23.14	24.50	25.05
전기	3.5	3.4	3.8	3.2	3.4	3.2	4.2	3.5	3.4	4.3	4.2	4.2	4.2	3.5	3.5	3.5	3.2
Time (h:m)	00:20	07:14	07:27	09:33	10:00	11:29	11:31	11:45	12:42	13:49	14:35	17:38	18:54	19:06	23:42	00:30	03:43
Date	2/10								,							/11	
No.	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33

Table 1 (continued)

First Motion Stations	22	22	26	26	26	23	26	25	24	27	26	25	26	28	23	30	27	23	22	25
Focal Mechanism Quality	В	A.	В	В	В	A	В	В	В	¥	A	A	A	A	A	A	A	A	A	А
Location	B+	А	B+	A+	В	Α	A	A	В	A	А	В	A	В	A	В	A	A	A	В
Depth	11.3	12.4	5.0	0.5	2.4	2.3	6.4	4.6	1.8	8.1	2.0	9.5	9.2	1.6	9.4	1.1	12.9	7.9	7.6	9.0
118°W Lon.	32.13	26.50	20.34	18.83	19.28	27.70	26.87	20.21	21.28	25.73	27.18	25.86	25.50	.32,80	23.03	30.67	24.63	26.48	26.12	32.61
Epicenter 34°N 118' Lat. Lon.	18,39	27.41	24.91	20.20	17.78	22.07	24.00	21.11	21.56	25.56	21.55	24.41	24.77	19.64	23.86	17.97	28.27	24.42	25.65	17.25
χ ¹	3.4	3,3	3,3	3.5	3.5	3.6	3.7	3.7	3.2	3,3	3.4	3.4	3.9	3.2	3,3	3.8	3.9	3.4	3.4	3.5
Time (h: n)	04:07	07:33	09:24	11:32	14:21	16:43	19:35	23:35	60:80	09:20	09:52	15:02	16:22	77:90	03:38	13:44	08:04	95:80	13:03	04:37
Date	2/11					4			/12					/13	/14		/15			/16
No.	34	35	36	37	38	39	40	41	42	43	77	45	94	47	84	64	20	51	52	53

Table 1 (continued)

First Motion Stations	22	23	20	17	22	21	20	27	26	21	19	21	17	20	20	18	19	33	27	23
Focal Mechanism Quality	д	A	В	A	В	, д	A	А	A	A	A	A	В	A	A	O	O	A	C	В
Location Quality	A	А	А	А	В	A	В	A*	A*	А	A	А	A	В	A	А	A	A*	А	A
Depth	9.3	10.0	5.3	4.4	-1.5	15.2	8.9	6.9	7.2	6.4	6.2	10.8	7.5	-2.0	7.5	10.0	4.4	3.2	6.4	8.0
nter 118°W Lon.	26.86	17.87	18.38	25.85	27.58	24.38	31.86	26.32	25.65	25.58	26.70	24.64	26.51	. 21,79	22.95	27.21	26.00	27.35	26.00	26.22
Epicenter 34°N 118 Lat. Lon	24:40	20.07	21.46	23.18	21.45	27.24	17.69	23.85	23.52	23.87	23.89	26.48	25.23	20.17	25.13	27.25	24.05	21,19	22,59	22.65
M N	3.3	3.1	3.5	3.2	3.5	3.6	3.6	4.7	4.5	3.5	3.5	3.7	3.2	3.5	3.5	3.3	3.4	4.5	3.9	3.3
Time (h:m)	80:10	14:39	10:15	22:09	02:45	60:80	02:42	05:50	07:15	07:43	14:06	16:04	11:27	20:27	03:33	21:22	04:28	01:33	95:90	07:11
Date	2/16		/17	/18	/19	/20	/21					/24	/25		/26		3/01	101		
No.	54	55	99	57	58	59	09	61	62	63	79	65	. 99	29	89	69	70	71	72	73

Table 1 (continued)

First Motion Stations	25	28	19	28	29	30	23	31	21	28	30	28	20	22	
Focal Mechanism Quality	В	A	A	A	A	A	В	A	A	д	A	A	Ą	А	
Location	A	A*	A	А	A*	A*	В	A*	А	А	A*	A*	B*	А	
Depth		4.6	11.3	5.7	2.6	2.1	6.3	7.1	7.9	7.3	3.0	4.2	-2.0	4.8	
Epicenter 34°N 118°W Lat. Lon.	22.85	28.47	27.68	28.39	27.84	30.89	35,34	25.19	25.85	25.73	31.70	34.62	18,86	24.15	
Epice 34°N Lat.	24.83	21.38	28.09	21.28	17.74	17.15	15.94	24.72	24.32	23.73	17.03	15.88	22.09	26.00	
되	3,3	4.2	3.3	3.7	4.1.	9.4	3.4	4.2	3.2	3.5	4.0	4.2	4.0	3.6	
Time (h:m)	21:36	22:54	20:55	17:16	08:54	14:52	01:54	15:03	21:15	21:18	05:40	11:14	14:48	04:25	
Date	3/25	3/25	/26	/28	/30	/31	4/01				/02	/15	/25	5/01	
No.	74	75	9/	77	78	79	80	81	82	83	84	85	98	87	

@Location modified from <u>Allen et al.</u> [1971] +Location from <u>Hanks et al.</u> [1971]

^{*}Location from <u>Allen et al.</u> [1972]

clarity at most of the CIT telemetry stations has an ${\rm M_L}$ of 3.1. Essentially all shocks with an ${\rm M_L}$ of 3.5 or larger fulfill the criterion and are included unless masked by a previous shock. The histogram of Figure 2b shows that most of the aftershocks above ${\rm M_L}$ = 3.0 after the first two days have first motions that are clear enough to be included in the second set, and it can be considered to have an approximate magnitude cutoff of ${\rm M_L}$ = 3.3.

The stations used for P-wave first motions in this study with their operating agencies, coordinates, and periods of operation are given in Table 2. The station locations in relation to the approximate epicentral distribution of aftershocks (Allen et al., 1972) are shown in Figure 3. All readings were made from short-period vertical seismometers. Although 47 stations were used for first motion studies, varying periods of operation for the portable stations and the weakness of the first arrival of smaller shocks at distant stations reduced the actual number of first motions read per event. The number of readings for most events ranged from 10-20 for the first twenty hours of the aftershock series and 20-30 for the remainder of the study time period. Some instrument polarity reversals did appear, usually in instrumentation that was temporary or involved complex electronics such as a telemetry link from seismometer to recorder. However, the station coverage and the number of events were sufficient to reveal the reversal. Also, in almost every case, a reversal could be confirmed by polarity checks with teleseismic events.

Table 2

Station	Agency	Lat. N.	Long. W.	Period of Operation
AGM	EML	34 29.5	118 19.3	2/10-4/24
ANM	EML	34 27.2	118 30.6	3/15-4/24
BAR	CIT	32 40.8	116 40.3	permanent
BHR	USC	34 00.5	118 21.7	2/27-present
BLA	CIT	34 14.8	118 26.7	3/02-present
BQR	CIT	34 17.6	118 35.4	2/09-5/07
BRC	CIT	34 17.6	118 35.4	2/09-5/07
BRCL	LGO	34 23.0	117 46.3	2/12-2/14
CLC	CIT	35 49.0	117 35.8	permanent
CSP	DWR	34 17.9	117 21.5	permanent
CWC	CIT	36 26.4	118 04.7	permanent
ENG	CIT	34 08.4	118 05.2	semi-permanent
GLA	CIT	33 03.1	114 49.6	permanent
GOK	CIT	34 23.1	118 28.3	2/10-5/06
GOR	LGO	34 46.9	118 48.0	2/10-2/14
GSC	CIT	35 18.1	116 48.3	permanent
HAY	CIT	33 42.4	115 38.2	permanent
HCC	USC	33 59.6	118 23.0	2/28-present
IND	CIT	34 25.2	118 16.2	2/10-4/22
IPC	USC	33 58.2	118 20.4	3/04-present
IRC	CIT	34 23.3	118 23.9	2/09-5/07
ISA	CIT	35 38.6	118 28.6	permanent
JBF	USC	33 59.6	118 20.7	3/25-present
LSV	LGO	34 36.4	118 19.5	2/10-2/12
MER	LGO	34 29.8	118 02.4	2/12-2/14
MLM	EML	34 23.4	118 04.8	2/10-4/24
MWC	CIT	34 13.4	118 03.5	permanent

Table 2 (continued)

Station	Agency	Lat. N.	Long. W.	Period of Operation
OMM	EML	34 19.8	118 36.0	2/25-4/24
PAS	CIT	34 08.9	118 10.3	permanent
PLM	CIT	33 21.2	116 51.7	permanent
PYR	DWR	34 34.1	118 44.5	permanent
RTM	EML	34 35.8	118 14.8	2/10-3/15
RTR	CIT	34 11.9	118 09.4	semi-permanent
RVR	CIT	33 59.6	117 22.5	permanent
SBC	CIT	34 26.5	119 42.8	permanent
SCF	NOS	34 26.3	118 17.3	2/10-2/17
SGM	NOS	34 23.1	118 24.8	2/10-2/17
SHC	NOS	34 30.5	118 21.8	2/10-2/17
SOC	CIT	34 26.1	118 21.7	2/10-5/06
SWM	CIT	34 43.0	118 35.0	permanent
SWML	LGO	34 42.1	118 32.1	2/10-2/14
SYP	CIT	34 31.6	119 58.7	permanent
TIN	CIT	37 03.3	118 13.7	permanent
USC	USC	34 00.8	118 17.3	2/06-2/28
USCB	USC	34 00.1	118 20.5	2/12-2/14
USCP	USC	34 02.7	118 32.1	2/12-2/14
WSM	EML	34 36.4	118 33.5	2/10-4/24

CIT: California Institute of Technology

DWA: California Department of Water Resources

EML: Earthquake Mechanisms Laboratory, NOS

LGO: Lamont-Doherty Geological Observatory

NOS: Las Vegas Branch of NOS

USC: University of Southern California

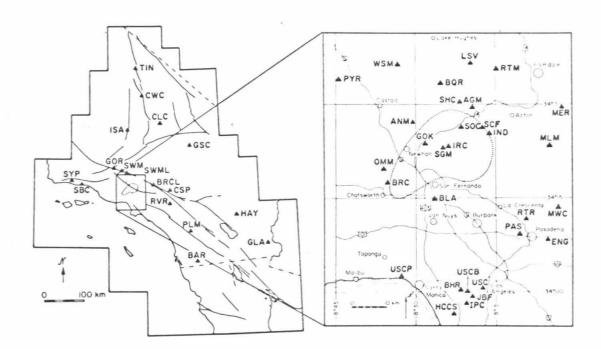


Figure 3.

Location map of stations used for first motion studies; station data are listed in Table 2. The approximate aftershock zone is shown for reference.

3. HYPOCENTRAL LOCATIONS

The hypocentral locations done by us are computed with the same method as that used by Allen et al. (1972) except that the closer stations are weighted more heavily, especially for shallow hypocenters. The stations used for locations are those of CIT and the Earthquake Mechanisms Laboratory (EML) shown in Figure 3 and Table 2, and in some cases SUS, which is a station of the United States Geological Survey's National Center for Earthquake Research (see Wesson et al., 1971). For shocks in the western extremity of the aftershock region, the westerly stations BRC, OMM, and SUS are given large weights to offset the bias introduced by the fact that most of the close stations lie to the east. Because the aftershocks in the set are all larger than M_{T} = 3.0, S-wave arrival times are difficult to measure on the high-gain film records of the CIT portable stations. These S-wave arrival times that are read from the CIT stations and those listed in the EML data reports are given half the weight of their associated P-wave arrival times.

In the earlier part of the aftershock sequence, approximately the first twenty-four hours, not enough portable stations were in place for precise hypocentral locations. Allen <u>et al</u>. (1972) recomputed the locations of the events with $M_L = 4.0$ or larger in this early period by applying time correction factors to arrival times from the permanent southern California stations. The corrections were computed from precise locations of later shocks by use of the

portable stations. The locations taken from Allen et al (1972) are indicated with stars in Table 1. The remainder of the locations in this early period are from Allen et al. (1971) with some modification to account for systematic epicentral shifts which are present when comparing locations from only the permanent station data to those from the closer portable station data. The modified locations are indicated in Table 1 with @ symbols. Four of the event hypocenters have been computed by Hanks et al. (1971) and are indicated by crosses in Table 1. The remaining locations were computed by us.

The accuracy of the hypocenters in this study is estimated following the definitions of Allen et al. (1972). Depending on the number and location of the stations and the standard error of the computer solution, the quality of the hypocentral locations is divided into three categories: "A" locations are generally accurate to within 2 km horizontally and 4 km vertically; "B" locations are felt to be accurate to within 4 km horizontally and 8 km vertically; and "C" locations include all those that are considered less accurate. The location qualities are given in Table 1. As can be seen by the definitions, the accuracy of the epicentral determination is much better than that of the depth; this is especially true for those events with shallow depths. Direct confirmation of the location accuracies is extremely difficult short of drilling down and firing a large explosive at hypocentral depths. However, the accuracies estimated for the different qualities are considered conservative

based on variations of the hypocenter as a function of reasonable changes of velocities, station corrections, station combination, and station weighting. Because all of the "A" and "B" quality events are located in essentially the same manner, hypocenters in the same region should be located more accurately relative to each other than is implied by the above estimates of absolute location accuracy.

4. FOCAL MECHANISM DETERMINATIONS

P-wave first motions are used exclusively for the focal-mechanism determinations. The first motion reading is classified as good or fair depending on a subjective estimate of the onset clarity and how confident we are that the motion is truly the first arrival; doubts in the latter situation occur most often at distances where P_n is the first arrival. A record is also kept of arrivals that have emergent character when, by a subjective judgment involving the epicentral distance and size of the aftershock, one would expect the first motion to be sharp; these arrivals are designated as having nodal character implying that they map on the focal sphere near one of the nodal planes of the double-couple mechanism to the data, it is found that these points indeed tend to map near the nodal planes. It is therefore believed that, with proper precautions, they can be

used in future studies as additional information in a focal mechanism fit.

The source takeoff angle is calculated by ray tracing as a function of the aftershock's epicentral distance and depth using the P-wave velocity model shown in Figure 4. The model is based mainly on the results of Healy (1963), who analyzed a reversed refraction profile between Santa Monica Bay and Camp Roberts, California, that passes very close to the epicentral area. Takeoff angles were calculated also for the velocity model shown as a dashed line in Figure 4, which includes a 7.2 km/sec layer at the base of the crust. However, the rays refracted along the top of this layer were first arrivals for only a very small epicentral distance range, which made the difference between the two velocity models insignificant. This is especially true in light of the large lateral variations in shallow crustal structure demonstrated by Wesson and Gibbs (1971). These variations probably have much greater effect on the ray takeoff angles and azimuths, and if one were to use a more sophisticated velocity model, lateral variations should be included. The use of the more distant stations helps to minimize these effects because the rays leaving the hypocenter in a downward direction presumably encounter less drastic lateral changes in velocity. Wesson and Gibbs' results generally confirmed the shallow part of Healy's (1963) model with crystalline basement rock velocities of around 6 km/sec. Although they obtained near-surface sediment velocites in the Santa Susana

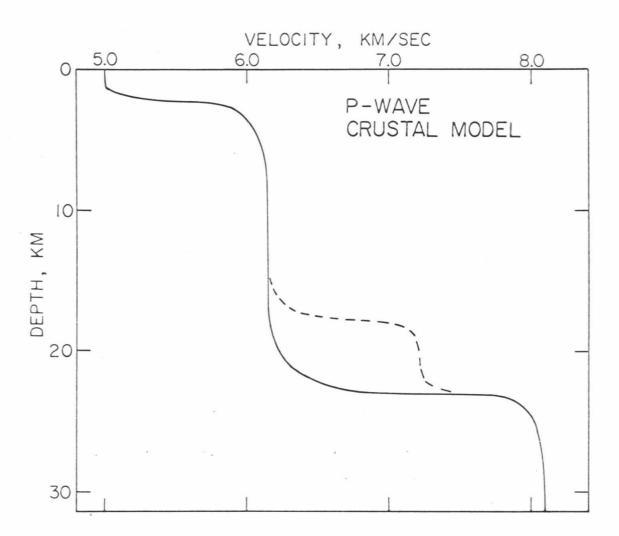
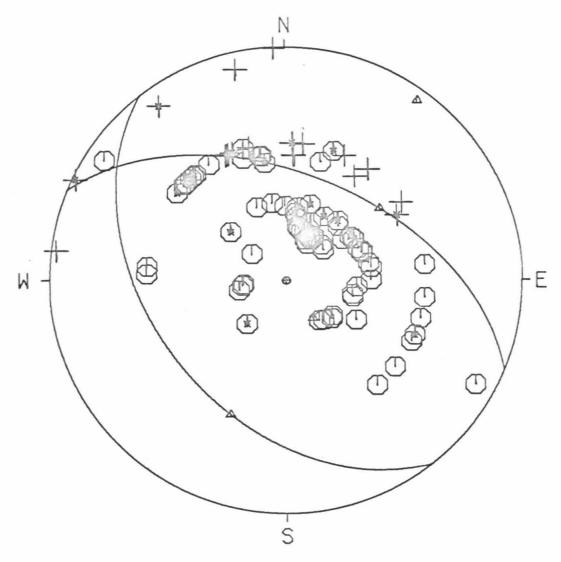


Figure 4.

P-wave velocity distribution used to map the first motion data onto the focal sphere. The dashed line indicates a variation of the velocity that produced no significant changes in the mapping.

Mountains as low as 3.4 km/sec, this velocity is not used here in the focal mechanism computations for shallow hypocenters in the southwest aftershock region. The initial ruptures of the larger aftershocks would be in the stronger, and therefore higher-velocity, rocks because they support most of the stress. Thus, the shallow hypocenters, which are always the most inaccurate, are assumed to be deep enough to be in higher-velocity sedimentary or crystalline rock.

The focal mechanism of the main shock has been recomputed using some new close-in station data and estimates of the P_g - P_n breakover distance based on the aftershock data at stations near this range. The best fit to the P-wave first motion data constrains the fault plane parameters to: strike, N 67° (±6°) W; dip 52° (±3°) NE; and rake 72° (67°-95°) left lateral. Choice of the northeast-dipping plane as the fault plane rather than the auxiliary plane is based upon its close correspondence to the observed surface faulting, the hypocentral locations of aftershocks, and the regional geology. The best fit is determined by minimizing the reading misfits to a double couple with an algorithm that is described in Appendix 1. The fit to the data is shown in Figure 5. Circles are compressions and crosses are dilatations. It is interesting to note that the fault plane is very well determined but the rake angle, which is tied to the auxiliary plane, is much less so; this illustrates that station distributions can selectively constrain some focal mechanism parameters much better than others.



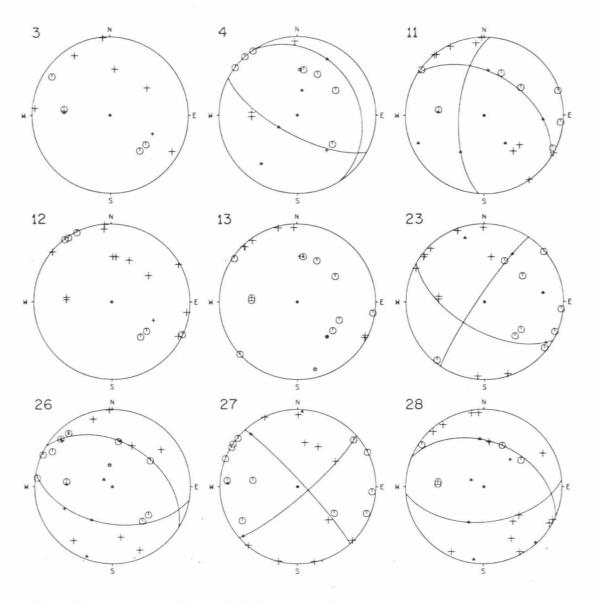
- O Compression (Good, Fair)
- + + Dilatation (Good, Fair)
 - * Nodal Character
 - Slip Vectors, C Axis, T Axis

Figure 5.

The main February 9, 1971, San Fernando shock first motion data and the best fit of the double-couple mechanism. The data are shown on an equal-area projection of the lower focal hemisphere. Canitez and Toksőz (1972) have estimated the rake angle from surface waves to be 45°, which would indicate a much greater average strike-slip over the fault plane than that of the initial rupture and, as seen later, the aftershocks. However, the determination was made using only six stations covering one quadrant at the source, and the effects of varying crustal structures were not calculated for the surface-wave paths. Thus, while their rake is interesting and has important implications, we prefer to withhold an attempt to explain this deviation pending a more complete confirmation of the value.

The double-couple focal mechanisms of the aftershocks are fit to the data by eye under the influence of the reading qualities, good or fair. An estimate of the quality of the solution is made based on the degree to which data constrain the orientation of the solution. "A" solution parameters are felt to be within 10° of the actual values, "B" solution parameters are felt to be within 20°, and "C" events are all others and are not assigned a solution. These definitions are intended to apply to the worst-constrained parameters of the solution.

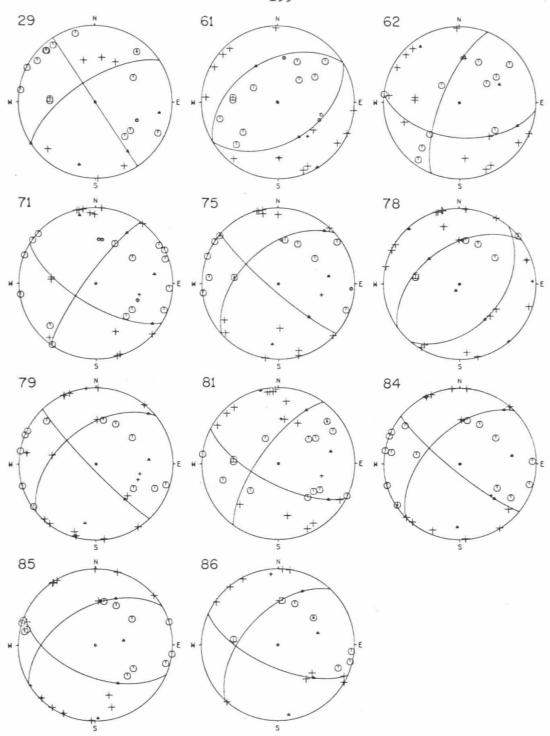
Figure 6 shows data for all aftershocks with $M_L = 4.0$ or larger and Appendix 2 shows first motion data and focal mechanism solutions for all the aftershocks investigated; the plots include first motion data and the focal-mechanism solutions mapped on equal-area stereo plots of the lower focal hemisphere. The event numbers correspond



- O · Compression (Good, Fair)
- + + Dilatation (Good, Fair)
- Nodal Character
- * Slip Vectors, T Axis, C Axis

Figure 6.

 ${\rm M}_{\rm L}$ of 4.0 or greater aftershock first motion data and their focal mechanism fits. The numbers correspond to the events in Table 1. The data are shown on an equal-area projection of the lower focal hemisphere.



to those in Table 1.

5. TECTONIC INTERPRETATION

5.1 Magnitude 4.0 or larger shocks and development of a fault model. As defined above, the first set of aftershocks consists of those with an M_T = 4.0 or larger. The fit of focal planes to the first-motion data shown in Figure 6 is transformed to schematic diagrams of the quadrants in the lower focal hemisphere delineating the areas of compressional (dark) and dilatational (light) first motions and are shown at their epicentral locations in Figure 7. larger diagrams denote "A" quality focal mechanisms, and the smaller are of "B" quality. Three of the twenty events have "C" quality focal mechanisms with no determination of the planes, but their epicentral locations are included in the figure. This set is complete after the first hour of the series and Figure 7 shows that most of the activity of these largest shocks is on the western limb, which is separated approximately from the rest of the aftershock sequence by the line A-A'. It is also apparent that over half of the focal mechanisms along the western limb have a steeply-dipping plane striking northeast parallel to the limb direction with left-lateral strike-slip fault motion. If these strike-slip mechanisms are connected to a single surface that is related to the tectonic motion of the main shock, then the strike-slip surface must be below the main thrust

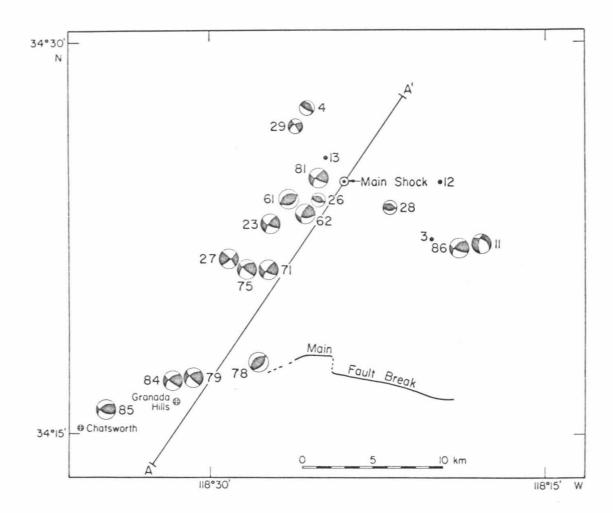


Figure 7.

 $\rm M_L=4.0$ or greater aftershocks as schematic diagrams of the compressional (dark) and dilatational (light) first-motion quadrants in the lower hemisphere. The diagrams are at the event's epicenters and the numbers refer to those in Table 1. The size of the diagram refers to its focal mechanism quality of "A" (larger) or "B" (smaller, see text). All events with "A" and "B" quality focal mechanisms are included and the locations of three "C" quality mechanisms are indicated by points (Events 3, 12, and 13).

fault plane defined by the surface rupture, focal mechanism and hypocenter of the main shock. If the strike-slip surface were above the main fault plane, the motion would be right lateral for northeast striking faults, contrary to the observed motion. This distribution of focal mechanisms can be explained by the fault surface model first presented in Allen et al. (1972) and shown in Figure 8. It was based on many of these same data. The figure is a schematic structural contour map showing simplified contours, in kilometers, on the fault plane. The fault surface associated with the main thrust rupture is in the eastern portion of the map. In the vicinity of the western limb of aftershocks, the surface has a steep flexure that is down-stepped to the west and is associated with left-lateral strike slip motion. This flexure tended to limit the initial rupture to the west and, because of the resulting stress concentration in this zone, it was responsible for most of the aftershock activity. Two events, numbers 4 and 85 in Figure 7, are on the western edge of the western limb of aftershocks but their mechanisms are mainly thrust, similar to the main shock. These events can be explained by the flattening of the surface to the west as shown in Figure 8. However, the model requires that the thrusts west of the flexure be deeper than those to the east; this is one of the important hypothesis to be tested with the second aftershock set.

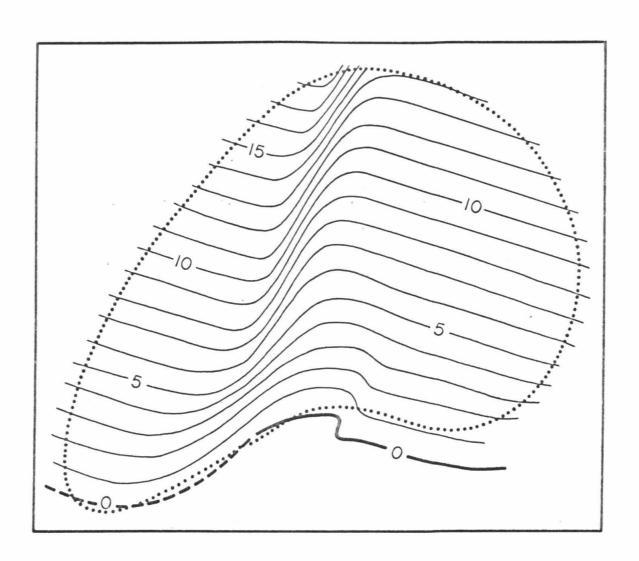


Figure 8.

San Fernando fault surface model showing the surface as simplified contours, in km, with a downstep to the west that explains the strike-slip events along the west limb of the aftershock zone (Allen et al., 1972).

5.2 Test of the model with the second aftershock set. The fault model developed for the twenty M_{L} = 4.0 or larger shocks should be representative of the major strain release of the aftershock series. The second and larger set of 87 aftershocks including smaller events can now be analyzed with the model as a test framework.

Figure 9 presents all of the "A" and "B" quality focal mechanisms that agree with the model of Figure 8. As before, they are shown as a map of schematic diagrams of the compressional (dark) and dilatational (light) first-motion quadrants in the lower focal hemisphere. The epicentral locations may be slightly in error due to crowding in the figure. Two-thirds (50/75) of the "A" and "B" focal mechanisms are included in Figure 9; certainly this represents strong support for the fault model of Figure 8. Certain characteristic features noted in Figure 6 are preserved here in Figure 9. Most of the activity is in the well-defined western limb of the aftershock sequence. Half of these events in the western limb have a plane dipping steeply to the northwest and striking to the northeast roughly parallel to the limb, and the motion on the planes is predominantly left-lateral strikeslip. The criterion for designating these aftershock focal mechanisms as mostly strike-slip or thrust is simply whether the rate (the angle in the fault plane between horizontal and the slip vector) is less than or greater than 45° respectively. While it appears that some thrust events appear to map within the western limb, a more complete location analysis done below shows that the thrusts in this area

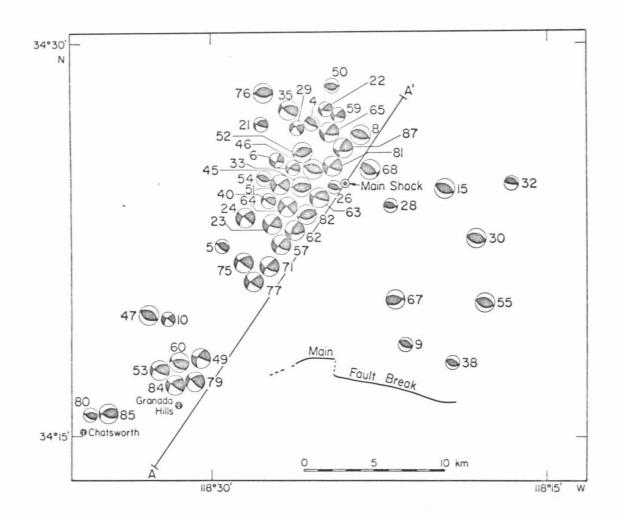


Figure 9.

Map of all "A" and "B" quality focal mechanisms that fit the model of Figure 8 (see caption of Figure 7). The epicenters may be slightly in error where the diagrams are crowded.

clearly tend to occur deeper and to the west of the strike-slip events.

The histograms of the thrust and strike-slip events that agree with the model are shown in Figures 2c and 2d. There is little difference in their overall time distribution, but if they are separated into east and west regions by A-A' (as indicated by different shading in the figure), they show that the model-related events east of A-A' larger than $M_{_{\rm T}}$ = 3.0 are absent after the first 18 days of the series for two months. Thus, at least two and perhaps three preliminary stages in the aftershock sequence (separated by the arrows in Figures 1c and 1d) are defined by the events that fit the fault model of Figure 8: the first 18 days during which thrusting activity extended east of A-A'; February 27 to about April 17 when activity was mostly confined to the west of A-A'; (this stage, from evidence presented below, may have started 6 days earlier); and perhaps a third stage beyond April 17 when model-related activity east of A-A' is presented again. This division also coincides with the overall distribution of aftershocks with time in Figure 2a. The first stage contains the initial surge of aftershocks defined by a rather sharp cutoff on February 26; the second stage is characterized by a burst of aftershock activity initiated by $M_T = 4.0$ or larger shocks (these series are discussed below); and the third stage is characterized by a low aftershock rate with few $M_{\tilde{L}}$ = 4.0 or larger events.

It is difficult to compare the whole set of focal mechanisms with the model of Figure 8 by placing them all on a single map because they are too numerous. A more compact method of comparison is provided by the classic parameters of the double-couple focal mechanism: the two slip vectors, the compression axis, and the tension axis. The model predicts certain ranges of these parameters which are shown in Figure 10; the approximate deviations from the ranges corresponding to the "A" (10° variation, shaded region) and "B" (20° variation, open region) quality focal mechanisms indicate the regions of expected scatter. The slip vector in the auxiliary plane, the compression axis, and the tension axis all sweep out extensive paths. The only fixed parameter is the north-northeast slip vector in the fault plane. This results from the requirements that the medium through which the fault surface passes be perfectly rigid and that no voids be created along the surface. The data for all of the "A" and "B" quality focal mechanisms are shown in Figure 10 with symbols representing strikeslip (squares) and thrust (circles) that agree with the model, and normal (N) and other (X) that do not agree with the model; the last two classifications are discussed below. "A" quality focal mechanisms are indicated by either solid points or circled letters. Most of the aftershocks fit the fault-surface model of Figure 8 very closely. The compression axes point generally north-south and nearly horizontally, and the tension axes point between vertical

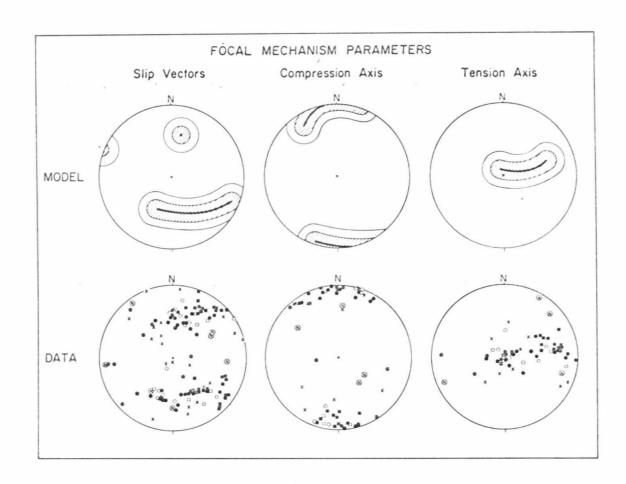


Figure 10.

The classic focal mechanism parameters (slip vectors, compression axis, and tension axis) on the lower focal hemisphere for the model of Figure 8 and for the data consisting of all "A" and "B" quality focal mechanisms. The symbol explanation is given in the text and in Figure 11.

and east depending on whether the mechanism is thrust or strike slip, respectively. The slip vectors in the fault plane scatter a little more than expected; the strike-slip data dip shallower and point more easterly than those of the thrust mechanisms. While it is difficult to completely rule out some systematic bias introduced by the station distribution or the focal-mechanism fitting technique, this consistent deviation between the thrust and strike-slip fault-plane slip vectors is considered real. As will be seen below, it has some bearing on the idealistic assumptions of rigidity and volume conservation used to formulate the initial model.

Precise locations of the aftershock hypocenters provide an important means of testing the three-dimensional fault surface model, especially because of the fault's complex non-planar nature. Only "A" and "B" quality locations in conjunction with "A" and "B" quality focal mechanisms are used, and these are presented in map view in Figure 11. The symbols represent strike-slip and thrust mechanisms that agree with the model, and normal and other mechanisms as in Figure 10. As identified earlier, there is a well-defined linear zone along the west of the line A-A' containing a majority of the events. We now project all of the points west of A-A' in Figure 11 onto a vertical plane along A-A' and present the resulting cross-section in Figure 12a. All of the strike-slip events south of the main event in this plot are limited to a shallow-dipping zone indicated by shading in the figure. Further, all but one thrust event,

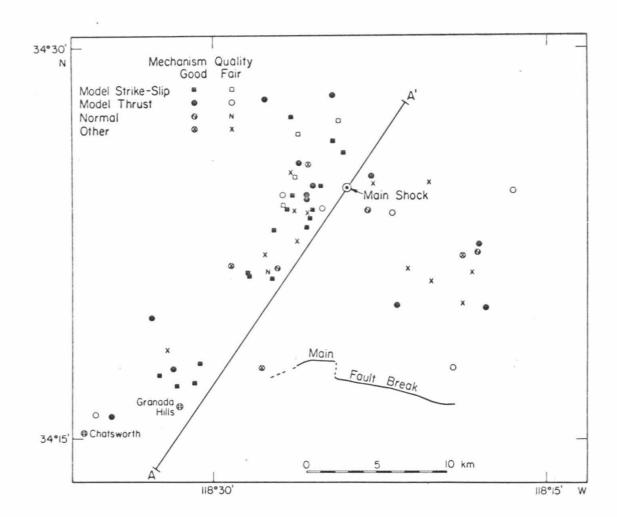


Figure 11.

Epicentral location of shocks with "B" or better quality for \underline{both} locations and focal mechanisms.

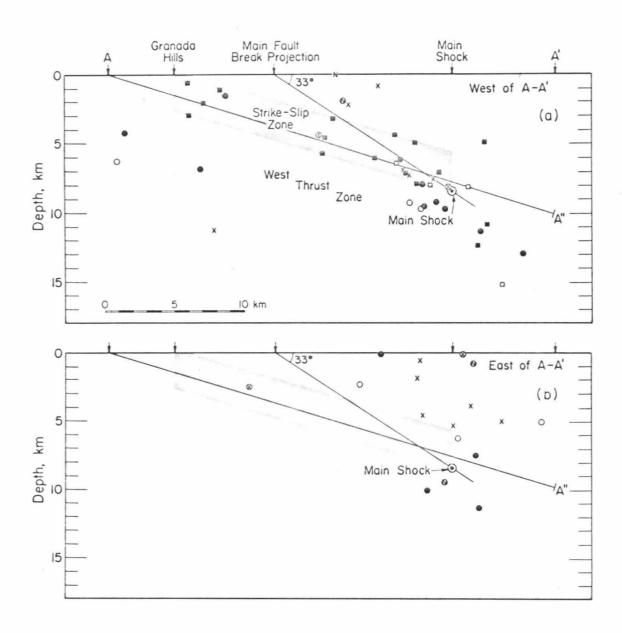


Figure 12.

Projection of hypocenters from Figure 11 onto the cross-section A-A' for (a) aftershocks west of A-A' and (b) aftershocks east of A-A'. The west thrust zone and strike-slip zone shown in (a) correspond to the structure in the westerly part of the model in Figure 8.

which is towards A and is fairly distant from A-A' (see Figure 11), plots below the strike-slip zone. This is strong confirmation of the downstep in the western portion of the fault surface model in Figure 8. The same cross-section for those events east of A-A' is shown in Figure 12b. The depths of these events are scattered but tend to plot above or in the upper part of the strike-slip zone with only three exceptions, Events 30, 48, and 55 (locations are shown in Figures 9 and 11). A further characteristic of the fault surface model is that the thrust mechanisms in the western limb of aftershocks should be not only deeper but further west compared to the strikeslip mechanisms. In Figure 13, we project all of the points of Figure 10 onto a plane perpendicular to the line A-A" (shown in Figure 12a); this corresponds to viewing the fault surface nearly edge-on but at a somewhat shallower angle. It is immediately apparent that the thrust events to the left (northwest) of the main shock and A-A' tend to be below and to the northwest of the strike-slip zone as the model predicts.

As noted previously, half of the focal mechanisms along the western limb have a steeply-dipping plane striking northeast nearly parallel to the limb direction with left-lateral strike-slip motion (Figure 9). The model shown in Figure 8 predicts that the strike of this plane should vary from a direction exactly parallel to the limb direction (the direction of A-A') for a perfectly vertical fault surface to a direction somewhat east of the A-A' azimuth for

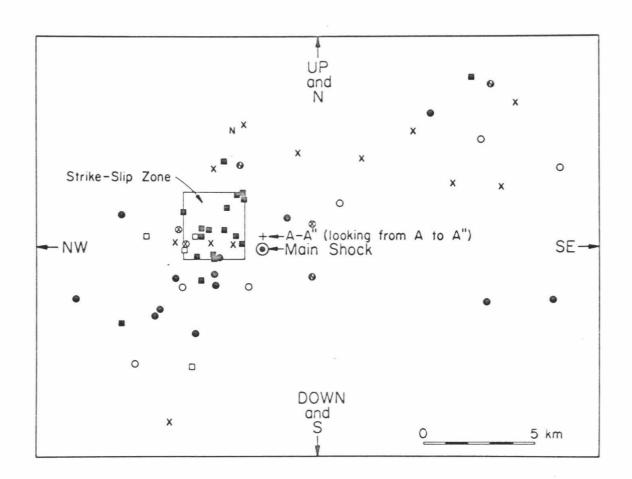


Figure 13.

Projection of hypocenters from Figure 11 onto a plane perpendicular to A-A" (see Figure 12). Here, the strike-slip zone of Figure 12 is given a third dimension.

a fault surface dipping steeply to the northwest. Northeast strikes of all of the strike-slip events in the western limb are plotted in the azimuthal histogram of Figure 14. The histogram interval is 5° and the direction of A-A' is shown for reference. The data have a well-defined peak just east of the direction of A-A' and thus indicate consistency with the model.

The hypocentral location of the main shock (Figure 12) is surprisingly close to the aftershock distribution in light of its estimated location accuracy (within 4 km horizontally and 8 km vertically). Hanks (1972), based on his analysis of the Pacoima Dam accelerogram and distant recordings of the main shock, suggested a hypocentral depth of 12 to 15 km. But, this would be in the range of both the aftershock distribution and the calculated main shock hypocenter if the latter is shifted down and to the northeast about 4 km, an adjustment within the stated location accuracy. Thus, the main shock depths estimated by Allen et al. (1972) and Hanks (1972) generally agree with the aftershock distribution and clearly show that the initial rupture of the main thrust fault was near its lower, northern-most edge.

5.3 Events that deviate from the model. One-third (25/75) of the "A" and "B" quality focal mechanisms do not fit the fault-surface model of Figure 8. An important subset of this group is composed of

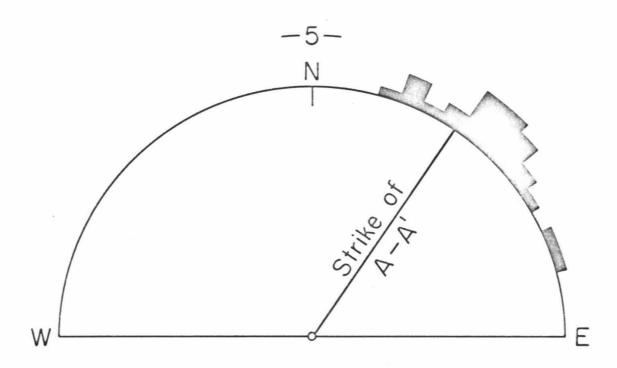


Figure 14.

Radial histogram in five degree intervals of fault-plane strikes for all strike-slip events in the western aftershock limb. The model of Figure 8 predicts that the strikes would group slightly to the east of the direction of A-A', as the data confirm.

focal mechanisms that have normal fault motion, that is, those for which the center of the equal-area projection falls in the dilatational quadrant. Figure 15 presents all seven of the "A" and "B" quality focal mechanisms that have normal fault motion. They are shown as a map of schematic diagrams of the double-couple mechanisms. For these events, the tension axis is nearly horizontal and the compression axis is shifted significantly from its usual north-south, nearly horizontal configuration. This is seen in the data for the normal mechanisms designated as "N" in Figure 10. Three of the normal events are scattered in the eastern aftershock region, one is near the main shock epicenter, and a clustered group of three centers on the line A-A' in the central portion of the west aftershock limb. The crosssections in Figure 12a and 12b (again, these include only "A" and "B" locations) show that the scattered normal events in the eastern region are shallow; the one near the main shock epicenter is deep, possibly a bad location; and the group straddling A-A' is shallow. The shallow depth and association with the upper thrust block of all but perhaps the normal event near the main shock agree with effects due to curvature of the main fault surface as discussed below. However, the tight clustering of normal events along the edge A-A' of the strike-slip zone indicates that other stress disturbances may play a role in these three events. A clue for such an inhomogeneous stress in this region has already been provided by the discrepancy of fault-plane slip vectors in Figure 10 between strike-slip and thrust

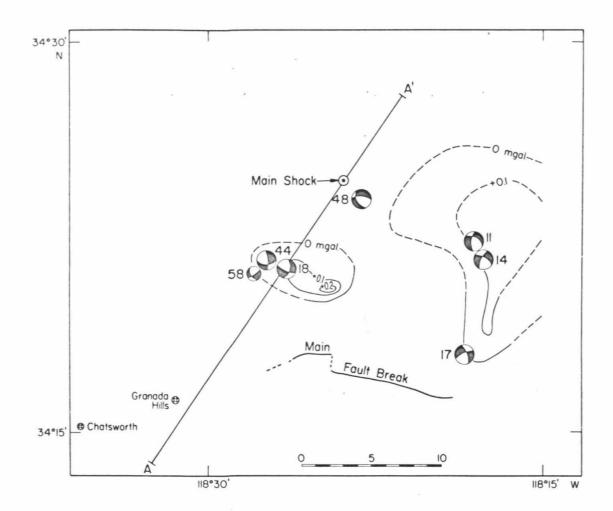


Figure 15.

