# ESTIMATION OF THE RADIAL VARIATION OF SEISMIC VELOCITIES AND DENSITY IN THE EARTH

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## ABSTRACT

An inversion procedure is developed to estimate the radial variations of compressional velocity, shear velocity, and density in the Earth. The radial distributions are defined as spherically symmetric averages of the actual distributions in the laterally heterogeneous Earth, and the nature of the averaging implied by averaging certain sets of eigenperiod and travel-time data is examined. For travel-time data, the spherical averaging yields the Terrestrial Monopole if the data sample a distribution derived from a uniform distribution of sources and receivers. Since this is difficult to obtain for absolute times, differential travel times are used to constrain the velocities. It is shown that the bias inherent in available sets of differential travel-time data is considerably less than that in equivalent sets of absolute travel-time data, if the phase combination is suitably chosen. Observations are presented for the phase combinations PcP-P, ScS-S, P'(AB)-P'(DF), and P'(BC)-P'(DF).

The inversion algorithm developed is based on a linear approximation to the perturbation equations and is shown to provide a stable method for estimating the radial distributions of velocities and density from a finite number of inaccurate data. The linear inversion theory presented is complete; it allows one to estimate the resolving power of the data and the resolvability of specified features in the model.

Three estimates of the radial distributions are derived using an extensive set of eigenperiod and travel-time data. One model,

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designated model B1, fits 127 of the 177 eigenperiods of the Dziewonski-Gilbert set within their formal 95% confidence intervals. This model satisfies extensive sets of auxillary data as well.

It is shown from resolving power calculations that little information is lost by using differential travel times in lieu of absolute times. It is demonstrated that the nature of the averaging in the estimation procedure for given sets of gross Earth data can be improved by judicious specification of the norm on the space of models.

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### Chapter 1

#### INTRODUCTION

1.1 <u>Statement of the problem</u>. This thesis addresses the problem of estimating the average radial distributions of compressional velocity, shear velocity, and density in the Earth from the observations of the Earth's mass, moment of inertia, body wave travel times, and periods of free oscillation.

1.2 <u>Motivation</u>. Seismological investigation of the structure of the Earth began with Oldham's correct identification of compressional, shear, and surface waves on seismograms of the Assam earthquake of 1897. Application of the theory of elastic wave propagation to the problem of interpreting seismological data proceeded rapidly, culminating with the publication of the Jeffreys-Bullen and Gutenberg-Richter tables. Bullen [1963, p.3] remarks:

The period from 1911 to 1940 saw the application of seismological data to problems of the Earth's internal structure to a quite remarkable degree. The period started with the vaguest notions about a molten central core and finished with well-determined values of the density, pressure, compressibility, rigidity, and gravity throughout practically the whole Earth.

Despite the progress made in the first part of this century, the problem of describing the variations of elastic parameters and density in the Earth remains an area of vigorous geophysical research. The interest in refining the descriptions currently available is not motivated by some misplaced concern for detail. Rather, it is dictated

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by the critical dependence on these parameters of nearly every inference about the composition and state of the Earth's interior. Much of the attention recently refocused on the problem of Earth structure has been stimulated by three technological advances: the extension of the observable seismic bandwidth to ultra-long periods, the development of laboratory techniques for measuring material properties at high pressures and temperatures, and the advent of the computer.

Ultra-long period seismology, heralded by Benioff's design of the strain seismometer, has provided an important new source of data, the periods of the Earth's free oscillation. Prior to mid-century, the only direct information about the density distribution in the Earth came from measurements of the Earth's gravity field and dynamic response. In particular, Bullen's classical density models were constrained only by the mean density and moment of inertia. The measurements of surface-wave velocities commencing in the 1950's and the reliable observations of free oscillation periods reported since the great Chilian earthquake of 1960 have yielded valuable independent constraints on the possible variations of density.

Additional impetus has come from our increasing knowledge of the behavior of materials at pressures and temperatures appropriate to the Earth's deep interior. To infer the Earth's composition and state, we must compare the density and velocity distributions found from geophysical data with observed material behavior at known conditions. Recent improvements in the precision and range of static compression, ultrasonic, and shock-wave experiments have set the stage for this

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comparison.

Finally, the problem of refining the estimates of Earth structure is feasibly approached only with the aid of modern computing systems. To evaluate the success of any model, the data functionals for that model must be calculated and compared with observations. This can be a laborious task. For example, calculating the eigenperiod of a spheroidal mode requires many numerical integrations of a sixth-order system of differential equations; hand computation of the currently well-observed eigenperiods for even one realistic Earth model is a lifetime effort. However, it takes only a few minutes on a fast computer.

1.3 <u>Approach</u>. To date, efforts towards modeling physical parameters in the Earth have involved only very simple, usually one-dimensional representations. A useful and often adequate approximation is to assume that the Earth behaves as a spherically symmetric, non-rotating, elastic and isotropic body to small mechanical excitations in the seismic frequency band  $(10^{-4} \text{ Hz} - 10 \text{ Hz})$ . We shall adopt these assumptions, thus allowing us to select an Earth model by specifying the compressional velocity, shear velocity, and density as functions of radius alone.

With these assumptions, it becomes feasible to solve the forward problem for a number of gross Earth data functionals (data functionals that depend on the radial variations) for which data are available. These include the Earth's mass and moment, its eigenperiods, and the

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ray-theoretical travel times of signals propagating through its interior. Our approach to the inverse problem of estimating the model given estimates of these data functionals follows closely the treatment of Backus and Gilbert [1967, 1968, 1969, 1970]. The inversion theory used is developed in Chapter 2.

Of course, the observations reflect the fact that the Earth is a rotating, laterally-varying body. The precision with which the data can now be measured is such that contamination by these departures from our assumptions can cause serious incompatibility and bias. We shall try to reduce these effects by using averaged sets of free oscillation and travel-time data. The motivation for this is discussed in Chapter 3.

Unfortunately, with the present-day distribution of seismic sources and receivers it is not possible to sample uniformly the velocity structure of the Earth's upper layers using body waves. For this reason averaged sets of absolute travel-time data generally are biased. At teleseismic distances this bias enters into the distance-time expression as approximately a constant term, called by seismologists the "baseline error". To reduce as much as possible the baseline error without eliminating the valuable information contained in travel-time data, we shall use in the inversion calculations differential travel times; that is, the differences between the arrival times of two body phases. If the phase combinations measured are judiciously chosen, the differential times will be relatively unbiased. In particular, baseline errors will cancel.