Map of focal mechanisms of the normal group (see the caption of Figure 7). Their locations correspond well with areas of shallow tensional stress associated with ground subsidence that is indicated by the outlined areas of positive gravitational acceleration change (Oliver et al., 1972). Negative changes are not shown.

events. If, as the slip vector data indicate, the upper block's southerly motion is more to the west in the strike-slip zone than that to the east of A-A', then the motion would tend to create a void along the main fault's downstep which would manifest itself as extension in an elastic material.

Exceptionally good confirmation of the areas of compressional release is seen in Oliver et al. (1972), Figure 3). Their data, which show the change in gravitational acceleration due to the tectonic motions of the San Fernando series, outline two areas of acceleration increase; this implies a decrease in the ground elevation that results from local compressional release. The areas of positive acceleration change (after Oliver et al, 1972) are outlined in the map of the normal events in Figure 15. One area, relatively confined in lateral extent, coincides with the location of the three normal events along the central west aftershock limb. A second much broader area coincides with the normal events in the eastern aftershock area.

A histogram showing the time sequence of the normal events is shown in Figure 2e. If the larger set of aftershocks is a fair representation of the aftershock activity, then we must conclude that events with normal faulting cease after only ten days (February 29) into the aftershock sequence. One might fairly inquire as to the statistical significance of this distribution. This can be easily estimated by assuming that the normal events are randomly distributed throughout the set and calculating the joint probability that they

would all occur before February 19. The probability is 4%, which indicates that the observed lack of normal events after February 19 is significant. Thus, no matter what their source, the tensional stresses causing the normal events seem to be compensated within a time period of about ten days. This falls within and further characterizes the first stage of the series defined earlier.

The remaining 18 events which do not fit the fault surface model are shown in the map of schematic focal mechanisms in Figure 16. A commonly occurring focal mechanism type in this set can be classified as northeast striking thrust faults. The events of this type which fall near the strike-slip zone, Events 61, 66, 76, 73, 74, 78, and 83, can be explained by southeasterly thrust motion on the fault surface model of Figure 8. This motion is consistent with the idea of compensation for the deviatory tectonic movements causing tension and normal events along A-A'. Support for this hypothesis comes from the fact that the last normal event occurred in the central west limb vicinity along A-A' on February 19 (Event 58) and the first compensatory thrust event described above occurred on February 21 (Event 61), less than three days later. Thus, this time would mark the initiation of a north or northwest compressional addition to the local stress in the strike-slip zone which stops the shallow normal events and even causes a series of compensatory southeasterly thrust movements on the main downstepped fault surface. As can be seen in

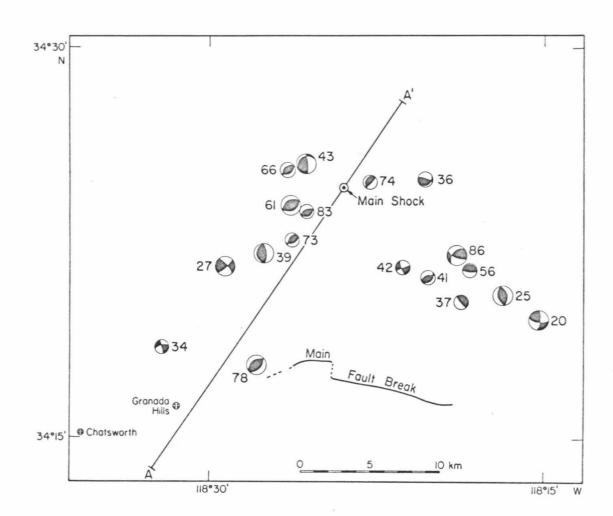


Figure 16.

Map of focal mechanisms of the other group (see the caption of Figure 7).

Figure 2a, February 21 also stands out as the first day after February 10 that had events of M_L = 4.0 or larger, initiating the series 61-64 which closely concentrate in the northern part of the west limb.

If the compensatory thrust events, which begin on February 21, are separated from the events on Figure 16, we find that, remarkably, all but one of the remaining events occur in the first stage between the 9th and 17th of February as shown in the histogram of Figure 2f.

The exception occurred late in this set on April 25 during the possible third stage, which was indicated above. Most of these events are in the upper thrust block east of A-A' (see Figures 16 and 12b).

From these considerations, we conclude that these remaining events represent complex fracturing in the upper thrust block resulting from the main tectonic motion. Their activity ceased at the same time, and probably for the same reason, as that of the normal events near February 19-21, and may have been reinitiated near the latter part of April.

5.4 The dip of the main thrust fault. As seen from the P-wave first motions of the main shock shown in Figure 5, the dip of the fault at the initial rupture point is well-determined at about 52°. But a line from the main surface rupture to the hypocenter of the main shock computed at 8.4 km depth by Allen et al.(1972) dips at

only about 33° (Figure 12a shows an approximation of the dip line). Also, the fault plane slip vector data in Figure 10 indicate an average plunge of around 40°, although the strike-slip event slip vectors plunge shallower and trend more to the east than those of the thrust events.

Additional evidence for steepening of the fault plane to the north is presented by the cross-section of Figure 12a. There is a notable steepening of the hypocentral distribution of strike-slip events to the north in the zone of the main shock's hypocenter.

Because of the seismometer station distribution, this region gives the best control for hypocentral determinations and therefore the steepening is probably real. Note that the thrust hypocenters in this zone can be accounted for in the existing model of Figure 8 without modification, and only the three deep strike-slip events to the north indicate steepening.

Most of the events that are near the hypocenter of the main shock are west of A-A' (see Figure 11). Thus, the slip vectors of the model-compatible events along the west limb should provide a good test to show a systematic steepening to the north. Figure 17 is a plot of the slip-vector plunge as a function of distance along A-A' for these events. Some increase of plunge to the north can be seen, especially if only the strike-slip events (square symbols) are considered. But the slip plunge of vectors from the thrust events in the southwest area (towards A) conflict with this interpretation, unless the fault-surface also includes a steepening in the extreme

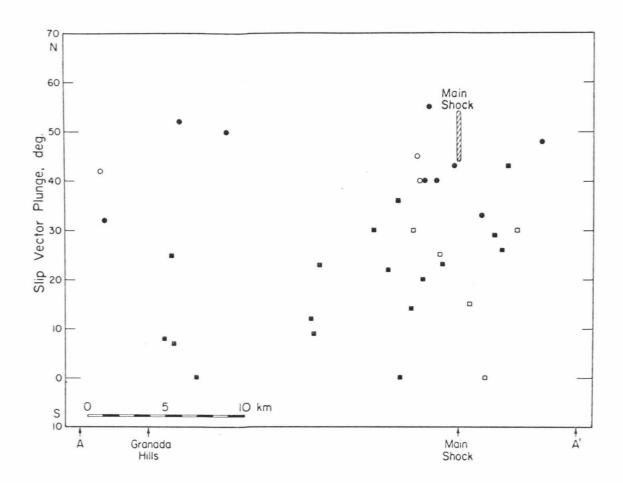


Figure 17.

Slip-vector plunges for all events west of A-A' (see Figure 11) as a function of distance along A-A'. Squares are strike-slip events and circles are thrust events. Steepening to the north is indicated if the thrust events near A can be ignored.

southwestern portion. The main characteristic of the data in Figure 17 is that the slip vectors of strike-slip events plunge less than those of the thrust events. The thrust events in turn have plunges that are not significantly different from the range of the main shock (a range is shown because of the uncertainty of the main shock's auxiliary plane determinations). East of A-A', the fault-plane slip vectors of thrust events are also not significantly different from that of the main shock and show no systematic steepening to the north (see Figure 9). One possibility that would reduce the steep thrust-fault dips is a change of the hypocentral velocity used to calculate the focal mechanisms, especially that of the main shock. An increase in P-wave velocity of about 0.8 km/sec (from 6.1 to 6.9) would have the effect of shallowing the thrust plane dip of the main shock focal mechanism (from about 50° to about 40°). This velocity is not totally unrealistic for certain crustal rocks but no evidence exists for a velocity this high at the main shock's hypocenter.

While it is apparent from the discussion above that the evidence is not conclusive, we believe that the arguments in favor of the fault steepening with depth are stronger. Thus, we support the early results of many investigators (Hanks et al., 1971; Wesson et al., 1971; Wesson and Wilson, 1972; and Allen et al., 1972) that the main thrust fault surface dips at 35°-40° near the surface and steepens to 52° at the main shock hypocentral depth, 8-12 km. Wesson and Wilson (1972) used this conclusion in their proposal that the

San Gabriel fault was the main rupture surface at depth; we discuss this possibility in a later section.

5.5 Early March and March-April series. During what is defined as the second stage of the overall aftershock series, at least two significant bursts of activity occurred in the set of events larger than M_{L} = 3.0. The first series began on March 7 with an M_{L} = 4.5 event in the central portion of the west limb. Three events followed on the same day and all were in or near (within 1.5 km) the west limb. The activity for several days both before and after the series was less than an event per day as seen in Figure 2b. The second series began 18 days later on March 25 with an M_{τ} = 4.2 event at nearly the identical hypocenter as the initial event of the first series. Eleven events followed over the next 8 days and all were also in or near (within 2.0 km) the west limb. Five of the aftershocks in this series had M_{T} 's of 4.0 or larger and one, on March 31, caused some further damage in the Granada Hills area. No intervening events above M_{τ} = 3.0 occurred in the time between the two series and the average activity of events this size was less than one per day after the end of the March 25 series.

The parallelism between the two series is striking: initiation at the same location by shocks of M_L = 4.0 or larger, relative quiescence both before and after each series, and a limitation

of epicenters to the west limb. But even more significant is the time sequence of the series' events along the west limb. Figure 18 is a plot of the event times as a function of distance along A-A' (see Figure 11). The symbols again represent the focal-mechanism types, and the adjacent set of numbers indicates the event numbers and M_{T} value. Blank numbers indicate aftershocks larger than $M_{T} = 3.0$ that are not in Table 1 and whose hypocentral locations should be considered as of "C" quality. Lines connect events that are adjacent in time, and are dashed where one of the events is not in Table 1. The data show a systematic sequencing of aftershocks along the west limb, especially when several events occur advancing in one direction along the limb, such as the sequences 71-74 and 76-80. Based on this sequencing in two separate aftershock series that have other strong similarities, we conclude that the time-space distribution of both series is not random and therefore a causal relationship must exist between the events within each series. This causal relationship may not be as simple as that implied by connecting successive events with lines as in Figure 18. However, where several events occur sequentially in one direction of advance as in the previously mentioned sequences 71-74 and 76-80, a propagating phenomenon that triggers events with an apparent horizontal velocity of 4 to 15 km/day is suggested. It is interesting to compare these rates with those observed for propagating creep events in Central California of 0.5 to 10 km/day (Robert Nason, personal communication, 1972). The slopes

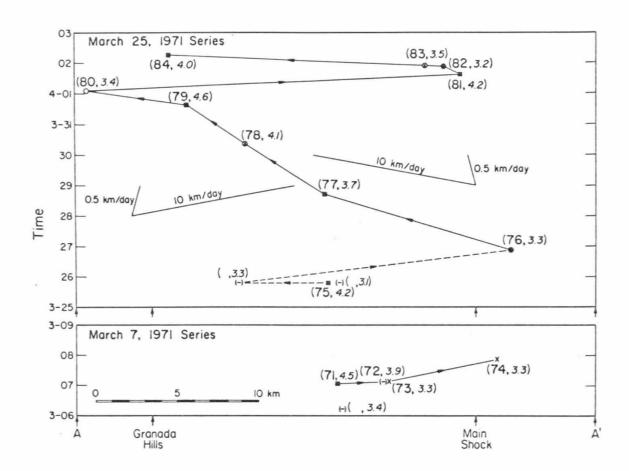


Figure 18.

Aftershock origin time as function of distance along A-A' (see Figure 10) for all events larger than $M_L = 3.0$ during March 7-8, 1971, and March 25-April 2, 1971. The larger numbers correspond to those of the events in Table 1 (events not in the table have no numbers) and the smaller to the magnitudes. The symbols are described in Figure 11 except for events with no focal mechanism, indicated by a dash.

corresponding to these velocities are shown in Figure 18. The propagation rates of the aftershocks in Figure 18 are at the higher range of the rates observed by Nason, but they are certainly comparable.

5.6 Regional tectonics and seismicity. Figure 19 outlines most of the major faults in an area from Santa Monica Bay on the southwest to the Mojave desert on the northeast (modified from Jennings and Strand, 1969). The approximate area of the aftershock epicenters is shown for reference. The San Fernando fault trace occurs in the southeastern edge of the Ventura basin, a highly folded synclinorium within the Transverse Range province that contains remarkably thick sections of Tertiary and Quaternary strata (up to 6 km in the Santa Susana mountains area, Wesson and Gibbs, 1971). The basin contains many thrust faults on which much of the uplift of the adjacent mountains has taken place. Of these thrusts, the Santa Susana fault, which shows evidence of late Quaternary movements (Wentworth et al., 1971), is the closest to the San Fernando fault and lies immediately to the west, as seen in Figure 19. Oil field data on the western and eastern part of the Santa Susana thrust show that it has a shallow north dip at the surface and steepens to about 50° when it reaches 0.7 km depth (Hall et al., 1958, and Roth and Sullwold, 1958). Similar oil field data on the San Cayetano thrust further to the west (not shown in Figure 19) indicate a 30° to 35° north dip at the surface steepening to about 50° as it reaches depths near 4 km shown in Figure 20

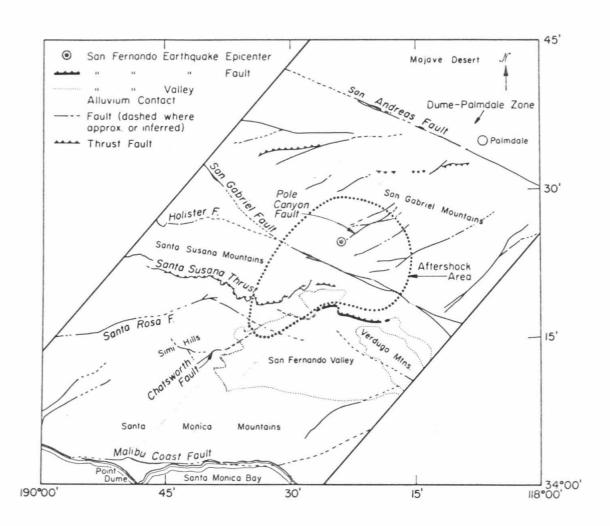


Figure 19.

Major tectonic features in the area around San Fernando.

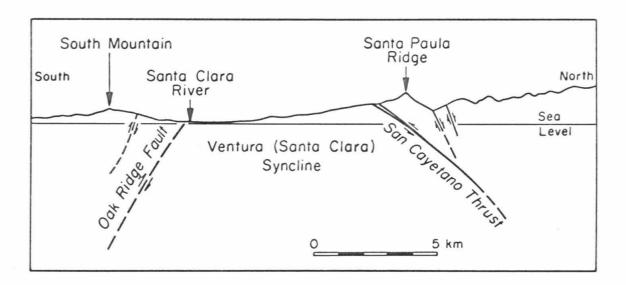


Figure 20.

Cross-section of the Ventura syncline showing the San Cayetano thrust fault (modified from Bailey and Jahns, 1954, Figure 8). Note the steepening with depth and the normal faulting to the north.

(Bailey and Jahns, 1954). This is precisely the dip behavior proposed for the San Fernando thrust fault, which is part of the same fault system.

Of further interest in the San Cayetano thrust area are the mapped normal dip-slip faults dipping to the north in the up-thrust block just north of the San Cayetano fault trace. This faulting is also in agreement with the San Fernando fault tectonics, specifically the focal mechanisms and gravity data in the northeast aftershock zone which indicate shallow normal faults (Figure 15).

The theoretical and experimental work of Sanford (1959) directly bears on the phenomena of thrust faults steepening to dips greater than 45° with depth and the occurrence of shallow normal dip-slip faults in the up-thrown block. He showed that the normal faulting is a result of the steepening of the thrust fault and that the steepening itself is directly related to laterally varying vertical forces at depth. The steepening can be simply explained by the fact that all vertical forces at depth must converge to zero at the earth's surface. Thus, while laterally-varying vertical forces can be supported by rock strength at depth and cause fractures dipping steeper than 45°, the only possible stresses at the earth's surface are horizontal, and fracture criteria require a thrust fault that dips shallower than 45°. Sanford's results are shown in Figure 21.

The implications of these laterally varying vertical forces are important to the regional stress picture. Emphasis in the vicinity

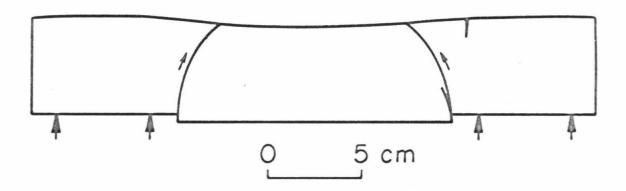


Figure 21.

Results of an experimental fracturing experiment by Sanford (1959, Figure 17) that shows a thrust fault steepening with depth and tensional fractures in the up-thrust block.

of the San Andreas fault is commonly placed on horizontal movements and stresses dominating the tectonics, especially since the emergence of concepts of plate tectonics. However, it is clear from the above that significant vertical stresses other than overburden pressure are also acting at depth in the Ventura basin. The question naturally arises as to the relative magnitude and origin of these stresses. First, the horizontal stresses must be a substantial part of the regional stress field because the extensive folding in the Ventura basin is due to north-south compression (Bailey and Jahns, 1954) which is still active. Isostatic imbalance is not the cause for the vertical stresses because it is apparent that the mountains north of the Ventura basin have been moving up, and this would require a mass deficiency under the mountains. But seismic and gravity evidence for the San Gabriel mountains, which were uplifted in the San Fernando earthquake, indicate no mass deficiency and perhaps even an excess (Mellman, 1972). It appears that the most likely cause for the vertical stresses is a partial upward redirection of the horizontal stress either by a deep obstruction over which the surface blocks are forced or by complex distortion due to buckling at depth as the crust is shortened. Indeed, the great bend in the San Andreas fault zone as it crosses the Transverse Ranges of southern California virtually demands vertical adjustments in the adjacent regions if lateral movements are to be continuous along the San Andreas fault. The stress at depth in the Ventura basin area is most likely a combination of a dominant horizontal stress and

laterally-varying vertical stress as in Sanford's model that would result in the major compressional stress axis dipping 10° or more at depth.

The existence of the left lateral strike-slip zone, which is the downstep in the fault surface model of Figure 8, is well established from the focal mechanisms and the southerly curvature of the aftershock zone and main fault break in this region. As pointed out by Allen et al. (1972), further support for the existence of the downstep comes from the mapped geology of the area (Wentworth et al., 1971, Figure 2). The trace of the Santa Susana thrust makes a sharp bend to the north when it enters the zone from the west (Figure 19) in exactly the manner postulated for the San Fernando fault. Further, basement rocks are widely exposed in the San Gabriel Mountains east of this zone, whereas only younger sedimentary rocks are exposed to the west. The latter strongly supports the concept of a flexural or faulted downstep to the west in this area. However, it is not clear that the thrust faulting to the west of the zone is associated with a single downstepped thrust fault as depicted in the model of Figure 8 or as two or more parallel thrust faults for which there are several candidates in the mapped geology of the area (Jennings and Strand, 1969). The western thrust mechanisms occur mainly in the extreme northwest or southwest corners of the aftershock zone with only one intervening thrust event (Event 5) in the central part of the zone

(Figure 9). Also, the steep slip vector plunges of thrust events near Granada Hills (Figure 17) and deeper hypocenters (Figure 12a) deviate from the model and the hypothesis of a shallow fault dip at the surface; however, these effects may be related to the greater hypocentral location inaccuracies in this region. Although these are not serious objections to this feature of the model, they point out the possibility of more than one thrust surface extending to the west of the established main fault downstep.

The San Gabriel fault is a major structural feature in the San Fernando area and its trace cuts through the center of the aftershock zone (Figure 19). Although it has some evidence of dip-slip, its main motion has been right-lateral strike slip with no evidence of late Quaternary displacements (Wentworth et al., 1971). Dip measurements of the San Gabriel fault in the aftershock region are complicated in many locations by nearby parallel thrust faulting that cuts across the San Gabriel fault plane. But where the fault is uncomplicated and clearly exposed, it is steeply north-dipping at 70° to 80° (Oakeshott, 1954, Oakeshott, personal communication, 1972). This steep dip agrees with the extreme linearity of the fault trace as it cuts through the varying topography of the western San Gabriel mountains. Wesson and Wilson (1972) have proposed that the San Gabriel fault was the initial rupture surface of the San Fernando earthquake. They based this on the steepening with depth of the San Fernando fault surface and on ground elevation changes in the

vicinity of the San Gabriel fault trace. As discussed above, evidence seems to favor a steepening of the San Fernando thrust fault surface with depth, but this is a characteristic of all of the north-dipping thrust faults along the Ventura basin. It is more likely that the steepening of the San Fernando fault is due to the same cause and not to its special geometrical relationship with the San Gabriel fault, which appears to have a very different geologic history. Also, as stated above, the dip of the San Gabriel fault is probably steeper than 52°, the dip of the initial San Fernando rupture surface. The positive gravity changes in the northeast aftershock zone shown in Figure 15 indicate that the ground surface just north of the San Gabriel fault experienced a decrease in elevation. If any shallow displacements took place on the San Gabriel fault, this evidence indicates that it was normal dip-slip instead of thrust.

Seismicity in the region of Figure 19 before 1971 shows some interesting earthquake distributions. Figure 22 is a map of epicenters for all events located by CIT for the time periods 1961-1962 (Figure 22a), 1969 (Figure 22b), and 1960-1970 (Figure 22c). The locations are believed to be accurate to within about 9 km. The San Fernando aftershock zone and some of the major faults are shown for reference. During 1961-1962 (Figure 22a), the earthquakes clearly define a zone that coincides with the location and direction of the west limb of San Fernando aftershocks but extends from Point Dume near Malibu on the southwest to the San Andreas fault near Palmdale on the northeast.

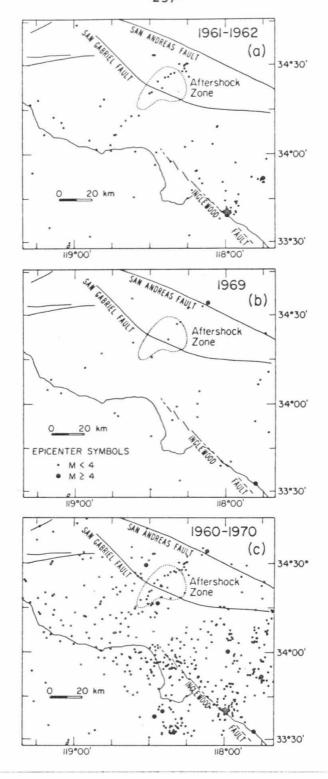


Figure 22.

Seismicity around the San Fernando region for the time periods (a) 1961-1962, (b) 1969, and (c) 1960-1970. The epicentral locations are believed to be accurate to within 9 km. The San Fernando aftershock zone and some of the major faults are shown for reference.

For discussion purposes it will be designated the Dume-Palmdale zone and is outlined in Figure 19. Figure 22b shows that the northeastern part of this zone was active in 1969 including an M_L = 4.0 event on the San Andreas fault. Figure 22c confirms that the Dume-Palmdale zone is suggestively outlined even when compared with the total seismicity over the ten-year period before the main shock, 1960-1970. No similar pattern in the zone is seen in the years prior to this interval back through 1935, although this may be because the earlier epicentral locations are considerably less accurate. There is a possible indication of activity along the zone from the M_T = 5.2 earthquake of August 30, 1930 (Wentworth et al., 1971). The original epicentral assignment, which was not well constrained, was in the Santa Monica Bay. But, minor damage at both the Chatsworth Dam and Lower Van Norman Dam, which lie along the western edge of the San Fernando valley, suggests that the epicenter was on or near the Dume-Palmdale zone. Other lineations that are outlined by seismicity but do not coincide with any obvious surface structure in Southern California are reported by Ryall et al. (1966) and Richter (1969). These lineations often strike in the direction nearly perpendicular to the major northwest-southeast strike-slip faults of the region; this is approximately the conjugate shear direction in association with a dominant horizontal compression.

The significance of activity on the Dume-Palmdale zone is that

it precedes the San Fernando series and exactly coincides with the west aftershock limb and the main shock epicenter as seen in Figure 19. While the zone is not obviously outlined by continuous geologic features of the area, there are some mapped structures that appear to be related. The sharp bend in the trace of the Santa Susana thrust has already been mentioned. The western edge of the San Fernando Valley also lies along this trend and is fault controlled with the east side down (Corbato, 1963). One of the members of this family of faults is the Chatsworth fault, which shows some evidence of Quaternary displacements (Wentworth et al., 1971). Although some maps show the northwest-trending Northridge Hills fault as cutting continuously across this zone, geologic relationships in the area of intersection are obscure. Still farther south, however, the Santa Monica Mountains and the Malibu Coast fault are clearly continuous across the Dume-Palmdale trend, and the zone must terminate in this area.

North of the San Gabriel fault, parallel to and within the Dume-Palmdale zone, are a number of northeast-trending faults that have had a history of left-lateral displacement. For example, Oakeshott (1958) points out that the east-trending Soledad fault is clearly offset by the northeast-trending Pole Canyon fault, which passes virtually through the epicenter of the San Fernando earthquake. However, most of these faults seem to have been active primarily in Miocene time, with no major displacements since that time (L. T. Silver,

personal communication, 1972). This represents a major problem, because the San Gabriel fault itself appears to have had about 50 km of right-lateral displacement in Plio-Pleistocene time (Crowell, 1954, 1962), and thus it should have displaced these earlier northeast-trending faults. If one accepts the large movement on the San Gabriel fault, he cannot argue for a continuous Dume-Palmdale zone that has been active since Miocene time. There are, however, many northeast-trending faults within the Transverse Ranges north of the San Gabriel fault, and it is not necessary to assume that the faults currently delineating the Dume-Palmdale zone have always been in their same relative positions.

Regardless of the complex geologic history of the region, the Dume-Palmdale zone appears to be an active zone at the present time, perhaps taking advantage of previously existing lines of weakness.

The location of the San Fernando main shock, the strike-slip zone of the main fault surface, and the seismicity represented in Figure 22 currently show the zone to be a linear region of weakness where stress can be concentrated. This leads us to believe that the zone represents a decoupling boundary between crustal blocks that permits them to deform separately in the prevalent crustal shortening mode of the region. The fact that this zone of weakness does not extend northeast across the San Andreas fault is evidence that it is being carried along in the crust or lithosphere as displacement takes place along the San Andreas. Apparently, most of the crustal shortening is done

south of the San Andreas in this area as reflected in the aseismicity of the Mojave block to the north (Allen et al., 1965). The aseismicity is probably related to greater strength in the Mojave block due to its thicker crust (Mellman, 1972).

6. SUMMARY AND CONCLUSIONS

The main shock of the San Fernando earthquake occurred at 14 00 41.8 GMT on February 9, 1971. Allen et al. (1972) assigned it a magnitude (ML) of 6.4 and a location at 34° 24.7′ N, 118° 24.0 W, h = 8.4 km; they estimated the hypocenter to be within 4 km horizontally and 8 km vertically. Hanks (1972), based on his analysis of the Pacoima Dam accelerogram and distant recordings of the main shock, suggested a hypocentral depth of 12 to 15 km, which is within the range given by Allen et al. A main shock depth of 12 km is compatible with the location of the aftershocks of Figure 12 if the epicenter is shifted northwest about 4 km, again within the range given by Allen et al. Thus, within the constraints of the data, the location of the main shock's initial rupture coincides with the lower, northernmost edge of the aftershock distribution.

The best focal mechanism fit to the P-wave first motions of the main shock gives the initial thrust plane parameters of: Strike, N 67° (\pm 6°) W; Dip, 52° (\pm 3°) NE; Rake, 72° (67°-95°) left lateral. Evidence from the slip vectors of the aftershocks suggests that the

rake is closer to 80°, but this assumes that the main shock and aftershock motions were the same. The evidence of fault-surface displacement from Kamb et al. (1971, Figure 2) scatters between the extremes of the rake angle.

In order to have as homogeneous a representation of the aftershock tectonics during the first three months as possible, the aftershocks were chosen for analysis on the basis of size. The first set of events were defined as all those of M_L = 4.0 or larger; twenty of these had onsets clear enough for anlaysis during the first three months of the series. The second set was defined as those with clear onsets at most of the CIT telemetered stations; this essentially corresponds to a magnitude cutoff at about M_L = 3.3 and a total of 87 aftershocks fulfilled the requirement. The second set, of course, contains the first. Of the second set of 87, only 12 focal mechanism solutions were poorly constrained, and most of these occurred during the first few hours of the series when the portable stations were not yet in operation.

In both sets of aftershocks, most of the activity was along a linear northeast striking region encompassing the main shock epicenter and bounding the aftershock region to the west. This region, the west aftershock limb, is dominated in both aftershock sets by focal mechanisms in which one plane strikes along the limb and dips steeply to the northwest with left-lateral strike-slip motion. Thrust mechanisms resembling that of the main shock occurred both to the west

and to the east of the west limb. From these considerations it is clear that the west limb outlines a major discontinuity in the main thrust fault surface. These data require a single non-planar fault surface that incorporates a downstep to the west in the north-dipping thrust fault plane as shown in Figure 8. Two-thirds of the focal mechanisms are either strike-slip or thrust with orientations and epicentral locations in agreement with the fault surface model and provide strong support for its validity. An interesting way of illustrating this is the comparison (shown in Figure 10) of slip vectors, tension axes, and compression axes of the focal mechanisms with the distribution of these parameters predicted by the fault surface model. Except for some scatter and minor deviations (which correlate with other phenomena in the series), the data clearly have the same distribution. Further confirmation for the model is provided by the agreement of fault-plane strikes for shocks with strike-slip mechanisms with that predicted from the orientation of the west aftershock limb. The hypocentral locations bear out the model's characteristics that the strike-slip events along the west aftershock limb are limited to a narrow zone, at least south of the main shock epicenter, and that the thrusts in and to the west of the west limb tend to be deeper.

While the dip of the main shock initial rupture surface is 51° (± 3°), evidence from the main shock hypocenter relative to the

surface faulting and the distribution of the aftershock hypocenters south of the main shock indicates a dip of around 35° at shallower depths on the main fault surface. There is also some indication of steepening with depth of the aftershock slip vectors although this is not as clear. The complication arises from the thrust event slip vectors west of the west aftershock limb, and may indicate that the thrusting to the west is not on a single downstepped surface but is on two or more unconnected thrust planes. However, within and to the east of the west aftershock limb, the data favor a fault surface whose slip vector starts with a 50° plunge at the initial rupture at depth, and curves to a 35° plunge as it extends to shallower depths.

A series of north-dipping thrust faults to the west of the San Fernando area exhibit steepening with depth in precisely the same manner as that proposed for the San Fernando fault. These faults strike along the trend of the Ventura basin and have late Quaternary movements that form mountains to the north, in the same tectonic setting as the San Fernando fault. Sanford (1959) showed that this steepening to dips greater than 45° may be related to laterally-varying vertical forces at depth, which has important implications to the regional stress picture. The most likely cause for the vertical stresses is a partial upward redirection of the horizontal compressive stress, which from the time of extensive folding in the Ventura basin to the present has been the dominant stress in the region.

The San Gabriel fault, a major structural feature cutting through the aftershock region, apparently played no significant role in the displacements of the main San Fernando event. There is no evidence for late Quaternary displacements of the main San Fernando event. There is no evidence for late Quaternary displacements on the fault and no direct evidence that it slipped in the main event. At depth, it is probably much steeper than the 52° dip of the initial rupture surface. Gravity data, which reflect ground surface displacements, indicate that, if any shallow displacements took place on the San Gabriel fault, they had a normal dip-slip component.

One-third of the focal mechanisms do not fit the fault surface model of Figure 8. This is not surprising because the strain release due to the aftershocks is minor compared to that of the main shock, and some of the aftershocks should represent a relief of complex stress concentrations due to motions of the main shock. According to the theoretical and experimental work of Sanford (1959), one of these stress concentrations should be a tension field in the shallow upper thrust block resulting from the steepening of the thrust fault with depth. Ground surface elevation decreases and shallow normal focal mechanisms north of the main fault break confirm the existence of this tension field after the main event. A close concentration of shallow focal mechanisms and localized ground subsidence on the west aftershock limb near the western projection of the main fault break indicates further complexity. The consistent deviation between the

strike-slip and thrust event slip-vector azimuths (Figure 10) predicts a divergence of motion along the downstep of the west aftershock limb. This divergence, which would produce a local tension field, would be most pronounced as the downstep of the main fault surface approaches the ground surface, which is the precise location of the observed concentration of shallow normal events and ground subsidence.

Another class of focal mechanisms can be separated from the events that do not fit the model. They are defined as those events which occur along the west aftershock limb with a thrust plane striking in the same direction as the limb. The motion of the these events is consistent with the idea of compensation (on the downstep fault surface) for the divergence that caused local tension along the west limb.

These compensatory thrust events did not begin until February 21, 12 days after the main shock. All of the remaining focal mechanisms in this set were located in the upper thrust block east of the west aftershock limb and were confined with only one exception to the time period of February 9-17, before the onset of the compensatory thrust events. They are presumably related to localized stress concentrations due to displacements of the main shock.

Other evidence points to this time as one of significant change in the stress field of the aftershock area. The last normal focal mechanism in the set occurred on February 19, three days before the first compensatory thrust event. February 21 was the first day since February 10 that an event with $M_{\tilde{L}}$ = 4.0 or larger occurred in the

series; this initiated a series of aftershocks that closely concentrated in the northern part of the west aftershock limb. After this time, at least until April 17, the aftershock activity was characterized by isolated bursts of events starting with $\rm M_L$ = 4.0 or larger events. These bursts were essentially confined to the west aftershock limb until April 17 when the bursts ceased and minor activity continued throughout the aftershock area. The time-space distribution of these events indicate that some time near February 21, 12 days after the main shock, a horizontal compressional stress in a north or northnorthwest direction was added to the stress in the aftershock area. As a result, events related to stress release of the main shock ceased and activity was concentrated in bursts of events along the downstep of the main fault surface. Effects due to this change of stress appear to have stopped by April 17, about two months later.

While the aftershock activity was by no means finished after May 7, 1971, the end of this investigation, the aftershock rate for M_L's larger than 3.0 by that time had dropped to about one every four days. Thus, this study covers the time period of most of the aftershocks. The question of whether the tectonic activity changes in character after this period even though the aftershock activity is very low is an important subject for future investigation.

The bursts of aftershocks along the west limb during the period between February 21 and April 17 show systematic time-space relationships in themselves. The events within two of the bursts have a systematic sequencing north and south along the west aftershock
limb that is not random and must be explained by a causal relationship.
While the relationship may not be as simple as a unidirectional front
that triggers events, there is some evidence for a triggering
phenomenon that propagates with speeds of 4 to 15 km/day. These
speeds are somewhat high but comparable to those observed for wave
fronts defined by the onset of creep events on the San Andreas fault.

Seismicity in 1961, 1962, and 1969 before the San Fernando series outlines a linear region extending from Point Dume, near Malibu, in the southwest to Palmdale, on the San Andreas fault, in the northeast. This region exactly coincides with the west aftershock limb and the main shock epicenter. While the zone is not obviously outlined by mapped geologic structures along its extent, it coincides with some major structural discontinuities such as the fault-controlled west edge of the San Fernando Valley, the sharp north bend of the Santa Susana fault, the downstep of the San Fernando fault, and the general trend of left-lateral strike-slip faulting in the San Gabriel mountains. The history of this zone of weakness is not clear but it was probably active in the San Gabriel mountain block during Miocene and lower Pliocene and is recently active along the western edge of the San Fernando Valley. It is interpreted as a decoupling boundary between crustal blocks that permits them to deform separately in the prevalent crustal-shortening mode of the Transverse Ranges region.

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Appendix 1

FOCPLT Program Description.

A computer program has been developed to easily reduce and plot P-wave first motion data, plot nodal planes, and, if desired, compute the constraints of the data on the program's choice of a double-couple focal mechanism solution. It was written to provide an efficient means of estimating the quality of a focal mechanism, a difficult task for even those workers experienced in the art of fitting mechanisms, and a nearly impossible task for those who are not.

The fitting of a double-couple mechanism to first-motion data is a rather unusual minimization problem because of the yes-no nature of each station's agreement with a particular solution orientation; we desire to minimize the number of no's. This characteristic produces stair-step slopes leading down to flat-bottomed minima. The problem's extreme non-linearity and the fact that multiple minima in the solution space are common prohibit use of any simple linear technique to find the minima and require that the entire solution space be investigated, which makes an efficient method of search desirable.

When estimating the constraints on the solution, we find that some data are obviously bad, that is they are clearly in the middle of a quadrant with which they disagree. Thus, only data that are near the nodes of the solution are meaningful constraints. As in fitting a line to a set of data, it may be desirable to define a norm related to the distance of the misfit to the nodal line so that a minimization criterion such as least-squares can be used to minimize the misfit; a procedure like this removes the flat bottom of the minimum unless there are no misfits. This criterion should only be applied to misfits close to the nodes because obviously bad data as mentioned above should not be used in the solution. The norm used in this program (as an option) is the smallest angular distance of the misfit from the node and the smallest linear sum of these distances out to a specified limit is the minimization criterion.

In order to evenly sample the solution space in the most efficient manner, the intrinsic character of the equal-area plot is used. The location of points on a computer printing plot, the mode of data presentation, is used to determine the orientation of the nodal-plane poles (slip vectors); this minimizes wasted computations. In the present configuration the program gives resolution of the focal mechanism solution to within the nearest 3 1/2 deg. This can be made finer but the need for greater resolution is questionable in light of uncertainties in near-focus velocities. In addition, efficiency is enhanced through the use of symmetries and anti-symmetries of the double-couple focal mechanism; these halve the number of computations over a straight sweep through the range of the Eulerian angles.

The following diagrams show solution-constraint plots (equalarea of the lower focal hemisphere) for the slip vectors (in one plot),
the compression axis, and tension axis for the San Fernando main
shock. A plus sign marks the minimum-misfit solution and the numbers
indicate the number of misfits above the minimum. The range of ones
for example indicates the range of possible solutions if the most
critical station in any direction were to be reversed. A weight of
1/2 for fair readings (as opposed to a weight of 1 for good) and
the use of the taper as described above allow numbers between the
integers; the fractional parts are dropped for plotting. The first
set of diagrams have a taper width of 0° and the second set has a
width of ± 3.5° (0.06) from the nodal lines.

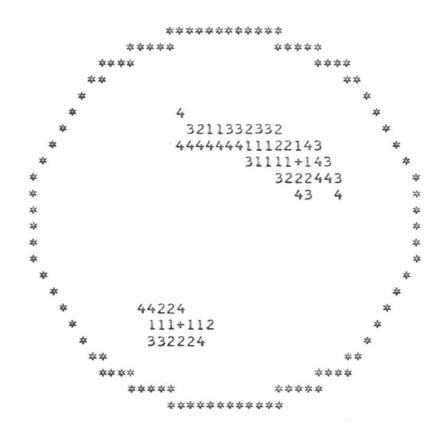
Following each set is a diagram of the focal mechanism quadrants of the chosen solution (an example of the program's ink plot is in Figure 5). It must be emphasized that this computed best solution is significant only if the constraint, measured by the steepness of the minima wells in the constraint plots, is tight. The program choses the best solution by fixing the pole in the center of the most constrained slip-vector minimum and finding the other pole closest to the center of the other minimum.

The time for the program on an IBM 370-55, if the solution constraint calculation is chosen, is approximately

time (sec) = 42 + 1.64 (No. of Stations)

Instructions for the program's use follow the diagrams.