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In Chapter 4 the use of differential travel times as gross Earth data is discussed. We also present in this chapter some observations of differential travel times useful in constraining the radial variations of seismic velocities.

These observations are combined in Chapter 5 with eigenperiod data and the observed mass and moment of inertia to derive estimates of the radial velocity and density distributions. Emphasis is placed on the construction of reasonable, but simple representations which are used to initiate the iterative inversion algorithm. This algorithm uses the inversion theory presented in Chapter 2 to provide a perturbation to the starting model which, in a sense that is welldefined, is the "smallest" necessary to satisfy the data. Therefore, the resulting representations will deviate in some least way from the starting model.

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### Chapter 2

### INVERSION THEORY

2.1 Introduction. The task of deducing the constraints provided by observables on the variations of physical parameters in the Earth has been called the geophysical inverse problem. The mathematical formulation of this problem characterizes possible variations as entities in an abstract function space, each entity representing an Earth model. In particular a spherically symmetric, non-rotating, linearly elastic, and isotropic (SNREI) Earth can be described by specifying the compressional velocity, the shear velocity, and the density as functions of radius. An observation is the value of a functional defined on this space of Earth models. Examples include the Earth's mass and moment of inertia, the measured travel times of seismic waves, and the observed periods of free oscillation. We will assume that the forward problem for each data functional has been solved: given any interesting Earth model the value of the data functional can be computed. In general the relationship between the data functional and the model is nonlinear.

Since the distributions of physical parameters are continuous on some interval and the number of data obtainable is necessarily finite, the inverse problem generally has no unique solution. Furthermore, the observations used as data are invariably contaminated by errors; only estimates of the values of data functionals for the

<sup>1</sup>The notation is due to Dahlen [1968].

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Earth are available. Inaccuracies act to increase the ensemble of acceptable models. These circumstances, unfortunate for the geophysicist, make the problem mathematically interesting and motivate the inversion theory presented in this chapter.

A variety of techniques, both theoretical and computational, have been applied towards the solution of the geophysical inverse problem. One potentially powerful technique is the Monte Carlo method described in the geophysical context by Keilis-Borok and Yanovskaya [1967] and applied to the determination of SNREI Earth models by Press [1968,1970,1972]. Monte Carlo calculations utilize a random selection procedure to generate arbitrary models, test the models against a set of data, and display those that satisfy the data sufficiently well. The idea is to sample uniformly some region of the model space thought to contain the best representation of the Earth and generate a fairly complete catalogue of acceptable models. Properties of the real Earth would then be those common to this entire ensemble.

In practice Monte Carlo techniques face severe limitations. Even with the most advanced computing systems, the calculations are laborious and time consuming; the number of trials necessary to sample even very restricted regions of the model space is large. The more efficient algorithms such as the one used by Press [1972] require a sieve-like series of tests against the data: at each of several steps models are rejected or retained depending on how well they satisfy some subset of the data. It is not clear in what

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way these algorithms sample the model space.

A supposed advantage of the Monte Carlo method is that nonlinear data functionals can be used directly without resorting to linear estimation. However, for geophysical inverse problems that use mode data, complete recalculation of the eigenfrequencies for each generated model is economically unfeasible. Instead, first-order variational parameters are used [Press, 1972], eliminating the advantage of Monte Carlo over the linear prediction method.

At the present time the linear prediction method offers the most efficient and informative approach to the solution of the geophysical inverse problem. Basically, this method employs an iterative perturbation algorithm that approximates the difference between the sought representation of the Earth and some initial model as a particular solution to the finite system of linear, inhomogeneous, integral equations relating changes in the model to first-order changes in the data. The data functionals are computed for the starting model and subtracted from the observed data; the system of perturbation equations is solved, and the calculated perturbation is added to the starting model. This process is iterated until the data are satisfied. For the one-dimensional case, this algorithm is simply Newton's method.

The first-order approximation reduces the nonlinear problem to the problem of solving an underdetermined system of linear equations. A general and extensive theory for the solution of the underconstrained linear inverse problem for inaccurately known data has been developed by Backus and Gilbert [1967,1968,1970] in an important series of papers. The central concept in this theory is the following: although

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the exact solution cannot be computed because the information provided by the data is insufficient, it is possible to estimate accurately <u>linear averages</u> of the desired model. The task to which their theory is addressed is the constuction of an optimal inverse filter from the constraints imposed by the observations, through which the correct solution may be viewed. They show that there exists a tradeoff between the ability to resolve detail and the accuracy with which this detail can be estimated. These concepts represent a major contribution to the theory of linear estimation and will see wide use outside the geophysical inverse problem.

Presented here is a variation on the Backus-Gilbert theory that incorporates the stochastic inverse theory of Franklin [1970]. A particular, unique solution to the linear system is obtained by minimizing a specified quadratic measure of error. This quadratic form is the sum of two terms, a measure of the resolution of the estimate and a measure of its accuracy, parameterized to yield a Backus-Gilberttype tradeoff curve. The generalized inverse of Penrose [1955] and Moore [1920] and the stochastic inverse of Franklin [1970] are shown to lie on this tradeoff curve, the stochastic inverse being, in one sense, an optimal point. Any particular solution computed by selecting a point on the tradeoff curve is shown to be an estimate of the correct solution convolved with a projection-like smoothing operator, termed here the response operator of the linear system. Convolving the response operator with delta functions yields Backus-Gilbert-type averaging kernels (except that they are not constrained to be uni-

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modular).

One important aspect of the approach presented here is that the model space is generalized to a Hilbert space with a fairly arbitrary norm, or measure of length. In the application to the construction of velocity and density profiles in the Earth (Chapter 5) the operator defining the norm is chosen to be a "roughing" operator, i.e., the inverse of a smoothing operator. The advantages of generalizing the norm in this way are severalfold. Most importantly, it allows one to introduce information about the solution not directly contained in the data. The "rougher" the norm is, the smoother the particular solution will be. If one is confident, say, that the variation of elastic parameters in some region of the Earth is well-behaved, then the method allows a solution embodying this information (or prejudice) to be constructed. The roughing can be discontinuous - a convenient way to allow for the possibility, or reality, of discontinuities in the model. Also, by manipulating the norm on the model space one can control to some degree the localization of the averaging kernels. Finally, if the roughing operator is chosen to be unbounded (see section 2.6), then the Fréchet kernels for travel times, which are not square-integrable, are members of the model space (this is shown in section 4.2).

Necessarily this introduction has been heuristic and vague. The presentation in the remaining sections of this chapter will be more formal and assumes that the reader has a basic understanding of the Backus-Gilbert theory (see Gilbert [1972] for an elementary treatment).

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2.2 Hilbert spaces of Earth models. A model of a spherically symmetric Earth of radius R is an ordered multiple of functions on the closed interval [0,R]. For example, each SNREI Earth model is described by the function triple  $[v_{p}(r), v_{s}(r), \rho(r)], 0 \le r \le R$ , where  $v_{p}$  is the compressional velocity,  $v_{_{\rm S}}$  is the shear velocity, and  $\rho$  is the density. Although constuction of SNREI Earth models is our ultimate goal, for the purposes of notational simplicity we retain in this chapter a general definition: a spherically symmetric Earth model m is an M-tuple of real-valued, piecewise-continuous functions  $[m_1(r), m_2(r), \dots, m_M(r)]$ defined and integrable on the interval [0,R]. The model m is a member of a vector space  ${f M}$  over the field of real numbers  ${f R}$  if the vector sum of two models m + m' is taken equal to  $[m_1(r) + m'_1(r)]$ ,  $m_2(r) + m'_2(r), \dots, m_M(r) + m'_M(r)$ ]. Formally III is the Cartesian product of M vector spaces,  $\mathfrak{M} = \mathfrak{M}_1 \otimes \mathfrak{M}_2 \otimes \cdots \otimes \mathfrak{M}_M$ . Each  $\mathfrak{M}_1$ , i = 1,2,...,M, is the vector space over R of real, piecewise-continuous functions integrable with respect to a weight w, (r) on the interval [0,R]. The weighting function w<sub>i</sub>(r) must be strictly positive on [0,R] but is otherwise arbitrary.<sup>2</sup>

A linear operator  $L: \mathfrak{M} \rightarrow \mathfrak{V}$  is a single-valued, linear mapping of  $\mathfrak{M}$  into a vector space  $\mathfrak{V}$ . Any linear operator of interest to us here can be represented as an  $\mathfrak{M} \times 1$  array of linear operators

<sup>&</sup>lt;sup>2</sup> Backus and Gilbert in their original 1967 paper used the volume measure  $w_i(r) \propto r^2$ . In this case the measure is singular at the origin; the domain of definition must be restricted to the semi-open interval (0,R], and  $\mathfrak{M}$  consists of functions regular at the origin. In subsequent papers by these authors [1968,1970] and in Chapter 5 of this work,  $w_i(r)$  is chosen to be a constant.

 $[L_i: \mathfrak{M}_i \rightarrow \mathfrak{V}; i = 1, 2, ..., \mathfrak{M}]$ , each characterized by a vector-valued integral kernel  $L_i(r)$ . For any  $m \in \mathfrak{M}$  the element  $L \cdot m \in \mathfrak{V}$  can be computed by integration:

(2.2.1) 
$$\mathbf{L} \cdot \mathbf{m} = \sum_{i=1}^{M} \mathbf{L}_{i} \mathbf{m}_{i} = \sum_{i=1}^{M} \int_{0}^{R} \mathbf{L}_{i}(r) \mathbf{m}_{i}(r) \mathbf{w}_{i}(r) dr$$

The weighting functions  $w_i(r)$  should be chosen to render this product dimensionally homogeneous.

Much of the analysis in this chapter will involve manipulation of linear operators that map the model space into itself. Any interesting linear operator L:  $\mathbb{M} \rightarrow \mathbb{M}$  can be represented as an M × M array of operators [ $L_{ij}: \mathbb{M}_{i} \rightarrow \mathbb{M}_{j}$ ; i,j = 1,2,...,M] with scalar-valued integral kernels  $L_{ij}(r,r')$ . If L has eigenvalues (scalars  $\lambda$  such that L ·  $\psi = \lambda \psi$ ), then, because  $\mathbb{M}$  is defined over R, they must be real.<sup>3</sup>

A class of operators whose eigenvalues are always real are the symmetric operators, for which L(r,r') = L(r',r).<sup>4</sup> If the transpose of L, denoted L<sup>\*</sup>, is defined as the operator with kernel L<sup>\*</sup>(r,r') = L(r',r), then L is symmetric if and only if  $L = L^*$ .

Associated with every symmetric operator L:  $\mathbb{M} \to \mathbb{M}$  is a unique, symmetric bilinear functional

(2.2.2) 
$$\lambda(\mathbf{m}, \mathbf{m}') = \sum_{i,j=1}^{M} \int_{0}^{R} \int_{0}^{R} m_{i}(r) L_{ij}(r,r') m_{j}'(r') \cdot w_{i}(r) dr w_{j}(r') dr',$$

<sup>&</sup>lt;sup>3</sup> Although the spaces we will consider are all real, the theory can be extended in a straightforward manner to spaces defined over the field of complex numbers, permitting the eigenvalues to be complex.

<sup>&</sup>lt;sup>4</sup> Most statements made here are proved in Courant and Hilbert [1937].

and a unique quadratic form

(2.2.3) 
$$\lambda(m) = \lambda(m, m).$$

A symmetric operator and its corresponding bilinear and quadratic forms are said to be positive definite, positive semi-definite, or indefinite depending on whether  $\lambda(\mathbf{m}) > 0$ ,  $\lambda(\mathbf{m}) \ge 0$ , or  $\lambda(\mathbf{m}) \gtrsim 0$  for all  $\mathbf{m} \neq 0$ .

Any symmetric, positive definite bilinear functional can be used as an inner product on  ${
m III}$ . The vector space  ${
m III}$  with an inner product

$$(2.2.4) mtextbf{m'} \equiv \lambda(m,m')$$

defines an inner product space  $\mathbb{M}_{L}$  which can be completed to a Hilbert space. The norm associated with this inner product is

(2.2.5) 
$$||\mathbf{m}||_{L} \equiv \lambda^{1/2}(\mathbf{m}),$$

Any  $m \in \mathbb{M}$  is a member of  $\mathbb{M}_{L}$  if

(2.2.6) 
$$||m||_{L} < \infty$$
.

The super- and subscription of the inner product, the norm, and the Hilbert space are dropped for the special case  $\mathbf{L} = \mathbf{I}$ , the identity operator on  $\mathfrak{M}: \mathbf{m} \cdot \mathbf{m}' \equiv \mathbf{m} \cdot \mathbf{I} \cdot \mathbf{m}' = \sum_{i} \int_{0}^{R} \mathbf{m}_{i}(\mathbf{r}) \mathbf{m}_{i}'(\mathbf{r}) \mathbf{w}_{i}(\mathbf{r}) d\mathbf{r}$  and  $||\mathbf{m}|| = (\mathbf{m} \cdot \mathbf{m})^{1/2}$ .