SLIP VECTOR PLOT

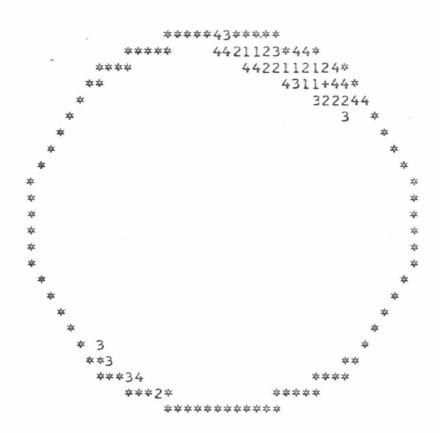


EVENT DATA MAIN 0 02 09 71 14 0 41.6 8.4 34.000 24.70 -118.000 24.00 6.4

NUMBER OF STATIONS=101 STATIONS IN ERROR= 8 MINIMUM SCORE= 8.00

TAPER= 0.0

COMPRESSION AXIS

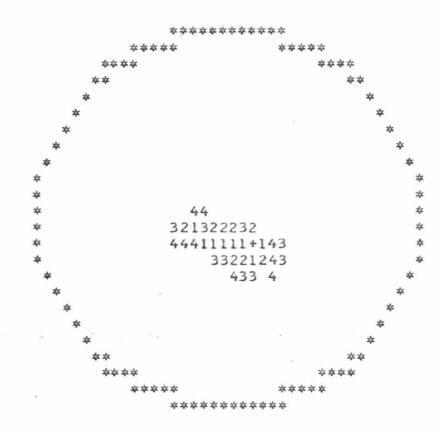


EVENT DATA 0 02 09 71 14 0 41.6 MAIN 8.4 34.000 24.70 -118.000 24.00 6.4

MINIMUM SCORE= 8.00

NUMBER OF STATIONS=101 STATIONS IN ERROR= 8 TAPER= 0.0

TENSION AXIS

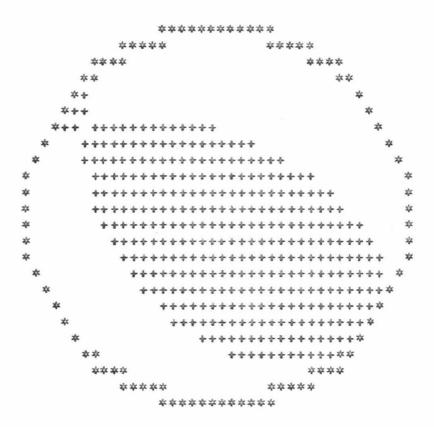


EVENT DATA 0 02 09 71 14 0 41.6 MAIN 8.4 34.000 24.70 -118.000 24.00 6.4

MINIMUM SCORE= 8.00

NUMBER OF STATIONS=101 STATIONS IN ERROR= 8 TAPER= 0.0

COMPRESSIONAL AND DILATATIONAL QUADRANTS SHADED QUADRANTS ARE COMPRESSIONAL



MAIN 0 02 09 71 14 0 41.6 8.4 34.000 24.70 -118.000 24.00 6.4

DIP1= 41.6

AZ1=142.1

AZ2=292.7 DIP2= 52.3

SLIP VECTOR PLOT

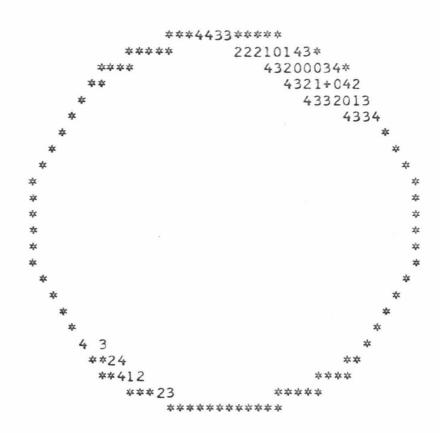
***** 本本本本 3222211012344 320011013 4220+00234 433201234 443334 3334 420+010134 433434 *** ****

EVENT DATA MAIN 0 02 09 71 14 0 41.6 8.4 34.000 24.70 -118.000 24.00 6.4

NUMBER OF STATIONS=101 STATIONS IN ERROR= 11 MINIMUM SCORE= 5.47

TAPER = 0.060

COMPRESSION AXIS

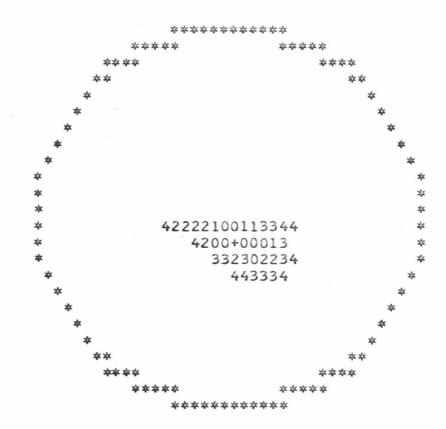


EVENT DATA 0 02 09 71 14 0 41.6 MAIN 8.4 34.000 24.70 -118.000 24.00 6.4

MINIMUM SCORE= 5.47

NUMBER OF STATIONS=101 STATIONS IN ERROR= 11 TAPER= 0.060

TENSION AXIS

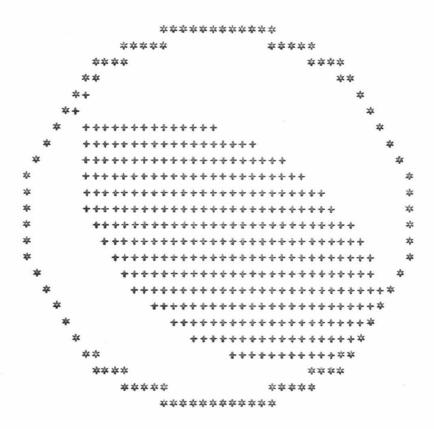


EVENT DATA 0 02 09 71 14 0 41.6 MAIN 8.4 34.000 24.70 -118.000 24.00 6.4

MINIMUM SCORE= 5.47

NUMBER OF STATIONS=101 STATIONS IN ERROR= 11 TAPER= 0.060

COMPRESSIONAL AND DILATATIONAL QUADRANTS SHADED QUADRANTS ARE COMPRESSIONAL



MAIN 0 02 09 71 14 0 41.6 8.4 34.000 24.70 -118.000 24.00 6.4

AZ2=296.9 DIP2= 53.8

DIP1= 38.1

AZ1=138.1

```
THIS PROGRAM PLCTS P-WAVE FIRST MCTICN DATA ON THE LOWER FOCAL
C HEMISPHERE IN AN EQUAL-AREA PROJECTION. A TAKEOFF ANGLE TABLE(VS. DEL)
C AND STATION PARAMETER TABLE ARE READ IN FIRST. THEN, READINGS FOR
C EACH EVENT ARE READ, REDUCED, AND PLOTTED (OPTIONAL) WITH STATION
C NAMES (OPTIONAL).
     OPTIONS ARE AVAILABLE TO PLOT THE NOCAL PLANES FOR A GIVEN FOCAL
C MECHANISM OR TO CALCULATE THE 'BEST' FOCAL MECHANISM FOR THE GIVEN
C DATA DISTRIBUTION. CARE MUST BE TAKEN IN USING THE CALCULATED FOCAL
C MECHANISM TO SEE THAT THE SOLUTION IS WELL-CONSTRAINED IN THE SLIP-
 VECTOR PLOTS. IF NOT WELL-CONSTRAINED, THE SCLUTION SHOULD BE IGNORED
C AND THE DISTRIBUTION OF EQUAL MISFIT AREAS IN THE SLIP-VECTOR PLOT
C SHOULD BE USED TO DETERMINE THE POSSIBLE CRIENTATIONS OF THE NODAL
C PLANES.
C INPUT DATA
   CARD
C
C
   1-5 15
                 NDEPTH=NUMBER OF DEPTHS IN TABLE
   6-77 18A4
                 TIDEN = IDENTITY OF VELOCITY MODEL USED TO GET TABLE.
   DO FOLLOWING NDEPTH TIMES
       CARD
       1-10 · F10.3
                      TDEPTH=CEPTH(KM) FCR THIS TABLE
C
      11-15
C
                      NENTRY=NUMBER OF ENTRIES IN THIS TABLE
            15
C
       CARDS
C
             5(2F8.3)
                      TDEL=DISTANCE (CEG)
       1-8
C
       8-16
                      TEANG=EMERGENCE ANGLE(DEG)
C
       ETC.
                         (FIVE ENTRIES OR PAIRS PER CARD NENTRY TIMES)
C
C
   CARD
                 NS=NUMBER OF STATIONS WITH COORDINATES
C
   1-5 15
   DO FCLLOWING NS TIMES
C
       CARDS
       7-10
                      STA = STATION NAME (RIGHT JUSTIFIED)
C
            44
C
      11-20 F10.3
                      SLATI=LATITUDE (DEG)
C
      21-25
            F5.2
                      SLAT2=LATITUDE (MIN)
C
            F5.2
                      SLAT3=LATITUDE (SEC)
      26-30
      31-40
            F10.3
                      SLON1=LCNGITUDE(DEG)
C
      41-45 F5.2
                      SLON2=LONGITUDE(MIN)
C
      46-50 F5-2
                      SLCN3=LCNGITUDE(SEC)
C
C
   CARD
C
   1-5 15
                 NC=NUMBER OF STATION DISTANCE CORRECTORS
C
   DO FCLLOWING NC TIMES
C
       CARDS
C
       2-5 A4
                      SNAM=STATION NAME (RIGHT JUSTIFIED)
       6-10 F5.3
                      COR=EPICENTRAL DISTANCE CORRECTION TO BE ADDED
                          TO ACCOUNT FOR VARIATION IN CRITICAL DIST.
                                       (DEGREES)
```

```
C
   THE FOLLOWING GROUP MAY BE REPEATED AS OFTEN AS NECESSARY
C
CI
        CARD OF EVENT PARAMETERS
CI
        1-8 A8
                         ENAM=NAME
CI
        9-13 15
                         IEVN = NUMBER
CI
       15-22 A8
                        DATE = DATE
CI
       26-27 12
                        IEHR =+CUR
CI
       29-30 12
                        IEMI =MINUTE
CI
       32-35 F4.1
                        ESEC = SECOND
       36-40 F5.0
                        DEPTH=CEPTH(KM)
CI
CI
       41-49 F9.3
                        ELATI=LAT(DEG)
       50-55 F6.2
CI
                        ELAT2=LAT(MIN)
CI
       56-64 F9.3
                         ELONI=LCNG(DEG)
CI
       65-70 F6.2
                         ELON2=LCNG(MIN)
       71-75 F5.1
CI
                        EMAG = MAGNITUDE
CI
        CARD OF FOCAL MECHANISM PLCT AND CALCULATION PARAMETERS
CI
        1-10 F10.3
                        R90 RADIUS OF PLOT CIRCLE
CI
       11-15 15
                         NSPAR IF 1, PLOT STATION NAMES
CI
                         NOPLT IF 1, NO PLCTS MADE
       16-20 15
CI
       21-25 15
                         NOMEC
                                EQUALS O IF FAULT PLANE SOLUTION DESIRED
CI
                         EQUALS 1 IF FAULT PLANE SCLUTION NOT DESIRED
CI
                         OTHER PARAMETERS MAY BE OMITTED IF NOMEC = 1
CI
       26-30 I5
                         MAXSCR
                                 SPECIFIES HIGHEST NUMBER OF DISAGREE -
CI
                         MENTS THAT WILL BE PLOTTED BY FLTPLN. HIGHEST
CI
                         NUMBER THAT WILL BE PLOTTED IS MAXSCR-1. MAXSCR
                         MAY HAVE VALUES FROM 1 TO 6.
CI
CI
       31-35 15
                         NSKIP CONTROLS RESCLUTION OF SEARCH FOR BEST
CI
                         SOLUTION. NSKIP=1 YIELDS HIGHEST RESOLUTION.
CI
                         NSKIP MAY HAVE VALUES OF 1,2, CR 3.
CI
       36-40 15
                         NPRNT
                                 SMALL PLCTS CNLY IF NPRNT = 1
                         LARGE PLCTS CNLY IF NPRNT = 2
CI
CI
                         BOTH SIZES FOR ANY OTHER VALUE OF MPRNT
CI
       41-45 F5.3
                         TAPER
                                  APPLIES WEIGHTING FUNCTION WHICH
                         TAPERS TO O FROM UNITY WITHIN A DISTANCE
CI
CI
                         ARSIN(TAPER) FRCM THE NCDAL PLANES.
CI
        CARDS OF READING DATA
CI
                         RSTA = STATION NAME (RIGHT JUSTIFIED)
        2-5 A4
CI
        7-8
            12
                         IRHR = EVENT HOUR
CI
        9-10 I2
                         IRMI = EVENT MINUTE
                        RDATE = EVENT DATE
CI
       13-20 A8
CI
       25
                         RCCDE=C(COMPRESSION), D(DILITATION), " "(NEITHER)
            Al
CI
       26-30 15
                         IQUAL=2(GOOD), 1(PCOR); MINUS=NODAL CHARACTER
        CARD OF FOCAL MECHANISM PARAMETERS IF GIVEN
CI
CI
                         (IF PLCTTING OF NODAL PLANES NOT DESIRED.
CI
                         LEAVE ELANK: IGNORED IF NOMEC=01
CI
         1-30
                         BLANK
CI
        31-40 F10.0
                         AZ1 =AZIMUTH OF FIRST PLANE STRIKE (DEG), MUST BE
                               CCUNTER CLCCKWISE FROM DIP DIRECTION
CI
CI
        41-50 F10.0
                         DIP1=DIP OF FIRST PLANE (CANNOT BE 9C UNLESS
CI
                               BCTH PLANES ARE 901
CI
        51-60 F10.0
                         AZZ =AZIMUTH OF SECOND PLANE STRIKE (DEG), MUST
CI
                               BE COUNTER CLOCKWISE FROM DIP DIRECTION
C
```

C THE LAST CARD SHOULD HAVE NINES IN COLUMNS 9-13 FOR A NORMAL STOP.

Appendix 2.

P-wave First Motion Data and Focal-mechanism Diagrams

This appendix is intended as a supplement to the thesis of Whitcomb (Part II, California Institute of Technology, 1973) entitled "The 1971 San Fernando Earthquake Series Focal Mechanisms and Tectonics" referred to here as the main paper. It contains the P-wave first-motion data, focal mechanism diagrams, and associated parameters for 87 aftershocks of the series discussed in the main paper.

The stations used for P-wave first motions in this study are described in the main paper. All first-motion readings were made personally by the author in order to insure consistency; short-period seismometers were used exclusively. Although seismograms from a total of 47 stations were read, varying periods of operation for the portable stations and the weakness of the first arrival of smaller shocks at distant stations reduced the actual number of first motions read per event. The number of readings for most events ranged from 10-20 for the first twenty hours of the aftershock series and 20-30 for the remainder of the study time period (February 9 to May 7, 1971). Some instrument polarity reversals did occur, usually in instrumentation that was temporary or involved complex electronics such as a telemetry link from seismometer to recorder. However, the station coverage and the number of events were sufficient to reveal the reversals. Also

in almost every case, a reversal could be confirmed by polarity checks with teleseismic events.

The first-motion readings are designated as compressional (C, circles) or dilatational (D, plus signs) with a quality assignment of good (weight 2, large symbols) or fair (weight 1, small symbols). A further classification of nodal character (minus in the tables, stars in the diagrams) was given if the arrival had emergent character when, by a subjective judgment involving the epicentral distance and size of the aftershock, one would expect the first motion to be sharp.

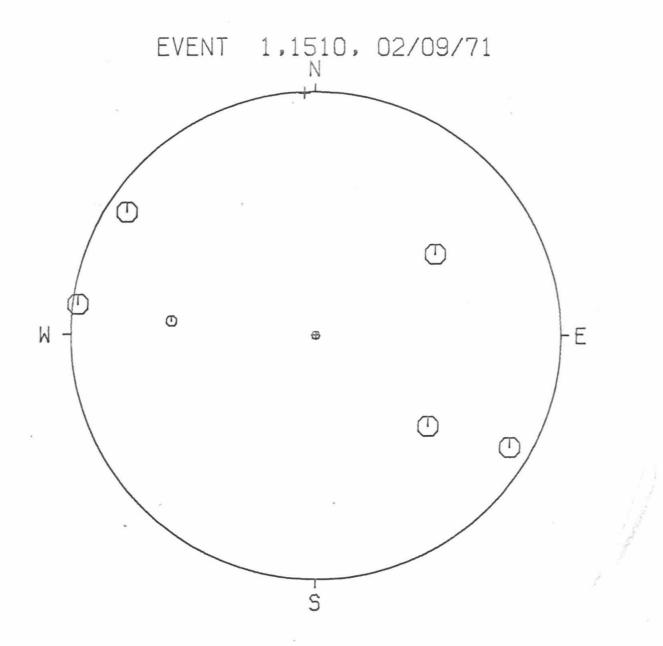
The readings are mapped onto the lower focal hemisphere of an equal-area stereographic projection by ray tracing through a smooth 23 km-thick crustal velocity model described in the main paper.

The double-couple focal mechanisms of the aftershocks are fit to the data by eye under the influence of the reading qualities, good or fair. An estimate of the quality of the solution is made, A, B, or C, as described in the main paper; the C quality rating implies that the parameters are not constrained within 20° and no solution is given.

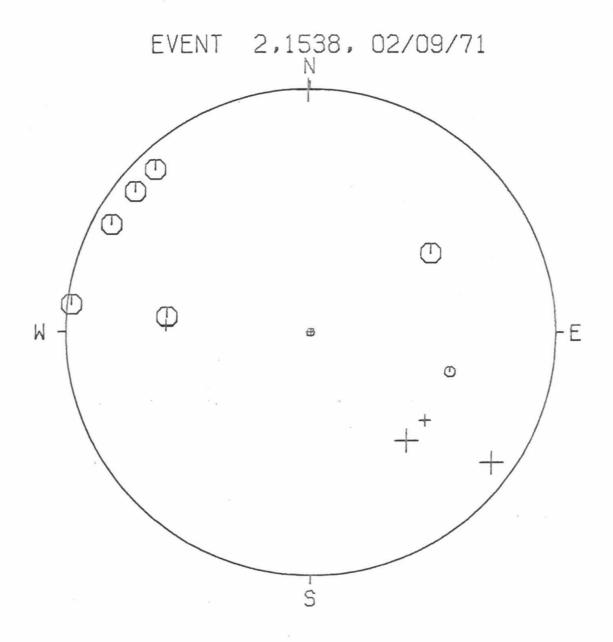
The table format begins with the event parameters: event number, origin time (hr, min), date, depth, epicentral location, and local magnitude. If the focal mechanism is of quality A or B, its parameters are given in terms of the nodal planes' orientations (azimuth, dip), the slip vectors in those planes (azimuth, take-off angle measured from vertical), and the directions of the principal

stress axes (azimuth, take-off angle measured from vertical). The locations of the slip vectors and the principal stress axes are shown as small triangles in the plots. The next parameters in the table are epicentral distance (deg), azimuth at the event (deg), take-off angle measured from vertical, and the x and y coordinates (inches) of the data in the plot. Rays that pierce the upper-focal hemisphere are projected backwards onto the lower hemisphere, a procedure permitted by the symmetry of the double-couple.

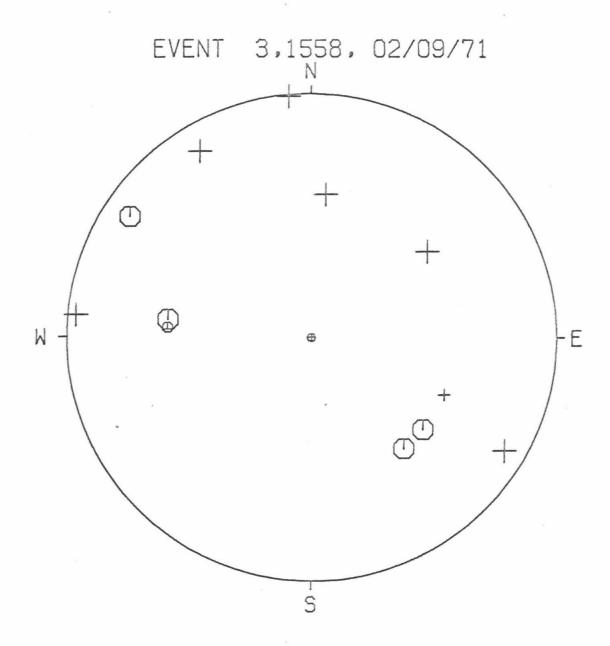
EVENT	DATA	1510	0 02	2/09/71 15 1 34.000 24.80		24.70	3.9
STA	DIR	QUAL	DIST	EVAZ	TOA	Х	Υ
C S P G S C	C	2 2	0.880	97.391 55.691	92.332 49.400	-2.428 1.220	0.315
ISA MWC PLM	Ω C	2 2	1.098 0.350 1.668	357.530 123.215 128.925	89.636 98.866 49.400	-0.107 -1.924 1.149	2.490 1.260 -0.928
PYR SYP	C	2	0.314	299.872 275.549	99.309 49.400	1.985 -1.470	-1.140 0.143



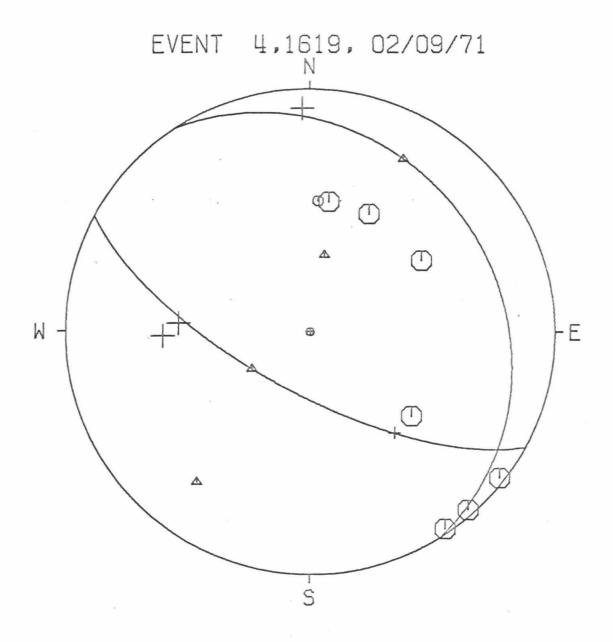
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			8.0	34.000 24.40	-118.000	28.00	3.9
STA	DIR	QUAL	DIST	EVAZ	TOA	Х	Υ
BAR	D	2	2.283	138.468	49.400	0.980	-1.106
CSP	C	2	0.924	96.679	91.783	-2.444	0.286
GSC	C	2	1.633	56.355	49.400	1.230	0.819
HFD	C	1	2.452	105.775	49.400	1.422	-0.402
ISA	D	2	1.104	359.621	89.565	-0.016	2.490
MWC	C	2	0.386	118.670	98.426	-2.026	1.108
PAS	C	2	0.357	136.682	98.784	-1.579	1.674
PLM	D.	1	1.699	127.767	49.400	1.168	-0.905
PYR	D	2	0.280	305.785	99.732	1.849	-1.333
SBC	D	1	1.199	272.818	49.400	-1.476	0.073
SYP	C	2	1.255	276.065	49.400	-1.469	0.156
RCTR	C	2	0.330	129-075	99-107	-1.781	1.446



E١	/ENT	1250013 0 0	1558	9.0		5 58 0.0 .46 -118.000	20.10	4.8
	STA	DIR	QUAL	DIST	EVAZ	TOA	Х	Υ
	BAR	C	2	2.188	140.118	49.400	0.947	-1.134
	CSP	D	2	0.813	95.485	93.688	-2.407	0.231
	CWC	D	2	2.071	5.744	49.400	0.148	1.470
	GLA	D	1	3.208	113.308	49.400	1.357	-0.585
	GSC	D	2	1.562	53.242	49.400	1.184	0.884
	ISA	D	2	1.142	354.794	89.103	-0.225	2.470
	MWC	C	2	0.276	123.682	102.009	-1.851	1.234
	PAS	D	2	0.265	149.206	102.249	-1.136	1.906
	PLM	C	2	1.594	129.315	49.400	1.143	-0.936
	PYR	D	2	0.389	300.297	99.505	1.972	-1.152
	SBC	C	1	1.309	273.922	49.400	-1.474	0.101
	SYP	C	2	1.366	277.003	49.400	-1.466	0.180



EVENT				9/71 16 19 -000 27-44		25.62	4.2
AZ1= DIP1= AZ2= DIP2=	11	3.000 8.300					
SLIP	VECT	ORS=	28.300	69.578	23	7.000	23.000
PRIN	AXES	=	10.780	26.154	21	6.640	66.161
STA	DIR	QUAL	DIST	EVAZ	TOA	X	Υ
BAR CLC CWC GSC ISA MWC PAS PLM SBC SYP TIN ENGN	D C C C C D D C C	2 2 2 2 2 2 2 2 2	1.518 1.998 1.578 1.054 0.386 0.375 1.705 1.230 1.283	26.405 8.098 57.252 358.042 127.612 145.599 129.801 268.413 273.789 3.510	44.933 81.397 87.808 87.912 44.933 50.437 44.933 44.933	0.601 0.190 1.136 -0.079 1.942 1.386 1.038 -1.506 -1.348 0.083	1.210 1.338 0.731 2.304 -1.496 -2.025 -0.865 -0.042 0.089 1.349



EVENT DATA 5,1703 0 02/09/71 17 3 0.0 8.0 34.000 22.20 -118.000 29.50 3.9 AZ1= 280.000 DIP1= 40.000 AZ2= 136.000 DIP2= 55.830 SLIP VECTORS= 46.000 55.830 190.000 40.000 PRIN AXES 96.913 20.146 210.335 81.690 STA DIR QUAL DIST EVAZ TOA X Y 137.449 BAR C 1 2.270 49.400 0.999 -1.088 CSP 2 94.385 D 0.941 91.571 -2.458 0.189 CWC C 1 2.092 9.176 49.400 0.236 1.458 GSC C 2 1.670 55.698 49.400 1.220 0.833 ISA 0.552 D 1 1.141 89.116 0.024 2.481 MWC C 2 0.388 112.316 98.395 -2.137 0.877 2 PAS D 0.346 129.915 98.914 -1.7631.475 SBC 2 1.180 274.668 49.400 0.120 D -1.472 SYP 1 1.238 277.818 49.400 -1.464 0.201 D

4.498

49.400

0.116

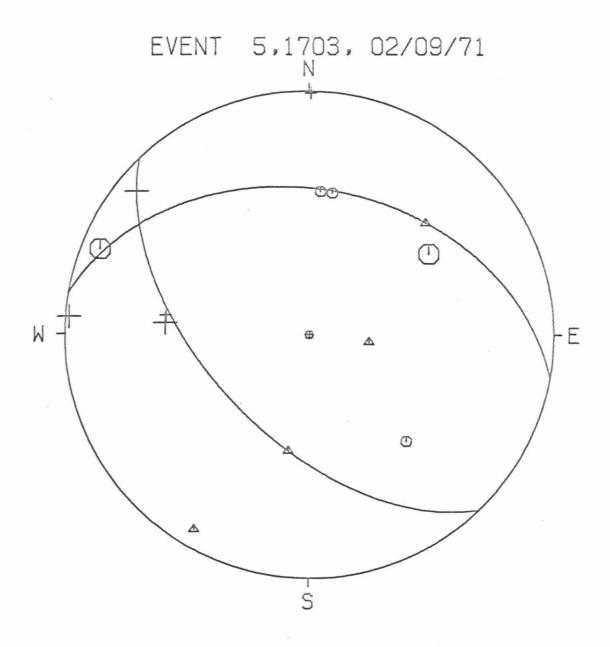
1.473

TIN

C

1

2.688



EVENT DATA 6,1719 0 02/09/71 17 19 0.0 34.000 24.70 -118.000 26.80 8.0 AZ1= 108.000 70.000 DIP1= AZ2= 198.000 D1P2= 90.000 SLIP VECTORS= 108.000 90.000 18.000 70.000 PRIN AXES = 64.779 76.005 331.219 76.005 STA DIR QUAL DIST EVAZ TOA Y X CSP C 2 0.908 97.131 91.978 -2.437 0.305 1.462 CWC 1 2.045 8.358 49.400 0.215 2 0.822 GSC C 1.616 56.194 49.400 1.228 2 1.099 2.491 ISA D 358.860 89.626 -0.050 2 1.169 MWC D 0.373 120.447 98.579 -1.988 2 PAS 0.349 139.173 98.879 -1.503 1.740 D 1.160 PLM 1 1.689 128.246 49.400 -0.915 D 2 -1.241 PYR D 0.290 302.933 99.605 1.915 1 1.215 272.384 0.061 SBC D 49.400 -1-476 0.147 2 1.270 275.718 -1.470 SYP 49.400 D 2 0.403 ENGN 132.269 98.206 -1.713 1.557 D

131.590

99.225

-1.713

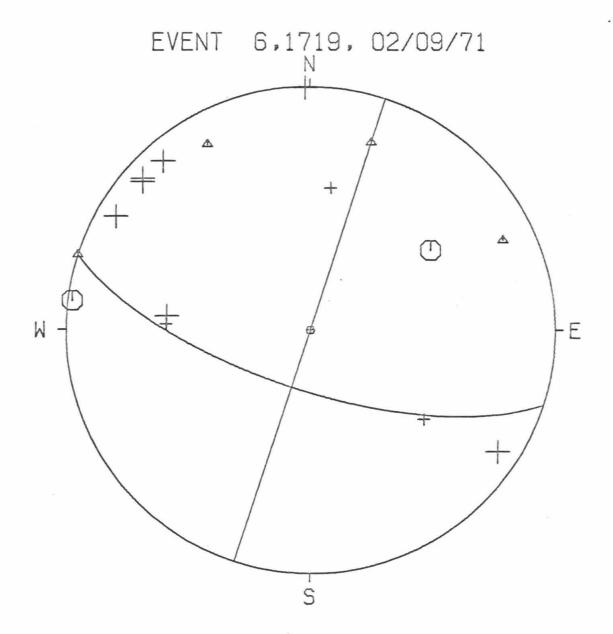
1.521

2

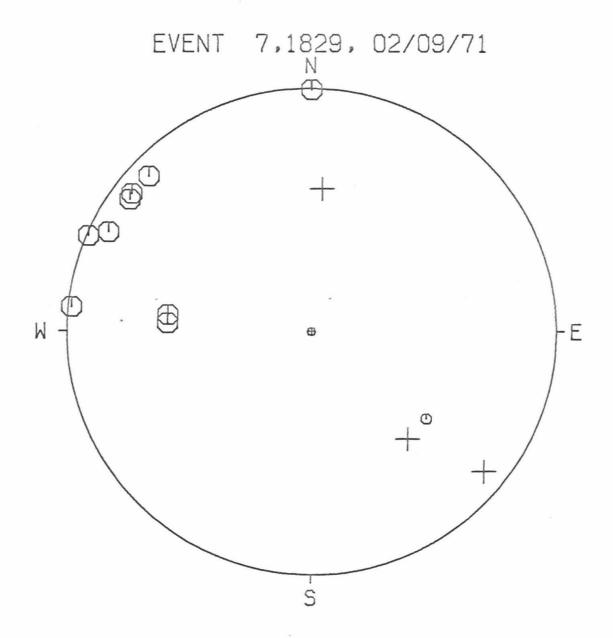
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D

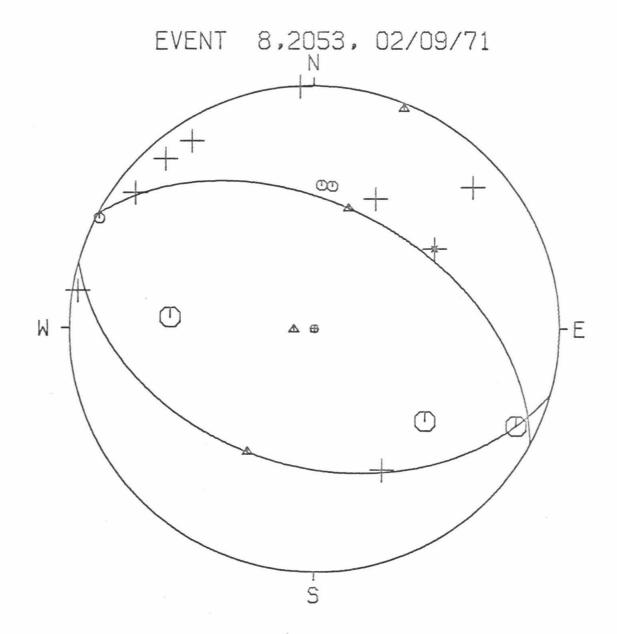
RCTR



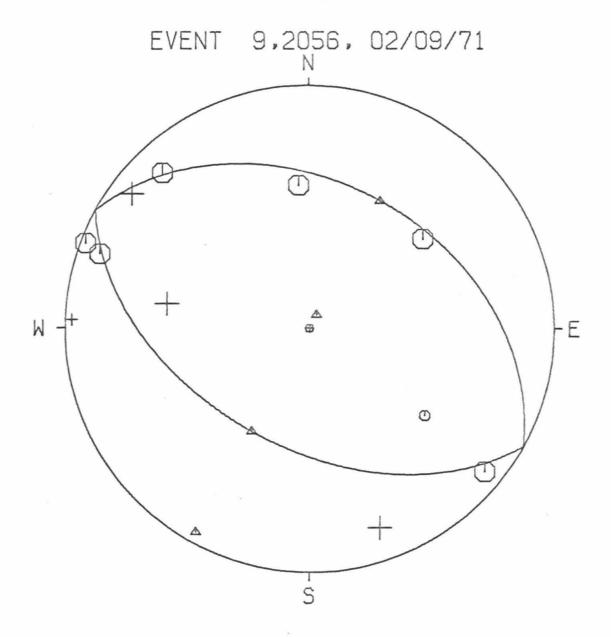
EVENT	DATA	4					
	7	1829	0 0	2/09/71 I8	3 29 0.0		
		9	8.0	34.000 23.	70 -118.000	28.90	3.8
STA	DIR	QUAL	DIST	EVAZ	TOA	Х	Υ
	_			* * * * * * * * * *		• • • • •	
BAR	D	2	2.283	138.032	49.400	0.988	-1.098
CSP	C	2	0.935	95.919	91.646	-2.451	0.254
ISA	C	2	1.116	0.188	89.423	0.008	2.487
MWC	C	2	0.391	116.259	98.358	-2.073	1.023
PAS	C	2	0.357	133.955	98.777	-1.657	1.597
PLM	C	1	1.702	127.187	49.400	1.177	-0.893
PYR	D	2	0.276	309.044	99.775	1.769	-1.435
SBC	C	2	1.187	273.439	49.400	-1.475	0.089
SYP	C	2	1.243	276.625	49.400	-1.468	0.170
TIN	D	2	2.662	4.368	49.400	0.113	1.473
RVR	C	2	1.001	113.298	90.836	-2.279	0.982
ENGN	C	2	0.414	127.774	98.070	-1.832	1.420
RCTR	C	2	0-333	126-214	99-070	-1-851	1.356



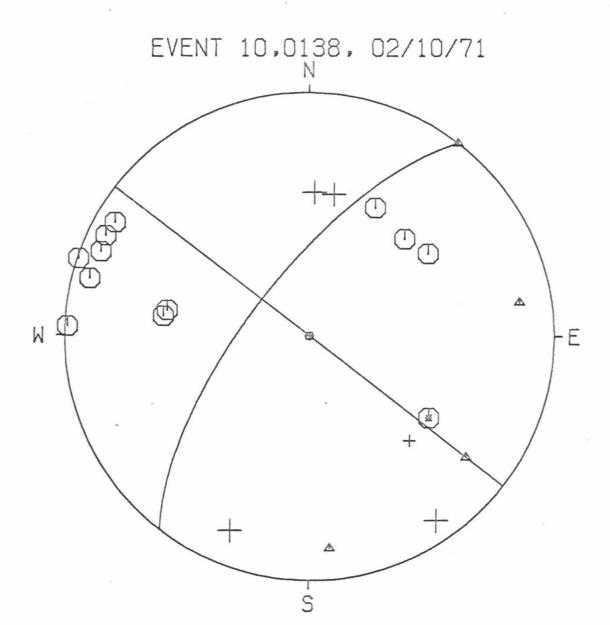
EVENT		4 ,2053		09/71 20 5 000 26.12		0 23.70	3.4
AZ1= DIP1= AZ2= DIP2=	10	98.000 48.000 05.800 42.652					
SLIP	VECT	TORS=	15.800	42.652	2	08.000	48.000
PRIN	AXE	S =	267.355	6.683		22.182	87.311
STA	DIR	QUAL	DIST	EVAZ	TOA	Х	Υ
CLC CSP CWC GSC ISA MWC PAS PLM PYR SYP TIN RVR BOUQ BRWN		2 1 -2 2 2 2 2 2 2 1 1 2 2	1.526 0.870 2.016 1.568 1.078 0.352 0.343 1.671 0.318 1.311 2.618 0.954 0.088 0.219	25.167 99.139 7.285 56.063 356.843 127.499 147.271 129.827 295.805 274.656 2.922 117.318 334.533 227.993	49.400 92.456 49.400 89.893 98.845 98.956 49.400 99.263 49.400 91.419 125.844 103.835	-2.194 0.692	0.388 1.465 0.825 2.494 1.400 1.932 -0.946 -0.997 0.120 1.475 1.133 -1.453
ENGN	D	2	0.390		98.370	1.620 -1.515	1.459 1.745



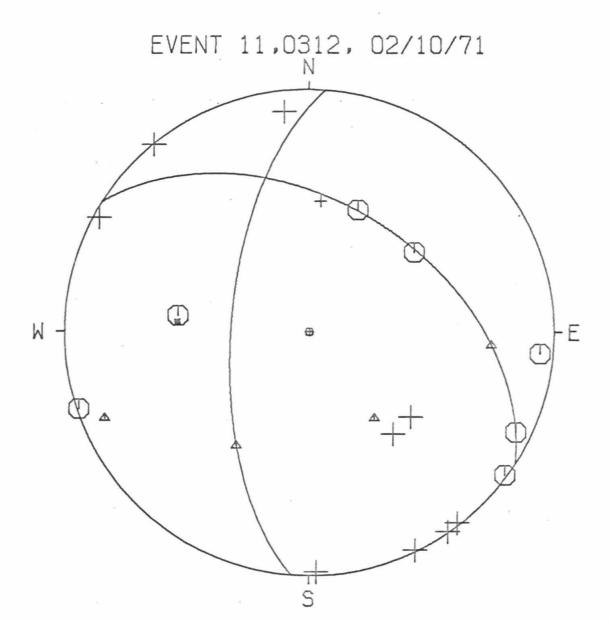
EVENT I	VENT DATA											
	9,	2056		09/71 20 5 000 18-50	66 0.0 -118.000	21.30	3.7					
AZ1= DIP1= AZ2= DIP2=	5 29	9.000 0.000 9.000 0.000										
SLIP	VECT	ORS=	209.000	40.000	1	29.000	50.000					
PRIN	AXES	=	28.958	5.007	2	08.999	85.000					
STA	DIR	QUAL	DIST	EVAZ	TOA	X	Υ					
CSP GSC ISA MWC PAS PLM PYR SYP RVR BOUQ ENGN	0000000000	1 2 2 2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0.826 1.616 1.206 0.261 0.222 1.566 0.412 1.360 0.872 0.213 0.280	92.068 51.713 355.746 109.584 136.774 127.061 309.265 279.793 110.929 340.514 127.292	92.994 49.400 49.400 99.964 103.490 49.400 98.099 49.400 92.431 104.363 99.732	-2.432 1.160 -0.110 -2.142 -1.499 1.179 1.794 -1.456 -2.285 0.723 -1.813	0.088 0.915 1.473 0.762 1.595 -0.890 -1.467 0.251 0.874 -2.044 1.381					



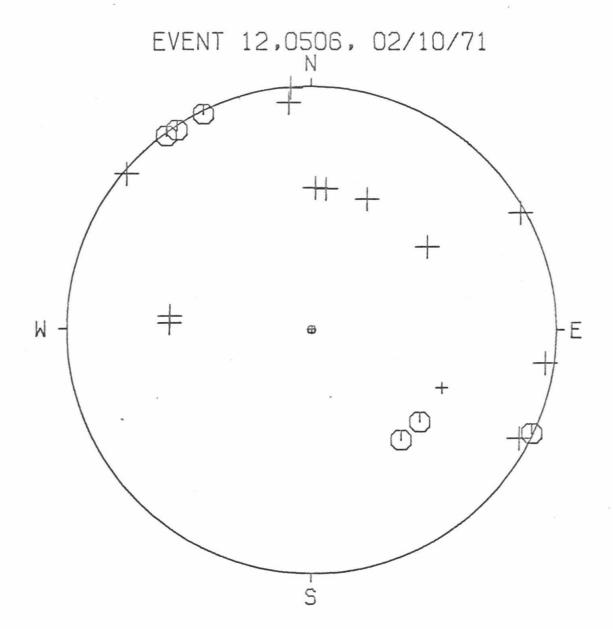
EVENT DATA 10,0138		10/71 1 3 4.000 19.30	88 0.0 -118.00	0 32.00	3.9
AZI= 217.500 DIPI= 70.000 AZZ= 307.500 DIPZ= 90.000					
SLIP VECTORS=	217.500	90.000	1	27.500	70.000
PRIN AXES =	174.281	76.005		80.715	76.005
STA DIR QUAL	DIST	EVAZ	TOA	Х	Y
BAR D 1 CLC C 2 CSP C 2 CWC D 2 GSC C 2 ISA D 2 MWC C 2 PAS C 2 PLM C -2 PYR D 2 SBC C 2 SYP C 2 RVR C 2 BOUQ D 2 BRWN C 2 ENGN C 2	0.974	135.959 26.982 92.286 9.855 54.991 2.004 104.677 120.394 124.324 325.206 277.653 280.258 108.610 21.961 224.302 116.256	49.400 49.400 91.171 49.400 49.400 98.164 98.893 49.400 99.466 50.496 49.400 90.659 105.275 133.558 98.088	1.027 0.670 -2.472 0.253 1.210 0.052 -2.240 -1.983 1.220 1.304 -1.495 -1.454 -2.356 -0.802 0.974 -2.078	-1.062 1.317 0.099 1.456 0.848 1.476 0.587 1.163 -0.833 -1.877 0.201 0.263 0.793 -1.990 0.998 1.025
RCTR C 2	0.336	112.018	99.034	-2.128	0.861



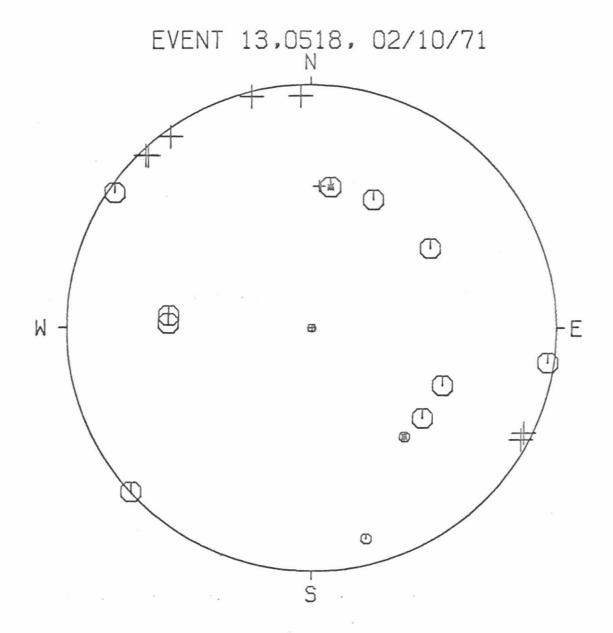
EVENT DATA 11,0312		10/71 3 1 4.000 22.20	2 0.0 -118.000	18.12	4.0
AZ1= 302.500 DIP1= 46.000 AZ2= 184.000 DIP2= 63.706					
SLIP VECTORS=	94.000	63.706	21	2.500	46.000
PRIN AXES =	142.808	36.445	24	6.981	79.749
STA DIR QUAL	DIST	EVAZ	TCA	Х	Υ
BAR D 2 CLC C 2 CSP C 2 CWC D 1 GSC C 2 ISA D 2 MWC C 2 PAS D 2 PLM D 2 PYR D 2 SBC -1 SYP C 2 RVR C 2 USC D 2 BOUQ D 2 BRWN C 2 ENGN D 2 RCTR D 2	2.167 1.555 0.785 2.073 1.543 1.149 0.250 0.247 1.570 0.414 1.337 1.394 0.856 0.357 0.181 0.253 0.291	140.614 21.635 95.308 5.000 52.526 353.611 126.197 154.048 129.845 298.797 274.219 277.069 115.857 178.249 320.698 251.391 142.097 145.184	44.933 83.978 44.933 84.933 89.106 89.136 44.933 87.536 44.933 44.933 83.299 88.086 89.937 89.084 88.718	0.857 0.498 2.355 0.118 1.072 -0.254 2.002 1.086 1.037 -2.143 -1.347 -1.341 2.114 0.075 -1.583 -2.350 1.519	-1.044 1.256 -0.219 1.346 0.822 2.270 -1.465 -2.231 -0.866 1.178 0.099 0.166 -1.025 -2.457 1.933 -0.791 -1.950



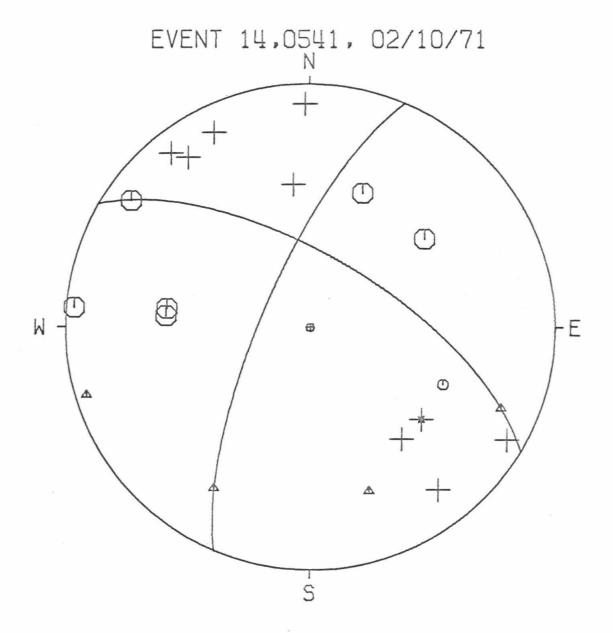
EVENT	NT DATA 12,0506		0 02	2/10/71 5	6 0.0		
		,0000	5.0	34.000 24.67		19.76	4.3
STA	DIR	QUAL	DIST	EVAZ	TOA	X	Υ
BAR	С	2	2.213	140.824	48.650	0.920	-1.129
CLC	D	2	1.526	22.974	48.650	0.568	1.341
CSP	D	2	0.812	98.020	86.079	2.389	-0.337
CWC	D	2	2.034	5.719	48.650	0.145	1.449
GLA	D	1	3.218	113.944	48.650	1.331	-0.591
GSC	D	2	1.537	54.231	48.650	1.182	0.851
ISA	D	2	1.106	354.427	83.064	-0.228	2.333
MWC	D	2	0.295	130.367	91.396	-1.881	1.599
PAS	C	2	0.295	153.659	91.396	-1.096	2.213
PLM	C	2	1.614	130.435	48.650	1.108	-0.945
PYR	C	2	0.376	295.138	90.563	2.252	-1.057
SBC	D	2	1.312	272.656	48.650	-1.455	0.067
SYP	D	2	1.367	275.468	48.650	-1.450	0.139
TIN	D	2	2.640	1.755	48.650	0.045	1.456
RVR	D	2	0.895	117.582	85.233	2.122	-1.108
USC	D	2	0.399	175.172	90.324	-0.210	2.484
BRWN	D	2	0.249	240.649	92.068	2.139	1.203
ENGN	C	2	0.337	143.386	90.957	-1.479	1.990
PCTP	C	2	0 257	146 205	01 800	-1 365	2 0/7



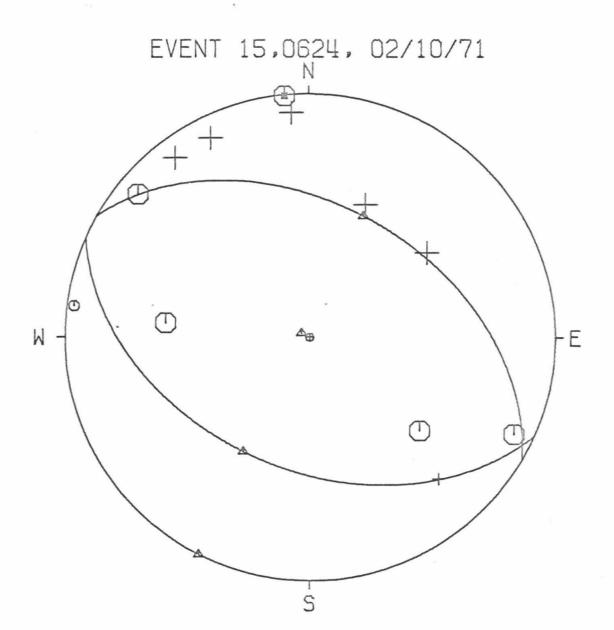
EVENT		0518	0 02	2/10/71 5	18 0.0		
			5.8	34.000 25.5	5 -118.000	24.85	4.5
STA	DIR	QUAL	DIST	EVAZ	TOA	Х	Υ
BAR	С	-1	2.269	139.634	48.850	0.947	-1.114
CLC	C	2	1.541	25.541	48.850	0.630	1.319
CSP	C	2	0.884	98.305	87.194	2.412	-0.352
CWC	C	-2	2.028	7.683	48.850	0.195	1.449
GLA	C	2	3.288	113.634	48.850	1.339	-0.586
GSC	C	2	1.586	56.103	48.850	1.213	0.815
ISA	D	2	1.086	357.600	85.005	-0.100	2.387
MWC	C	2	0.359	124.745	92.876	-2.002	1.389
PAS	D	2	0.343	144.059	93.051	-1.428	1.969
PLM	C	2	1.677	129.213	48.850	1.133	-0.924
PYR	D	2	0.306	298.123	93.443	2.138	-1.142
SBC	C	2	1.241	271.910	48.850	-1.461	0.049
SYP	C	2	1.296	275.085	48.850	-1.456	0.130
TIN	D	1	2.628	3.244	48.850	0.083	1.460
RVR	D	2	0.963	116.348	86.332	2.167	-1.073
USC	D	2	0.425	165.838	92.158	-0.600	2.378
BOUQ	C	1	0.088	345.436	101.562	0.562	-2.164
BRWN	C	2	0.199	227.479	89.599	-1.836	-1.684
ENGN	D	2	0.394	136.443	92.494	-1.685	1.772
RCTR	D	2	0.312	136.866	93.388	-1.658	1.770



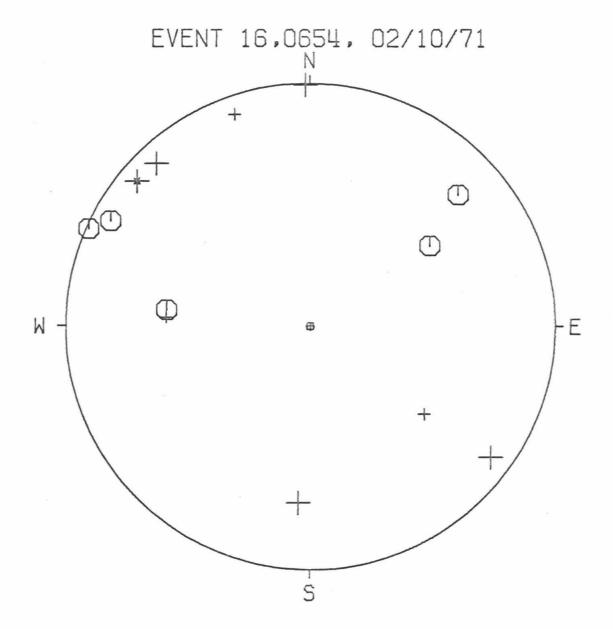
EVENT DATA 14,0541		10/71 5 4	0.0	17.80	3.7
AZ1= 300.500 DIP1= 66.000 AZ2= 203.000 DIP2= 73.661					
SLIP VECTORS=	113.000	73.661	21	0.500	66.000
PRIN AXES =	160.144	60.887	25	2.983	84.912
STA DIR QUAL	DIST	EVAZ	TCA	×	Υ Υ
BAR D 2 CLC C 2 CSP C 2 GLA C 1 GSC C 2 ISA D 2 MWC C 2 PAS D 2 PLM D -2 PYR D 2 SBC C 2 SYP C 2 USC D 2 BOUQ D 2 ENGN D 2 RCTR D 2	2.157 1.563 0.780 3.173 1.546 1.159 0.242 0.237 1.560 0.423 1.342 1.400 0.347 0.193 0.281 0.200	140.543 21.351 94.855 113.322 52.126 353.469 125.398 154.102 129.672 299.840 274.582 277.438 178.934 321.790 141.723 144.639	49.400 49.400 93.562 49.400 49.400 101.526 102.001 49.400 97.961 49.400 49.400 98.907 106.329 99.714 105.651	0.939 0.538 -2.412 1.357 1.166 -0.168 -1.823 -0.972 1.137 2.013 -1.473 -1.465 -0.043 1.311 -1.412 -1.236	-1.141 1.376 0.205 -0.585 0.907 1.468 1.295 2.002 -0.943 -1.155 0.118 0.191 2.298 -1.665 1.789 1.742



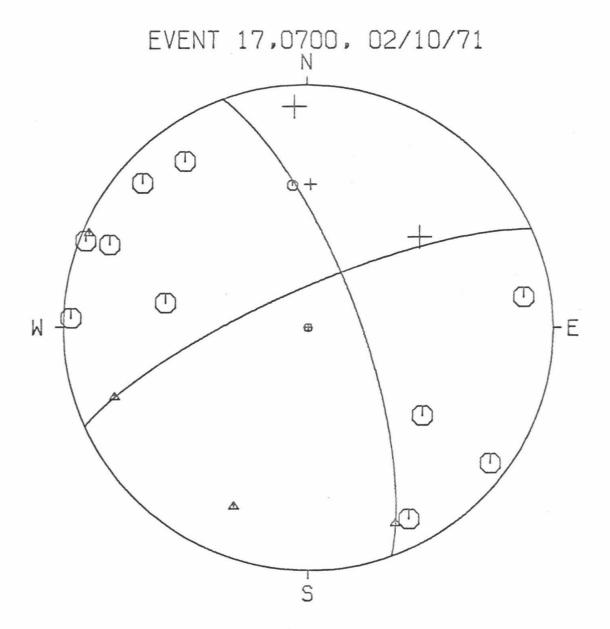
DIP1=	30	0.000		10/71 · 6 2 4.000 24.40		0 19.50	3.4
AZ2= DIP2=		4.000 5.157					
SLIP	VECT	ORS=	24.000	45.157	2	10.000	45.000
PRIN	AXES	=	298.875	3.016	2	06.995	89.921
STA	DIR	QUAL	DIST.	EVAZ	TOA	Х	Y
CLC CSP GSC ISA MWC PAS PLM PYR SYP USC BOUQ ENGN		2 1 2 -2 2 2 2 2 2 2 2 2 2 2 2		130.053 153.924	49.400 93.218 49.400 89.487 99.621 99.613 49.400 98.483 49.400 98.315 112.520 99.085	-1.746 -1.003 1.125 2.083 -1.470 -0.176	0.323 0.868 2.476 1.468 2.049 -0.958 -0.995 0.145 2.305



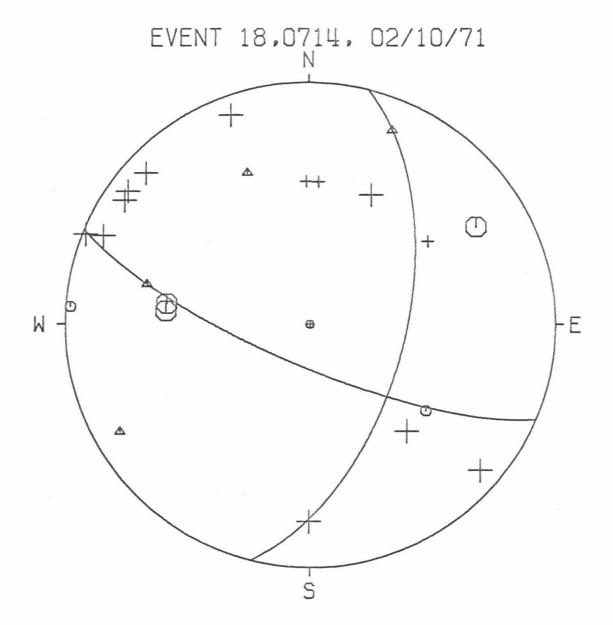
EVENT		4 ,0654		/10/71 6 34.000 23.7	54 0.0 0 -118.000	27.00	3.4
STA	DIR	QUAL	DIST	EVAZ	TCA	Х	Υ
GSC	С	2	1.628	55.760	49.400	1.221	0.831
ISA	D	2	1.116	359.000	89.421	-0.043	2.487
MWC	C	2	0.367	117.963	98.650	-2.035	1.081
PAS	D	2	0.339	137.022	99.006	-1.565	1.680
PLM	D	1	1.681	127.748	49.400	1.168	-0.904
PYR	D	2	0.297	305.965	99.514	1.849	-1.341
SBC	D	1	1.213	273.525	49.400	-1.475	0.091
SYP	C	2	1.269	276.495	49.400	-1.468	0.167
RVR	C	2	0.977	113.934	91.131	-2.262	1.004
USC	D	1	0.404	160.657	98.200	-0.767	2.184
BOUQ	D	2	0.115	3.656	118.092	-0.116	-1.815
BRWN	C	2	0.157	228.090	109.804	1.513	1.358
ENGN	0	-2	0 305	130 222	09 315	-1 765	1 403



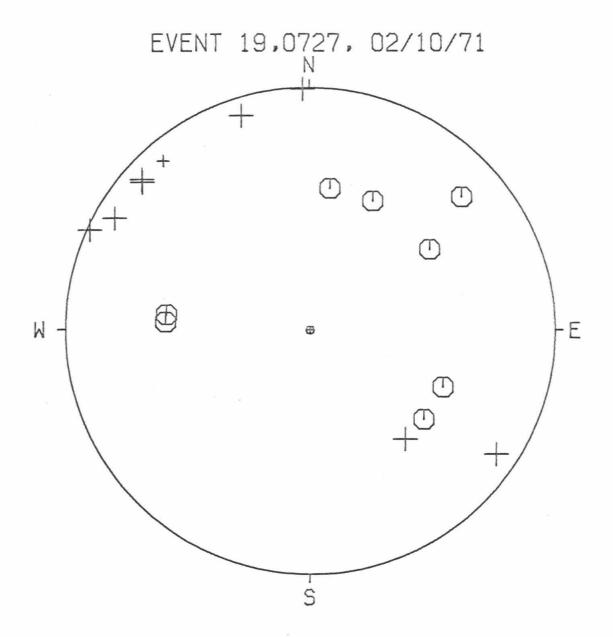
EVENT				10/71 7	0 0.0	00 18.50	3.5
AZ1= DIP1= AZ2= DIP2=	24	0.000 3.000 6.000 7.148					
SLIP	VECT	DRS=	156.000	77.148		250.000	73.000
PRIN	AXES	=	202.406	68.652	:	293.517	87.166
STA	DIR	QUAL	DIST	EVAZ	TOA	Х	Υ
CSP GSC ISA MWC PAS PLM PYR SYP TIN RVR USC BOUQ BRWN ENGN	0000000000000	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0.788 1.590 1.216 0.225 0.193 1.532 0.447 1.399 2.748 0.833 0.289 0.236 0.237 0.245	92.335 50.678 354.152 112.792 143.999 127.768 306.821 279.799 1.335 111.502 176.801 332.280 261.822 131.515	93.469 49.400 49.400 103.235 106.329 49.400 97.672 49.400 92.904 99.621 102.162 102.081 101.214	1.143	0.099 0.936 1.470 0.850 1.715 -0.905 -1.395 0.251 1.477 0.893 2.278 -1.966 0.316 1.487



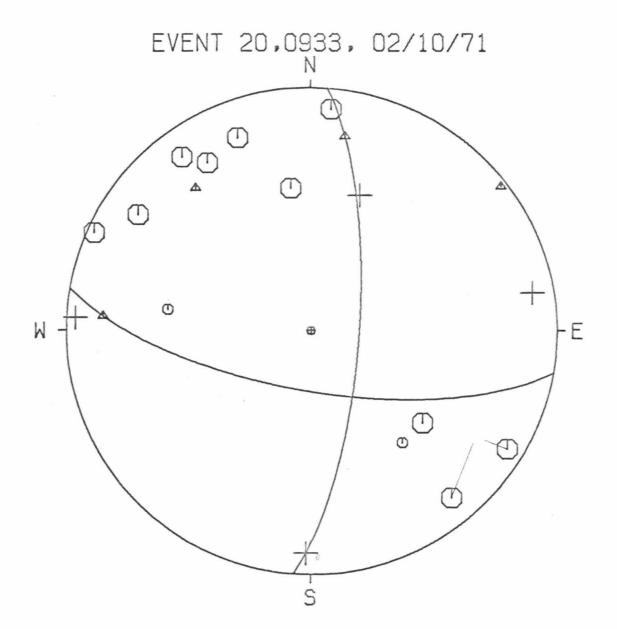
EVENT DATA 18,0714 0 02/10/71 7 14 0.0 8.0 34.000 21.40 -118.000 26.50	3.4
AZ1= 14.000	
DIP1= 58.000 AZ2= 113.000	
DIP2= 75.945	
SLIP VECTORS= 23.000 75.945 283.999	58.000
PRIN AXES = 337.992 56.877 240.218	78.289
STA DIR QUAL DIST. EVAZ TCA X	Υ
BAR D 2 2.232 138.031 49.400 0.98	88 -1.098
CLC D 2 1.613 25.197 49.400 0.62	9 1.337
CSP C 1 0.900 94.262 92.085 -2.44	7 0.182
GSC D 1 1.644 54.526 49.400 1.20	0.857
ISA D 1 1.155 358.729 49.400 -0.03	
MWC D 2 0.346 113.370 98.914 -2.11	
PAS D 2 0.307 133.177 99.394 -1.66	
PLM C 1 1.653 126.856 49.400 1.18	
PYR D 2 0.327 310.766 99.151 1.73	
SBC C 2 1.222 275.250 49.400 -1.47	
SYP C 2 1.281 278.202 49.400 -1.46	
TIN D 1 2.698 3.629 49.400 0.09	
RVR D 2 0.956 112.070 91.388 -2.28 USC D 2 0.366 159.703 98.670 -0.79	
BOUQ D 2 0.155 0.184 110.101 -0.00	
BRWN C 2 0.144 239.218 112.241 1.69	
ENGN D 2 0.366 126.517 98.664 -1.85	
RCTR D 2 0.285 124.049 99.672 -1.88	



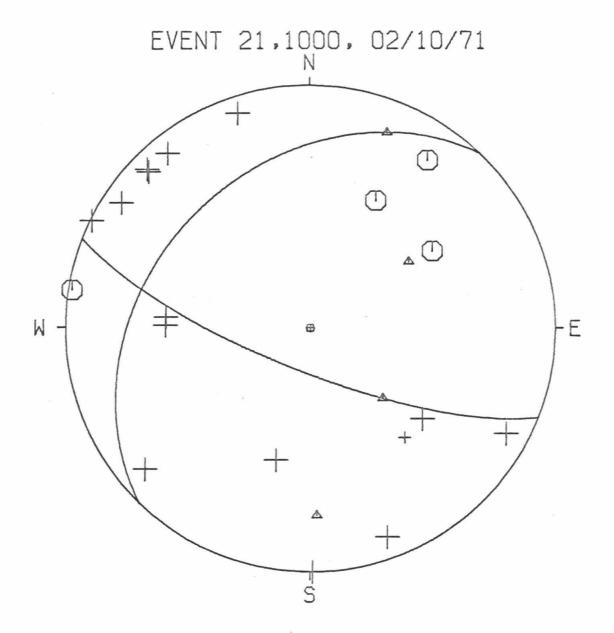
EVENT	DATA	4					
	19	0727	0 02	2/10/71 7	27 0.0		
			8.0	34.000 24.1	0 -118.000	26.10	3.8
STA	DIR	QUAL	DIST	EVAZ	TCA	X	Υ
BAR	D	2	2.262	138.898	49.400	0.971	-1.113
CLC	C	2	1.570	25.716	49.400	0.641	1.331
CWC	C	2	2.054	8.058	49.400	0.207	1.463
GLA	C	2	3.295	113.120	49.400	1.359	-0.580
GSC	C	2	1.614	55.712	49.400	1.221	0.832
ISA	D	2	1.110	358.432	89.497	-0.068	2.488
MWC	D	2	0.360	120.008	98.737	-1.994	1.151
PAS	D	1	0.336	139.411	99.042	-1.493	1.743
PLM	C	2	1.676	128.199	49.400	1.161	-0.914
PYR	D	2	0.304	303.623	99.434	1.904	-1.266
SBC	C	2	1.225	273.244	49.400	-1.475	0.084
SYP	C	2	1.281	276.182	49.400	-1.469	0.159
RVR	D	2	0.969	114.638	91.233	-2.248	1.031
USC	D	2	0.407	162.644	98.164	-0.691	2.210
BRWN	C	2	0.172	228.542	108.305	1.552	1.371
ENGN	D	2	0.390	132.226	98.370	-1.711	1.553
RCTR	D	2	0.308	131.686	99.379	-1.708	1.521



EVENT			0 02/10/71 9 33 0.0 8.0 34.000 19.60 -118.000 15.20 3.2					
AZ1= DIP1= AZ2=	7	4.000 4.000 0.000	×					
DIP2=		9.971	**	*				
SLIP	VECT	ORS=	10.000	69.971	2	73.999	74.000	
PRIN	AXES	=	321.272	64.082		52.589	87.290	
STA	DIR	QUAL	DIST	EVAZ	TOA	Χ .	Υ	
BAR	С	1	2.108	140.747	49.400	0.935	-1.144	
CTC	D	2	1.581	19.727	49.400	0.499	1.391	
CSP	D	2	0.743	93.184	94.024	-2.407	0.134	
AZI	C	2	1.197	352.118	49.400	-0.203	1.463	
MWC	C	2	0.195	123.964	106.133	-1.762	1.187	
PAS	C	2	0.193	159.429	106.329	-0.745	1.984	
PLM	С	2	1.512	129.596	49.400	1.138	-0.942	
PYR	С	2	0.471	301.100	97.378	1.999	-1.206	
SYP	C	1	1.440	278.545	49.400	-1.461	0.220	
RVR	С	2	0.801	114.365	93.302	-2.211	1.001	
USC	С	2	0.315	185.377	99.294	0.215	2.279	
BOUQ	С	2	0.241	319.890	101.683	1.438	-1.707	
BRWN	D	2	0.284	260.058	99.680	2.246	0.394	
NRTM	D	2	0.271	1.162	99.837	-0.046	-2.276	
ENGN	C	2	0.233	143.653	102.405	-1.313	1.784	
RCTR	С	2	0.153	148.655	110.361	-1.050	1.724	



EVENT				10/71 10 4.000 26.80		27.70	3.4
AZ1= DIP1= AZ2= DIP2=	: 3 11	4.000 4.000 1.500 5.527					
SLIP	VECT	ORS=	21.500	75.527	13	34.000	34.000
PRIN	AXES	=	55.906	40.276	17	77.895	65.827
STA	DIR	QUAL	DIST	EVAZ	TOA	X	Υ
BAR CLC CSP GSC ISA MWC PAS PLM PYR SBC SYP RVR USC BOUQ BRWN NRTM		1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2.311 1.540 0.925 1.608 1.064 0.403 0.383 1.721 0.262 1.202 1.255 1.008 0.456 0.069 0.188 0.234	139.202 27.166 99.022 57.467 359.414 123.864 141.104 128.898 298.310 271.036 274.305 116.371 161.649 14.374 214.824 49.270	49.400 49.400 91.770 49.400 90.058 98.218 98.457 49.400 99.945 49.400 90.754 97.560 133.558 106.828 102.323	0.965 0.675 -2.431 1.246 0.026 -1.922 -1.450 1.150 2.002 -1.477 -1.473 -2.225 -0.733 -0.346 1.203 -1.680	-1.118 1.314 0.386 0.795 -2.499 1.290 1.797 -0.928 -1.078 0.027 0.111 1.103 2.211 -1.350 1.730 -1.447
ENGN SWM RCTR	D D	2 2 2	0.437 0.289 0.353	134.564 339.693 134.410	97.798 99.621 98.824	-1.656 0.792 -1.643	1.631 -2.140 1.610



EVENT DATA 0 02/10/71 11 29 0.0 22,1129 8.0 34.000 27.20 -118.000 25.60 AZ1= 211.500 DIP1= 58.000 108.000 AZ2= DIP2= 69.515 SLIP VECTORS= 18.000 69.515 121.500 58.000 PRIN AXES 66.140 161.994 51.526 82.689 STA DIR QUAL DIST EVAZ TOA Y X CLC 1.521 26.327 49.400 D 1 0.655 1.324 CSP C 2 0.898 99.830 92.106 -2.418 0.419 2 1.463 CWC D 2.002 8.074 49.400 0.208 GSC C 2 1.580 57.122 49.400 1.241 0.802 ISA D 2 1.058 358.036 90.129 0.086 -2.496 2 127.081 MWC D 0.383 98.464 -1.842 1.392 2 98.598 PAS D 0.372 145.318 -1.312 1.896 -2 PLM D 1.703 129.708 49.400 1.137 -0.944 2 294.636 99.655 PYR D 0.286 2.073 -0.951 SBC C 2 1.231 268.235 49.400 -1.477-0.046 2 1.284 SYP D 273.912 49.400 -1.4740.101 2 0.985 117.531 91.030 RVR D -2.197 1.145 USC D 2 0.454 165.406 97.581 -0.587 2.254 2 D 0.063 136.401 0.250 -1.289 BOUQ 349.021 BRWN -1 0.213 219.725 104.363 1.385 1.667 2 NRTM D 0.208 45.432 104.814 -1.537 -1.514 2 97.978 ENGN D 0.422 138.067 -1.5501.726 2 0.295 99.547 SWM D 334.034 1.000 -2.053 0.495 2 117.409 NSCF D 0.119 105.631 -1.769

138.813

-1.512

1.728

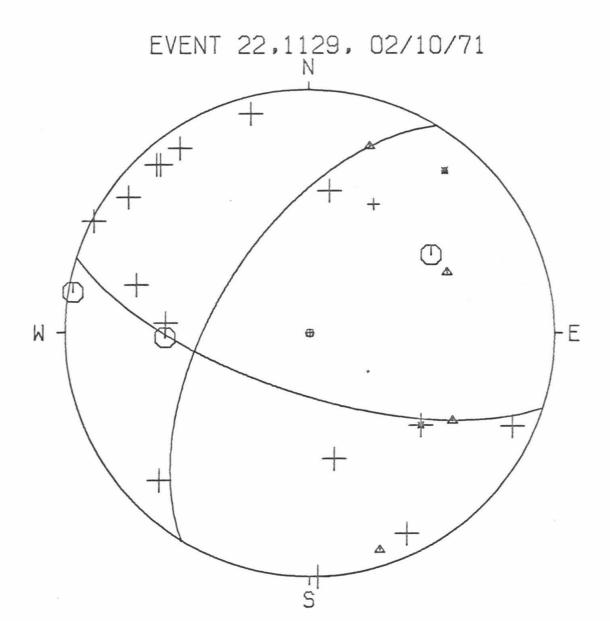
98.999

RCTR

2

0.339

D



EVENT DATA 23,1131 0 02/10/71 11 31 0.0 34.000 23.06 -118.000 27.30 6.0 AZ1= 120.000 DIP1= 60.000 AZ2= 214.000 DIP2= 83.110 SLIP VECTORS= 124.000 83.110 30.000 60.000 PRIN AXES = 81.178 64.000 343.361 74.411 X . STA DIR QUAL DIST EVAZ TOA Υ BAR C 2 138.282 48.900 0.974 -1.092 2.260 CLC C 2 1.593 25.971 48.900 0.641 1.316 CSP C 2 0.913 95.493 87.342 2.430 -0.234 2 CWC D 2.073 8.433 48.900 0.215 1.448 2 GSC C 1.637. 55.536 48.900 1.207 0.828 2 ISA D 1.126 359.196 84.997 -0.034 2.388 MWC D 2 0.366 116.209 93.328 -2.1771.072 2 135.175 -1.705 PAS D 0.333 93.690 1.715 2 PLM C 1.678 127.363 48.900 1.163 -0.888 PYR C 2 0.300 307.956 94.055 1.900 -1.482 2 SBC D 1.209 273.722 48.900 -1.460 0.095 SYP 2 D 1.267 277.029 48.900 -1.452 0.179 2 RVR C 0.977 113.268 86.638 2.228 -0.958 2 USC D 0.395 159.563 93.013 -0.850 2.280 2 BOUQ D 0.127 5.212 94.739 -0.218 -2.385 2 C 229.572 BRWN 0.148 91.400 1.880 1.601 2 NRTM C 0.274 38.831 94.339 -1.507-1.872 D 2 0.391 128.555 93.062 -1.902 ENGN 1.516 2 SWM D 0.349 342.394 93.514 0.733 -2.309

126.817

93.964

-1.931

1.445

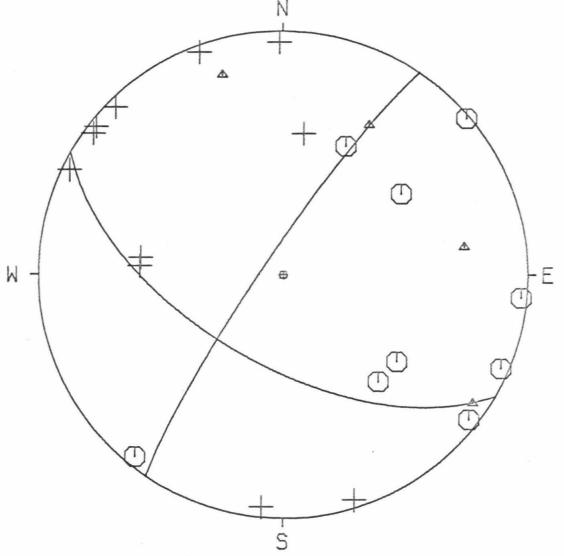
2

0.308

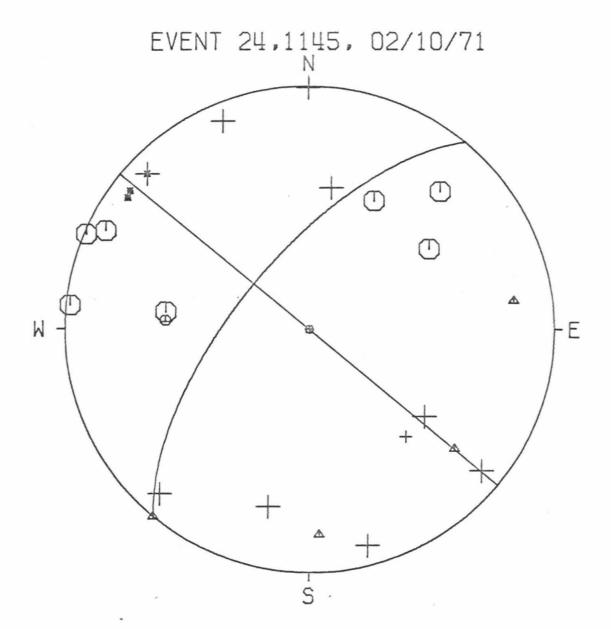
D

RCTR

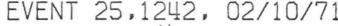
EVENT 23,1131, 02/10/71

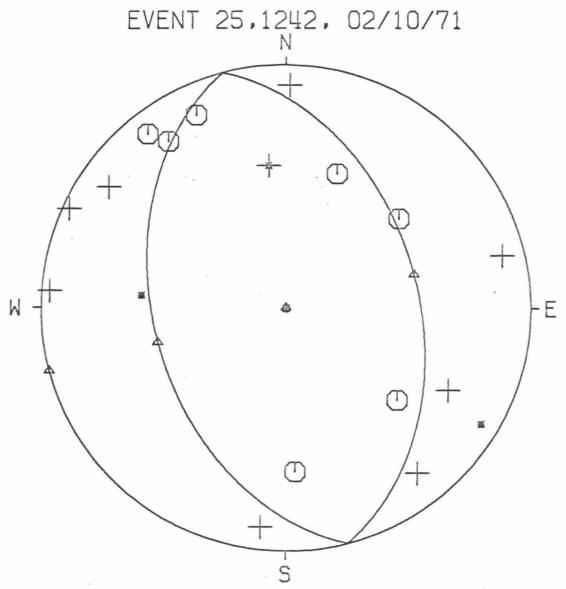


EVENT				.0/71 11 4		28.50	3.5
AZ1= DIP1= AZ2= DIP2=	12	19.500 66.000 29.500 90.000					
SLIP	VECT	rors=	39.500	90.000	12	9.500	66.000
PRIN	AXES	= 2	81.909	73.286	17	7.087	73.285
STA	DIR	QUAL	DIST	EVAZ	TCA	X	Υ
BAR CLC CSP CWC GSC ISA MWC PAS PLM PYR SBC SYP RVR USC BOUQ BRWN NRTM			1.595 0.930 2.070 1.648 1.121 0.384	138.056 26.583 95.721 8.896 56.006 359.938 115.984 134.038 127.170 309.363 273.639 276.851 113.212 157.669 12.942 223.412 42.066		0.987 0.661 -2.450 0.228 1.225 -0.003 -2.076 -1.653 1.177 1.763 -1.474 -1.467 -2.279 -0.880 -0.419 1.340 -1.527	2.486 1.012 1.598 -0.893 -1.446 0.094 0.176
ENGN SWM RCTR	D	-1 2 -1	0.408 0.339 0.326	127.834 344.750 126.149	98.152 98.999 99.15 8	-1.829 0.604 -1.851	1.421 -2.215 1.352

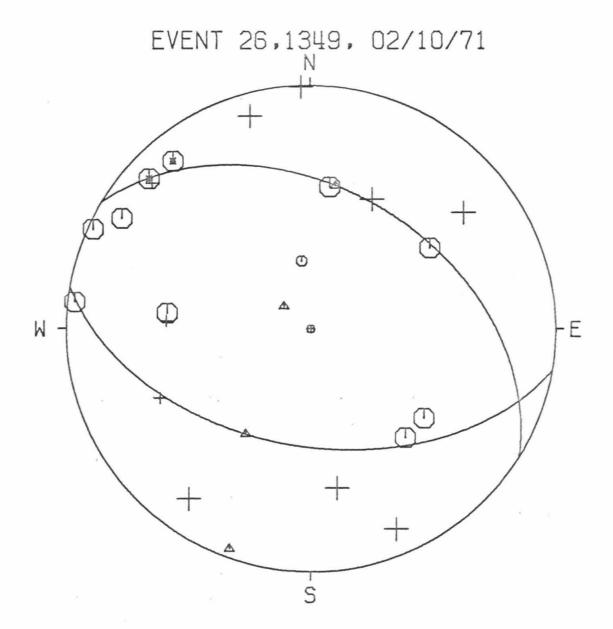


EVENT DATA 25,1242 AZ1= 165.000		10/71 12 4		0 16.90	3.4
DIP1= 45.000 AZ2= 345.000 DIP2= 45.000					
SLIP VECTORS=	255.000	45.000		75.000	45.000
PRIN AXES =	0.000	0.256	2	54.998	90.000
STA DIR QUAL	DIST	EVAZ	TOA	×	Υ
CLC C 2 CSP D 2 GSC C 2 ISA D -2 MWC D 2 PAS C 2 PLM C 2 PYR -1 SBC -1 RVR D 2 USC D 2 BOUQ D 2 BRWN D 2 NRTM D 2 NRTM D 2 NSCF C 2 NSGM D 2	1.572 0.767 1.545 1.176 0.225 0.219 1.542 0.441 1.355 0.830 0.332 0.211 0.264 0.255 0.262 0.097 0.122	20.739 94.179 51.422 353.012 124.535 155.311 129.554 300.701 275.239 114.807 181.033 321.450 256.088 6.509 141.824 356.740 296.783	49.400 93.724 49.400 103.235 103.835 49.400 97.738 49.400 92.947 99.085 104.542 99.927 100.303 99.954 123.029 116.746	0.523 -2.411 1.155 -0.180 -1.808 -0.911 1.139 2.000 -1.471 -2.210 0.041 1.348 2.208 -0.257 -1.405 0.096 1.655	1.382 0.176 0.921 1.466 1.245 1.981 -0.941 -1.187 0.135 1.022 2.294 -1.692 0.547 -2.251 1.787 -1.683 -0.835

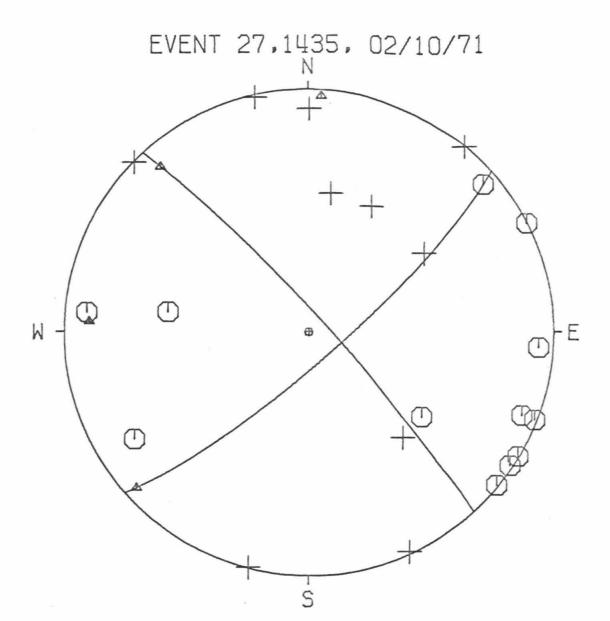




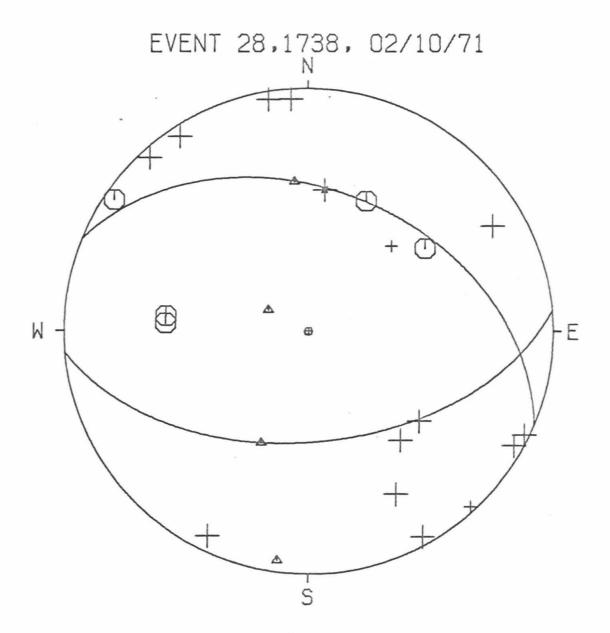
EVENT				.0/71 13 4 .000 23.94		0 25.12	4.3
AZ1= DIP1= AZ2= DIP2=	3 (00.000 50.000 01.500 42.046					
SLIP	VEC	TORS=	211.500	42.046		10.000	50.000
PRIN	AXE	s =	310.227	11.589	2	200.020	85.952
STA	DIR	QUAL	DIST	EVAZ	TOA	X	Υ
BAR CLC CSP CWC GSC ISA MWC PAS PLM SBC SYP RVR USC BOUQ BRWN NRTM ENGN SWM NSCF		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0.884 2.055 1.604 1.113 0.347 0.324 1.663 1.239 1.295 0.955 0.400 0.114 0.180 0.245 0.377 0.346	273.140 276.226 114.809 164.369 350.630 232.391 35.444 133.147 336.926	101.505 102.148 49.400 49.400 92.273 99.955 124.023 112.165 105.264 100.612 101.521	0.967 0.630 -2.414 0.198 1.216 -0.095 -1.927 -1.403 1.158 -1.475 -1.469 -2.224 -0.613 0.270 1.563 -1.244 -1.648 0.877 -1.536	-1.117 1.336 0.276 1.464 0.839 2.486 1.136 1.723 -0.918 0.081 0.160 1.028 2.190 -1.637 1.204 -1.748 1.544 -2.058 -0.711
	D	2				0.877 -1.536 -0.091	-2.05



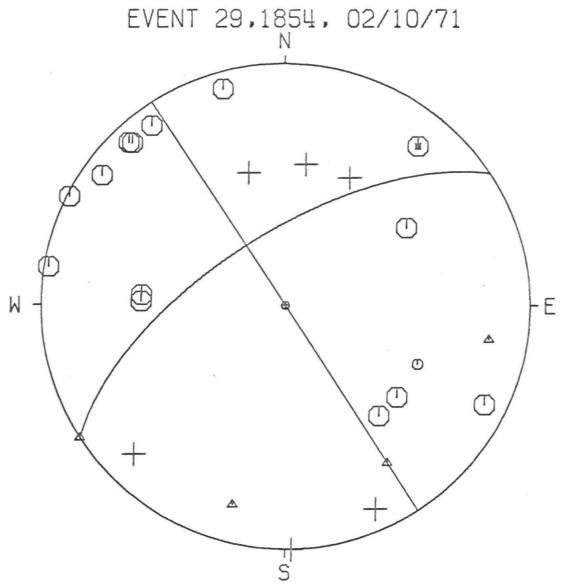
EVENT DATA 27,1435		10/71 14 3 4.000 21.69		0 29.20	4.2
AZ1= 48.500 DIP1= 80.000 AZ2= 317.500 DIP2= 84.349					
SLIP VECTORS=	227.500	84.349	3	18.499	80.000
PRIN AXES =	272.707	78.906		3.293	86.953
STA DIR QUAL	DIST	EVAZ	TOA	X	Υ
BAR D 2 CLC D 2 CSP C 2 CWC D 2 GSC D 2 ISA D 2 MWC C 2 PAS C 2 PLM C 2 PYR D 2 SBC C 2 SYP C 2 RVR C 2 USC D 2 BOUQ D 2 BRWN C 2 NRTM D 2 NRTM D 2 NSCF C 2 NSGM C 2 RCTR C 2	2.261 1.625 0.937 2.100 1.672 1.149 0.381 0.337 1.686 0.295 1.185 1.244 0.992 0.385 0.153 0.114 0.309 0.399 0.364 0.183 0.071 0.318	137.384 26.433 93.861 9.030 55.379 0.365 111.335 129.271 126.201 314.571 275.097 278.202 111.440 154.718 14.217 229.565 39.842 123.667 347.372 63.299 58.239 120.930	48.500 48.500 83.435 48.500 81.340 88.915 89.345 48.500 89.759 80.146 48.500 82.887 88.880 90.589 96.775 89.625 88.742 89.081 89.746 107.474 89.533	0.983 0.646 2.347 0.228 1.195 0.015 2.307 1.924 1.172 -1.777 -2.267 -1.437 2.178 1.057 -0.611 1.787 1.596 2.058 -0.542 2.228 -1.778 2.136	-1.069 1.300 -0.158 1.434 0.825 2.304 -0.901 -1.573 -0.858 1.751 0.202 0.207 -0.855 -2.238 -2.411 1.523 1.913 -1.371 2.420 1.121 -1.101 -1.280



EVENT		1738		10/71 17 3 -000 23.74		21.98	4.2
AZ1= DIP1= AZ2= DIP2=	29	35.000 52.000 92.500 41.374					
SLIP	VECT	OR S=	202.500	41.374	35	4.999	52.000
PRIN	AXES	S =	298.478	14.995	18	7.520	84.532
STA	DIR	QUAL	DIST	EVAZ	TOA	Х	Υ
BAR CLC GSC ISA MWC PAS PLM PYR SBC SYP RVR USC BOUQ BRWN NRTM		2 2 -2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2.221 1.552 2.053 1.571 1.118 0.309 0.296 1.628 0.355 1.282 1.338 0.915 0.388 0.131 0.215 0.226	139.938 23.772 6.504 54.410 355.871 124.316 146.952 129.311 299.244 273.134 276.199 115.837 170.450 331.938 240.006 25.955	48.950 48.950 48.950 85.517 94.498 94.642 48.950 93.988 48.950 48.950 87.772 93.625 114.853 104.185 96.937	0.943 0.590 0.166 1.191 -0.173 -1.982 -1.307 1.133 2.104 -1.463 -1.456 2.206 -0.401 0.895 1.881 -1.026	-1.121 1.340 1.455 0.852 2.394 1.353 2.009 -0.928 -1.178 0.080 0.158 -1.068 2.386 -1.680 1.086 -2.108
ENGN SWM LGOR NSGM	D D D	2 2 1 1	0.345 0.369 0.527 0.056	137.826 330.984 317.334 223.993	94.093 93.838 92.082 139.546	-1.617 1.171 1.663 0.849	1.785 -2.112 -1.805 0.879



EVENT DATA 29,1854		10/71 18 5 4.000 26.75		26.16	4.2
AZ1= 237.000 DIP1= 66.000 AZ2= 147.000 DIP2= 90.000					
SLIP VECTORS=	57.000	90.000	14	7.000	66.000
PRIN AXES =	99.417	73.286	19	4.586	73.285
STA DIR QUAL	DIST	EVAZ	TOA	. X	Υ
BAR C 2 CLC D 2 CSP C 2 CWC D 2 GLA C 1 GSC C 2 ISA D 2 MWC C 2 PAS C 2 PLM C 2 PYR C 2 SBC C 2 SYP C 2 RVR C 2 USC C 2 BRWN C -2 NRTM D 2 SWM D 2 NSGM D 2	1.531 0.905 2.010 3.313	139.605 26.456 99.328 8.257 113.815 57.037 358.412 125.649 143.733 129.337 296.498 271.714 274.256 116.926 164.207 219.540 45.390 136.517 336.029 164.756	49.400 92.078 49.400	-2.422 0.212 1.352 1.240 0.069 -1.874 -1.362 1.143 2.036 -1.477 -1.473 -2.209 -0.633 1.359 -1.550 -1.595 0.926	-1.125 1.323 0.398 1.462 -0.597 0.804 -2.497 1.344 1.856 -0.936 -1.015 0.044 0.110 1.122 2.239 1.646 -1.529 1.682 -2.083 1.372



EVENT DATA 0 02/10/71 19 6 0.0 30,1906 11.3 34.000 22.51 -118.000 18.07 3.5 A Z 1 = 286.000 DIP1= 48.000 AZZ= 106.000 DIP2= 42.000 42.000 196.000 48.000 SLIP VECTORS= 16.000 PRIN AXES = 195.941 3.011 16.000 87.000 STA DIR QUAL TCA Y DIST EVAZ X BAR C 1 2.171 140.718 49.400 0.935 -1.144 CLC 2 1.550 49.400 0.546 1.373 D 21.677 CSP 2 0.785 95.851 95.259 -2.370 0.243 D 2 GSC 1.540 52.655 49.400 1.175 0.896 D ISA D 2 1.144 353.555 49.400 -0.166 1.468 2 -1.647 MWC D 0.253 127.417 108.187 1.260 2 PAS 0.253 154.834 108.233 -0.881 1.876 D 1 PLM D 1.573 130.016 49.400 1.131 -0.950 PYR D 2 0.413 298.225 101.002 1.981 -1.064C 2 SBC 1.337 273.952 49.400 -1.474 0.102 2 276.823 SYP C 1.394 49.400 -1.467 0.176 2 0 116.187 94.338 RVR 0.858 -2.1571.061 USC D 2 0.362 178.391 103.259 -0.062 2.194 2 319.825 116.634 BOUQ D 0.179 1.198 -1.4191 0.256 BRWN D 249.906 108.050 1.950 0.714 2 -1.567 NAGM D 0.124 352.231 126.843 0.214 NRTM 2 0.227 11.404 111.030 D -C.396 -1.9622 1.697 ENGN 0.296 143.072 106.208 -1.275D 2 142.978 NSCF C 0.071 8.520 -0.166 -1.110 C NSGM 1 0.099 290.287 133.538 1.308 -0.484