For our purposes (indeed, for most physical problems) quadratic convergence is sufficient for the identification of vectors. That is, a sequence of vectors {  $\mathbf{m}_{\alpha}$ :  $\alpha = 1, 2, ...$ }, members of  $\mathbb{M}$ , is said to converge to the element  $\mathbf{m} \in \mathbb{M}$  if  $\lim_{\alpha \to 0} || \mathbf{m} - \mathbf{m}_{\alpha}|| = 0$ . 2.3 <u>The perturbation equations</u>. Interesting data functionals such as the mass, moment of inertia, eigenfrequencies, and travel times of an SNREI Earth model are each Fréchet-differentiable. Paraphrasing Backus and Gilbert [1967, p.249] in our own notation, we say that a data functional D on 111 is Fréchet-differentiable at a point m in 111 if there exists a member a of 111, determined by D and m, such that for any member  $\delta m$  of 111

(2.3.1) 
$$D(m + \delta m) = D(m) + a \cdot \delta m + \varepsilon(\delta m)$$

where  $\varepsilon(\delta \mathbf{m}) ||\delta \mathbf{m}||^{-1}$  approaches zero uniformly as  $\delta \mathbf{m}$  approaches zero. The vector  $\mathbf{a}$  is called the Fréchet kernel of D.

Associated with each ordered set  $\mathscr{D}^{\mathbb{N}}$  of N Fréchet-differentiable data functionals and each Earth model m are the linear perturbation equations

(2.3.2) 
$$a_i \cdot \delta m = \delta D_i \equiv D_i (m + \delta m) - D_i (m), \quad i = 1, 2, ..., N,$$

which are correct to first order in  $\delta \mathbf{m}$  . These equations can be written

$$(2.3.3) A \cdot \delta m = \delta d,$$

where  $A = \begin{bmatrix} a \\ 1 \\ . \\ . \\ a \end{bmatrix}$  and  $\delta d = \begin{bmatrix} \delta D_1 \\ . \\ . \\ . \\ \delta D_N \end{bmatrix}$ . The operator A maps a change in the

model into a change in the data. This can be made accurate enough by making  $\delta m$  small enough. The vector  $\delta d$  is a member of the N-dimensional Euclidian space  $E^N$  associated with the set  $\mathscr{D}^N$ . The inner

product between two vectors d and d' in  $E^N$  is written dd' and equals  $\sum_{i=1}^{N} \upsilon_i d_i d'_i$ , the  $\upsilon_i$ , i = 1, 2, ..., N, being positive weights rendering the inner product dimensionally homogeneous.

Suppose  $\epsilon(\delta \mathbf{m}) \in \mathbf{E}^{N}$  is the vector representing the error committed in the linear approximation (2.3.3). Then the constraint

$$(2.3.4) \qquad ||\epsilon(\delta m)|| < \xi, \xi > 0,$$

which limits the error to an open ball in  $\mathbb{E}^{\mathbb{N}}$  about the origin, defines for each point  $m \in \mathbb{M}$  a subset of  $\mathbb{M}$  that is, in general, multiply connected. We will define the domain of A to be  $\mathcal{P}(\xi,m)$ , the simply connected part of this subset that includes the origin. All perturbations in  $\mathcal{P}(\xi,m)$  map into a region  $\mathcal{R}(\xi,m) \subset \mathbb{E}^{\mathbb{N}}$ , the range of A, with an error whose norm is less than  $\xi$ . A vector  $\mathbf{m}' \in \mathcal{P}(\xi,m) + \mathbf{m}$ is said to be  $\xi$ -near  $\mathbf{m}$ .<sup>5</sup> Obviously,  $\mathcal{R}(\xi,m) \subset \mathbb{K}(A)$ , the range space of A (spanned by the eigenvectors of  $A \cdot A^*$ ).

Given a set of N observations  $d_0$  and a starting model  $m_s$ , we define  $\delta d = d_0 - d(m_s)$ . Now the linear inverse problem can be formally stated:

We seek to estimate the difference  $\delta m_0$  between the representation  $m_0$  of the "real" Earth and the initial guess  $m_s$  by an application of some bounded linear operator  $L: E^N \to \mathfrak{M}$  to the duta residual vector  $\delta d$ .

If  $m_0$  is an exact representation of the Earth, if the functionals in  $\mathscr{D}^N$  depend linearly on the model, and if the data are perfectly

<sup>&</sup>lt;sup>5</sup> This is a variation on the terminology used by Backus and Gilbert [1970, p.125].

known, then  $\delta m_0$  can be expected to satisfy equation (2.3.3).<sup>6</sup> If the set  $\mathscr{D}^N$  contains nonlinear data functionals (such as travel times and eigenfrequencies) and if  $m_0$  is  $\xi$ -near  $m_s$ , then  $\delta m_0$  can be expected to satisfy (2.3.3) with an error of norm less than  $\xi$ , again assuming  $d_0$  and  $m_0$  are exact. Thus, in the nonlinear case, the success of the estimate will depend largely upon proper specification of the starting model.

2.4 <u>The generalized inverse</u>. For finite N the problem of computing the solution to (2.3.3) is ill-posed in the sense that the solution is not unique. In fact, it is obvious that A possesses a null manifold  $\mathbb{N}(A)$  of infinite dimension. If  $h \in \mathbb{N}(A)$ , then it solves the homogeneous equation  $A \cdot h = 0$ . The general solution to equation (2.3.3) can be written

(2.4.1) 
$$\delta m = \overline{\delta m} + \sum_{n=1}^{\infty} \alpha_n h_n$$
,

where  $\overline{\delta m}$  is any particular solution to (2.3.3), {  $h_n$ : n = 1, 2, ...} is a basis for  $\mathfrak{N}(\mathbf{A})$ , and the coefficients  $\alpha_n$ , n = 1, 2, ..., are arbitrary scalars. If  $\mathfrak{R}(\mathbf{A}^*)$  is the range space of  $\mathbf{A}^*$ , the space spanned by the set of Fréchet kernels {  $a_i$ : i = 1, 2, ..., N}, then  $\mathfrak{M}$  is the direct sum of  $\mathfrak{N}(\mathbf{A})$  and  $\mathfrak{R}(\mathbf{A}^*)$ .

One particular and interesting solution to (2.3.3) is given by the generalized inverse of A [Moore, 1920; Tseng, 1949; Bjerhammar, 1952; Penrose 1955]. The operator A has a unique generalized inverse

<sup>&</sup>lt;sup>6</sup> Implicit in this statement is the assumption that  $d_0 \in \mathfrak{k}(A)$ .

 $A^{\dagger}: E^{N} \rightarrow III$  such that

(2.4.2) 
$$\begin{array}{rcl} \mathbf{A} \cdot \mathbf{A}^{\dagger} &= & \mathbf{P}_{\mathfrak{K}(\mathbf{A})}, \\ \mathbf{A}^{\dagger} \mathbf{A} &= & \mathbf{P}_{\mathfrak{K}(\mathbf{A})}, \end{array}$$

where  $P_{\mathfrak{L}(A)}$  is the orthogonal projection operator mapping  $\mathbb{E}^{\mathbb{N}}$  onto  $\mathfrak{L}(A)$ , and  $P_{\mathfrak{L}(A)}$  is the orthogonal projection operator mapping  $\mathfrak{M}$  onto  $\mathfrak{L}(A)$ . The estimate

$$(2.4.3) \qquad \overline{\delta m} = A^{\dagger} \delta d$$

is the unique solution that minimizes the norm  $||\delta \mathbf{m}||$ . Substituting (2.3.3) into (2.4.3) and using (2.4.2) we obtain

(2.4.4) 
$$\overline{\delta m} = A^{\dagger} A \cdot \delta d = P_{\mathfrak{K}(A^{\star})} \cdot \delta m.$$

Therefore, the solution given by the generalized inverse corresponds to the orthogonal projection of any solution, in particular  $\delta m_0$ , onto the subspace  $\mathfrak{k}(\mathbf{A}^*)$ .

Using equations (2.4.2) one can easily show that

(2.4.5) 
$$A^{\dagger} = A^{*}(A \cdot A^{*})^{\dagger},$$

reducing the computation of  $A^{\dagger}$  to determining the generalized inverse of a symmetric, positive semi-definite operator on  $E^{N}$ . If A has rank N,  $A \cdot A^{*}$  is positive definite and  $(A \cdot A^{*})^{\dagger} = (A \cdot A^{*})^{-1}$ . Otherwise,  $A \cdot A^{*}$  can be diagonalized by an orthogonal transformation  $U: E^{N} \neq E^{N}; A \cdot A^{*} = U \Delta U^{*}$  where  $\Delta = \text{diag}(\mu_{1}^{2}, \mu_{2}^{2}, \dots, \mu_{N}^{2})$  and the ith column of  $U, u_{1}$ , solves the eigenvalue equation

<sup>&</sup>lt;sup>7</sup> P is an orthogonal projection operator if  $P \cdot P = P$  and  $P^* = P$ .

(2.4.6) 
$$\mathbf{A} \cdot \mathbf{A}^* \mathbf{u}_i = \mu_i^2 \mathbf{u}_i, i = 1, 2, ..., N.$$

Then,  $(\mathbf{A} \cdot \mathbf{A}^*)^{\dagger} = \mathbf{U} \Delta^{\dagger} \mathbf{U}^*$ . Since  $\mathbf{A} \cdot \mathbf{A}^*$  is degenerate, some of the  $\mu_1^2$ 's, say N - K of them, will be zero, and dim $[\mathbf{R}(\mathbf{A} \cdot \mathbf{A}^*)] = K$ . The generalized inverse of  $\mathbf{A} \cdot \mathbf{A}^*$  is easily computed by ordering the eigenvalues so that  $\mu_1^2 \leq \mu_1^2$  if i > j. Then,

(2.4.7) 
$$(\mathbf{A} \cdot \mathbf{A}^*)^\dagger = \sum_{i=1}^K \mu_i^{-2} u_i u_i^*.^8$$

The dyadic  $\mathbf{u}_{i}\mathbf{u}_{i}^{*}: \mathbf{E}^{N} \to \mathbf{E}^{N}$  is the linear operator defined by  $(\mathbf{u}_{i} \mathbf{u}_{i}^{*})\mathbf{v} = (\mathbf{u}_{i}\mathbf{v})\mathbf{u}_{i}, \mathbf{v} \in \mathbf{E}^{N}$ .

The form of equation (2.4.4) illustrates an important point: Since the data kernels are not a complete set, the value of a component  $\delta m_{0i}$ , i = 1,2,...,M, of  $\delta m_0$  at a point  $r \in [0,R]$  cannot be determined. Rather, a linear average

(2.4.8) 
$$\overline{\delta m}_{i}(r) = \sum_{j=1}^{M} \int_{0}^{R} P_{ij}(r,r') \delta m_{0j}(r') w_{j}(r') dr'$$

is obtained. It is desirable to compute an average which is <u>localized</u> at each point. Roughly speaking, this means that we want the ith term in this sum to dominate and the contributions to this term to be small away from the point r.<sup>9</sup> As we add more linearly independent data to the data set, the kernel  $P_{ij}(r,r')$  should look more like the identity kernel  $\delta_{ij}$   $\delta(r-r')$ , where  $\delta_{ij}$  is the Kronecker delta and  $\delta(r-r')$  is

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<sup>&</sup>lt;sup>8</sup> This approach is suggested by Penrose [1955, p.408]. See also the discussions by Lanczos [1961], Wiggins [1972], and Jackson [1972].

<sup>&</sup>lt;sup>9</sup> Backus and Gilbert [1968] provide an exhaustive discussion.

is the Dirac delta distribution. The kernel  $P_{ij}(r,r')$  with i and r fixed is an example of an averaging kernel [Backus and Gilbert, 1968], except that it is not constrained to be unimodular.

In practice, considerations of localization limit the usefulness of the generalized inverse. Backus and Gilbert [1968] examined the kernels of the operator  $P_{\mathbf{R}}(\mathbf{A}^*)$  and found that, for typical sets of eigenfrequency data, the linear averaging associated with this projection was not as localized as averaging kernels obtained by minimizing the integral of the absolute value of the kernel times the weighting function  $(\mathbf{r} - \mathbf{r'})^2$ . The former had better resolution, i.e., the minimum scale length of features not appreciably damped by the averaging was smaller, but had substantially larger sidebands than the latter.

Furthermore, the inverse (2.4.3) was derived under the assumption that the data are perfectly well known. Actually  $\delta d$  is only an estimate of the vector  $\mathbf{A} \cdot \delta \mathbf{m}_0$  that has been corrupted by errors or "noise" entering through observational errors, finite sampling, computational inaccuracies, etc. Neglecting this error can yield model estimates with large statistical uncertainties [Backus and Gilbert, 1970].

These limitations of the generalized inverse can be overcome by appealing to a stochastic formulation of the linear inverse problem.