146.266

112.472

-1.091

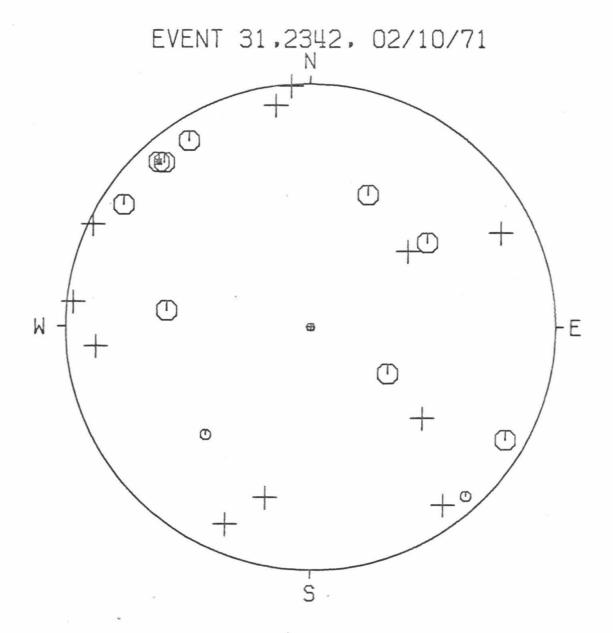
1.634

0.215

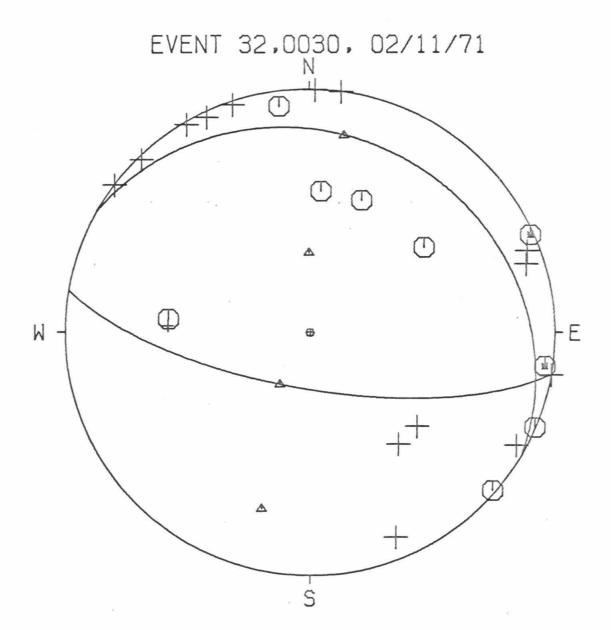
RCTR

EVENT 30,1906, 02/10/71 W - E 2 O 0 + (1) S

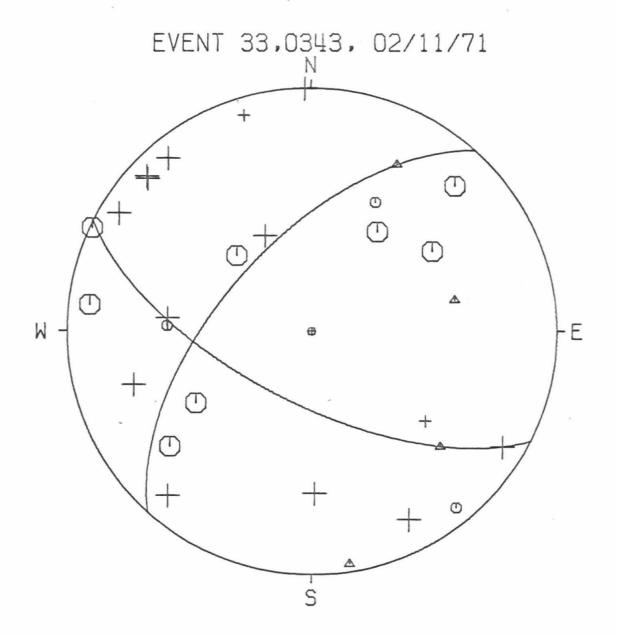
EVENT	DAT	Α					
	31	,2342	0 02/	/10/71 23	42 0.0		
			8.1 3	34.000 23.1	4 -118.000	21.41	3.5
STA	DIR	QUAL	DIST	EVAZ	TOA	X	Y
CTC	C	2	1.558	23.364	49.400	0.586	1.356
CSP	D	2 '	0.832	96.100	92.977	-2.420	0.259
GSC	C	. 2	1.570	53.957	49.400	1.195	0.869
ISA	D	2	1.129	355.552	89.261	-0.193	2.476
MWC	C	2	0.296	123.341	99.733	-1.904	1.253
PAS	C	2	0.283	147.165	99.904	-1.233	1.911
PLM	D	2	1.615	129.213	49.400	1.145	-0.934
PYR	C	2	0.367	300.052	98.790	1.992	-1.152
SYP	C	2	1.347	276.524	49.400	-1.468	0.168
RVR	D	2	0.904	115.462	92.091	-2.216	1.055
USC	D	2	0.376	171.367	98.671	-0.346	2.278
BRWN	D	2	0.217	243.528	104.259	1.943	0.967
IRON	C	2	0.040	301.188	149.887	0.786	-0.476
NAGM	D	2	0.115	14.710	118.416	-0.460	-1.751
NMLM	D	2	0.230	84.843	102.975	-2.193	-0.198
NRTM	D	2	0.232	23.108	102.810	-0.866	-2.029
NWSM	D	2	0.278	323.353	99.978	1.357	-1.824
ENGN	C	-2	0.333	137.678	99.244	-1.542	1.693
LGOR	C	1	0.539	317.390	96.593	1.592	-1.731
NSCF	C	1	0.082	43.930	128.474	-1.066	-1.107
NSGM	D	2	0.059	231.938	138.228	0.992	0.777
RCTR	C	2	0.250	138.597	100.985	-1.488	1.687



EVENT DATA 32,0030	0 02/1	11/71 0 3 4.000 24.50	0 0.0 -118.000	16.63	3.5
AZ1= 300.000 DIP1= 20.000 AZ2= 100.000 DIP2= 71.118		e.			
SLIP VECTORS=	10.000	71.118	21	0.000	20.000
PRIN AXES =	359.395	26.711	19	5.272	64.175
STA DIR QUAL	DIST	EVAZ	TOA	X	Υ
BAR D 2 CLC C 2 CSP C -2 CWC C 2 GSC C 2 ISA C 2 MWC D 2 PAS D 2 PLM D 2 PYR C 2 SBC D 1 SYP C 2 RVR D 2 USC D 2 BOUQ D 2 BRWN C -2 IRON D 2 NAGM D 2 NMLM D 2 NWSM C 2	2.184 1.512 0.769 2.033 1.504 1.113 0.261 0.276 1.580 0.416 1.355 1.410 0.855 0.395 0.170 0.285 0.105 0.095 0.166 0.192 0.306	141.682 21.458 98.184 4.531 53.224 352.488 135.980 161.483 131.402 292.979 272.593 275.401 118.755 181.417 307.298 245.966 252.314 337.365 99.920 7.536 310.958	48.650 48.650 48.650 48.650 48.650 82.988 91.743 91.594 48.650 90.147 48.650 85.640 90.370 89.874 91.500 98.175 99.707 89.918 89.666 91.276	0.903 0.533 2.398 0.115 1.166 -0.306 -1.711 -0.783 1.092 2.299 -1.455 -1.450 2.107 0.062 -1.987 2.253 2.206 0.877 2.461 0.327 1.867	-1.143 1.355 -0.345 1.452 0.872 2.322 1.770 2.337 -0.963 -0.975 0.066 0.137 -1.156 2.491 1.513 1.005 0.703 -2.104 -0.430 2.471 -1.620
ENGN D 2 NSGM D 2 RCTR D 2	0.312 0.120 0.232	149.527 249.368 154.661	91.224 95.729 92.579	-1.254 2.220 -1.046	2.132 0.836 2.208



EVENT DATA 33,0343		11/71 3 4		0 26.32	3.2
AZ1= 222.000 DIP1= 60.000 AZ2= 117.000 DIP2= 65.854					
SLIP VECTORS=	27.000	65.854	1	32.000	60.000
PRIN AXES =	77.545	49.999	1	70.649	86.313
STA DIR QUAL	DIST	EVAZ	TCA	Х	Υ
CLC C 1 GSC C 2 ISA D 2 MWC D 2 PAS D 2 PLM D 1 PYR D 2 SBC C 1 SYP D 2 RVR C 2 USC D 1 BOUQ D 2 BRWN C 2 IRON C 2 IRON C 2 SOLE C 2 NAGM C 2 NAGM C 2 NRTM D 2 NRTM D 2 NWSM D 2 ENGN D 2	1.608 1.094 0.371 0.349 1.688 0.293 1.221 1.276 0.978 0.422 0.095 0.180 0.048 0.056 0.069 0.125 0.299	26.069 56.241 358.551 121.747 140.594 128.546 301.340 272.275 275.431 115.381 162.872 358.800 224.453 135.694 213.035 58.088 50.759 96.792 40.993 332.804 133.503	49.400 49.400 89.693 98.611 98.879 49.400 99.571 49.400 91.119 97.972 123.709 107.551 144.090 139.546 133.558 116.099 99.498 101.604 104.185 98.218	0.649 1.228 -0.063 -1.960 -1.459 1.155 1.950 -1.476 -1.471 -2.237 -0.683 0.035 1.463 -0.761 0.666 -1.183 -1.449 -2.268 -1.466 0.993 -1.679	1.327 0.821 2.492 1.213 1.776 -0.921 -1.187 0.059 0.140 1.061 2.217 -1.667 1.491 0.780 1.025 -0.737 -1.184 0.270 -1.687 -1.932 1.593
LGOR C 1 NSCF D 2 NSGM D 2 RCTR D 2	0.471 0.130 0.048 0.320	320.803 73.284 154.359 133.223	97.378 115.159 144.090 99.233	1.475 -1.815 -0.472 -1.669	-1.809 -0.545 0.983 1.569



EVENT DATA 34,0407 C 02/11/71 4 7 0.0 11.3 34.000 18.39 -118.000 32.13 3.4 A Z 1 = 255.000 DIP1= 70.000 AZ2= 165.000 DIP2= 90.000 SLIP VECTORS= 75.000 90.000 165.000 70.000 PRIN AXES 113.220 76.005 211.780 76.005 = STA DIR QUAL DIST EVAZ TOA X Υ CLC D 1 1.692 26.802 49.400 0.666 1.319 ISA D 2 1.205 2.058 49.400 0.053 1.476 MWC C 2 0.404 102.146 101.366 -2.190 0.471 2 PAS C 104.153 -1.9171.023 0.342 118.095 2 C 1.227 -C.823 PLM 1.687 123.855 49.400 PYR C 2 326.974 105.490 1.167 -1.7940.312 2 C 1.151 -1.505 0.220 SBC 278.327 50.967 2 -1.450 SYP C 1.213 280.965 49.400 0.281 C 1.471 TIN 1 2.754 5.122 49.400 0.132 RVR C 2 1.012 107.715 92.370 -2.332 C. 745 C 1 103.454 -1.2541.795 USC 0.358 145.068 2 -0.707 -1.842 BOUQ 0.218 20.998 112.156 D -0.995 IRCN D 1 0.141 53.743 123.162 -1.357GOCK 2 0.099 30.079 133.538 -0.699 -1.207 D 2 NAGM 0.259 43.137 107.879 -1.423 -1.519D 2 0.387 76.966 102.162 -2.164 -0.501 NMLM D 2 0.376 39.276 102.620 -1.399 -1.711 NRTM D 2 NWSM D 0.302 356.517 105.945 0.129 -2.125 2 ENGN C 0.408 114.104 101.215 -2.048 0.916 LGCR C 2 0.523 335.398 98.593 0.960 -2.096 NSCF 0 1 56.593 109.003 -1.7140.245 -1.130

109.561

104.568

-2.038

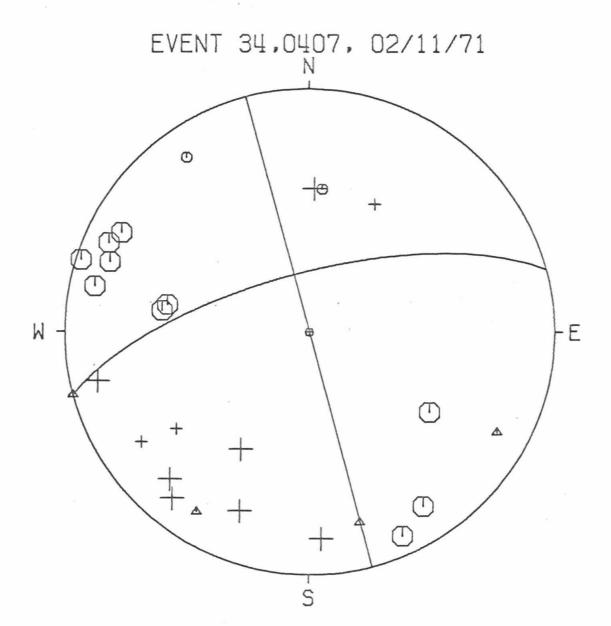
0.724

RCTR

C

2

0.333



EVENT DATA 35,0733 0.02/11/71 7 33 0.0 34.000 27.41 -118.000 26.50 12.4 3.3 A Z 1 = 132.000 DIP1= 64.000 A72= 252.000 44.288 DIP2= SLIP VECTORS= 162.000 44.288 42.000 64.000 PRIN AXES 89.481 35.300 196.146 78.685 EVAZ STA DIR QUAL DIST TOA X Υ BAR C 2 2.308 139.687 49.420 0.956 -1.1272 1.524 CLC D 26.795 49.420 0.666 1.319 CSP C 2 94.376 0.911 99.880 -2.367 0.412 GSC C -2 1.588 57.464 49.420 1.246 0.795 2 ISA D 358.621 92.183 0.059 -2.451 1.054 2 0.395 103.181 MWC D 126.399 -1.768 1.303 2 144.058 PAS D 0.382 103.819 -1.2801.766 PLM C 2 1.714 129.520 49.420 1.140 -0.940 C 2 PYR 0.273 294.788 109.581 1.851 -0.855 2 SBC D 1.218 268.185 49.420 -1.477-0.047 2 SYP 1.271 273.929 49.420 0.101 0 -1.4742 BOUQ D 0.059 0.479 150.592 -0.897 -0.008 C -2 BRWN 0.207 216.803 116.049 1.122 1.499 2 C 0.082 153.549 IRON 142.144 -0.511 1.027 2 NAGM 0.110 64.462 133.483 -1.260D -0.602 NMLM D 2 0.308 103.613 107.660 -2.028 0.491 2 48.202 114.905 -1.268NRTM D 0.216 -1.418 NWSM 2 327.915 119.294 -1.514 D 0.180 0.949 -1 0.432 137.038 101.359 -1.527ENGN 1.639 LGOR D 2 0.440 317.920 100.965 1.508 -1.670 NSCF 0 1 0.133 107.266 128.054 -1.4790.460

163.289

142.144

-0.330

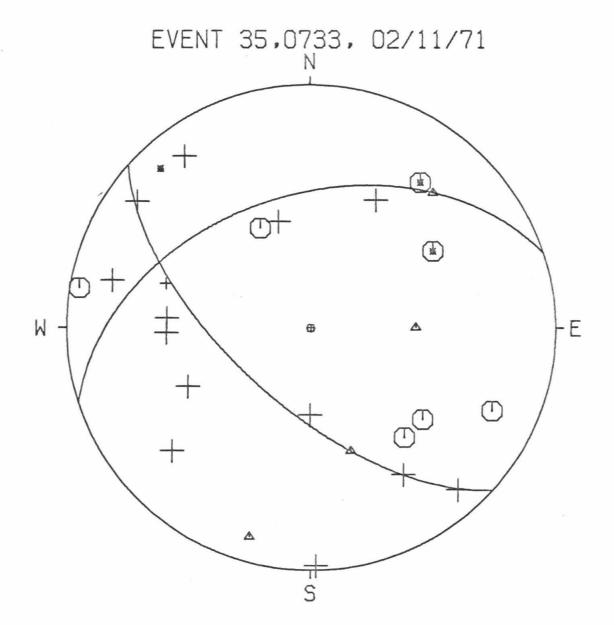
1.098

NSGM

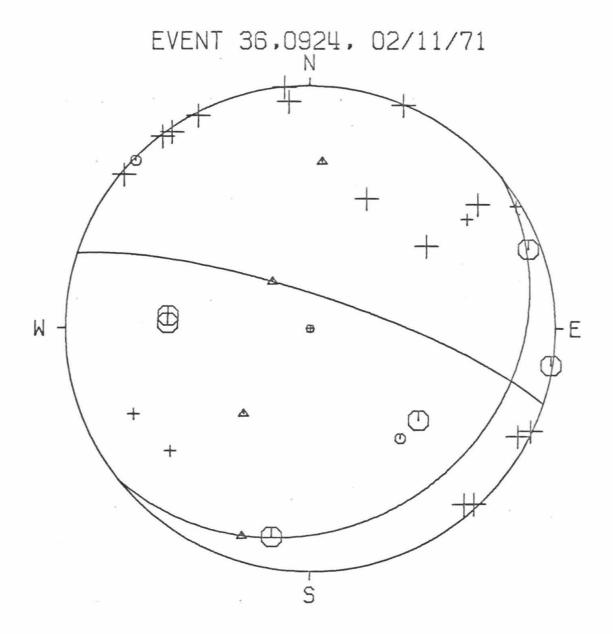
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0

0.082

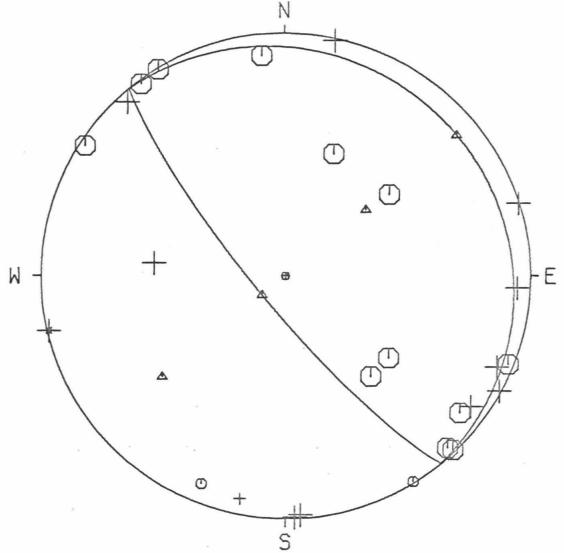


EVENT DATA 36,0924 0 02/11/71 9 24 0.0 5.0 34.000 24.91 -118.000 20.34 3.3 AZ1= 51.500 DIP1= 20.000 AZ2= 288.000 DIP2= 78.641 SLIP VECTORS= 198.000 78.641 321.499 20.000 PRIN AXES 217.811 36.513 4.291 58.319 STA DIR QUAL DIST TOA Y EVAZ X BAR C 2.221 140.723 48.650 0.922 -1.1271 CLC D 2 1.525 23.303 48.650 0.576 1.338 GSC D 2 1.541 54.531 48.65C 1.186 0.845 ISA 2 1.101 354.773 83.115 -0.214 2.336 D 2 129.772 91.315 MWC D 0.303 -1.8991.581 2 91.329 -1.138 PAS D 0.301 152.570 2.193 PLM C 2 1.623 130.355 48.650 1.110 -0.943 PYR 2 0.367 295.091 90.655 2.251 -1.054D 2 SBC C 1.304 272.173 48.650 -1.455 0.055 2 -1.450 SYP C 1.359 275.265 48.650 0.134 2 117.538 85.144 2.121 RVR D 0.903 -1.1062 174.079 90.279 -0.257 USC D 0.403 2.481 2 94.499 0.128 318.891 1.578 -1.808 BOUQ D 1 0.243 BRWN D 239.167 92.243 2.104 1.256 1 112.737 1.125 IRON D 0.059 234.938 1.603 GOOK C 2 0.120 249.799 95.729 2.226 0.819 1 D 63.836 110.849 -1.801 -0.885 INDN 0.063 2 NAGM C 10.296 103.943 -0.389 -2.143 0.082 2 NMLM C 0.217 98.739 89.428 2.459 -0.378NRTM 2 0.198 22.649 89.609 0.959 2.299 D -1.802 NWSM D 2 0.265 317.024 91.705 1.679 2 ENGN D 0.346 142.785 90.869 -1.5011.976 C 1 0.529 314.161 88.990 1.726 LGOR -1.778 NSCF 1 48.436 -1.427-1.265 D 0.056 114.734 NSGM D 2 0.077 233.336 105.649 1.714 1.276 RCTR D 2 0.264 145.175 91.713 -1.406 2.021

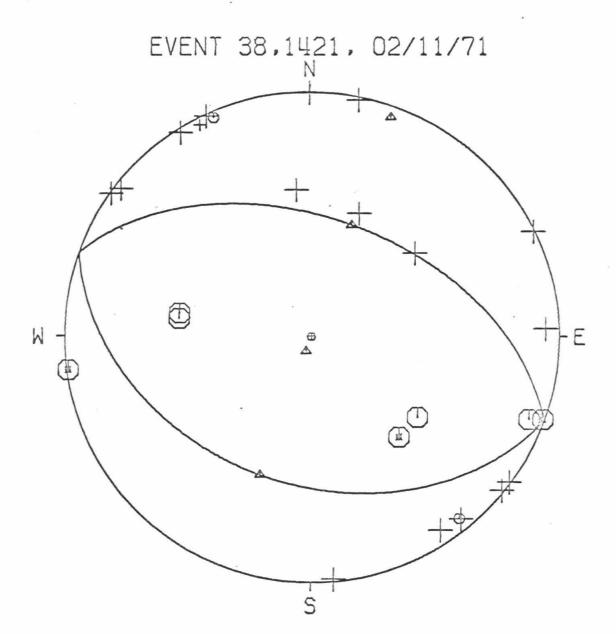


37.1132		11/71 11 3		18.83	3.5
AZ1= 140.500 DIP1= 80.000 AZ2= 320.500 DIP2= 10.000	A.				
SLIP VECTORS=	230.500	10.000	9	50.500	80.000
PRIN AXES =	50.498	35.001	23	30.499	55.000
STA DIR QUAL	DIST	EVAZ	TOA	×	Y
BAR C 2 CLC C 2 CSP D 2 GSC C 2 ISA C 2 MWC D 2 PAS C 1 PLM C 2 PYR C 2 SBC D 2 RVR D 2 USC D 2 BOUQ C 2 BRWN D -2 IRON C 2 GOOK C 2 INDN C 1 NAGM D 2 NMLM D 2	2.148 1.590 0.793 1.571 1.181 0.241 0.224 1.557 0.422 1.329 0.851 0.323 0.203 0.203 0.236 0.088 0.144 0.095 0.157 0.203	139.844 21.513 92.933 51.772 354.192 118.393 148.207 128.667 303.300 275.679 113.546 176.329 328.771 256.887 308.320 291.753 21.859 357.726 72.529	44.933 83.907 44.933 80.185 89.198 89.359 44.933 87.455 44.933 83.347 88.406 89.562 89.245 100.128 92.379 98.730 90.701 89.562	0.871 0.495 2.360 1.061 -0.230 2.184 1.310 1.055 -2.043 -1.344 2.155 0.158 -1.291 -2.419 1.781 2.273 -0.857 0.099 2.376	-1.033 1.257 -0.121 0.836 2.265 -1.180 -2.113 -0.844 1.342 0.134 -0.939 -2.460 2.130 -0.563 -1.407 -0.907 -2.137 -2.483 0.748
NRTM D 2 NWSM C 2 ENGN C 2 LGGR D 2 NSCF D 1 NSGM D 2 RCTR C 2	0.266 0.338 0.273 0.599 0.107 0.101	12.014 323.473 136.298 318.081 11.394 305.332 136.818	88.954 88.264 88.891 85.762 97.224 97.955 86.627	0.516 -1.465 1.710 -1.607 -0.462 1.893 1.660	2.423 1.978 -1.790 1.790 -2.291 -1.342 -1.769

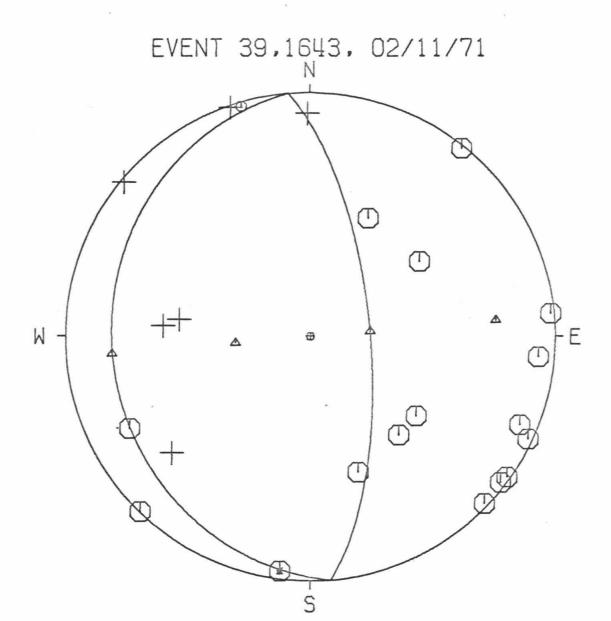




EVĖNI		A ,1421		11/71 14 2: 4.000 17.78		00 19.28	3.5
AZ1= DIP1= AZ2= DIP2=	2	10.000 40.000 90.000 50.000					
SLIP	VEC	TOR S=	200.000	50.000		20.000	40.000
PRIN	AXE	S =	199.972	5.007		20.000	85.000
STA	DIR	QUAL	DIST	EVAZ	TCA	Х	Υ
BAR CLC CSP GSC ISA MWC PAS PLM PYR SBC SYP RVR USC BOUQ BRWN IRON GOOK NAGM NMLM NRTM NWSM ENGN SWM		-2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2.121 1.629 0.798 1.601 1.220 0.232 0.196 1.537 0.441 1.328 1.389 0.841 0.284 0.235 0.226 0.114 0.158 0.198 0.221 0.308 0.367 0.250 0.473	139.012 21.194 87.972 50.776 354.622 109.757 140.668 127.355 308.206 277.666 280.050 110.859 174.560 335.097 262.057 326.199 306.284 359.986 64.452 11.542 327.890 128.948 332.832	44.933 83.852 44.933 50.439 89.285 85.122 44.933 87.273 44.933 84.933 89.253 89.343 96.305 90.662 89.609 89.385 88.555 87.987 89.106 86.973	0.886 0.488 2.361 1.047 -0.141 2.338 1.516 1.074 -1.917 -1.339 -1.330 2.199 0.234 -1.046 -2.462 1.312 2.004 -0.001 2.243 0.494 -1.305 1.929 -1.111	-1.020 1.260 0.084 0.854 1.500 -0.840 -1.850 -0.820 1.509 0.180 0.236 -0.838 -2.462 2.253 -0.343 -1.960 -1.471 2.491 1.072 2.418 2.080 -1.559 2.165
LSWM NSGM RCTR	C	1 1 2	0.442 0.120 0.168	336.543 320.770 125.855	87.264 95.440 90.360	-0.971 1.504 -2.020	2.238 -1.842 1.460



EVENT DATA 39,1643		11/71 16 4 4.000 22.70		00 27.70	3.6
AZ1= 175.000 DIP1= 20.000 AZ2= 355.000 DIP2= 70.000	8				
SLIP VECTORS=	265.000	70.000		85.000	20.000
PRIN AXES =	264.963	25.001		84.992	65.000
STA DIR QUAL	DIST	EVAZ	TCA	X	Υ
BAR C 2 CLC C 2 CSP C 2 GSC C 2 ISA D 2 MWC C 2 PAS C 2 PLM C 2 PYR D 2 SBC D 2 SYP D 2 RVR C 2 BOUQ C -2 IRON C 2 GOOK C 2 NAGM C 2 NMLM C 2 NMLM C 2 NMLM C 2 NMSM D 2 ENGN C 2		138.073 26.050 95.071 55.460 359.446 115.259 133.820 127.095 309.783 274.077 277.354 112.853 7.284 62.983 340.427 44.052 84.423 38.773 341.041 127.522	44.933 82.709 44.933 80.648 87.962 88.309 44.933 88.623 50.441 44.933 82.111 93.652 108.307 130.818 90.397 88.465 88.790 89.167 87.745	0.903 0.593 2.327 1.113 -0.022 2.220 1.777 1.078 -1.898 -1.503 -1.340 2.140 -0.307 -1.845 0.493 -1.732 2.455 1.549 -0.806 1.943	-1.005 1.214 -0.206 0.766 2.288 -1.048 -1.705 -0.815 1.580 0.107 0.173 -0.902 -2.400 -0.941 -1.386 -1.791 0.240 1.928 2.347 -1.492
SWM C 1 NSGM D 2 RCTR C 2	0.354 0.052 0.310	343.552 49.829 125.564	88.112 116.859 88.530	-0.696 -1.414 2.007	2.358 -1.194 -1.435



EVENT DATA 40,1935 02/11/71 0 19 35 0.0 6.4 34.000 24.00 -118.000 26.87 3.7 AZ1= 134.000 DIP1= 60.000 AZ2= 249.000 DIP2= 53.796 SLIP VECTORS= 159.000 53.796 44.000 60.000 PRIN AXES 98.335 39.537 192.789 86.324 DIST . STA DIR QUAL EVAZ TOA X Y BAR C 2 2.268 138.660 49.000 0.968 -1.101 2 1.577 CLC 0 26.031 49.000 0.643 1.317 C CSP 1 96.367 88.310 -0.2730.908 2.448 2 8.337 CWC D 2.057 49.000 0.213 1.451 GSC C 2 1.624 55.869 49.000 1.214 0.823 1 HFD C 2.435 105.730 49.000 1.411 -0.397 2 1.111 358.917 86.029 2.411 ISA 0 -0.046 MWC C 2 0.369 118.997 94.365 -2.102 1.165 PAS D -2 0.341 137.871 94.675 -1.6071.777 C 2 -0.901 PLM 1.683 127.919 49.000 1.157 2 PYR 0.297 95.177 -1.375D 305.205 1.948 2 1.214 0.079 SBC D 273.094 49.000 -1.464 SYP D 2 1.271 276.341 49.000 -1.457 0.162 2 C 0.978 114.266 87.526 -1.005 RVR 2.229 2 BOUQ D 0.112 2.866 118.795 -0.090 -1.798 2 BRWN D 0.163 226.646 109.211 1.489 1.406 IRON D 2 0.052 127.654 141.663 -0.919 0.709 GOOK C 2 0.040 215.386 149.647 0.536 0.755 2 NAGM D 0.144 46.509 .112.241 -1.430 -1.356 39.910 2 0.259 NRTM D 95.605 -1.524 -1.822 0 2 0.228 336.591 97.466 0.926 -2.140NWSM 2 ENGN C 0.397 130.950 94.055 1.580 -1.820SWM 0 2 0.336 340.621 94.733 0.795 -2.259 C 1 93.117 LGOR 0.480 322.858 1.468 -1.938 NSCF D 2 0.141 68.928 112.801 -1.826 -0.703

143.886

144.090

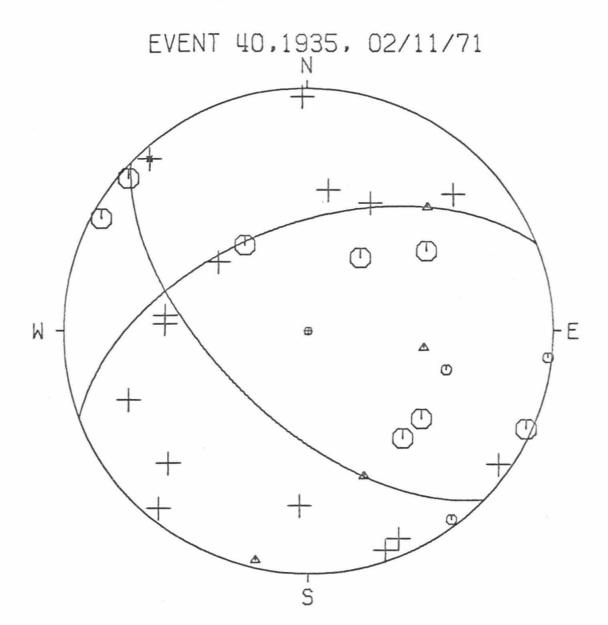
-0.642

0.880

C

NSGM

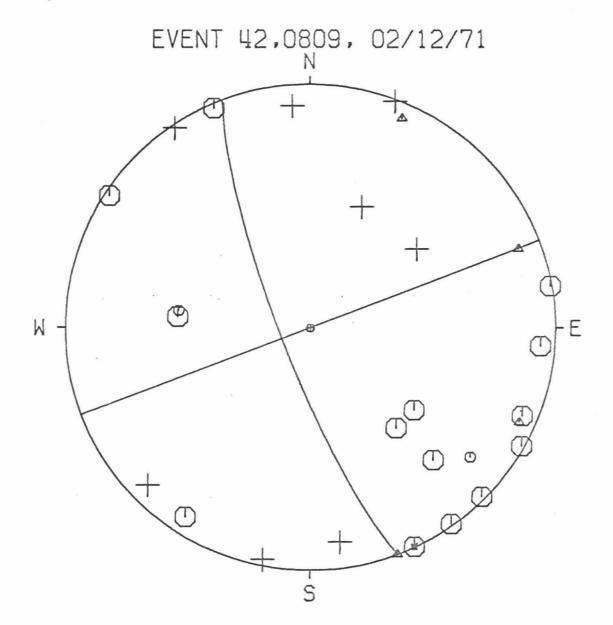
2



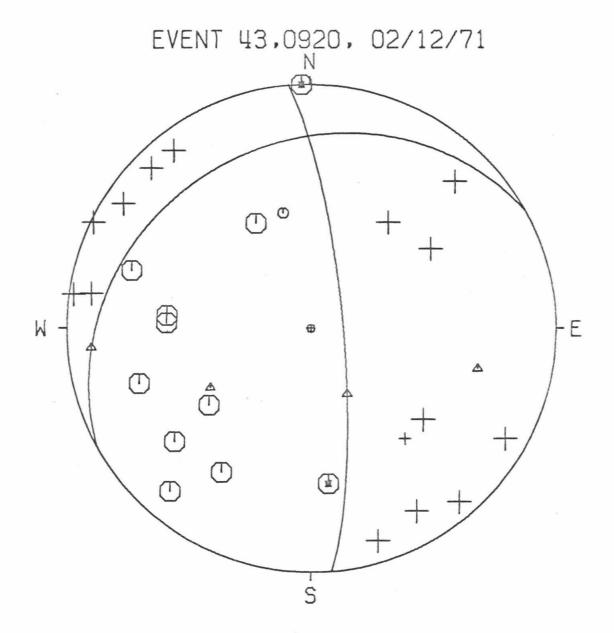
EVENT DAT			11/71 23 3 4.000 21.11		20.21	3.7
AZ1= DIP1= AZ2= DIP2=	32.000					
SLIP VEC	TORS=	162.000	61.580	31	1.999	32.000
PRIN AXE	S =	194.210	20.579	33	10.802	74.745
STA DIR	QUAL	DIST	EVAZ	TOA	X	Υ
BAR C CLC D CSP D CWC D GSC D. ISA D MWC D PAS D PLM G PYR D SBC C SYP C BOUQ D BRWN D IRON D GOOK D NAGM D NMLM D NRTM D	-2 2 2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2.172 1.583 0.813 2.094 1.5.77 1.164 0.266 0.246 1.581 0.399 1.368 0.180 0.222 0.069 0.124 0.144	139.704 22.341 94.244 5.722 52.615 354.949 119.876 146.205 128.657 303.055 275.091 277.897	48.550 48.550 85.130 48.550	0.940 0.553 2.385 0.145 1.155 -0.201 -2.156 -1.379 1.135 -2.082 -1.448 -1.440 -1.192 2.339 1.520 2.214 -0.218	-1.109 1.344 -0.177 1.446 0.883 2.272 1.239 2.060 -0.908 1.355 0.129 0.200 2.192 0.784 -1.401 -0.884 -2.446 0.494
NWSM D ENGN D SWM D LSWM D NSCF C NSGM C	2 2 1 1 2 2	0.315 0.297 0.418 0.387 0.101	324.611 135.637 330.956 335.018 23.399 304.335	90.110 90.290 89.075 89.391 98.770	1.446 -1.744 -1.204 -1.050 -0.914	2.254 -2.112

EVENT 41,2335, 02/11/71 + E W 0 S

PRIN AXES = 23.561 82.947 114.439 82. STA DIR QUAL DIST EVAZ TOA X BAR C 2 2.187 139.528 44.933 0.877 -1. CLC 0 2 1.582 22.928 44.933 0.526 1. CSP C 2 0.828 94.423 83.569 2.349 -0. GSC D 2 1.584 53.149 44.933 1.081 0. ISA D 2 1.155 355.566 80.429 -0.176 2. MWC C 2 0.282 119.390 88.803 2.155 -1. PAS C 2 0.261 144.425 89.003 1.442 -2. PLM C 2 1.597 128.527 44.933 1.057 -0. PYR C 2 0.383 303.412 87.837 -2.047 1. SBC C 2 1.294 274.885 44.933 -1.346 0. SYP C 1 1.352 277.696 44.933 -1.339 0. BOUQ C -2 0.167 334.659 90.397 1.066 -2. IRON C 2 0.052 317.129 116.859 1.259 -1. GOOK C 2 0.108 292.698 96.988 2.162 -0. SOLE D 2 0.082 352.074 101.888 0.307 -2. INDN D 2 0.097 45.490 98.467 -1.646 -1. NAGM D 2 0.140 11.351 92.914 -0.479 -2.	EVENT DA			12/71 8 4.000 21.58		00 21.28	3.2
PRIN AXES = 23.561 82.947 114.439 82. STA DIR QUAL DIST EVAZ TOA X BAR C 2 2.187 139.528 44.933 0.877 -1. CLC 0 2 1.582 22.928 44.933 0.526 1. CSP C 2 0.828 94.423 83.569 2.349 -0. GSC D 2 1.584 53.149 44.933 1.081 0. ISA D 2 1.155 355.566 80.429 -0.176 2. MWC C 2 0.282 119.390 88.803 2.155 -1. PAS C 2 0.261 144.425 89.003 1.442 -2. PLM C 2 1.597 128.527 44.933 1.057 -0. PYR C 2 0.383 303.412 87.837 -2.047 1. SBC C 2 1.294 274.885 44.933 -1.346 0. SYP C 1 1.352 277.696 44.933 -1.339 0. BOUQ C -2 0.167 334.659 90.397 1.066 -2. IRON C 2 0.052 317.129 116.859 1.259 -1. GOOK C 2 0.108 292.698 96.988 2.162 -0. SOLE D 2 0.082 352.074 101.888 0.307 -2. INDN D 2 0.097 45.490 98.467 -1.646 -1. NAGM D 2 0.140 11.351 92.914 -0.479 -2.	DIP1= AZ2=	80.000					
STA DIR QUAL DIST EVAZ TOA X BAR C 2 2.187 139.528 44.933 0.877 -1. CLC 0 2 1.582 22.928 44.933 0.526 1. 0.877 -1. CSP C 2 0.828 94.423 83.569 2.349 -0. 0.828 94.423 83.569 2.349 -0. 0.850 0 2 1.584 53.149 44.933 1.081 0. 0.851 0. 0.854 0.429 -0.176 2. 0.854 0.429 -0.176 2. 0.856 0.429 2.047 1. 0.856 0.429 2.047 1. 0.856 0.429 2.047 1. 0.856 0.429 2.047 1. 0.856 0.429 2.047 1. 0.856 0.429 2.	SLIP VE	ECTORS=	338.999	90.000		69.000	80.000
BAR C 2 2.187 139.528 44.933 0.877 -1. CLC 0 2 1.582 22.928 44.933 0.526 1. CSP C 2 0.828 94.423 83.569 2.349 -0. GSC D 2 1.584 53.149 44.933 1.081 0. ISA D 2 1.155 355.566 80.429 -0.176 2. MWC C 2 0.282 119.390 88.803 2.155 -1. PAS C 2 0.261 144.425 89.003 1.442 -2. PLM C 2 1.597 128.527 44.933 1.057 -0. PYR C 2 0.383 303.412 87.837 -2.047 1. SBC C 2 1.294 274.885 44.933 -1.346 0. SYP C 1 1.352 277.696 44.933 -1.339 0. BOUQ C -2 0.167 334.659 90.397 1.066 -2. IRON C 2 0.052 317.129 116.859 1.259 -1. GOOK C 2 0.108 292.698 96.988 2.162 -0. SOLE D 2 0.082 352.074 101.888 0.307 -2. INDN D 2 0.097 45.490 98.467 -1.646 -1. NAGM D 2 0.140 11.351 92.914 -0.479 -2.	PRIN A	XES =	23.561	82.947	1	114.439	82.947
CLC 0 2 1.582 22.928 44.933 0.526 1. CSP C 2 0.828 94.423 83.569 2.349 -0. GSC 0 2 1.584 53.149 44.933 1.081 0. ISA 0 2 1.155 355.566 80.429 -0.176 2. MWC C 2 0.282 119.390 88.803 2.1551. PAS C 2 0.261 144.425 89.003 1.442 -2. PLM C 2 1.597 128.527 44.933 1.057 -0. PYR C 2 0.383 303.412 87.837 -2.047 1. SBC C 2 1.294 274.885 44.933 -1.346 0. SYP C 1 1.352 277.696 44.933 -1.339 0. BOUQ C -2 0.167 334.659 90.397 1.066 -2. IRON C 2 0.052 317.129 116.859 1.259 -1. GOOK C 2 0.108 292.698 96.988 2.162 -0. SOLE D 2 0.082 352.074 101.888 0.307 -2. INDN D 2 0.097 45.490 98.467 -1.646 -1. NAGM D 2 0.140 11.351 92.914 -0.479 -2.	STA D	IR QUAL	DIST	EVAZ ,	TOA	Х	Y
NRTM D 2 0.254 20.530 89.069 0.870 2. NWSM D 2 0.300 326.064 88.629 -1.379 2. ENGN C 2 0.313 134.708 88.506 1.753 -1. LSWM C 2 0.374 336.579 87.922 -0.976 2.	CLC CSP CSP CSP CSP CSP CSP CSP CSP CSP CS	0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1.582 0.828 1.584 1.155 0.282 0.261 1.597 0.383 1.294 1.352 0.167 0.052 0.108 0.082 0.097 0.140 0.231 0.254 0.300 0.313 0.374	22.928 94.423 53.149 355.566 119.390 144.425 128.527 303.412 274.885 277.696 334.659 317.129 292.698 352.074 45.490 11.351 79.946 20.530 326.064 134.708 336.579	44.933 83.569 44.933 80.429 88.803 89.003 44.933 87.837 44.933 90.397 116.859 96.988 101.888 98.467 92.914 89.293 89.069 88.629 88.506 87.922	0.526 2.349 1.081 -0.176 2.155. 1.442 1.057 -2.047 -1.346 -1.339 1.066 1.259 2.162 0.307 -1.646 -0.479 2.446 0.870 -1.379 1.753 -0.976	-1.028 1.244 -0.182 0.810 2.276 -1.214 -2.016 -0.842 1.350 0.115 0.181 -2.252 -1.357 -0.904 -2.206 -1.618 -2.388 0.434 2.322 2.049 -1.736 2.252 -1.948



EVENT DATA 02/12/71 43,0920 0 9 20 0.0 8.1 34.000 25.56 -118.000 25.73 AZI= 241.000 DIP1= 25.000 A Z Z = 355.000 DIP2= 79.260 SLIP VECTORS= 265.000 79.260 151.000 25.000 PRIN AXES 239.529 39.411 103.495 59.397 STA DIR QUAL DIST TOA EVAZ Х Y BAR D 1 2.277 139.399 49.400 0.961 -1.122CSP 2 0.896 D 92.185 -2.427 0.350 98.216 GSC 2 56.332 D 1.596 49.400 1.230 0.819 C -2 ISA 1.086 358.164 89.844 -0.080 2.495 2 MWC D 0.369 123.700 98.762 -1.915 1.277 2 PAS D 0.351 142.589 99.000 -1.3951.824 2 -0.929 128.958 49.400 1.149 PLM D 1.687 PYR 2 0.297 299.544 D 99.724 1.983 -1.124 SBC C 2 1.229 272.276 49.400 -1.476 0.059 C 2 SYP 1.284 275.184 49.400 -1.471 0.133 2 RVR D 0.975 116.071 91.212 -2.222 1.087 -1.590 C -2 BOUQ 0.088 353.439 126.172 0.183 BRWN D 2 0.192 224.469 106.692 1.479 1.506 C 2 0.056 IRON 152.643 139.844 -0.558 1.078 2 GOOK D 0.066 216.078 135.260 0.792 1.088 2 SOLE C 0.063 53.123 136.707 -1.043 -0.783 INDN C 2 0.137 107.919 113.976 -1.833 0.593 2 NAGM C 0.115 50.320 118.416 -1.393 -1.156 2 NMLM D 0.292 99.013 99.786 -2.250 0.357 102.975 C 2 NRTM 0.230 40.832 -1.439 -1.666 NWSM D 2 0.212 329.921 104.705 1.082 -1.8692 ENGN D 0.403 135.302 98.303 -1.627 1.644 LGCR D 2 0.470 319.476 97.440 1.516 -1.7732 99.804 LSWM D 0.291 342.490 0.685 -2.172NSCF C 2 0.122 72.203 117.062 -1.757-0.564 NSHC C 2 31.759 -1.4710.103 121.412 -0.911 C 1 NSGM 0.056 166.740 139.844 -0.278



EVENT DATA 44,0952 0 02/12/71 9 52 0.0 3.0 34.000 21.55 -118.000 27.18 3.4 354.000 AZ1= DIP1= 80.000 AZ2= 90.000 DIP2= 59.340 SLIP VECTORS= 359.999 59.340 264.000 80.000 45.479 76.243 PRIN AXES 307.711 61.094 STA DIR QUAL Υ DIST X EVAZ TOA 2 0.906 -1.002 BAR C 2.240 137.888 44.933 2 CLC C 1.615 25.530 44.933 0.582 1.219 2 CSP C 0.909 93.998 82.791 2.332 -0.1632 0.779 GSC C 1.104 1.650 54.791 44.933 ISA 0 -2 1.152 359.138 80.464 -0.034 2.283 2 MWC D 0.355 112.889 2.265 -0.956 88.102 -2 1.826 -1.659 PAS D 0.315 132.261 88.482 2 PLM 1.083 -0.808 C 1.662 126.719 44.933 2 PYR D 0.317 311.308 -1.8531.628 88.465 2 SBC D 1.213 275.068 50.440 -1.5010.133 2 SYP D 1.272 278.131 -1.338 0.191 44.933 C 2 2.157 RVR 0.966 111.927 82.248 -C.868 2 BOUQ C 0.151 3.744 91.521 -0.161 -2.461 BRWN D 1 0.134 238.471 93.652 2.062 1.265 2 -1.322IRON C 0.059 50.336 108.307 -1.594 2 0.720 -1.547 GOOK D 0.044 335.044 122.304 2 C -1.536 -1.762SOLE 0.107 41.080 97.224 2 -1.041 C 65.304 90.434 -2.263 INDN 0.166 2 C 38.485 90.145 -1.554 -1.954 NAGM 0.175 2 C 0.311 82.795 88.524 0.309 NMLM 2.448 2 C 35.550 2.011 NRTM 0.293 88.698 1.437 NWSM D 2 0.264 340.890 88.975 -0.811 2.341 -2 ENGN -1.437 D 0.375 125.846 87.912 1.989 2 -1.3572.010 LGOR D 0.511 325.977 86.611 LSWM D 1 0.349 348.849 88.155 -0.476 2.413

38.817

116.859

-1.160

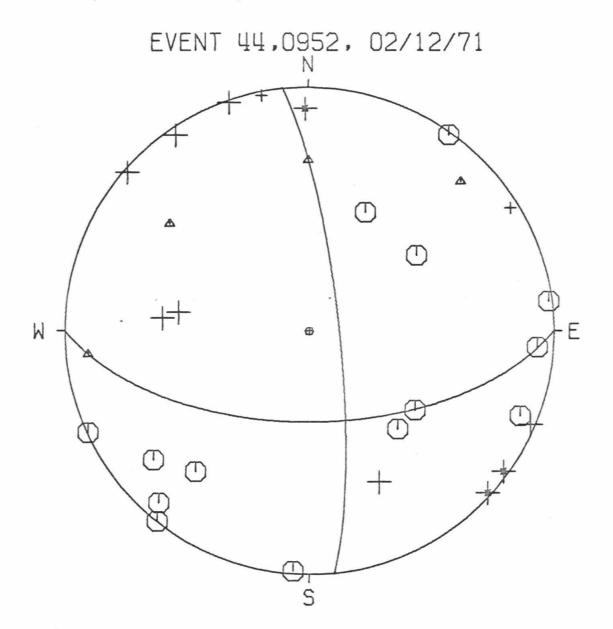
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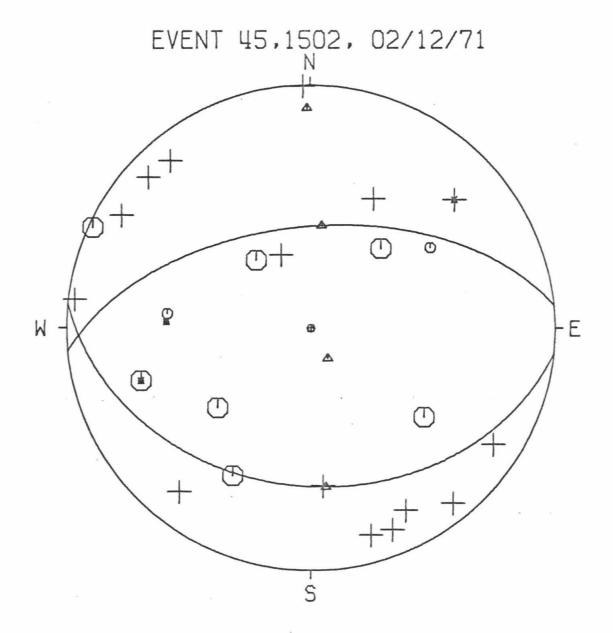
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NSGM



EVENT DATA 45,1502 0 02/12/71 15 2 0.0 9.5 34.000 24.41 -118.000 25.86 3.4 AZI= 96.000 35.000 DIP1= AZZ= 264.500 DIP2= 55.544 SLIP VECTORS= 174.500 55.544 6.000 35.000 359.214 PRIN AXES 150.968 11.684 79.679 TCA X Υ STA DIR QUAL DIST EVAZ CLC D 2 1.564 25.692 49.400 0.641 1.331 2 92.922 -2.417 0.298 CSP 0 0.895 97.030 GSC C 1 1.608 55.804 49.400 1.222 0.830 2.489 2 1.105 358.274 89.559 -0.075 ISA D 2 0.360 121.042 100.825 -1.930 1.162 MWC D 0 2 101.463 -1.429 1.722 PAS 0.337 140.316 2 1.676 C 128.408 49.400 1.158 -0.918 PLM 2 PYR D 0.305 302.675 102.337 1.866 -1.197-1 1.228 0.069 SBC 272.691 49.400 -1.476SYP C 1 1.284 275.945 49.400 -1.4690.153 2 92.010 -2.226 RVR C 0.968 115.002 1.038 2 BOUQ 0.107 355.530 125.057 0.127 -1.626 D -2 BRWN D 0.178 228.115 111.853 1.475 1.322 2 IRON C 0.044 141.528 150.592 -0.558 0.703 GOOK C 2 0.056 221.165 144.011 0.719 0.822 SOLE 2 49.165 C 0.069 138.350 -0.951-0.822 -2 INDN C 0.138 72.704 118.086 -1.736 -0.541 2 NRTM D 0.245 38.429 104.797 -1.341-1.690 2 NWSM D 0.227 332.621 106.640 0.971 -1.87599.995 ENGN D 2 0.391 133.101 -1.6591.553 SWM D 2 0.336 338.057 101.494 0.836 -2.075 2 321.107 98.069 1.455 -1.804 LGOR D 0.484 2 LSWM D 0.308 343.869 102.233 0.617 -2.1322 NSHC C 27.686 121.818 -0.799 -1.522 0.120 NSGM D 2 0.040 158.280 153.250 -0.303 0.760



EVENT DATA 02/12/71 16 22 46, 1622 0 34.000 24.77 -118.000 25.50 AZ1= 108.000 DIP1= 50.000 AZZ= 288.000 DIP2= 40.000 SLIP VECTORS= 198.000 40.000 18.000 50.000 17.975 5.007 197.999 85.000 PRIN AXES STA DIR QUAL DIST TOA X Y EVAZ 139.245 49.400 0.964 -1.119 2 2.265 BAR C 2 1.557 49.400 0.639 1.332 CLC D 25.628 2 0.202 C 2.042 7.878 49.400 1.463 CWC GSC C 2 1.601 55.883 49.4CO 1.223 C.829 HFD 2 49.400 1.419 -0.411 C 2.420 106.166 2 0.085 -2.494 ISA 0 1.099 358.038 90.227 2 100.447 -1.9151.203 MWC D 0.359 122.134 2 0.339 -1.3971.765 PAS D 141.643 100.934 2 128.674 49.400 1.153 -0.923 PLM C 1.676 2 PYR 0.305 301.104 101.739 1.910 -1.153D 2 SBC C 1.233 272.467 49.400 -1.4760.064 2 SYP C 1.288 275.625 49.400 -1.470 0.145 RVR C . 2 0.966 115.442 91.882 -2.220 1.056 2 0.214 BUUD D 0.099 352.292 126.426 -1.579 2 D 228.187 110.361 1.505 1.346 BRWN 0.185 2 IRON C 0.040 145.255 152.529 -0.478 0.690 2 224.776 141.511 0.821 0.827 GOOK C 0.059 2 C 48.538 140.070 -0.905 -0.799 SOLE 0.063 2 C 73.510 118.329 -1.738-0.514 INDN 0.133 2 38.300 -1.692 NRTM D 0.237 104.857 -1.336 2 0.225 330.839 106.179 1.035 -1.854 NWSM 0 2 ENGN 0.392 134.235 99.655 -1.634 1.591 D 1 0.332 SWM C 336.844 101.102 0.883 -2.065 2 193.926 0.547 PACP C 0.379 99.949 2.207 NSCF 2 0.120 69.826 120.869 -1.637-0.602

167.372

149.819

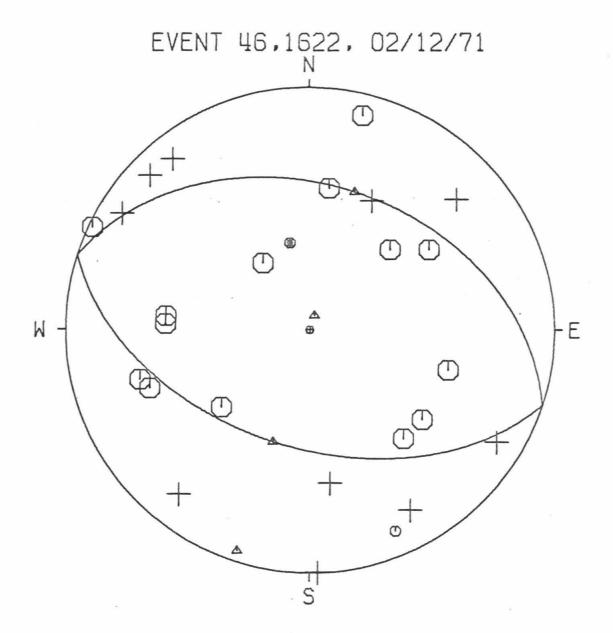
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0.898

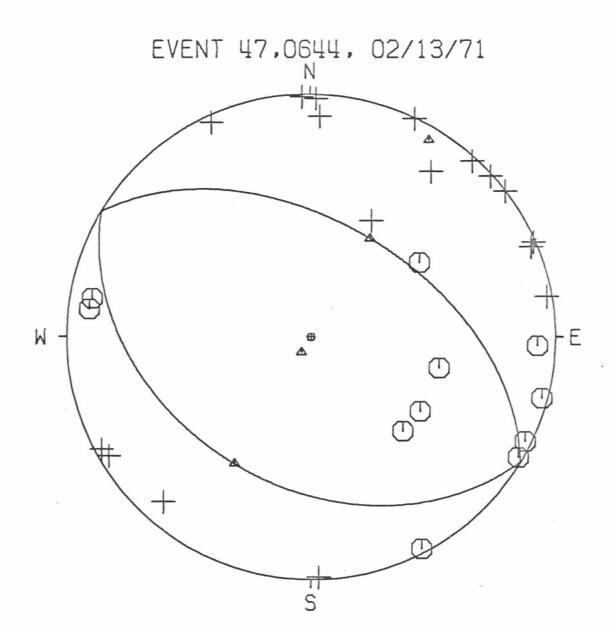
NSGM

C

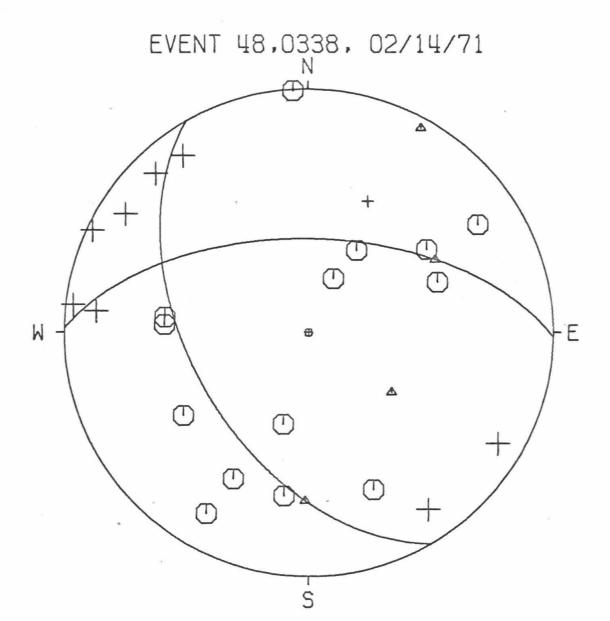
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EVENT DATA 47,0644		13/71 6 4 4.000 19.64		0 32.80	3.2
AZ1= 301.000 DIP1= 51.000 AZ2= 121.000 DIP2= 39.000	*:				
SLIP VECTORS=	31.000	39.000	2	211.000	51.000
PRIN AXES =	210.968	6.005		30.999	84.000
STA DIR QUAL	DIST	EVAZ	TCA	X	Υ
BAR C 2 CLC D 2 CSP C 2 GSC C 2 HFD C 2 ISA D 2 MWC C 2 PAS C 2 PLM C 2 SBC C 2 SYP C 2 BOUQ D 2 BRWN D 2 IRON D 2	0.985 1.732 2.496 1.184 0.419 0.360 1.706 1.139 1.200 0.203 0.063 0.140 0.088 0.185 0.248 0.250 0.392 0.367 0.280	27.396 92.200 55.354 103.572 2.486 104.900 120.217 124.254	44.933 82.062 44.933 44.933 80.149 87.491	0.622 2.319 1.112 1.313 0.099 2.362 2.123 1.117 -2.268 -2.238 1.071 1.238 -2.144 -1.508 1.994 2.280 1.845 2.414 1.656 -0.081	-1.156 -1.696 1.501 0.978 1.658
LSWM D 2 LMER D 2 NSGM D 2	0.374 0.452 0.128	1.468 67.659 59.324	87.917 87.168 94.423	0.063 2.254 -2.066	2.453 0.927 -1.225



EVENT DATA 48,0338	0 02/1	14/71 3 3 4.000 23.86	38 0.0 5 -118.00	00 23.03	3.3
AZ1= 150.000 DIP1= 50.000 AZ2= 271.000 DIP2= 58.458					
SLIP VECTORS=	181.000	58.458		60.000	50.000
PRIN AXES =	125.881	34.471		28.773	85.146
STA DIR QUAL	DIST	EVAZ -	TOA	X	Υ
CLC D 1 CSP D 2 GSC C 2 ISA C 2 MWC D 2 PAS D 2 PYR D 2 RVR D 2 SBC C 2 SYP C 2 BOUQ C 2 BRWN C 2 IRON C 2 IRON C 2 GOOK C 2 SOLE C 2 NAGM C 2 NMLM D 2 NRTM C 2	0.114 0.253 0.232 0.256 0.357	96.803 54.755 356.518 123.120 144.874 300.473 115.510 273.284 276.185 337.493 237.427 204.323 248.470 15.349 26.997 95.864 29.251 325.862 136.370	93.367 49.400 89.427 101.687 102.109 101.150 92.451 49.400 49.400 120.842 160.213 132.757 147.915 123.038 103.797 105.948 103.547 100.771	1.207 -0.151 -1.870 -1.279 1.935 -2.208 -1.475 -1.469 0.668 1.733 0.250 1.318 -0.259 -0.765 -2.170 -1.040 1.228 -1.555	1.347 0.287 0.853 2.483 1.220 1.818 -1.139 1.053 0.085 0.159 -1.612 1.107 0.554 0.520 -0.942 -1.502 0.223 -1.858 -1.811 1.632
NSCF C 2 NSHC C 2 NSGM C 2	0.095 0.115 0.048	56.265 8.436 210.238	128.395 122.635 147.915	-1.280 -0.249 0.492	-0.855 -1.679 0.844



EVENT DATA 49,1344 C 02/14/71 13 44 0.0 34.000 17.97 -118.000 30.67 3.0 AZ1= 202.000 DIP1= 62.000 AZZ= 292.000 DIP2= 90.000 202.000 90.000 112.000 62.000 SLIP VECTORS= 63.441 PRIN AXES 160.557 70.612 70.612 STA DIR QUAL DIST EVAZ TCA Х Y 44.933 0.940 -0.970 BAR 2 2.230 135.913 0 2 C 1.690 44.933 0.594 1.213 CLC 26.101 2 CSP 0.956 87.907 82.344 2.326 0.085 C CWC C 2 2.164 9.289 44.933 0.218 1.333 2 C 1.724 54.056 44.933 1.094 0.793 GSC 2.461 HFD C 1 103.130 44.933 1.316 -0.307 C 2 1.202 50.440 0.032 1.506 ISA 1.211 2 MWC C 0.385 102.668 87.818 2.392 -0.538 2 PAS D 0.321 118.628 88.429 2.164 -1.181 2 PLM D 1.667 124.063 44.933 1.119 -0.757 2.013 PYR D 2 0.330 324.784 88.343 -1.421 SBC C 2 1.172 278.687 80.268 -2.253 0.344 2 SYP C 1.234 281.123 50.436 -1.478 0.291 0.656 -2 0.219 15.300 89.402 2.399 BOUG D C 1 0.077 239.750 103.149 1.898 BRWN 1.107 IRON C -2 0.131 45.636 94.033 -1.723-1.685 2 0.099 17.330 98.208 -0.689 -2.210 GOOK D -2 SOLE C 0.182 40.357 89.903 1.618 1.903 C NAGM 2 0.251 38.656 89.099 1.549 1.937 NMLM C 2 0.370 74.763 87.962 2.369 0.645 36.130 NRTM C 2 0.370 87.957 1.448 1.983 2 0.311 352.905 NWSM D 88.524 -0.305 2.449 -2 D 0.387 114.569 87.793 2.229 -1.019FNGN 2 PACP D 0.257 184.411 89.040 -0.191-2.4722 0.329 154.810 88.349 -2.229 INGL D 1.049 2 D 0.538 333.781 86.346 -1.0692.170 LGOR D 2 357.208 87.641 -0.119 LSWM 0.403 2.445 LMER C 2 0.438 62.709 87.307 2.169 1.119 C 2 0.244 89.167 1.243 NSHC 30.043 2.148

40.930

95.026

-1.564

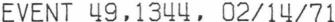
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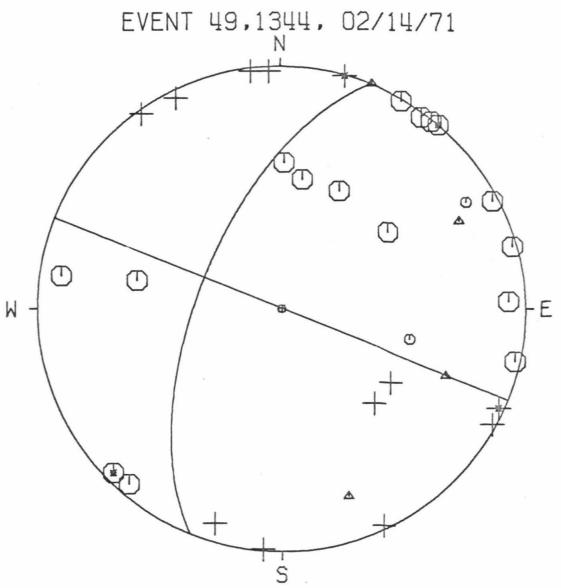
NSGM

C

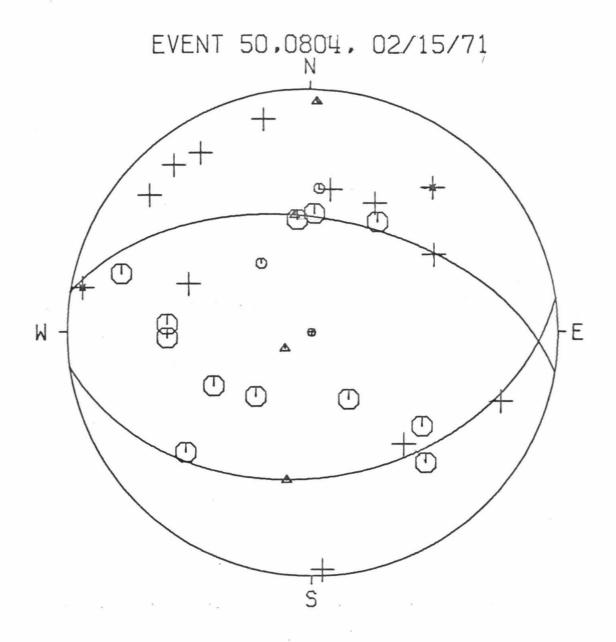
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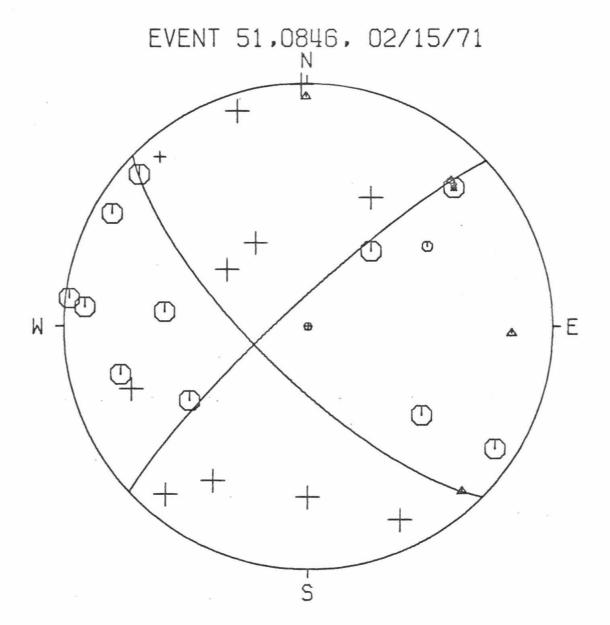




EVENT DATA 50,0804 0 02/15/71 8 0.0 34.000 28.27 -118.000 24.63 3.9 12.9 AZ1= 82.000 DIP1= 40.000 AZ2= 279.500 DIP2= 51.331 SLIP VECTORS= 189.500 51.331 351.999 40.000 PRIN AXES 238.521 10.429 1.604 84.269 Υ STA DIR QUAL DIST. EVAZ TCA Χ 2 140.424 49.445 BAR D 2.302 0.942 -1.140 2 CLC D 1.499 26.180 49.445 0.652 1.327 101.061 CSP D -2 0.888 95.139 -2.341 C. 458 CWC 2 1.982 7.773 49.445 0.200 1.465 D 2 GSC 1.559 57.411 49.445 1.246 D 0.796 2 357.362 92.985 ISA D 1.041 0.112 -2.431 MWC D 2 0.384 130.472 104.477 -1.647 1.405 2 PAS D 0.379 148.488 104.686 -1.129 1.841 C 2 1.704 -0.960 PLM 130.461 49.445 1.125 2 PYR D 0.291 290.305 109.416 1.916 -0.709 2 SBC C 1.245 267.730 49.445 -1.477-C. C59 C 2 SYP 1.296 273.247 49.445 -1.476 0.084 1 C 2.583 49.445 TIN 3.236 0.083 1.476 USC 0 2 0.468 167.542 101.382 2.187 -0.483 2 BOUQ C 0.052 331.131 154.604 0.375 -0.681 BRWN -2 0.234 219.714 113.642 D 1.236 1.488 2 141.569 IRON C 0.086 172.986 -0.142 1.155 C 2 GOOK 0.105 210.941 136.178 0.678 1.132 SCLE C · 1 0.059 144.020 151.499 -0.511 C. 704 C 2 NAGM 0.084 61.290 142.317 -0.548 -1.001 2 -1.944 NMLM C 0.286 107.136 109.735 0.599 C 2 NRTM 0.187 46.395 119.590 -1.288 -1.227NWSM C 2 0.185 318.830 119.858 -1.3341.166 ENGN 0 2 0.426 140.880 102.576 -1.3951.715 2 NSCF 111.321 D 0.108 135.104 -1.258 0.491 NSHC C 2 0.059 41.009 151.499 -0.571 -0.657 2 NSGM C 0.093 181.451 139.653 0.031 1.219



EVENT DA	ATA 51,0846		15/71 8 4 4.000 24.42		0 26.48	3.4
	134.500 73.000 227.000 81.880					
SLIP VE	CTORS=	137.000	81.880		44.500	73.000
PRIN AX	(ES =	91.805	72.145	3	59.801	83.866
STA DI	R QUAL	DIST	FVAZ	TCA	Х	Υ
GSP CGSC GSC GSC GSC GSC GSC GSC GSC GSC GS	2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1.568 0.904 1.615 1.104 0.367 0.342 1.683 0.297 1.275 0.413 0.105 0.171 0.044 0.044	25.969 96.849 55.976 358.665 120.256 139.163 128.224 303.365 275.948 162.147 0.123 226.368 125.392 219.756	49.375 91.810 49.375 89.349 98.384 98.695 49.375 99.251 49.375 97.824 120.441 108.416 146.728 146.728	0.647 -2.443 1.224 -0.058 -1.996 -1.506 1.160 1.913 -1.469 -0.712 -0.004 1.497 -0.825 0.647	1.328 0.293 0.826 2.485 1.164 1.743 -0.914 -1.260 0.153 2.212 -1.756 1.427 0.586 0.778
SOLE (INDN (2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0.071 0.145 0.300 0.249 0.224	57.842 75.519 95.105 40.080 334.599	132.226 111.965 99.211 100.538 102.970	-1.212 -1.915 -2.282 -1.455 0.944	-0.762 -0.495 0.204 -1.729 -1.989
	2 2	0.398 0.134 0.124	132.282 70.472 31.439	98.014 114.251 116.420	-1.716 -1.809 -0.971	1.560 -0.641 -1.589



EVENT DATA 52,1303 0 02/15/71 13 3 0.0 34.000 25.65 -118.000 26.12 9.7 AZ1= 86.500 DIP1 = 46.000 AZ2= 246.500 DIP2= 45.782 SLIP VECTORS= 156.500 45.782 356.499 46.000 PRIN AXES 75.826 10.159 166.518 89.889 STA DIR QUAL DIST EVAZ TCA X Υ CLC 1.547 49.400 D 1 26.140 0.651 1.326 CSP D -2 0.901 98.218 -2.410 0.348 92.949 GSC C 2 1.599 56.498 49.400 1.232 0.815 ISA D 2 1.084 358.411 90.664 0.069 -2.485 2 MWC 0 0.374 123.299 100.717 -1.8851.238 2 PAS 0.354 141.900 101.278 -1.384 1.764 D PLM C 2 1.692 128.874 49.400 1.150 -0.927 2 299.369 103.145 -1.078 PYR 0.290 1.915 D 1.224 SBC 1 271.740 . 49.400 -1.4770.045 D 1.278 275.053 49.400 SYP C 1 -1.4720.130 BOUQ D 2 0.084 356.763 132.905 0.080 -1.410 2 BRWN C 0.188 223.412 111.368 1.370 1.448 2 -0.5970.894 IRON C 0.056 146.245 144.606 C 2 214.085 143.003 0.629 0.929 GOOK 0.059 C 2 62.355 141.599 -1.030 -0.540 SOLE 0.063 2 C 0.138 101.318 118.715 -1.767 0.354 INDN 2 122.799 NAGM C 0.119 52.485 -1.342-1.0312 0.297 102.932 -2.176 0.339 NMLM D 98.849 NWSM D 2 0.207 330.736 109.349 0.999 -1.7832 134.701 99.758 -1.619 1.603 ENGN 0.407 D 0.125 76.165 121.466 -1.678 -0.413 NSCF C 1

35.351

-0.914

-1.289

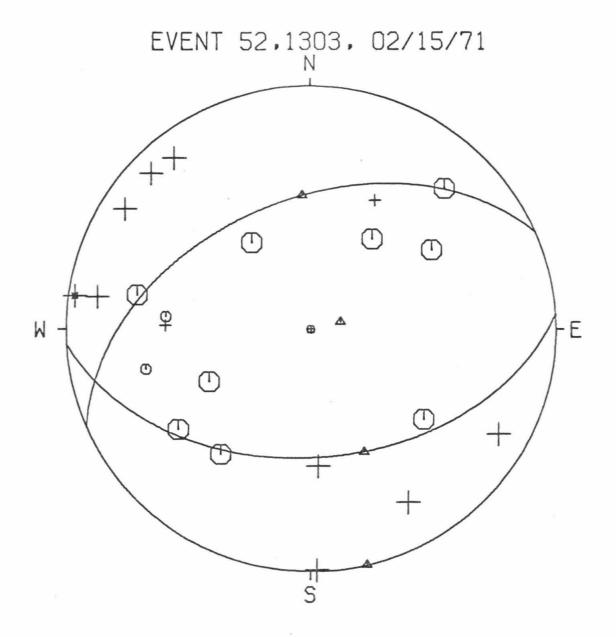
126.891

2

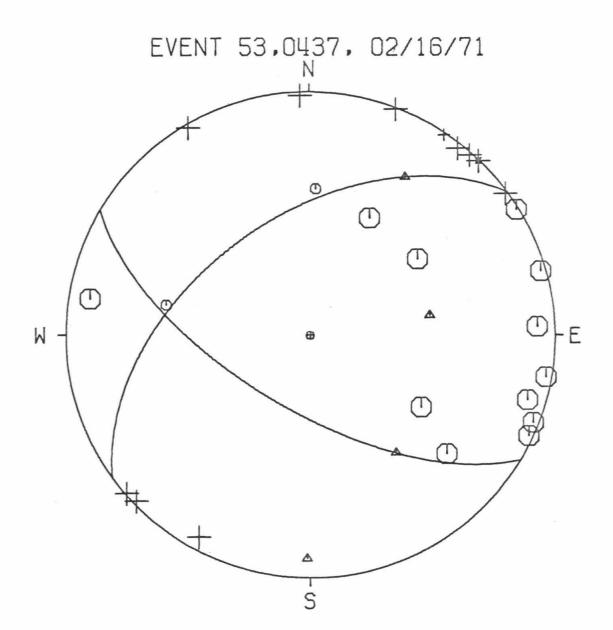
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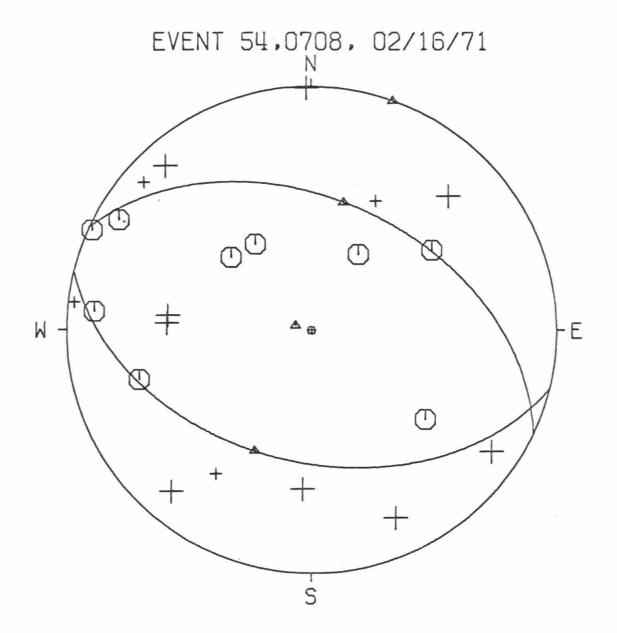
NSHC



EVENT DATA 53,0437 0 02/16/71 4 37 0.0 3.0 34.000 17.25 -118.000 32.61 3.5 AZ1= 121.000 DIP1= 65.000 AZ2= 234.000 DIP2= 50.039 SLIP VECTORS= 144.000 50.039 31.000 65.000 PRIN AXES 80.295 180.666 41.151 81.065 STA DIR QUAL DIST EVAZ TOA X Y CLC C 2 1.712 26.711 44.933 0.607 1.207 2 C CSP 0.982 87.741 82.086 2.320 0.092 2 GSC C 54.238 1.753 44.933 1.096 0.790 ISA C 1 1.224 2.304 50.438 0.061 1.505 MWC C 2 87.591 2.409 -0.428 0.408 100.074 C 2 PAS 0.340 114.824 88.248 2.234 -1.0332 PLM C 123.193 44.933 1.131 -0.740 1.682 2 2.131 PYR D 0.326 329.853 88.383 -1.238 C 2 -2.253 SBC 1.147 279.477 80.506 0.376 1 50.440 SYP C 1.210 281.894 -1.4740.310 2 RVR C 1.013 106.585 81.793 2.218 -0.661 2 BOUQ D 0.237 20.868 89.229 0.885 2.320 C 2 0.052 311.087 116.859 1.395 -1.216BRWN 2 D 0.159 49.081 90.623 -1.879-1.629 IRON 2 95.867 -1.137-2.078 GOOK D 0.117 28.682 SOLE D -2 0.208 44.005 89.507 1.729 1.790 INDN C 2 0.264 58.558 88.975 2.114 1.292 NAGM D 2 0.277 41.486 88.850 1.639 1.854 C 2 74.311 NMLM 0.398 87.688 2.358 0.662 NRTM D 2 0.396 38.234 87.712 1.516 1.924 NWSM n 2 0.320 357.894 88.435 -0.091 2.464 C 2 ENGN 0.407 111.546 87.600 2.276 -0.899 NSCF D 2 0.261 53.906 89.003 2.002 1.460 33.775 1 NSHC D 0.268 88.939 1.377 2.059 NSGM D 2 0.149 46.115 91.690 -1.775-1.707



EVENT DATA 54,0708		16/71 7 4.000 24.40		00 26.86	3.3
AZ1= 104.000 DIP1= 45.000 AZ2= 295.000 DIP2= 45.531					
SLIP VECTORS=	205.000	45.531		14.000	45.000
PRIN AXES =	286.972	5.538		19.525	89.733
STA DIR QUAL	DIST	EVAZ	TOA	x	Υ
CLC D 1 CSP D 1 GSC C 2 ISA D 2 MWC C 2 PAS D 2 PLM C 2 PYR D 2 RVR C 2 SBC D 2 SYP D 2 BOUQ D 2 BRWN D 2 IRON C 2 GOOK C 2 NMLM C 2 NRTM D 2	***************************************	272.748 275.962 2.990 225.432 132.425 211.400 94.913 40.739	49.400 92.650 49.400 89.561 100.252 100.908 49.400 102.245 91.755 49.400 49.400 124.916 112.505 143.415 150.077 101.933 103.436	0.651 -2.424 1.226 -0.048 -1.965 -1.489 1.163 1.839 -2.238 -1.476 -1.469 -0.085 1.399 -0.819 0.476 -2.218 -1.429	1.326 0.289 0.825 2.490 1.130 1.688 -0.912 -1.242 1.025 0.071 0.153 -1.633 1.378 0.749 0.779 0.191 -1.660
NWSM D 2 ENGN D 1 NSCF C 2 NSHC D 1 NSGM C 2	0.222	335.871	106.700 99.529 117.749 119.883 145.403	0.863 -1.705 -1.756 -0.974 -0.571	-1.926 1.519 -0.506 -1.479 0.883



EVENT DATA

SOLE

INDN

NAGM

NMLM

NRTM

NWSM

ENGN

NSCF

NSHC

NSGM

C

D

D

D

D

C

D

D

2

1

2

2

2

2

2

1

-2

-1

0.120

0.093

0.161

0.190

0.267

0.348

0.262

0.107

0.182

0.112

55,1439 0 02/16/71 14 39 0.0 10.0 34.000 20.07 -118.000 17.87 3.1 AZ1= 108.000 DIP1= 40.000 AZ2= 288.000 DIP2= 50.000 SLIP VECTORS= 198.000 50.000 18.000 40.000 PRIN AXES 197.976 5.007 18.000 85.000 STA DIR QUAL DIST EVAZ TCA X Υ CLC 2 D 1.587 21.049 49.400 0.531 1.379 CSP 2 0.779 93.040 94.638 -2.393 0.127 D GSC 0 2 1.562 51.422 49.400 1.155 0.921 2 1.184 353.636 49.400 -0.164 1.468 ISA D 2 107.673 MWC 0 0.229 119.935 -1.808 1.041 2 PAS D 0.215 150.861 109.208 -0.997 1.789 PLM C 2 1.545 128.929 49.400 1.149 -0.928 PYR 2 0.435 99.134 1.930 -1.238D 302.688 RVR C 2 0.838 113.785 93.902 -2.208 0.973 BOUQ 2 0.211 325.933 109.607 1.142 -1.688 D BRWN 258.438 D 2 0.248 105.620 2.094 0.428 C 2 IRON 0.101 304.978 128.521 1.258 -0.880 C 2 GOOK 0.157 290.574 115.942 1.755 -0.659

331.041

13.772

71.669

9.096

4.206

353.048

321.934

137.997

342.743

301.385

123.399

131.057

115.378

111.943

104.510

101.928

104.676

126.779

112.744

125.441

0.812

0.229

-0.349

-1.878

-0.342

-1.446

-0.116

C. 581

1.383

1.373

-1.467

-1.422

-1.876

-0.622

-2.137

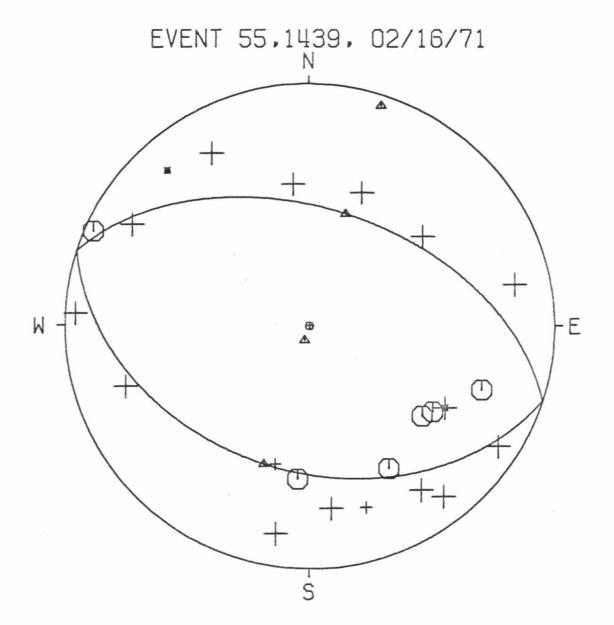
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1.605

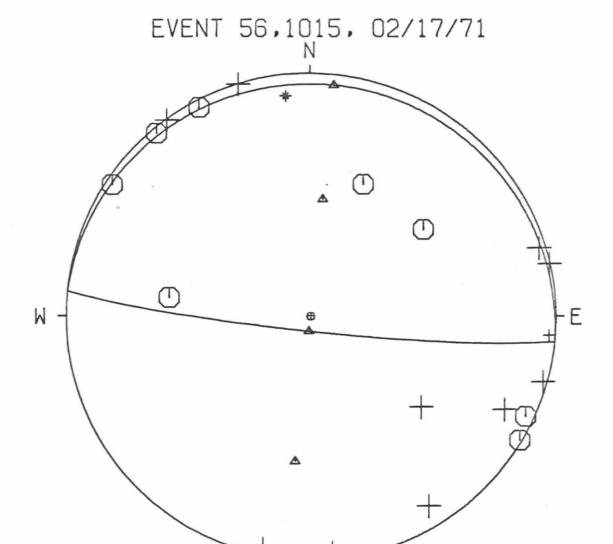
-1.579

-1.870

-0.844



EVENT DATA 56,1015		17/71 10 1 4.000 21.46		0 18.38	3.5
AZ1 = 96.000 DIP1 = 85.000 AZ2 = 276.000 DIP2 = 5.000					
SLIP VECTORS=	186.000	5.000		6.000	85.000
PRIN AXES =	6.000	40.001	18	86.000	50.000
STA DIR QUAL	DIST	EVAZ	TOA	X	Υ
CLC C 2 CSP D 1 GSC C 2 ISA D -1 MWC C 2 PAS C 2 PLM D 2 PYR C 2 RVR C 2 SYP C 2 BOUQ D 2 BRWN D 2 IRON D 2 IRON D 2 GOOK D 2 SOLE D 2 NAGM D 2 NMLM D 2 NRTM D 2	1.568 0.788 1.554 1.160 0.247 0.239 1.565 0.418 0.854 1.392 0.190 0.246 0.084 0.145 0.097 0.137 0.192 0.245	21.588 94.593 52.242 353.828 123.721 152.139 129.418 300.694 115.008 277.545 324.094 253.207 295.741 285.690 328.097 354.804 77.385 11.567	48.725 87.044 48.725 80.379 93.012 93.318 48.725 90.922 86.352 48.725 89.686 93.042 103.128 91.817 99.389 93.116 89.666 93.072	0.537 2.427 1.153 -0.245 -2.024 -1.134 1.127 2.132 2.192 -1.446 -1.462 2.329 1.980 2.368 1.209 0.220 2.433 -0.488	1.356 -0.195 0.893 2.268 1.351 2.145 -0.926 -1.266 -1.023 0.191 2.019 0.703 -0.955 -0.665 -1.942 -2.421 0.544 -2.383
ENGN C 2 NSHC D 2	0.285	140.199 342.971	92.317	-1.568 -0.732	1.881



EVENT DATA 57,2209 0 02/18/71 22 9 0.0 4.4 34.000 23.18 -118.000 25.85 3.2 AZ1= 125.000 DIPI= 70.000 AZ2= 218.000 81.817 DIP2= SLIP VECTORS= 128.000 81.817 35.000 70.000 PRIN AXES 83.063 69.971 350.087 81.883 STA DIR QUAL DIST TCA Χ EVAZ GSC C 2 1.620 55.200 48.500 1.192 0.829 ISA D 2 1.125 358.296 81.577 -0.069 2.309 2 0.350 89.221 MWC C 118.113 2.190 -1.17089.497 2 PAS D 0.322 138.120 1.662 -1.853PLM D 1 1.664 127.858 48.500 1.146 -0.891 2 305.559 -2.026 PYR D 0.315 89.564 1.448 RVR C 2 0.959 113.880 83.211 2.147 -0.950 2 SYP C 1.286 276.858 48.500 -1.442 0.173 BOUQ D 2 0.125 356.132 94.982 0.161 -2.384 C 2 233.290 BRWN 0.166 89.918 -2.003 -1.493 IRON C 2 0.040 43.799 126.196 -1.107-1.155C 2 229.716 119.143 GOOK 0.048 1.366 1.158 SOLE D 2 0.079 40.807 104.783 -1.410 -1.633 2 C 0.291 84.662 89.799 NMLM 2.485 0.232 2 0.261 35.613 90.099 NRTM D -1.455 -2.031 2 0.245 334.766 NWSM 90.358 1.062 -2.254

130.854

88.951

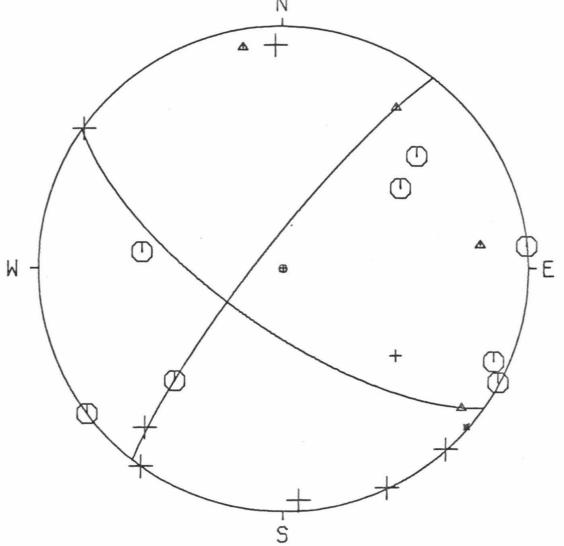
1.874

-1.620

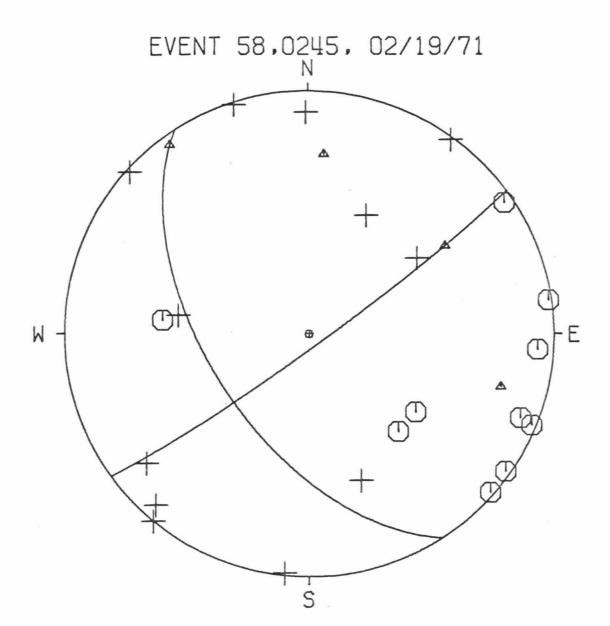
-1

ENGN





EVENT		0245		19/71 2 4 000 21-45		27.58	3.5
AZ1 = DIP1 = AZ2 = DIP2 =	5	7.000 6.000 4.000 5.563					
SLIP	VECT	ORS=	323.999	85.563	!	57.000	56.000
PRIN	AXES	=	4.963	63.250	. 10	05.490	70.080
STA	DIR	QUAL	DIST	EVAZ	TOA	x	Υ
BAR CLC CSP GSC ISA MWC PAS PLM PYR RVR SBC SYP BOUQ BRWN IRON GOOK SOLE NAGM		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	0.315 0.971 1.208 1.266 0.153 0.131 0.066 0.040 0.114 0.179	137.752 25.677 93.846 54.845 359.381 112.482 131.260 126.560 312.426 111.792 275.349 278.183 5.746 236.045 51.292 340.587 41.643 39.619	44.933 82.739 44.933 80.449 88.055 88.459 44.933 88.482 82.200 50.441 44.933 91.189 94.033 105.955 126.196 96.305 90.005	0.908 0.585 2.331 1.105 -0.025 2.270 1.854 1.085 -1.821 2.158 -1.500 -1.337 -0.248 1.999 -1.661 0.532 -1.567 -1.594	-1.000 1.218 -0.157 0.778 2.283 -0.940 -1.626 -0.805 1.664 -0.863 0.140 0.192 -2.462 1.346 -1.331 -1.509 -1.763 -1.926
NMLM NRTM NWSM ENGN	C D C	2 2 2 2	0.317 0.298 0.264 0.378	81.888 36.123 342.149 125.173	88.465 88.648 88.975 87.877	2.442 1.456 -0.759 2.005	0.348 1.995 2.358 -1.413