2.5 <u>The stochastic inverse</u>. The equation corresponding to (2.3.3) for inaccurate data can be cast in the form

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$$(2.5.1) A \cdot \delta m + n = \delta d,$$

where  $\mathbf{n} \in \mathbf{E}^{N}$  is a vector containing the components of noise. Since these components have some unknown scalar value, the error is described only in terms of its statistics. Following Franklin [1970] we consider (2.5.1) to be a sample of the stochastic equation

(2.5.2) 
$$A \cdot p_{e} + p_{p} = p_{d}$$

where  $\mathbf{p}_{\mathbf{s}}$  is the stochastic process describing the solution and is defined over  $\mathbf{M}$ ;  $\mathbf{p}_{\mathbf{n}}$  is the noise process, and  $\mathbf{p}_{\mathbf{d}}$  is the data process, both defined over  $\mathbf{E}^{\mathbf{N}}$ . In its stochastic formulation the inverse problem becomes to construct the best linear unbiased estimate of the solution process  $\mathbf{p}_{\mathbf{s}}$  as an application of some linear operator to the data process  $\mathbf{p}_{\mathbf{d}}$ .

We digress briefly on the properties of stochastic processes that shall be needed for this section.<sup>10</sup> The process  $p_x$  defined over a real, separable Hilbert space  $\mathfrak{l}$  maps an element  $\mathbf{u}$  of  $\mathfrak{l}$  into the random variable  $p_x \mathbf{u}$ . If E{ } is the expectation operator, then the mean  $m_x(\mathbf{u})$  of  $p_x \mathbf{u}$  always equals E{  $p_x \mathbf{u}$  } and is a linear functional on  $\mathfrak{l}$ . The variance of this random variable, since it is the expectation of a square, is a positive semi-definite quadratic form on  $\mathfrak{l}$ ;  $\sigma_x^2(\mathbf{u}) =$  $\mathbb{E}\{(p_x \mathbf{u} - m_x(\mathbf{u}))^2\} = \mathbf{u} C_{xx} \mathbf{u}$ . The linear operator  $C_{xx}: \mathfrak{l} \rightarrow \mathfrak{l}$  is called the autocorrelation operator of the process  $p_x$ . Similarly, for two processes  $p_x$  and  $p_y$  defined over  $\mathfrak{l}$  and  $\mathfrak{V}$  respectively,

<sup>&</sup>lt;sup>10</sup> The reader may refer to Doob [1953] for details and proofs.

there exists a  $C_{xy}: \mathfrak{V} \to \mathfrak{U}$ , called the cross-correlation operator of  $p_x$  and  $p_y$ , such that  $E\{(p_x u - m_x(u))(p_y v - m_y(v))\} = u C_{xy} v$ . Evidently,  $C_{yx} = C_{xy}^*$ .

Since on all spaces quadratic convergence identifies vectors, two stochastic processes  $p_x$  and  $p_{x'}$  defined over  $\mathfrak{l}\mathfrak{l}$  are taken to be identical if  $\mathfrak{m}_x = \mathfrak{m}_{x'}$  and  $C_{xx} = C_{x'x'}$ ; all distributions are equivalently normal. Then a process  $p_x$  can be represented by the decomposition  $\sum_n a_n \mathfrak{u}_n$ , where { $\mathfrak{u}_n$ :  $n = 1, 2, \ldots$ } is some orthonormal basis for  $\mathfrak{l}\mathfrak{l}$  and { $a_n$ :  $n = 1, 2, \ldots$ } is a set of independent Gaussian random variables. The Karhunin-Loève theorem [Loève, 1955, p.478] asserts that  $\mathfrak{u}_n$  is an eigenvector of  $C_{xx}$  and that  $\alpha_n^2$ , the variance of the variable  $a_n$ , is its eigenvalue:

(2.5.3) 
$$C_{xx} = \sum_{n} \alpha_{n}^{2} u_{n} u_{n}^{*}.$$

Returning to the inverse problem, we seek a linear operator B:  $\textbf{E}^N \twoheadrightarrow \textbf{M}$  such that the process

$$(2.5.4) \qquad \qquad \overline{\mathbf{p}_s} = \mathbf{B}\mathbf{p}_d$$

is the best linear unbiased estimate of  $p_s$  given equation (2.5.2) and the Gaussian statistics of  $p_s$  and  $p_n$ .

Any bias can be removed at the outset by subtracting from  $\mathbf{p}_{g}$  and  $\mathbf{p}_{n}$  their expectations, E{  $\mathbf{p}_{g}$ } and E{  $\mathbf{p}_{n}$ }, which are supposed known. We assume this has been done, so that each process in (2.5.2) has zero mean. This will insure that the estimate is unbiased, i.e., E{( $\mathbf{p}_{g} - \overline{\mathbf{p}_{g}}$ )  $\cdot \mathbf{g}$ } = 0 for all  $\mathbf{g} \in \mathbb{M}$ . The process  $\overline{p_s}$  is said to be the best linear estimate of  $p_s$  if it minimizes the variance  $\varepsilon^2(g) \equiv E\{[(p_s - \overline{p_s}) \cdot g]^2\}$  for all  $g \in \mathbb{M}$ . As shown by Franklin [1970], this can be done if the autocorrelation operator  $C_{dd}$  is positive definite. Substitution using (2.5.4) and expansion of the autocorrelation operator of  $p_s - \overline{p_s}$  yields

(2.5.5) 
$$\varepsilon^2(g) = g \cdot C_{ss} \cdot g - 2 g \cdot C_{sd} B^* \cdot g + g \cdot B C_{dd} B^* \cdot g$$
.

The first and second variations of the quadratic functional  $\epsilon^2$  with respect to a variation of the vector  $\mathbf{f} \equiv \mathbf{B}^* \cdot \mathbf{g}$  are

(2.5.6) 
$$\delta(\varepsilon^2) = 2(fC_{dd} - g \cdot C_{sd}) \delta f,$$
$$\delta^2(\varepsilon^2) = 2(fC_{dd} - g \cdot C_{sd}) \delta^2 f + \delta f C_{dd} \delta f.$$

The functional  $\varepsilon^2$  is stationary if and only if  $\delta(\varepsilon^2) = 0$  for all arbitrary variations  $\delta f$ . Therefore the linear combination  $C_{dd} f - C_{ds} \cdot g$  is required to be zero for all  $g \in \mathbb{M}$ . This is true if and only if  $B = C_{sd} C_{dd}^{-1}$ . With this choice the second variation  $\delta^2(\varepsilon^2)$  reduces to the positive definite quadratic form  $\delta f C_{dd} \delta f$ , and the stationary point is a minimum. Therefore the best linear estimate of  $\mathbf{p}_{s}$  is