EVENT DATA

2

2

0.200

0.411

C

D

NWSM

ENGN

59,0809 02/20/71 34.000 27.24 -118.000 24.38 15.2 AZ1= 120.000 DIP1= 60.000 AZZ= 222.000 DIP2= 70.195 SLIP VECTORS= 132.000 70.195 30.000 60.000 PRIN AXES 53.621 349.079 83.456 83.919 STA DIR QUAL TCA Υ DIST EVAZ Х CLC C 1.513 49.560 0.645 1.334 1 25.782 CSP C 2 0.882 100.128 97.352 -2.298 0.411 2 1.565 49.560 GSC C 56.820 1.240 0.811 ISA D 2 1.058 357.237 49.600 -0.071 1.481 2 1.297 MWC D 0.370 128.815 108.351 -1.612 2 PAS D 0.363 147.537 108.567 -1.1081.741 PLM C 2 1.690 130.101 49.560 1.133 -0.955 C 2 0.301 293.016 PYR 112.660 1.804 -0.766 268.263 SBC C 2 1.248 49.560 -1.481 -0.045 1 49.560 SYP D 1.300 273.907 -1.4780.101 BOUQ C -2 0.071. 336.274 151.445 0.351 -0.798 223.126 BRWN C 2 0.224 119.251 1.222 1.305 C 2 174.291 IRON 0.071 151.445 -0.087 0.868 C 2 216.213 143.433 0.895 GOOK 0.097 0.655 SOLE C 2 0.052 143.088 158.265 0.533 -0.400 C INDN 1 0.122 113.541 136.695 -1.196 0.521 2 NAGM D 0.088 52.494 145.860 -0.823 -0.632 2 114.389 NMLM D 0.278 104.198 -1.8570.470 NRTM C 2 0.197 42.003 123.122 -1.127-1.251

321.309

139.792

122.697

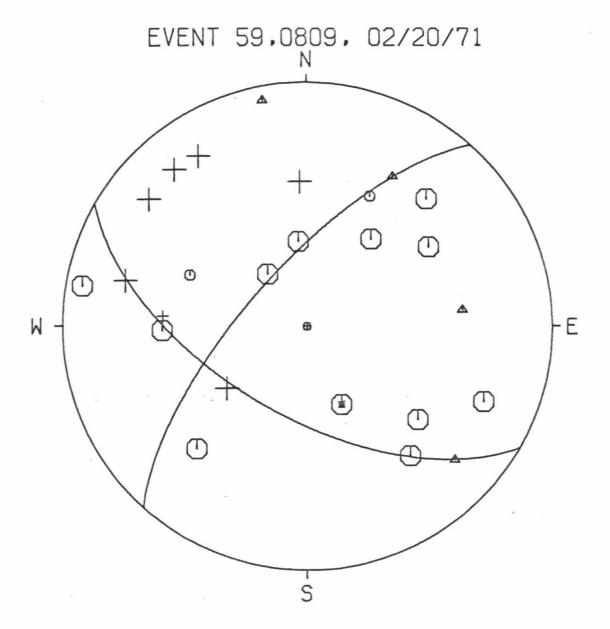
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-1.323

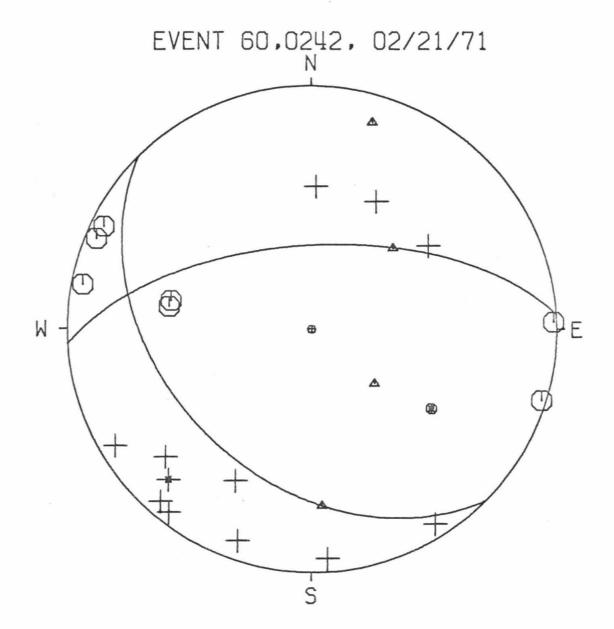
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1.060

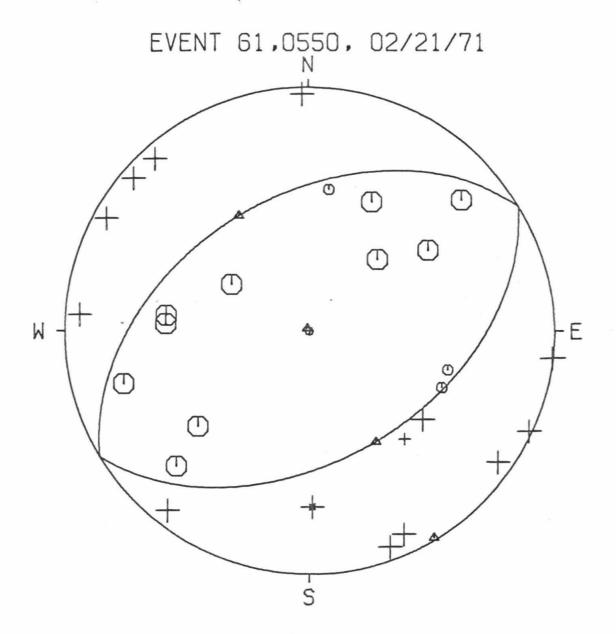
-1.355



EVENT DATA 60,0242		21/71 2 4 4.000 17.69		00 31.86	3.6
AZ1= 135.000 DIP1= 39.000 AZ2= 266.500 DIP2= 61.783				*	
SLIP VECTORS=	176.500	61.783		45.000	39.000
PRIN AXES =	131.063	27.890		16.454	77.573
STA DIR QUAL	DIST	EVAZ	TOA	Х	Υ
CLC D 2 CSP C 2 GSC D 2 ISA D 2 MWC C 2 PAS C 2 PLM C -1 PYR D 2 RVR C 2 SBC C 2 SYP C 2 BOUQ D 2 IRON D 2 GOOK D 2 SOLE D -2	1.701 0.972 1.740 1.216 0.399 0.333 1.677 0.324 1.005 1.156 1.219 0.226 0.147 0.103 0.196	26.519 88.233 54.238 1.885 101.057 116.415 123.598 327.604 107.158 279.016 281.446 19.150 48.698 26.501 43.376	49.100 88.495 49.100 95.086 95.849 49.100 95.945 88.110 49.400 49.100 98.947 111.692 121.069 106.035	-2.122 1.224 1.268 2.349 -1.459 -1.440 -0.754 -1.491 -0.776	1.314 0.076 0.858 1.468 0.458 1.054 -0.813 -1.999 -0.725 0.232 0.292 -2.170 -1.310 -1.556 -1.546
INDN D 2 NAGM D 2 NRTM D 2 NWSM D 2 ENGN C 2	0.250 0.264 0.383 0.313 0.400	59.173 41.006 37.759 355.959 112.898	97.260 96.641 95.270 96.079 95.074		-1.197 -1.774 -1.884 -2.358 0.929



EVENT DATA 61,0550		21/71 5 5 4.000 23.8	50 0.0 5 -118.00	0 26.32	4.7
AZ1= 59.000 DIP1= 46.000 AZ2= 239.000 DIP2= 44.000					
SLIP VECTORS=	149.000	44.000	3	28.999	46.000
PRIN AXES =	330.058	1.032	1	49.000	89.000
STA DIR QUAL	DIST	EVAZ	TCA	×	Υ
CLC C 2 CSP D 2 CWC C 1 GLA C 1 GSC C 2 HFD C 1 ISA D 2 MWC D 2 PAS D 2 PLM D 2 PYR D 2 RVR D 2 SBC C 2 SYP C 2	1.575 0.900 2.059 3.296 1.619 2.427 1.114 0.361 0.334 1.675 0.304 0.970 1.222	25.749 96.284 8.123 113.032 55.655 105.728 358.574 119.184 138.461 128.014 304.638 114.336 272.939	49.125 89.548 49.125 49.125 49.125 87.076 95.791 96.104 49.125 96.452 88.741 49.125	0.638 2.475 0.208 1.353 1.213 1.415 -0.061 -2.070 -1.567 1.158 1.938 2.253 -1.468	1.324 -0.273 1.455 -0.575 0.829 -0.398 2.435 1.156 1.769 -0.905 -1.339 -1.019 0.075
SYP C 2 80UQ D -2 8RWN C 2 IRON C 2 GOOK C 2 SOLE C 2 INDN C 2 NAGM C 2 NMLM D 2 NRTM D 2 NRTM D 2 NWSM D 2 ENGN D 2 SWM D 2	1.279 0.114 0.167 0.040 0.044 0.077 0.144 0.138 0.297 0.256 0.233 0.389 0.341	276.362 358.999 229.218 121.189 223.596 49.398 74.145 44.408 94.160 38.153 335.096 131.307 339.580	49.125 118.441 108.865 149.647 146.728 129.794 112.241 113.372 96.528 97.100 98.792 95.471 96.017	-1.461 0.032 1.557 -0.792 0.698 -1.139 -1.896 -1.359 -2.347 -1.446 0.969 -1.786 0.825	0.163 -1.809 1.343 0.479 0.733 -0.976 -0.538 -1.387 0.171 -1.840 -2.087 1.570 -2.217



EVENT DATA 02/21/71 62,0715 0 7 15 7.2 34.000 23.52 -118.000 25.65 AZ1= 96.000 DIP1 = 52.000 AZZ= 202.000 DIP2= 70.567 SLIP VECTORS= 112.000 70.567 6.000 52.000 PRIN AXES 47.887 65.775 325.139 78.458 STA DIR QUAL DIST TOA Y EVAZ Х BAR D 2 2.251 49.200 138.859 0.968 -1.108 C 2 49.200 CLC 1.576 25.367 0.631 1.330 2 CSP C 0.891 96.115 90.352 -2.478 0.266 7.853 CWC D 1 2.063 49.200 0.201 1.458 GSC C 2 1.614 55.319 49.200 1.210 0.837 2 ISA 1.119 358.162 87.656 -0.079 2.447 D 2 1.141 MWC 0 0.350 119.073 96.722 -2.053 2 PAS D 0.324 139.069 97.030 -1.534 1.769 2 C PLM 1.665 128.068 49.200 1.159 -0.907 PYR D 2 0.314 304.346 97.146 1.931 -1.3202 114.265 89.544 RVR D 0.959 2.270 -1.0232 49.200 SBC D 1.231 273.270 -1.469 0.084 D 2 276.599 SYP 1.288 49.200 -1.462 0.169 TIN C 1 2.662 3.433 49.200 0.088 1.469 2 BOUQ 0 0.119 354.568 117.409 0.174 -1.828 C 2 BRWN 0.170 232.768 108.527 1.644 1.249 C 2 IRON 0.034 134.156 153.383 -0.584 0.567 2 GOOK C 0.048 235.152 144.050 0.894 0.623 SULE C 2 0.071 43.295 132.226 -0.982 -1.042 2 -1.825 INDN D 0.137 70.605 113.662 -0.642 2 C 39.755 NAGM 0.137 113.662 -1.237-1.487 2 NMLM 0 0.289 95.578 97.444 -2.321 0.227 2 NRTM C 0.254 35.943 98.116 -1.360-1.8762 NWSM D 0.242 333.673 99.057 -2.057 1.018 2 96.381 ENGN 0.379 131.766 D -1.7581.570

338.517

96.716

0.860

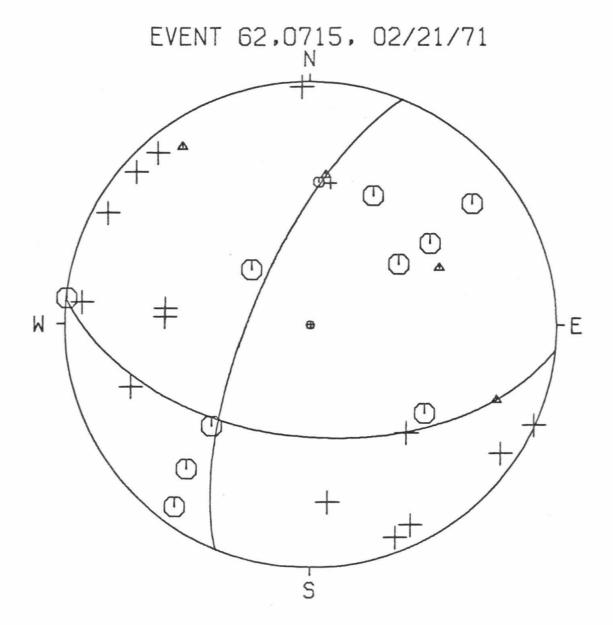
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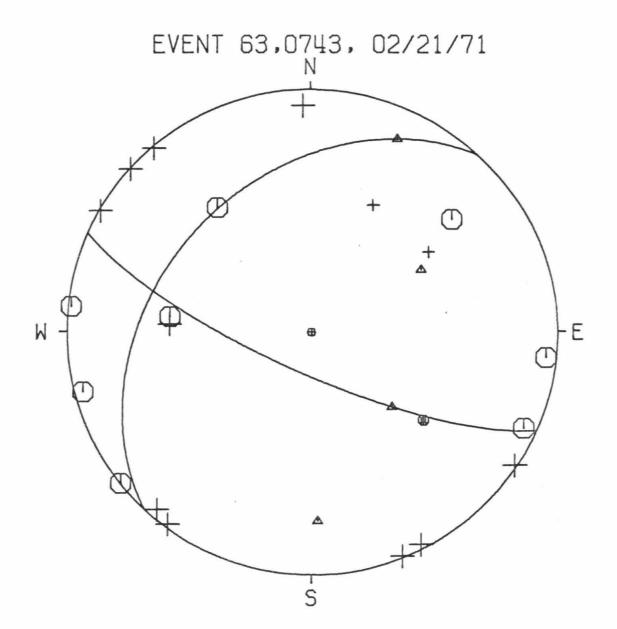
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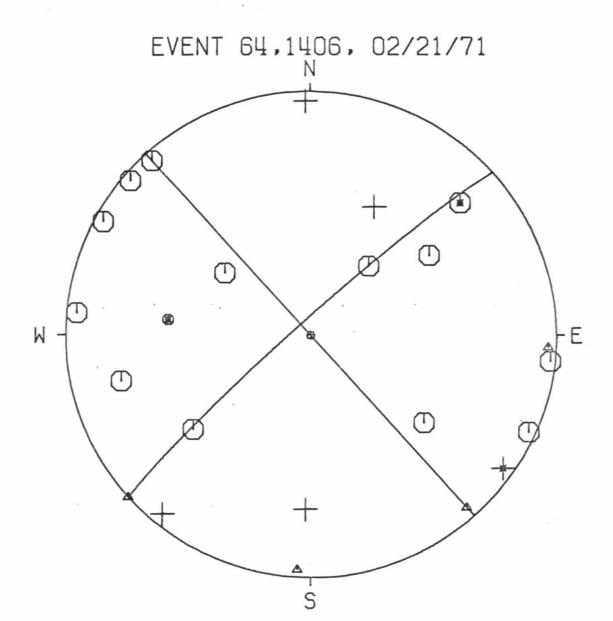
SWM



EVENT DATA 63,0743		21/71 7 4 4.000 23.87		25.58	3.5
AZ1= 223.000 DIP1= 37.000 AZ2= 114.000 DIP2= 76.216					
SLIP VECTORS=	24.000	76.216	13	3.000	37.000
PRIN AXES =	60.275	42.845	17	8.008	66.657
STA DIR QUAL	DIST	EVAZ	TOA	х	Υ
CLC D 1 CSP C 2 GSC D 1 ISA D 2 MWC D 2 PAS D 2 PLM C -1 PYR D 2 RVR C 2 SBC D 2 SYP C 2 BRWN C 2 IRON C 2 IRON C 2 INDN C 2 NAGM D 2	0.890 1.610 1.114 0.352 0.327 1.668 0.312 0.961 1.232 1.289 0.175 0.040 0.052 0.133	25.426 96.291 55.473 358.111 120.029 139.832 128.245 303.526 114.616 273.241 276.283 231.347 143.320 231.071 75.249 40.793	85.050 48.625 82.768 90.538 90.791 48.625 90.947 84.327 48.625 48.625 48.625 89.830 126.196 116.859 93.796 93.796	-1.447 -1.949 -0.956 1.440 -2.336 -1.578	1.315 -0.262 0.825 2.336 1.245 1.897 -0.901 -1.369 -0.989 0.082 0.159 -1.559 1.283 1.163 -0.615 -1.829
NMLM C 2 NRTM D 2 NWSM D 2 ENGN D 2 SWM D 2	0.288 0.249 0.237 0.382 0.344	96.112 36.587 332.830 132.410 337.941	91.193 91.773 92.103 90.239 90.618	-2.460 -1.467 1.120 -1.842 0.934	0.263 -1.976 -2.183 1.683 -2.304



EVENT		A ,1406		21/71 14 4.000 23.89		00 26.70	3.5
AZ1= DIP1= AZ2= DIP2=	1	28.000 85.000 38.000 90.000					
SLIP	VEC	TORS=	48.000	90.000		138.000	85.000
PRIN	AXE	s =	92.902	86.467	1	183.109	86.467
STA	DIR	QUAL	1210	EVAZ	TCA	Х	Υ
CLC CSP GSC ISA MWC PAS PLM PYR RVR SYP BOUQ BRWN IRON GOOK SOLE INDN NMLM		2 2 2 2 2 2 2 -2 2 -1 2 -2 2 2 2 2 2 2 2	1.577 0.905 1.623 1.113 0.366 0.338 1.680 0.299 0.975 1.273 0.112 0.162 0.048 0.040 0.082 0.148 0.303	25.929 96.240 55.773 358.811 118.854 137.880 127.918 304.960 114.212 276.320 1.664 228.337 126.229 219.678 51.025 76.223 95.519	48.950 87.879 48.950 85.578 93.868 94.176 48.950 94.613 87.110 48.950 118.795 109.328 144.090 149.647 128.145 111.421 94.562	C.640 2.439 1.211 -0.050 -2.114 -1.615 1.156 1.965 2.222 -1.456 -0.052 1.528 -0.879 0.591 -1.202 -1.935 -2.387	1.317 -0.267 0.824 2.401 1.165 1.786 -0.900 -1.374 -0.999 0.161 -1.799 1.359 0.644 0.712 -0.972 -0.474 C.231
NML M NR TM ENGN	C D C	2 2 2	0.303 0.259 0.393	95.519 39.237 130.892	94.562 95.057 93.564	-2.387 -1.510 -1.830	C. 23 -1.84 1.58



EVENT DATA 16 4 0.0 65,1604 0 02/24/71 10.8 34.000 26.48 -118.000 24.64 3.7 AZ1= 104.000 DIP1= 60.000 208.000 AZZ= DIP2= 67.265 67.265 14.000 SLIP VECTORS= 118.000 60.000 PRIN AXES 68.304 51.184 334.591 85.395 STA DIR QUAL DIST EVAZ TOA X Υ CLC C 2 1.526 25.693 49.400 0.641 1.331 C 2 93.754 CSP 0.883 99.167 -2.386 0.385 2 56.508 49.400 1.232 GSC C 1.575 0.815 2 91.376 0.111 ISA D 1.071 357.433 -2.467 2 102.443 -1.770 MWC D 0.365 126.948 1.331 D 2 0.354 145.936 102.897 -1.234 1.825 PAS 2 129.688 49.400 1.137 PLM C 1.685 -0.9432 0.303 295.484 104.937 1.944 PYR D -0.927 2 0.968 117.254 92.677 -2.170 1.118 RVR D 2 271.630 49.400 1.244 -1.4770.042 SBC D 49.400 0.112 2 1.298 274.342 SYP D -1.4731 2.612 3.202 49.400 1.475 TIN D 0.083 BRWN C 2 0.212 224.778 111.528 1.401 1.412 2 C 0.059 169.648 146.286 -0.184 1.009 IRCN 2 GOOK C 0.082 221.162 137.368 0.846 0.968 2 NAGM C 0.095 51.016 133.080 -1.094 -0.885 NMLM 0 2 0.280 102.217 105.845 -2.083 0.451 2 NRTM C 0.207 40.692 112.058 -1.288 -1.4982 0.207 324.211 112.058 1.155 -1.603 NWSM D 138.243 ENGN D 2 0.403 100.924 -1.499 1.679

332.774

104.607

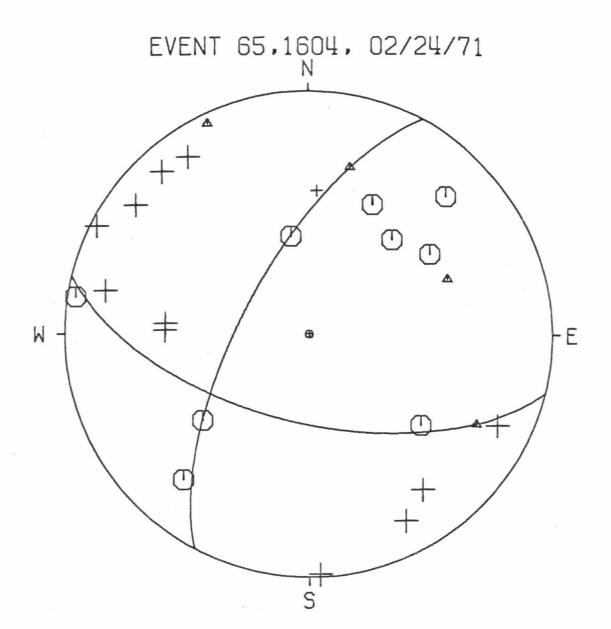
0.989

-1.922

SWM

2

0.311



EVENT DATA 66,1127 0 02/25/71 11 27 32.9 7.5 34.000 25.23 -118.000 26.51 AZ1= 58.000 42.000 DIP1= AZ2= 224.000 DIP2= 48.858 SLIP VECTORS= 134.000 48.858 327.999 42.000 76.543 7.820 320.584 PRIN AXES 86.546 STA DIR QUAL DIST EVAZ TCA Υ Х GSC C 2 1.608 56.375 49.275 1.227 0.816 2 358.669 2.470 ISA 0 1.091 88.645 -0.057 2 0.374 121.893 97.235 1.235 MWC D -1.984 D 2 0.353 140.637 97.486 -1.479 1.803 PAS PLM C 1 1.692. 128.574 49.275 1.152 -0.919 2 98.253 PYR D 0.289 301.243 1.978 -1.200 SYP 0 2 1.274 275.367 49.275 -1.467 0.138 2 0.390 124.404 BOUQ D 0.093 -0.011 -1.649 -2 107.657 C 0.179 223.625 1.510 BRWN 1.440 2 C 135.833 141.663 IRON 0.052 -0.809 0.833 C 2 0.056 209.888 139.546 1.060 GOOK 0.609 2 134.947 SOLE C 0.066 67.900 -1.255 -0.510 2 76.175 0.145 111.965 INDN D -1.921 -0.473D 2 0.302 97.715 98.102 -2.296 0.311 NMLM C 2 0.162 233.919 109.328 NOMM 1.653 1.204 2

333.216

133.611

104.452

96.844

0.976

-1.699

-1.933

1.618

0.212

0.407

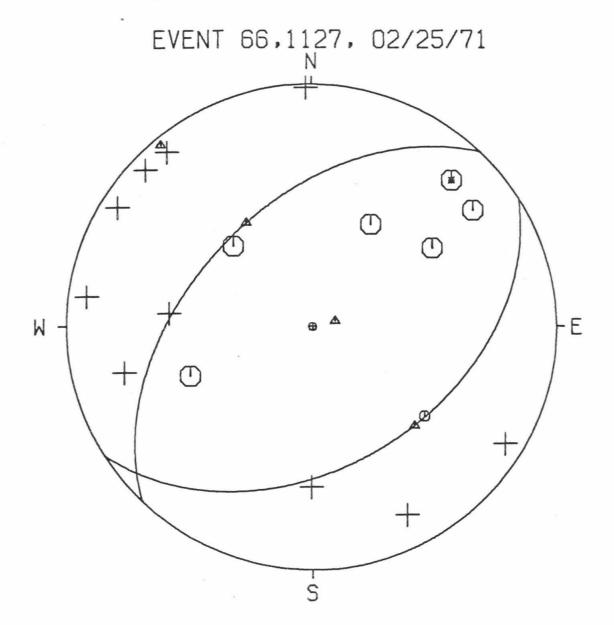
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ENGN

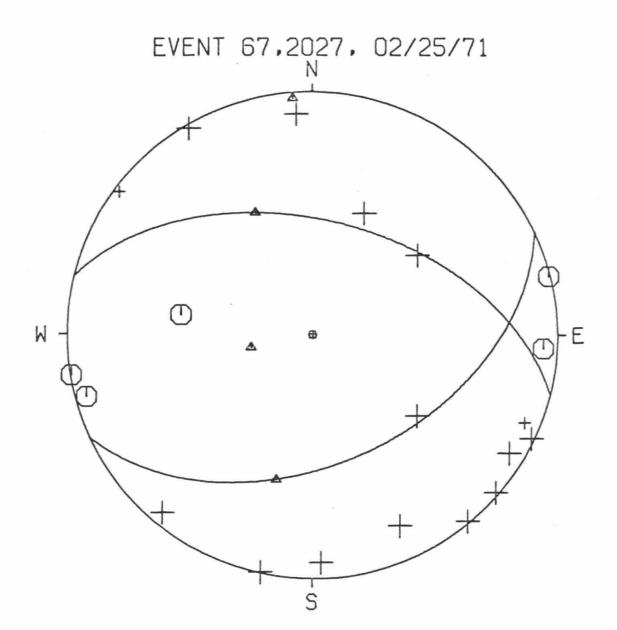
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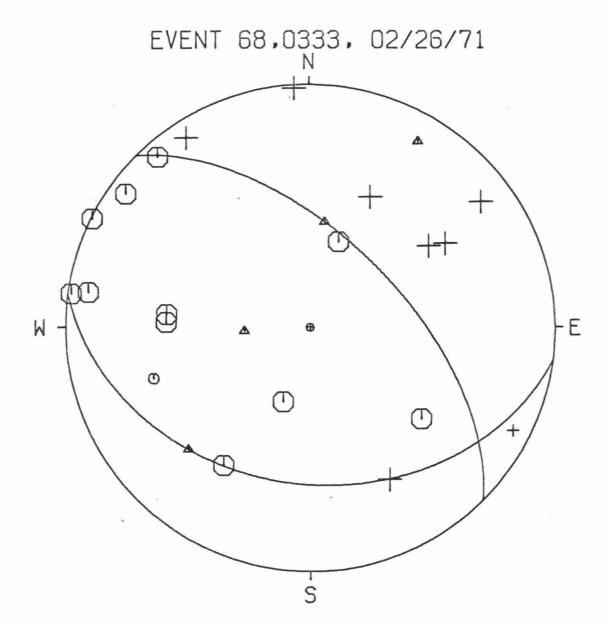
2



EVENT DATA 67,2027 0 02/25/71 20 27 0.0 34.000 20.17 -118.000 21.79 3.5 3.0 AZ1= 65.000 DIP1= 46.000 AZ2= 284.000 51.174 DIP2= SLIP VECTORS= 51.174 334.999 46.000 194.000 PRIN AXES 258.057 20.851 355.308 87.256 EVAZ STA DIR QUAL DIST TCA Υ X CLC 0 2 1.606 22.833 44.933 0.524 1.245 CSP C 2 93.253 83.512 0.834 2.351 -0.134GSC 2 52.634 44.933 1.074 0.820 D 1.604 2 355.946 ISA D 1.178 80.213 -0.161 2.272 MWC 2 0.279 115.155 88.830 2.240 -1.052D PAS D 2 0.247 139.996 89.136 1.595 -1.901 2 PLM D 1.589 127.714 44.933 1.069 -0.826 PYR 1 306.816 87.764 -1.962 D 0.390 1.469 82.989 RVR D 1 0.888 112.431 2.165 -0.894 SYP C 2 1.348 278.669 44.933 -1.336 0.204 2 254.526 BRWN C 0.196 85.122 -2.305-0.638 2 335.328 0.896 -1.951 IRON D 0.069 105.211 GOOK D 2 0.108 300.918 96.988 2.010 -1.204 2 97.463 SOLE D 0.105 357.675 0.095 -2.3302 95.652 INDN D 0.119 39.885 -1.522 -1.821 2 90.509 NAGM D 0.163 12.219 -0.527 -2.432 NMLM C 2 0.241 75.863 89.190 2.407 0.606 2 MMDN C 0.199 260.324 89.599 -2.456 -0.419 2 -1.253NWSM D 0.316 329.464 88.477 2.124 ENGN 2 0.302 130.586 1.875 0 88.610 -1.607



EVENT		0333		26/71 3 3 4.000 25.13	33 0.0 3 -118.00	00 22.95	3.5
AZ1 = DIP1 = AZ2 = DIP2 =	= 3 31	98.000 86.000 5.000 9.876					
SLIP	VEC 1	ORS=	225.000	59.876		8.000	36.000
PRIN	AXES	<u> </u>	266.736	22.039		30.152	77.457
STA	DIR	QUAL	DIST.	EVAZ	TOA	X	Υ
CLC CSP GSC ISA MWC PAS PLM PYR RVR SBC SYP BOUQ BRWN IRON GOOK SOLE		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1.537 0.857 1.568 1.094 0.333 0.323 1.653 0.333 0.937 1.268 1.322 0.105 0.215 0.040 0.091 0.034	24.564 98.067 55.373 356.408 126.177 147.179 129.620 297.048 116.713 272.079 275.198 332.476 233.491 198.581 238.095 20.042	49.275 91.450 49.275 88.603 97.732 97.854 49.275 97.732 90.487 49.275 120.441 104.185 149.647 125.115 153.383	0.613 -2.444 1.213 -0.155 -1.877 -1.259 1.135 2.071 -2.224 -1.473 -1.468 0.811 1.746 0.295 1.383 -0.279	1.340 0.346 0.838 2.464 1.373 1.952 -0.940 -1.058 1.119 0.053 0.134 -1.557 1.292 0.877 0.861 -0.765
I NDN NAGM NML M ENGN	C C C	1 2 -2 2	0.097 0.095 0.253 0.371	71.872 32.163 99.087 138.544	123.029 123.709 99.031 97.279	-1.603 -0.888 -2.267 -1.547	-0.525 -1.412 0.363 1.751



EVENT DATA 69,2122 0 02/26/71 21 22 33.5 34.000 27.25 -118.000 27.21 10.0 STA DIR QUAL DIST EVAZ TOA Х Υ GSC -11.598 57.570 49.400 1.247 0.792 2 1.057 359.088 91.149 ISA 0.039 -2.474 D MWC 2 0.401 125.268 100.225 -1.851 1.309 0 2 PAS 0.385 142.632 100.734 D -1.3691.792 2 PLM 0 1.720 129.237 49.400 1.144 -0.934 2 PYR D 0.265 296.357 104.557 1.938 -0.960 2 91.799 RVR D 1.005 116.948 -2.1931.115 SYP 1 1.261 273.846 49.400 -1.474 0.099 D BOUQ D 2 0.059 9.939 143.898 -0.189-1.079C -2 0.199 214.973 110.957 BRWN 1.642 1.148 C 2 146.689 IRON 0.084 133.884 -0.760 1.157 C 2 193.785 136.509 GOOK 0.077 0.312 1.272 SOLE C 2 0.079 117.151 135.607 -1.188 0.609 C 1 0.158 107.685 115.752 INDN -1.7910.571 C 2 0.120 65.083 123.399 -1.520NAGM -0.706 NMLM D 2 0.316 102.121 102.945 -2.1530.462

330.920

135.878

113.336

99.076

0.944

-1.597

-1.698

1.647

NWSM

ENGN

2

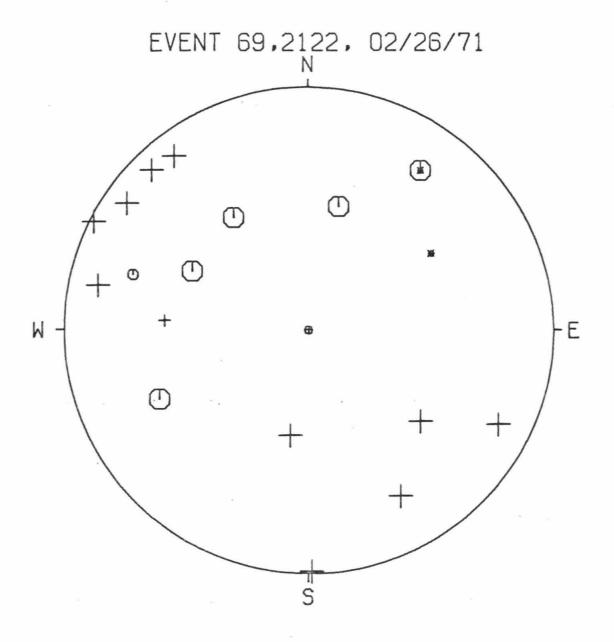
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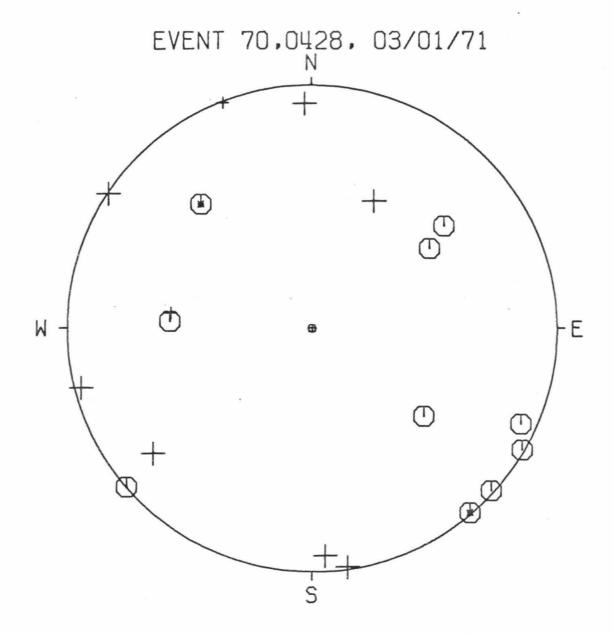
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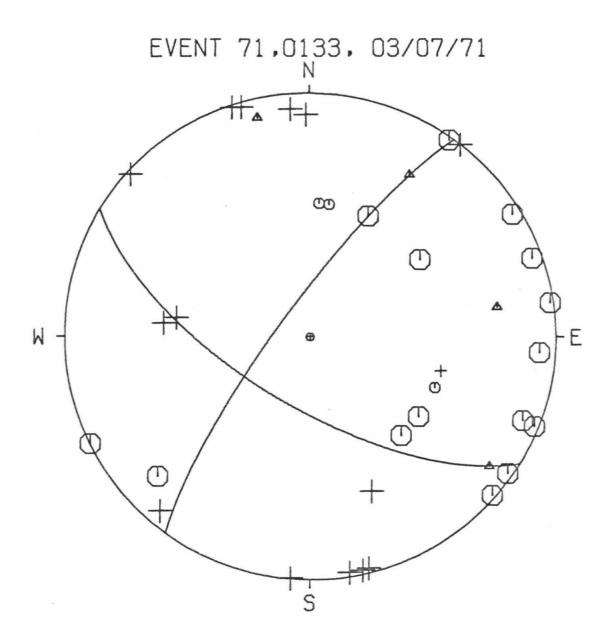
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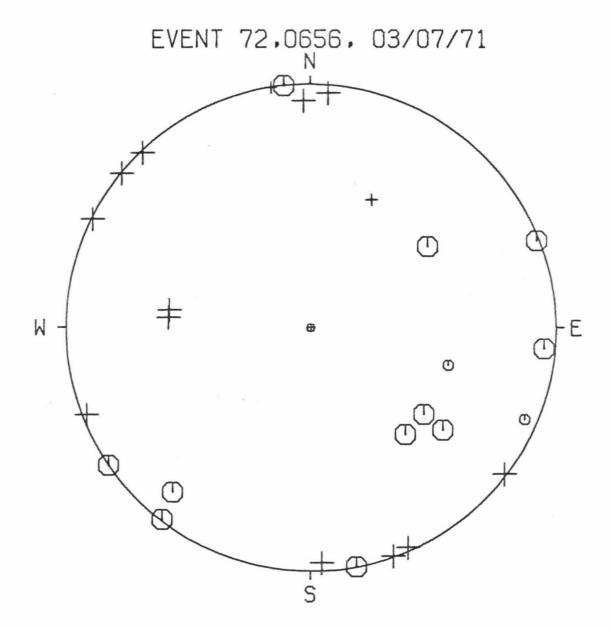
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		70	0428	0 0	3/01/71 4 2	28 0.0		
				4.4	34.000 24.0	5 -118.000	26.00	3.4
ST	Α	DIR	QUAL	DIST	EVAZ	TOA	Х	Υ
CL	С	D	2	1.570	25.660	48.500	0.629	1.309
GS	C	C.	2 .	1.6.13	55.662	48.500	1.199	0.819
15	Α	D	2	1.110	358.369	81.723	-0.066	2.312
MW	С	C	2	0.359	120.004	89.134	2.149	-1.241
PA	S	C	-2	0.333	139.385	89.385	1.619	-1.888
PL	M	C	2	1.674	128.201	48.500	1.141	-0.898
PY	R	D	2	0.306	303.693	89.657	-2.074	1.383
RV	R	C	2	0.967	114.630	83.133	2.132	-0.978
SB	C	C	2	1.226	272.952	48.500	-1.450	0.075
SY	P	D	1	1.283	276.231	48.500	-1.444	0.158
BOU	Q	D	2	0.110	356.664	97.321	0.136	-2.331
BRW	N	C	2	0.172	229.251	89.852	-1.891	-1.630
IRO	N	C	-2	0.044	138.315	122.304	-1.134	1.274
G00	K.	C	2	0.044	232.157	122.304	1.347	
SCL	E	D	2	0.069	51.653	108.439	-1.621	-1.283
IND	IN	D	2	0.138	75.577	92.894	-2.359	-0.607
ENG	N	C	2	0.388	132.208	88.845	1.833	-1.663
SW	М	D	1	0.340		89.322	-0.904	2.315
BH		D	2	0.397	171-422	88-756	0.369	-2-445



EVENT				07/71 1 3 4.000 21.19		00 27.35	4.5
	21	21.500 57.000 6.000 79.527					
SLIP	VECT	ORS=	126.000	79.527		31.500	67.000
PRIN	AXES	; =	80.790	66.120		347.002	81.503
STA	DIR	QUAL	DIST	EVAZ	TOA	Х	Υ
BAR	С	2	2.238		45.627		-1.015
CLC	С	2		25.510			1.237
CSP	C	2		93.807	82.770		-0.155
CWC	C	1		8.326	45.627		1.356
GLA	C	1	3.292	112.216	45.627		-0.518
GSC	C	2	1.656	54.658			0.793
HFD	0	1	2.429	104.622	45.627		-0.346
ISA	D	2	1.158	359.245	80.407		2.282
MWC	C	2	0.355	111.891	88.102		-0.917
PAS PLM	C	2	0.313	131.234	88.500		-1.626
PYR		2	1.660	126.505	45.627		-0.815
RVR	D C		0.320	312.553	88.435		1.667
SBC	D	2	0.966	111.579	82.246 50.032		-0.855 C.142
SYP	D	2	1.211	275.468 278.342	45.627		0.199
TIN	C				45.627		
BOUQ	D	1	2.702 0.157	3.864 4.450	90.561		1.368
BRWN	C.	2 .	0.131	238.606	94.032		1.256
IRON	C	2		47.065			-1.438
GOOK	D	2	0.044	338.358	122.304		-1.586
SOLE	D	2		40.282	96.633		-1.794
INDN		2	0.170	63.824	90.205		-1.101
NAGM	D	2	0.181	37.779	89.903	1.530	1.974
NMLM	C	2	0.314	81.767	88.494	2.442	0.353
NOMM	C	2	0.127	250.346	94.645	2.257	0.806
NRTM	c	2	0.299	35.198	88.635	1.424	2.018
NWSM	D	2	0.268	341.744	88.932	-0.776	2.352
ENGN	C	2	0.373	124.883	87.927	2.013	-1.404
SWM	0	2	0.378	343.890	87.877	-0.681	2.357
IPC		2	0.395	165.820	87.721	0.600	-2.375
нсс	D	2	0.365	170.493	88.008	0.406	-2.422
BHR	D	2	0.354	167.297	88.107	0.541	-2.398
BLNY	D	2	0.110	175.474	96.870	-0.185	2.338
AND THE RESERVE		-	- Colores Andreas				

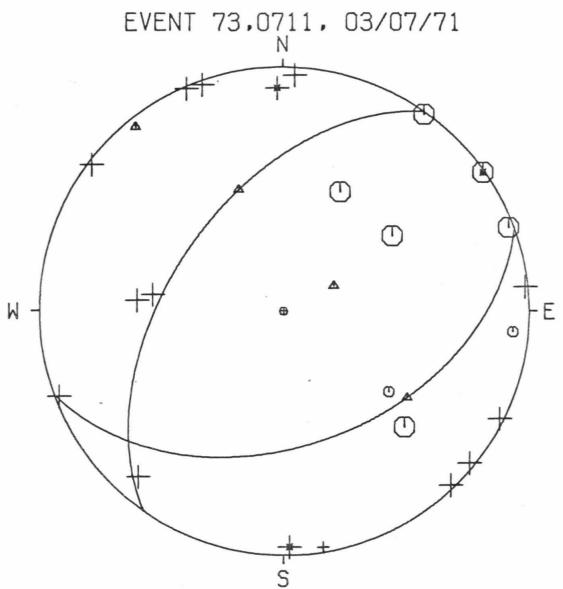


EVENT		4 ,0656	0 03	/07/71 6 34.000 22.5	56 0.0 9 -118.000	26.00	3.9
STA	DIR	QUAL	DIST	EVAZ	TCA	х	Υ
BAR	С	2	2.242	138.502	48.625	0.964	-1.090
CLC	D	1	1.592	25.283	48.625	0.622	1.316
CSP	C	2	0.894	95.085	85.010	2.379	-0.212
GSC	C	2	1.627	54.959	48.625	1.192	0.836
HFD	C	1	2.417	105.282	48.625	1.404	-0.384
ISA	D	2	1.135	358.400	82.554	-0.065	2.331
MWC	D	2	0.348	116.674	90.584	-2.223	1.117
PAS	D	2	0.315	136.501	90.915	-1.707	1.799
PLM	C	2	1.659	127.542	48.625	1.154	-0.887
PYR	D	2	0.319	307.087	90.877	1.979	-1.496
RVR	C	1	0.957	113.267	84.364	2.181	-0.938
SBC	D	2	1.228	274.224	48.625	-1.452	0.107
SYP	D	2	1.285	277.212	48.625	-1.444	0.183
BCUQ	D	2	0.133	357.232	93.796	0.117	-2.413
BRWN	C	2	0.158	235.644	89.988	-2.064	-1.411
GOOK	C	2	0.044	307.843	122.304	1.347	-1.047
SOLE	C	2	0.084	39.818	103.128	-1.407	-1.688
INDN	D	2	0.144	68.626	92.028	-2.286	-0.895
NAGM	C	2	0.152	37.488	90.789	-1.511	-1.970
NOMM	C	2 .	0.148	248.694	91.400	2.301	0.897
NWSM	D	2	0.253	336.102	91.636	0.998	-2.253
ENGN	D	2	0.373	129.522	90.329	-1.923	1.586
SWM	D	2	0.362	340.046	90.437	0.850	-2.341
IPC	C	2	0.413	169.119	89.917	0.472	-2.453
HCC	C	2	0.386	173.816	90.197	-0.269	2.481
BHR	D	1	0.373	170.855	90.329	-0.396	2.461
BLNY	D	2	0.133	184.303	93.796	0.181	2.409

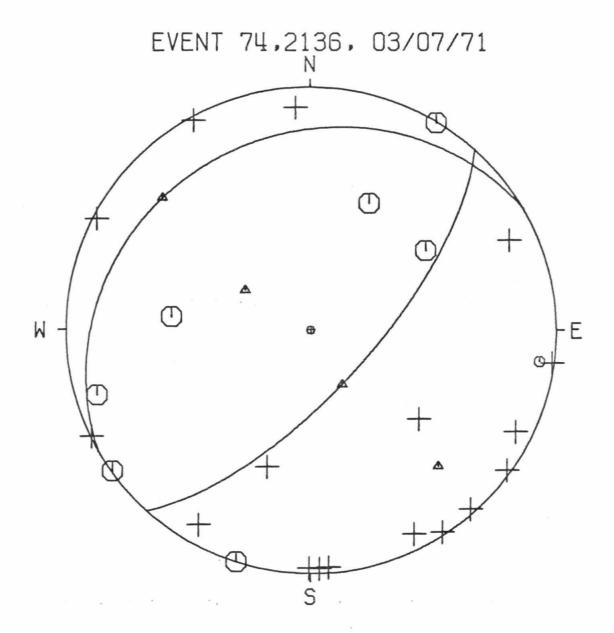


73,0711		07/71 7 1 4.000 22.65		0 26.22	3.3
AZ1= 70.000 DIP1= 44.000 AZ2= 215.000 DIP2= 51.654					
SLIP VECTORS=	125.000	51.654	33	39.999	44.000
PRIN AXES =	63.368	18.678	32	21.405	85.988
STA DIR QUAL	DIST	EVAZ	TCA	x	Υ
CLC C 2 CSP C 1 GSC C 2 ISA D -2 MWC D 2 PAS D 2 PLM C 1 PYR D 2 SBC D 2 SYP D 2 BOUG D -2 BRWN C -2 GOOK C 2 SCLE D 2 INDN D 2 NMLM D 2 NMLM D 2 NRTM C 2 NRTM C 2 NWSM D 2	1.593 0.897 1.629 1.134 0.351 0.318 1.662 0.317 1.224 1.282 0.133 0.156 0.044 0.086 0.147 0.297 0.144 0.271 0.252	25.395 95.097 55.046 358.534 116.481 136.168 127.506 307.403 274.004 277.157 358.538 235.014 313.842 41.176 69.189 84.187 249.492 35.477 336.696	44.933 82.905 44.933 80.636 88.144 88.459 44.933 88.471 50.438 44.933 93.842 90.861 122.304 100.699 92.032 88.660 92.379 88.912 89.091		1.221 -0.208
ENGN D 2 SWM D 2 BHR D 1 BLNY D 2	0.375 0.360 0.374 0.134	129.277 340.462 170.422 182.958	87.907 88.049 87.917 93.652	1.900 -0.822 0.408 0.125	-1.554 2.316 -2.420 2.416





EVENT		2136		07/71 21 3 4.000 24.83		0 22.85	3.3
AZ1= DIP1= AZ2= DIP2=	7 24	2.000 0.000 0.000 0.942					
SLIP	VECT	ORS=	150.000	20.942	3	11.999	70.000
PRIN	AXES	=	301.569	25.547	1	36.933	65.257
STA	DIR	QUAL	DIST	EVAZ	TCA	X	Υ
CLC CSP GSC ISA MWC PAS PLM PYR RVR SYP BOUQ BRWN GOOK SOLE INDN NAGM NAGM NOMM NRTM		2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1.540 0.855 1.570 1.099 0.329 0.318 1.648 0.336 0.933 1.324 0.110 0.214 0.086 0.034 0.095 0.099 0.251 0.202 0.215	24.443 97.758 55.185 356.359 125.601 146.911 129.513 297.688 116.444 275.439 333.135 234.464 245.331 17.569 72.950 29.765 97.682 244.034 30.995	47.707 83.310 47.707 80.965 88.354 88.459 47.707 88.281 82.557 47.707 97.208 89.454 102.008 130.818 99.512 98.903 89.099 89.571 89.445	0.592 2.328 1.174 -0.146 2.003 1.346 1.103 -2.180 2.088 -1.423 1.056 -2.025 2.022 -0.444 -2.184 -1.141 2.458 -2.239	1.302 -0.317 0.816 2.291 -1.434 -2.066 -0.910 1.144 -1.039 0.136 -2.086 -1.446 0.929 -1.403 -0.670 -1.995 -0.332 -1.090
ENGN SWM IPC HCC BHR BLNY	D D D D C	2 2 2 2 2 2	0.367 0.346 0.444 0.420 0.405 0.176	138.324 331.180 175.566 180.285 177.792 197.699	87.987 88.187 87.247 87.477 87.618 89.877	1.633 -1.186 0.189 -0.012 0.094 -0.759	-1.834 2.155 -2.432 -2.444 -2.446 -2.379



EVENT DATA 75,2254 03/25/71 22 54 0 0 . C 34.000 21.38 -118.000 28.47 4.6 AZ1= 228.000 DIP1= 50.000 AZ2= 131.000 DIP2= 81.736 SLIP VECTORS= 81.736 138.000 50.000 41.000 56.210 PRIN AXES 81.304 185.928 69.336 STA DIR QUAL DIST EVAZ TCA Х Υ BAR D 1 2.250 48.550 0.982 -1.071137.491 CLC C 2 1.625 26.040 48.550 0.638 1.306 83.991 CSP C 1 0.927 93.887 2.360 -C.160 0.221 CWC C 2 2.103 8.744 48.550 1.437 2 48.55C 1.191 0.833 GSC C 1.666 55.046. HFD 1 48.550 1.407 -0.366 2.445 104.587 2.283 2 ISA 1.154 359.920 80.439 -0.003 D 2 MWC C 0.370 111.295 89.556 2.320 -0.904C -2 -1.596 PAS 0.326 129.667 89.994 1.924 2 PYR 1.796 -1.733D 0.306 313.987 90.192 2 RVR C 0.981 111.406 83.445 2.191 -0.859 2 SBC C 1.195 275.115 80.049 -2.265 0.203 SYP C -2 1.254 278.258 48.550 -1.438 0.209 2.700 TIN C 1 48.550 1.450 4.184 0.106 BOUQ 2 0.156 -0.442 -2.456 D 10.195 90.193 BRWN C 2 0.119 234.462 95.985 1.925 1.375 IRON 2 0.077 55.902 105.649 -1.769 -1.198 D 2 GOOK D 0.034 358.488 0.039 -1.471130.818 2 SCLE 0.120 46.824 95.729 -1.730-1.623 D 2 NAGM 0 0.188 42.365 89.706 1.680 1.842 2 NMLM C 0.329 83.012 89.970 2.481 0.304 NWSM 2 D 0.261 344.738 90.647 0.654 -2.398 ENGN C 2 0.387 123.820 89.385 2.066 -1.384 2 NANM 0 0.103 343.409 98.470 0.659 -2.212 IPC D 2 0.401 163.759 89.246 0.695 -2.384 2 HCC D 0.371 168.210 89.551 0.509 -2.438 2 BHR D 0.360 164.956 89.658 0.647 -2.407

167.927

96.508

-0.492

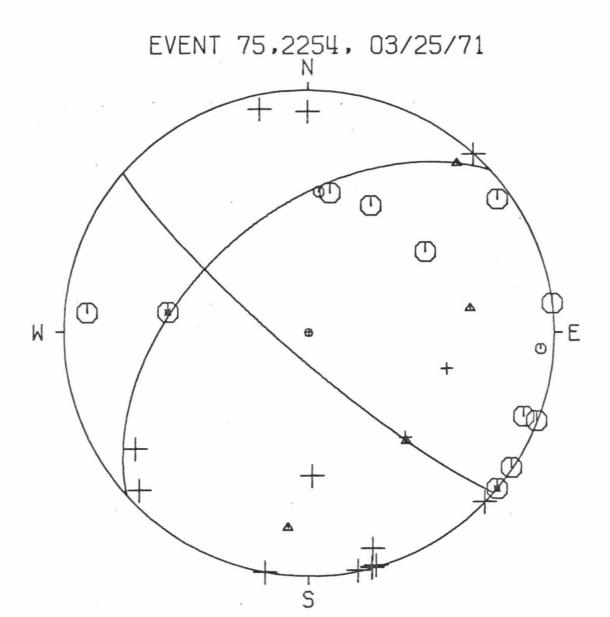
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D

BLNY



EVENT DATA

BLNY

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0.223

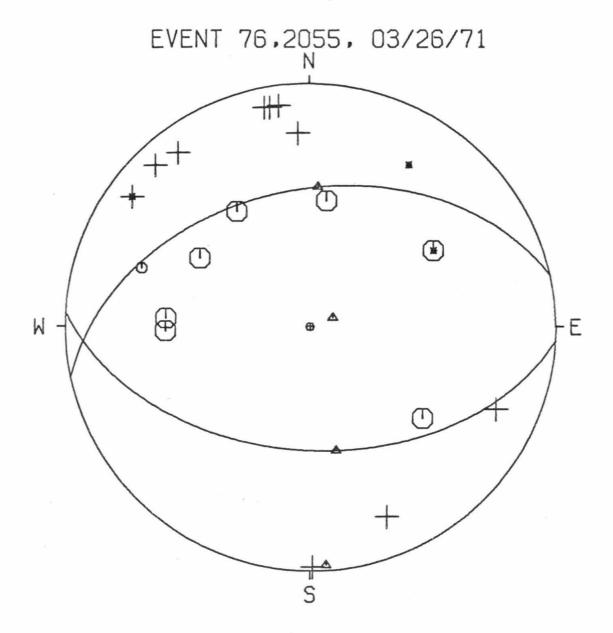
76,2055 03/26/71 20 55 0 11.3 34.000 28.09 -118.000 27.68 3.3 AZI= 93.500 DIP1= 48.000 AZZ= 258.000 DIP2= 43.057 SLIP VECTORS= 168.000 43.057 3.500 48.000 PRIN AXES 68.385 8.191 176.080 87.506 STA DIR QUAL DIST EVAZ . TOA Х Υ -2 GSC C 1.596 49.400 58.105 1.254 0.781 2 ISA D 1.043 359.388 91.980 0.026 -2.456 -2 MWC D 0.414 126.242 100.938 -1.8151.330 PAS D 2 0.400 143.098 101.561 -1.342 1.788 2 PLM C 1.734 129.463 49.400 -0.939 1.141 2 PYR D 0.253 294.037 108.187 -0.845 1.894 2 SBC C 1.202 268.366 49.400 -1.477-0.042 2 SYP C 1.254 273.463 49.400 -1.475 0.089 BRWN -1 0.207 211.202 113.335 1.006 1.662 2 IRCN C 0.099 147.905 133.538 -0.7411.181 2 GOOK C 0.088 187.661 136.681 0.174 1.293 2 SOLE C 0.091 122.012 136.023 -1.1220.702 INDN C 1 0.167 109.385 118.105 -1.7150.603 ENGN 2 0.452 136.518 99.503 -1.572 1.657 D 2 SWM D 0.269 338.064 107.415 0.782 -1.9412 IPC 0 0.507 168.494 98.791 -0.459 2.255 2 HCC D 0.478 172.218 99.160 -0.310 2.271 2 0.467 169.834 99.302 -0.404 2.253 BHR 0

176.601

111.536

-0.118

1.985



EVENT DATA 77,1716 03/28/71 17 16 0.0 34.000 21.28 -118.000 28.39 5.7 3.7 AZ1= 132.000 DIP1= 75.000 AZ2= 225.000 DIP2= 78.947 SLIP VECTORS= 135.000 78.947 42.000 75.000 88.946 71.424 358.066 PRIN AXES 87.280 STA DIR QUAL TOA Y DIST EVAZ Х BAR C 2 2.248 137.485 48.825 0.987 -1.077CLC 2 1.626 25.980 48.825 0.640 D 1.314 93.292 86.521 2.419 -0.139CSP D 1 0.925 2 54.981 48.825 1.197 0.839 GSC C 1.666 ISA 0 2 1.156 359.873 80.423 -0.005 2.283 2 MWC C 0.369 111.125 92.505 -2.280 0.881 C 2 0.325 129.712 92.972 -1.8731.555 PAS 2 PLM C 1.672 126.245 48.825 1.178 -0.864 2 PYR D 0.308 314.065 93.151 1.746 -1.690 2 RVR C 0.979 111.312 85.935 2.245 -0.876 C 2 SBC 1.196 275.264 80.036 -2.264 0.209 2 SYP C 1.256 278.403 48.825 -1.446 0.214 0.157 2 BOUQ D 9.712 90.000 0.422 2.464 2 BRWN C 0.117 236.569 96.245 1.970 1.300 IRON C 2 0.077 54.481 105.649 -1.739-1.241 2 122.304 GOOK D 0.044 357.423 0.077 -1.7042 44.551 95.228 SOLE D 0.124 -1.672-1.698 2 C 66.330 89.757 2.285 1.002 INDN 0.182 2 41.919 89.706 NAGM 0 0.188 1.666 1.855 2 C NMLM 0.328 82.337 92.940 -2.413-0.3252 C NOMM 0.112 249.699 97.046 2.196 0.812 NWSM D 2 0.262 344.582 93.645 0.643 -2.332 2 ENGN C 0.386 123.773 92.321 1.361 -2.036343.097 2 0.105 98.175 -2.215 MANM D 0.673 2 IPC D 0.399 92.176 2.355 163.840 -0.682 2 HCC D 0.369 168.314 92.505 -0.495 2.394 2 BHR D 0.358 165.066 92.615 -0.629 2.360

168.119

97.046

-0.482

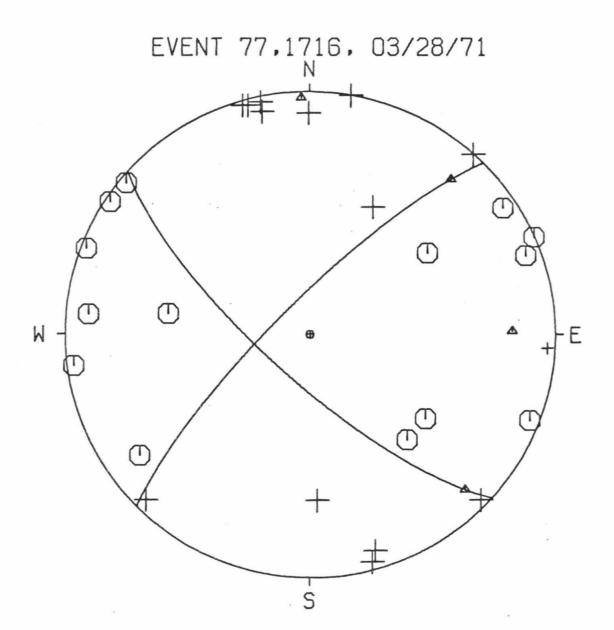
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2

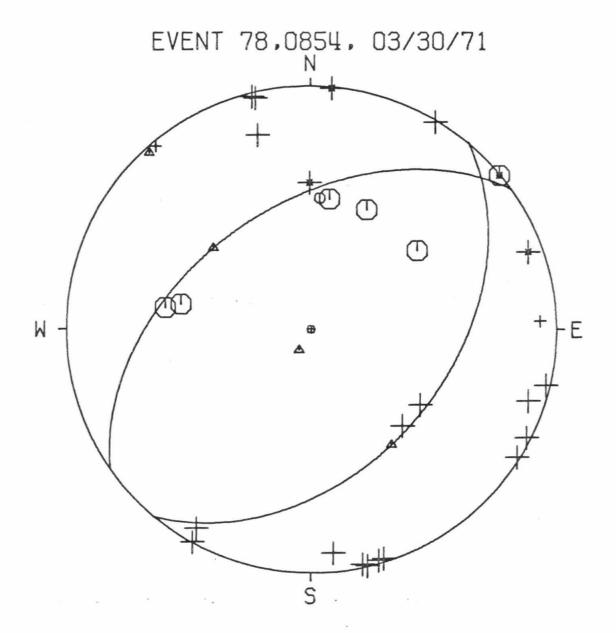
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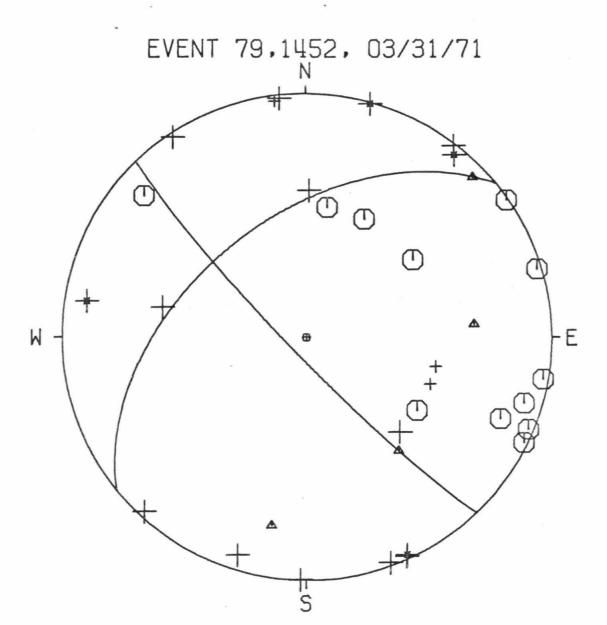
BLNY



EVENT		0854		30/71 8 9 4.000 17.7		27.84	4.1
A Z 2 =	: 4 23	0.000 3.000 5.000 7.989			,		
SLIP	VECT	ORS=	145.000	47.989	30	9.999	43.000
PRIN	AXES	=	209.465	7.954	31	7.823	87.484
STA	DIR	QUAL	DIST	EVAZ	TOA	х	Υ
BAR CLC CSP CWC GSC ISA MWC PAS PLM PYR RVR SBC SYP TIN BOUQ	D D D C C C D	2 2 1 2 2 -2 2 2 2 1 2 2 2 1 2	0.916 2.162 1.695 1.215 0.345 0.285 1.632 0.357 0.953 1.211 1.273 2.760 0.215	24.870 87.885 8.278 53.202 359.560 103.362 121.814 124.741 320.016 108.240 278.504 280.963 3.918 5.048	44.933 44.933 82.719 44.933 50.439 88.193 88.770 44.933 88.086 82.372 50.440 44.933 44.933 89.445	0.568 2.335 0.195 1.082 -0.012 2.394 2.101 1.110 -1.579 2.211 -1.490 -1.326 0.092 0.219	1.506 -0.569 -1.304 -0.770 1.883 -0.729 0.223 0.257 1.348 2.478
BRWN IRON GOOK SOLE INDN NAGM NWSM ENGN SWM NANM HCC IPC BHR BLNY	D D	-2 2 2 -2 2 2 2 2 2 2 2 2 2 2 2	0.112 0.110 0.095 0.163 0.207 0.230 0.322 0.350 0.433 0.163 0.310 0.341 0.300 0.059	250.171 29.818 354.204 28.998 50.538 30.830 346.103 116.601 346.862 346.522 167.528 162.336 163.601 164.925	96.529 96.757 98.730 90.509 89.525 89.302 88.418 88.150 87.359 90.509 88.530 88.237 88.629 108.307	2.214 -1.168 0.233 -1.207 1.922 1.273 -0.592 2.199 -0.555 0.580 0.533 0.747 0.697 -0.538	0.798 -2.037 -2.291 -2.177 1.582 2.134 2.393 -1.101 2.378 -2.420 -2.409 -2.345 -2.369 1.999



EVENT				31/71 14 5 4.000 17.1		30.89	4.6
A Z 1 =	2	31.000					
DIP1=	:	50.000					
AZ2=		36.000					
DIP2=	:	84.070					
SLIP	VEC	TORS=	46.000	84.070	14	1.000	50.000
PRIN	AXE	S =	85.425	58.159	19	90.284	67.576
STA	DIR	QUAL	DIST	EVAZ	TOA	х	Υ
BAR	D	2	2.222	135.611	44.933	0.945	-0.965
CLC	C	2		25.990	44.933		1.214
CMC	C	2	2.178	9.309	44.933	0.219	
GLA	D	1	3.313	110.791	44.933	1.263	-0.480
GSC	C	2		53.752	44.933	1.090	0.799
HFD	D	1	2.461	102.789	44.933	1.318	-0.299
ISA	D	2	1.225	1.316	50.438	0.035	1.506
MWC	C	2	0.384	99.987	87.823 88.471	2.415	-0.425
PLM	C	2	0.317	115.939 123.608	44.933	2.218	-1.079 -0.748
PYR	D	2	0.339	326.507	88.253	-1.358	2.053
RVR	C	2	0.990	106.887	82.016	2.220	-0.674
SBC	D	-2	1.171	279.434		-2.248	0.374
SYP	D	2	1.234	281.758	50.436	-1.475	0.307
BOUQ	D.	-2	0.231	15.311	89.293	0.656	2.396
BRWN	C	2	0.069	292.842	105.211	1.979	-0.834
IRON	D	2	0.143	42.753	92.556	-1.659	-1.794
GOOK	D	2	0.108	17.450	96.988	-0.703.	-2.235
SOLE	D	-2	0.193	38.919	85.812	1.512	1.873
INDN	C	2	0.245	55.437	89.159	2.044	1.408
NAGM	D	2	0.262	37.514	88.989	1.509	1.965
	C	2	0.375	73.347	87.907	2.351	0.703
NWSM	D	2	0.323	353.716	88.406	-0.270	2.450
ENGN	C	2	0.385	112.580	87.818	2.264	-0.941
SWM	D	1	0.434	352.530	87.346	-0.317	2.421
NANM	D	2	0.168	1.372	90.360	-0.060	-2.491
IPC	D	-2	0.347	155.182	88.177	1.033	-2.233
HCC BHR	D D	2	0.313	159.552	88.506	0.862	-2.312
BLNY	C	2	0.305 0.077	155.417	88.579 103.149	1.027	-2.245
DENT	C	2	0.011	131.501	1030147	-1.651	1.450



EVENT		0154		01/71 1 5	54 36.1 4 -118.00	00 35.34	3.4
AZ1= DIP1= AZ2= DIP2=	: 4 26	26.000 6.000 7.000 51.174					
SLIP	VEC1	ORS=	177.000	51.174		36.000	46.000
PRIN	AXES	5 =	112.932	20.851		15.691	87.256
STA	DIR	QUAL	DIST	EVAZ	TOA	х	Υ
CLC CSP GSC MWC PAS PLM PYR RVR SBC SYP BRWN IRON GOOK SOLE INDN NOMM ENGN SWM NANM		1 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1.749 1.020 1.796 0.443 0.366 1.702 0.328 1.043 1.114 1.178 0.040 0.202 0.155 0.250 0.306 0.071 0.436 0.451 0.199 0.361	27.466 87.236 54.351 96.747 109.138 121.857 337.415 104.835 281.155 283.266 357.444 51.626 37.387 46.802 59.040 352.678 106.998 0.595 19.173 144.944	48.975 86.825 48.975 93.275 94.128 48.975 94.556 86.569 85.780 49.400 149.647 105.462 110.101 95.804 94.797 132.226 93.355 93.182 105.747 94.188	0.676 2.427 1.191 -2.411 -2.275 1.245 0.921 2.343 -2.361 -1.438 0.041 -1.678 -1.230 -1.728 -2.052 0.182 -2.320 -0.025 -0.701 -1.383	1.300 0.117 0.854 0.285 0.790 -0.773 -2.215 -0.621 0.466 0.339 -0.925 -1.329 -1.609 -1.622 -1.231 -1.420 0.709 -2.429 -2.016 1.970
HCC BHR BLNY	C C C	1 1 2	0.322 0.320 0.124	147.952 143.924 105.584	94.623 94.644 116.420	-1.272 -1.411 -1.794	2.032 1.937 0.500

EVENT 80,0154, 04/01/71 Ø O (1) W E

EVENT DATA 0 04/01/71 15 3 0.0 81,1503 34.000 24.72 -118.000 25.19 7.1 4.2 117.500 AZ1= DIP1= 68.000 AZ 2= 216.000 DIP2= 69.905 69.905 27.500 SLIP VECTORS= 126.000 68.000 PRIN AXES 77.172 59.481 346.434 88.743 TCA STA DIR QUAL DIST EVAZ X Υ BAR C 2 2.262 139.318 49.175 0.959 -1.116 2 49.175 CLC D 1.556 25.472 0.633 1.328 2 97.316 90.170 CSP C 0.886 -2.476 0.318 CWC D 2 2.042 7.759 49.175 0.199 1.458 2 55.773 49.175 GSC C 1.598 1.216 0.827 1 106.177 49.175 HFD D 2.416 1.413 -0.410 2 87.670 ISA D 1.100 357.843 -0.092 2.447 2 MWC D 0.355 122.452 96.396 -1.989 1.265 2 142.109 PAS D 0.335 96.629 -1.444 1.856 2 49.175 PLM C 1.672 128.747 1.147 -0.921 2 96.927 PYR 0 0.310 300.936 2.011 -1.205 2 C 0.962 115.481 89.289 RVR 2.243 -1.069 2 272.593 49.175 C 1.237 -1.470SBC 0.067 2 -1.464 C 275.666 49.175 SYP 1.293 0.145 49.175 1 TIN D 2.642 3.326 0.085 1.469 121.069 BCUQ D 2 0.103 350.167 0.297 -1.714C -2 229.087 BRWN 0.188 106.828 1.592 1.380 C 2 0.040 152.521 149.647 IRON -0.427 C.821 2 0.059 137.930 GOOK C 230.957 0.986 0.799 2 SOLE C 0.059 45.859 137.930 -0.911 -0.884 INDN C 2 0.128 73.547 115.469 -1.810-0.535 2 0.119 43.251 117.409 NAGM D -1.258-1.3382 NOMM C 0.174 239.189 108.195 1.781 1.062 NWSM 2 0.227 329.965 99.910 D 1.139 -1.969 2 -1.686 ENGN 0.388 134.537 96.013 D 1.659 SWM D 2 0.334 336.217 96.642 0.948 -2.151 2 C 302.632 125.844 NANM 0.088 1.355 -0.868 IPC D 2 0.446 171.389 95.331 -0.356 2.354 2 HCC D 0.420 175.860 95.633 -0.1712.368 2 BHR D 0.406 173.213 95.794 -0.280 2.354 2

187.184

108.639

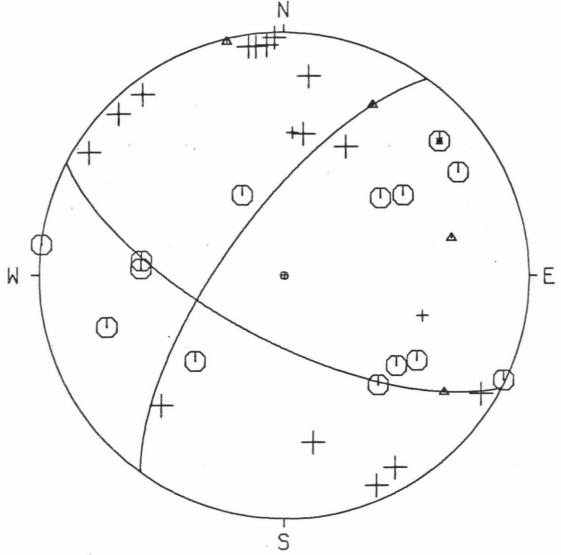
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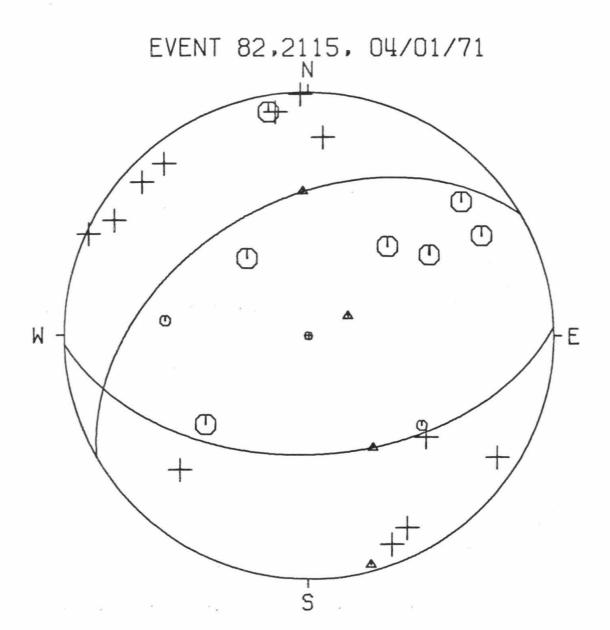
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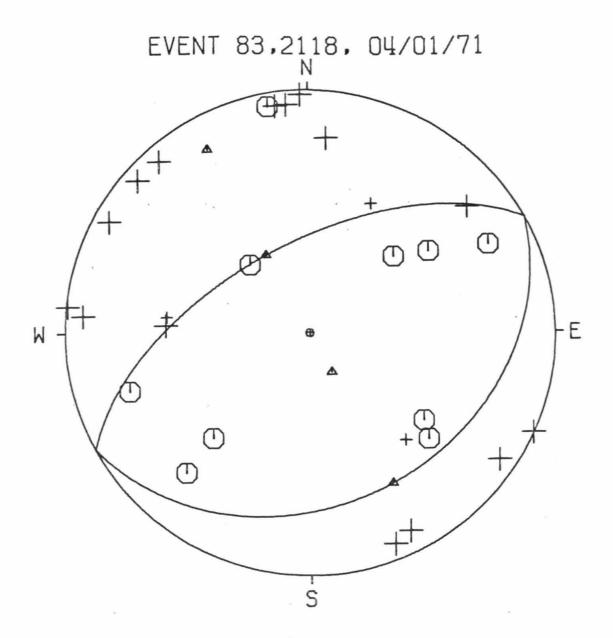




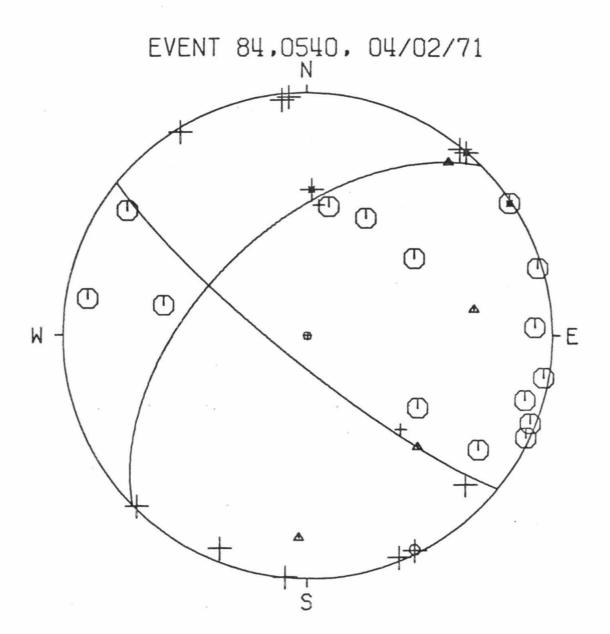
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AZI=		4.000					
AZZ=		88.000					
		9.547					
SLIP	VECT	ORS=	357.999	49.547	15	0.000	44.000
PRIN	AXES	=	63.631	14.664	16	4.650	87.142
STA	DIR	QUAL	TZIO	EVAZ	TOA	×	Υ
GSC	C	2	1.609	55.751	49.375	1.221	0.831
ISA	D	2	1.106	358.271	89.324	-0.075	2.484
MWC	D	2	0.359	120.795	98.483	-1.983	1.182
PAS	D	2	0.336	140.181	98.773	-1.474	1.768
PLM	C	1	1.675	128.370	49.375	1.158	-0.917
PYR	D	2	0.305	302.815	99.147	1.927	-1.242
RVR	D	2	0.967	114.893	91.030	-2.247	1.043
SYP	C	1	1.284	276.016	49.375	-1.469	0.155
BRWN	C	2	0.177	228.581	107.870	1.561	1.377
IRCN	C	2	0.044	141.752	146.728	-0.627	C.795
GOOK	C	2	0.056	221.349	139.546	0.808	0.918
SCLE	C	2	0.069	48.992	133.558	-1.052	-0.915
NAGM	D	2	0.131	43.572	114.853	-1.312	-1.379
NOMM	C	2	0.162	239.805	109.328	1.767	1.028
NWSM	D	2	0.229	332.805	102.478	1.012	-1.969
ENGN	D	2	0.390	132.973	98.105	-1.695	1.579
SWM	D	2	0.337	338.112	98.758	0.858	-2.136
NANM	D	2	0.086	310.690	126.590	1.205	-1.036
IPC	C	2	0.441	170.096	97.476	-0.401	2.297
BHR	D	2	0.402	171.811	97.966	-0.331	2.297
BLNY	Ð	2	0.162	184.248	109.328	0.151	2.039



EVENT				01/71 21 1		00 25.73	3.5
DIP1= AZ2=	24	01.500 80.000 1.500 60.000					
SLIP	VEC1	ORS=	151.500	60.000		331.499	30.000
PRIN	AXES	S =	151.505	15.002		331.500	75.000
STA	DIR	QUAL	DIST	EVAZ	TOA	×	Υ
BAR CLC CSP GSC ISA MWC PAS PLM PYR RVR SBC SYP BRWN IRON GOOK SOLE INDN NAGM NMLM NWSM ENGN SWM	D	2	1.574 0.892 1.613 1.116 0.353 0.327 1.668 0.312 0.962 1.230 1.287 0.172 0.040 0.052 0.074 0.137 0.134 0.289 0.158 0.238	276.509 231.177 139.467 227.579 42.537 72.081 41.427 94.555 243.497	49.225 90.564 49.225 87.914 96.957 97.257 49.225 97.439	0.633 -2.472 1.213 -0.077 -2.040 -1.522 1.158 1.929 2.271 -1.470 -1.463 1.613 -0.602 0.857 -0.992 -1.840 -1.270 -2.319 1.822 1.018 -1.745	1.330 0.275 0.835 2.453 1.154 1.773 -0.910 -1.311 -1.031 0.085 0.167 1.298 0.703 C.783 -1.082 -0.595 -1.439 0.185 0.908 -2.040 1.577 -2.178
NANM IPC HCC BHR BLNY	C D D	2 2 2 2 2	0.091 0.432 0.404 0.391 0.152	312.297 170.094 174.628 171.841 185.161	125.115 96.023 96.351 96.502 110.622	-0.407 -0.221 -0.334	-1.097 2.330 2.347 2.330 2.004



EVENT DATA 84,0540	0 04/0 3.0 34	02/71 5 4 4.000 17.03	40 0.0 3 -118.000	31.70	4.0
AZ1= 225.500 DIP1= 54.000 AZ2= 129.000 DIP2= 81.144					
SLIP VECTORS=	39.000	81.144	13	35.500	54.000
PRIN AXES =	80.875	58.367	18	32.332	72.136
STA DIR QUAL	DIST	EVAZ .	TCA	X	Υ
BAR D 1 CLC C 2 CSP C 2 CWC C 2 GSC C 2 ISA D -2 MWC C 2 PAS C 2 PLM C 2 PYR D 2 RVR C 2 SBC C 2 SYP C 2 TIN D 1 BRWN C 2 IRON D 2 GOOK D 2 SOLE D -2 INDN C -2 NAGM D 2 NMLM C 2 NOMM D 2 NWSM D 2 ENGN C 2	0.970 2.182 1.745 1.227 0.396 0.327 1.670 0.336 1.000 1.160 1.223 2.776 0.063 0.153 0.153 0.115 0.203 0.255 0.271 0.387 0.082 0.325 0.394	135.364 26.288 87.881 9.582 53.906 1.778 100.140 115.169 123.331 328.374 106.603 279.616 281.951 4.962 303.807 44.814 22.237 40.737 56.551 39.072 73.522 313.379 355.721 111.662	44.933 82.208 44.933 44.933 50.437 87.712 88.371 44.933 88.286 81.918 80.381 50.438 44.933 106.968 91.189 96.084 89.562 89.062 88.905 87.798 101.888 88.389 87.726	0.598 2.323 0.225 1.092 0.047 2.411 2.230 1.129 -1.291 2.221 -2.250 -1.474 0.117 1.748 -1.744 -0.895 1.625 2.069 1.561 2.351 1.619 -0.184 2.277	0.086 1.332 0.796 1.506 -0.431 -1.048 -0.742 2.097 -0.662 0.381 0.312 1.346 -1.171 -1.755 -2.188 1.887 1.367 1.922 0.695 -1.530 2.458 -0.904
SWM D 2 NANM D 2 IPC C 1 BHR D 2 HCC D 2 BLNY C 2	0.435 0.170 0.351 0.310 0.315 0.084	354.027 5.115 153.403 153.498 157.532 124.994	87.333 90.287 88.144 88.536 88.482 101.285	-0.254 -0.222 1.101 1.101 0.943 -1.837	2.428 -2.484 -2.199 -2.209 -2.279 1.286



EVENT DATA 85,1114 0 04/15/71 11 14 0.0 34.000 15.88 -118.000 34.62 4.2 4.2 AZI= 113.000 DIP1= 56.000 239.500 AZZ= DIP2= 48.592 SLIP VECTORS= 149.500 48.592 23.000 56.000 80.566 PRIN AXES 30.335 177.695 85.855 STA DIR QUAL DIST EVAZ TCA X Y 87.949 -0.725 ENGN C 0.426 107.165 2.346 2 C 2 GSC 1.789 54.145 48.450 1.176 0.850 ISA 0 2 1.248 3.401 48.45C 0.086 1.448 C 2 96.916 87.879 -0.295 MWC 0.433 2.435 C 2 122.015 48.450 1.230 -0.769 PLM 1.693 C 2 SYP 1.188 283.220 80.116 -2.215 0.520 C 2 2.244 134.260 48.450 1.039 -1.012 BAR C 2 CLC 1.745 27.170 48.45C 0.662 1.291 C 2 CWC 2.208 10.504 48.45C 0.264 1.426 2 RVR C 1.034 104.936 82.037 2.242 -0.598 C 2 SBC 1.124 281.090 81.159 -2.257 0.442 C TIN 1 2.799 5.723 48.450 0.145 1.443 PAS C 2 0.356 109.236 88.626 2.332 -0.814 SWM D 2 0.452 359.343 87.694 -0.028 2.449 -2 BOUQ D 0.270 24.590 89.465 1.035 2.263 2 BRWN D 0.044 344.700 122.304 0.450 -1.645 IKON D 2 0.196 49.208 89.628 1.887 1.628 GOOK D 2 0.149 34.1/85 91.195 -1.390 -2.046 SOLE 0 -2 0.244 45.022. 89.777 1.765 1.764 1.328 1 0.299 57.654 89.178 2.097 INDN D MMON D 2 0.074 345.132 106.545 0.543 -2.043 2 NANM 0.198 16.264 89.609 0.698 2.392 D NWSM D 2 0.343 2.661 88.757 0.115 2.470 2 NMLM C 0.431 72.426 87.896 2.339 0.741 IPC 2 88.637 D 0.355 146.214 1.374 -2.053HCC D 2 0.317 149.438 89.011 1.260 -2.134 2 BHR 0 0.314 145.336 89.035 1.410 -2.039

108.968

96.508

-2.226

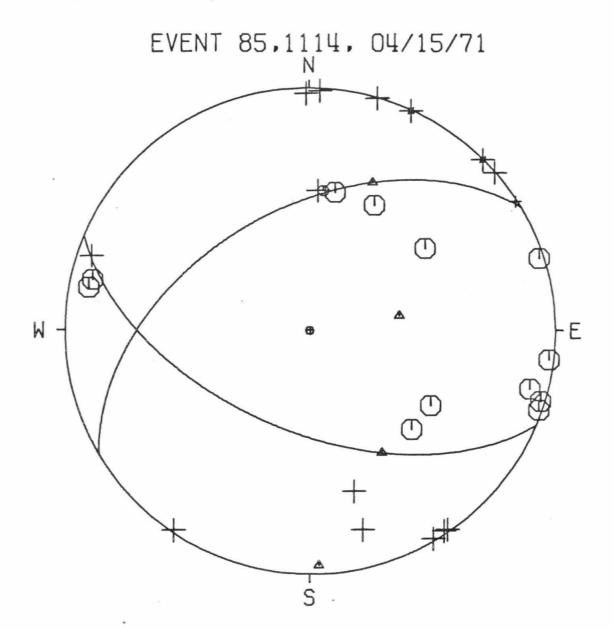
0.765

BLNY

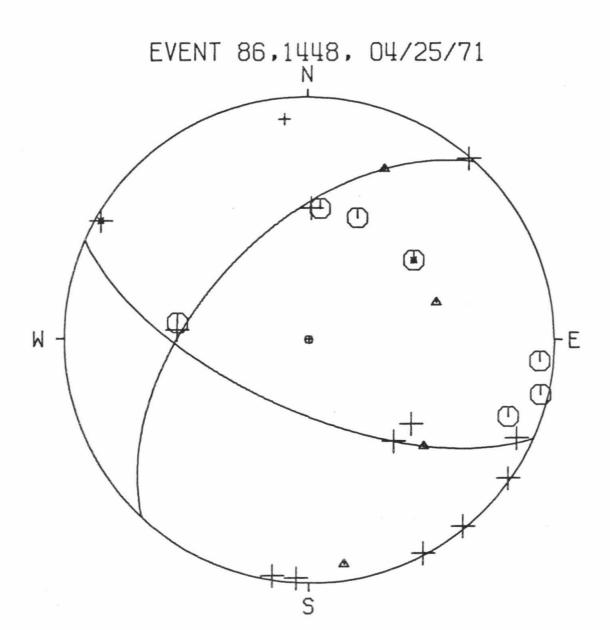
D

2

0.115



EVENT				25/71 14 4			
			3.0 34	.000 22.09	-118.COC	18.86	4.0
AZ1= DIP1= AZ2= DIP2=	= 6 22	4.000 6.000 23.000 53.824					,
SLIP	VEC 1	ORS=	133.000	53.824	2	4.000	66.000
PRIN	AXES	S =	73.544	45.172	17	11.024	82.543
STA	DIR	QUAL	DIST	EVAZ	TCA	X	Υ
ENGN	D	2	0.297	140.485	88.660	1.572	-1.906
CSP	C	2	0.795	95.255	83.881	2.353	-0.216
GSC	C	-2	1.552	52.692	44.933	1.075	C.819
ISA	D	1	1.149	354.067	80.484	-0.236	2.272
MWC	D	2	0.259	124.916	89.025	2.032	-1.419
PLM	D	2	1.577	129.547	44.933	1.042	-0.860
PYR	D	-2	0.406	299.793	87.609	-2.124	1.216
SYP	C	2	1.384	277.143	44.933	-1.341	C.168
BAR	D	2	2.172	140.370	44.933	0.862	-1.041
CLC	С	2	1.561	21.948	44.933	0.505	1.253
CMC	C	2	2.075	5.268	44.933	0.124	1.345
RVR	D	2	0.864	115.453	83.218	2.120	-1.009
SBC	D	2	1.326	274.177	44.933		0.098
TIN	D	2	2.682	1.471	44.933	0.035	1.351
PAS	D	2	0.251	151.876	89.099	1.169	-2.187
IRCN	C	2	0.074	291.214	103.812	2.033	-0.789
GOOK	C	2	0.137		93.279	2.362	-0.560
IPC	D	2	0.398	183.014	87.688	-0.129	-2.446
HCC	D	2	0.379	188.702	87.872	-0.371	-2.425
BLNY	D	2	0.164	221.341	90.471	1.645	1.869



EVENT DATA 87,0425		01/71 4 2 4.000 26.00		24.15	3.6
AZ1= 90.50					
DIP1= 55.00 AZ2= 200.00					
DIP2= 64.51					
0112- 01171	•				
SLIP VECTORS=	110.000	64.511		0.500	55.000
PRIN AXES =	59.174	44.776	32	23.286	84.187
STA DIR QUAL	DIST	EVAZ	TCA	×	Υ
ENGN D 2	0.393	138.220	89.855	1.664	-1.862
CSP C 2	0.875	98.862	84.967	2.359	-0.368
GSC C 2	1.574	56.132	48.600	1.208	0.811
ISA D 2	1.079	357.136	82.903	-0.117	2.338
MWC D 2	0.354	126.422	90.248	-2.007	1.481
PLM 0 -2	1.675	129.631	48.600	1.121	-0.928
PYR D 2	0.312	296.049	90.683	2.233	-1.091
SYP D 2	1.305	274.691	48.600	-1.450	0.119
BAR C 2	2.269	139.949	48.60C	C.936	-1.114
CLC C 2	1.530	25.340	48.600	0.623	1.315
CWC C 2	2.019	7.447	48.60C	0.189	1.443
RVR C 1	0.958	117.028	84.126	2.110	-1.076
PAS D 2	0.344	146.219	90.350	-1.386	2.072
SWM D 2	0.321	332.336	90.589	1.155	-2.203
BOUQ D 1	0.086	338.318	102.335	0.819	-2.060
IRON C 2	0.052	175.692	116.859	-0.139	1.846
GOOK C 2	0.082	227.795	103.943	1.613	1.463
SOLE C 2	0.044	39.728	122.304	-1.090	-1.312
IPC D 2	0.465	173.537	89.125	0.279	-2.465
HCC D 2	0.440	177.923	89.384	0.090	-2.485
BHR D 2	0.426	175.473	89.521	0.197	-2.482
BLNY D 2	0.191	190.720	89.676	-0.464	-2.449