(2.5.7) 
$$\overline{p_s} = C_{sd} C_{dd}^{-1} p_d$$

The correlation operators in (2.5.7) can be expanded in terms of the correlation operators for  $p_s$  and  $p_n$ , which are supposed known:

(2.5.8)  

$$C_{sd} = C_{ss} \cdot A^* + C_{sn},$$

$$C_{dd} = A \cdot C_{ss} \cdot A^* + A \cdot C_{sn} + C_{ns} \cdot A^* + C_{nn}.$$

It is convenient and usually reasonable to assume that the solution and noise processes are uncorrelated, i.e.,  $C_{sn} = 0$ . With this assumption equations (2.5.8) simplify to

(2.5.9) 
$$C_{gd} = C_{ss} \cdot A^{*},$$
$$C_{dd} = A \cdot C_{ss} \cdot A^{*} + C_{nn}$$

Using (2.5.9) in equation (2.5.7), we obtain for a sample  $\delta d$  of  $\ensuremath{\,p_d}$  the estimate

(2.5.10) 
$$\delta \overline{m} = C_{ss} \cdot A^* (A \cdot C_{ss} \cdot A^* + C_{nn})^{-1} \delta d$$
.

The operator in this equation will be called the stochastic inverse of A.

The statistical information embodied in an emsemble of samples can be used to estimate the autocorrelation operators  $C_{ss}$  and  $C_{nn}$ appearing in (2.5.10). For example, suppose {  $d_1, d_2, \ldots, d_L$ } is a set of L independent observations of the data functionals and assume that the sample mean  $\overline{d} = \frac{1}{L} \sum_{i=1}^{L} d_i$  is an unbiased estimator of  $d_0$ . Then the sample variance matrix

(2.5.11) 
$$V = \frac{1}{L-1} \sum_{i=1}^{L} \sum_{j=1}^{L} (d_i - \overline{d}) (d_j - \overline{d})^*$$

is an unbiased estimator of  $\,C_{\!\!nn}$  . If the data components are statistically independent, then, in the limit L  $\rightarrow$   $^\infty,~V$  converges to the diagonal form

(2.5.12) 
$$C_{nn} = \begin{bmatrix} \sigma_1^2 & \cdots & 0 \\ \vdots & \vdots & \vdots \\ \vdots & \ddots & \vdots \\ 0 & \cdots & \sigma_N^2 \end{bmatrix}$$

When all the variances  $\sigma_i^2$ , i = 1,2,...,N, are nonzero,  $C_{nn}$  will be positive definite, thus insuring that  $C_{dd}$  be positive definite as we have assumed.

If independent samples of  $p_{\rm g}$  are available, a similar procedure can be used to construct an estimate of the autocorrelation operator  $C_{\rm ss}$ . In the geophysical inverse problem this is not the case. Answering questions raised by this fact will be the purpose of the next section.

Of course, using information about the solution and noise processes in deriving an estimate of the solution is not a new idea; its roots lie in the linear filtering and prediction theories of Kolmogoroff and Wiener [Wiener, 1949]. In fact, equation (2.5.10) is analogous to the results of Wiener's theory for the construction of the optimum infinite-lag smoothing filter [Davenport and Root, 1958] and has been explicitly obtained by Strand and Westwater [1968]. It reduces to Twomey's [1963] results for the special case  $C_{\rm ss}=I$ ,  $C_{\rm nn}=\gamma I.$ 

2.6 <u>Specification of the solution autocorrelation operator</u>. As outlined in the previous section, the statistics formed from an ensemble of samples can be used to estimate the autocorrelation operator of a stochastic process. However, at least in the inverse problem that concerns us, this approach cannot be applied to the construction of the solution autocorrelation operator  $C_{ss}$  appearing in (2.5.10). The Earth itself is presumably unique, and the mind twists to imagine what a sample ensemble of  $p_{s}$  might be (the radial variations of elastic

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parameters in a number of Earth-like planets taken at random from our galaxy perhaps?). The resulting notions are generally absurd, and we dismiss the possibility that the probability distribution of  $p_s$  is describable in terms of the limits of relative frequencies. Then we must ask, what is the significance of characterizing the solution as a sample of a Gaussian process with zero expectation and an autocorrelation operator  $C_{ss}$  in this estimation procedure?

To begin to answer this question, we must first examine the behavior of the stochastic inverse in the limit of zero noise. One measure of the size of the noise is the operator norm  $|| C_{nn} ||$ , equal to the largest eigenvalue of  $C_{nn}$ . Suppose for the moment that  $p_s$  is a "white" process, i.e.,  $C_{ss} = I$ . We assert that by requiring  $|| C_{nn} ||$ to be small enough the solution given by the stochastic inverse  $A^s = A^* (A \cdot A^* + C_{nn})^{-1}$  can be made arbitrarily close to the solution given by the generalized inverse  $A^{\dagger}$ . Put more formally, for any  $\varepsilon > 0$  there exists a positive number  $\gamma(\varepsilon)$  such that, if  $|| C_{nn} || < \gamma(\varepsilon)$ , then, for all  $\delta d \neq 0$ ,  $|| A^{\dagger} \delta d - A^s \delta d ||^2 < \varepsilon || \delta d ||^2$ . To show this we first note that  $\gamma(\varepsilon) I - C_{nn}$  will be positive definite, so it is sufficient to find a  $\gamma(\varepsilon)$  such that

(2.6.1) 
$$||[(A \cdot A^*)^{\dagger} - (A \cdot A^* + \gamma I)^{-1}]^* A \cdot A^*[(A \cdot A^*)^{\dagger} - (A \cdot A^* + \gamma I)^{-1}]|| < \varepsilon.$$

Equation (2.4.7) and the completeness relation

(2.6.2) 
$$I = \sum_{i=1}^{N} u_{i} u_{i}^{*}$$

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can be substituted into (2.6.1). Computation shows that the resulting inequality is true when

(2.6.3) 
$$\gamma(\varepsilon) < \mu_K^2 \frac{\mu_K^{\sqrt{\varepsilon}}}{1 - \mu_K^{\sqrt{\varepsilon}}},$$

thus proving the assertion by construction. Using the terminology of A. N. Tikhonov [1963a, 1963b], we say that the stochastic inverse solution  $A^8 \delta d$  regularizes the generalized inverse solution (2.4.3).

Identical arguments can be made to show that equation (2.5.10) regularizes the computation of

(2.6.4) 
$$\overline{\delta m} = C_{ss} \cdot A^* (A \cdot C_{ss} \cdot A^*)^\dagger \delta d$$
,

This solution has a simple geometrical interpretation. Assume that  $C_{ss}$  is positive definite and define L to be the inverse of  $C_{ss}$ :  $L = C_{ss}^{-1}$ .  $C_{ss}$  is idempotent with respect to the product defined in (2.2.4); that is,  $C_{ss} \stackrel{L}{\cdot} C_{ss} = C_{ss}$ . In fact,  $C_{ss}$  is the identity operator on  $\mathfrak{M}_{L}$ . Let  $A_{L} = A \cdot C_{ss}$ , so that equation (2.3.3) becomes

$$(2.6.5) A_L \stackrel{L}{\cdot} \delta m = \delta d .$$

Substituting (2.6.5) into (2.6.4) we obtain

(2.6.6) 
$$\overline{\delta m} = A_L^* (A_L \overset{L}{\cdot} A_L^*)^{\dagger} A_L \overset{L}{\cdot} \delta m.$$

The operator  $P_{\mathfrak{U}(A_{L}^{*})}^{L} \equiv A_{L}^{*}(A_{L} \stackrel{L}{\cdot} A_{L}^{*})^{\dagger}A_{L}$  is an orthogonal projection operator on  $\mathfrak{M}_{L}$  in the sense that  $P_{\mathfrak{U}(A_{L}^{*})}^{L} \stackrel{L}{\cdot} P_{\mathfrak{U}(A_{L}^{*})}^{L} = P_{\mathfrak{U}(A_{L}^{*})}^{L}$  and  $P_{\mathfrak{U}(A_{L}^{*})}^{L*} \equiv P_{\mathfrak{U}(A_{L}^{*})}^{L}$ . Therefore, for perfectly known data, the solution (2.6.4) is the symmetric projection of any solution, in particular  $\delta m_{0}$ , onto the manifold  $\mathfrak{k}(A_{L}^{*}) \subset \mathfrak{M}_{L}$ , the inner product on  $\mathfrak{M}_{L}$  being defined by (2.2.4).  $A_{L}^{\dagger} \equiv A_{L}^{*}(A_{L}^{L}A_{L}^{*})^{\dagger}$  is the generalized inverse of  $A_{L}$ .

As pointed out in §2.1, it will be useful to prescribe the solution autocorrelation operator as a smoothing operator, or, looked at another way, to prescribe the inner product on the model space in terms of a "roughing" operator, the inverse of a smoothing operator. The arguments in the preceeding paragraph were intended to suggest that these viewpoints are identical. The rationale for such a choice can come from either of two considerations: we may wish to incorporate <u>a priori</u> assumptions about the smoothness of the solution, or we may wish to manipulate averaging kernels so that they are, say, more localized.

. To clarify what is meant by choosing the solution autocorrelation operator to be a smoothing operator, we write  $C_{_{SS}}$  in terms of its Karhunin-Loève expansion,

(2.6.7) 
$$C_{ss} = \sum_{n=1}^{\infty} \kappa_n^2 \psi_n \psi_n^*,$$

and assume that the set of eigenvectors {  $\psi_n$ : n = 1,2,...} has been ordered so that, if  $\psi_i$  is smoother (say, has fewer zero crossings) than  $\psi_j$ , then i < j. We will call  $C_{ss}$  a smoothing operator if  $\kappa_i^2 > \kappa_j^2$ for all i < j. Note that the definition implies that any smoothing operator is positive definite. This definition is not the most general one, but it will be convenient for our purposes.

If  $C_{ss}$  is a smoothing operator, then

(2.6.8) 
$$L \equiv C_{ss}^{-1} = \sum_{n=1}^{\infty} \kappa_n^{-2} \psi_n \psi_n^*$$

is a "roughing" operator in the sense that rougher eigenvectors have larger eigenvalues. L can be used to define an ordering on the model space: a model m is said to be smoother than a model m' if

(2.6.9) 
$$\frac{||\mathbf{m}||_{L}}{||\mathbf{m}||} < \frac{||\mathbf{m}'||_{L}}{||\mathbf{m}'||}.$$

Since they are orthogonal projections, the solution (2.4.3) minimizes  $||\delta \mathbf{m}||$  and the solution (2.6.4) minimizes  $||\delta \mathbf{m}||_{L}$ . Therefore, with  $\mathbf{C}_{ss}$  chosen as a smoothing operator, (2.6.4) provides a smoother solution than the generalized inverse.<sup>11</sup>

Since a member of the model space  $\mathfrak{M}$  is an M-tuple of functions on the interval [0,R], defining  $C_{ss}$  to be a smoothing operator does not make much sense. Basically the ordering of the eigenvectors of a smoothing operator requires characterizing them by generalized wavenumbers, or numbers of zero crossings. But the total number of zero crossings of a vector in  $\mathfrak{M}$  does not really coincide with our notion of its smoothness: Suppose  $\psi(r) = [\sin M\pi r/R, 0, ..., 0]$  (M terms) and  $\psi'(r) = [\sin 2\pi r/R, \sin 2\pi r/R, ..., \sin 2\pi r/R]$  (M terms) where M > 2. Now  $\psi$  has fewer (M-1) zero crossings than  $\psi'(M)$ , but intuitively  $\psi$  is not smoother than  $\psi'$ .

To avoid this difficulty comparisons of smoothness will be made component by component. In the example given above  $\psi_1$  ( $\psi_1(r) = \sin M\pi r/R$ ) is less smooth than  $\psi_1$ ', but  $\psi_2$  is smoother than  $\psi_2$ '. One form of the solution autocorrelation operator that is compatible with this decision is

<sup>&</sup>lt;sup>11</sup> This assumes that the solutions are distinct. They will be identical when the eigenvectors of  $C_{_{SS}}$  and  $A^*A$  are the same.

(2.6.10) 
$$C_{ss} = \begin{bmatrix} C_{1} & 0 & \cdots & 0 \\ 0 & C_{2} & \cdots & 0 \\ \vdots & \vdots & \vdots & \vdots \\ \vdots & \vdots & \vdots & \vdots \\ 0 & 0 & \cdots & C_{ss} \end{bmatrix}.$$

Now  $C_i: \mathfrak{M}_i \neq \mathfrak{M}_i$  can be chosen to be a smoothing operator on  $\mathfrak{M}_i$ ,  $i = 1, 2, \ldots, M$ . In this case  $C_{ss}$  will still be positive definite but will not always be a smoothing operator in the strict sense that we have defined the term. If the process  $p_s$  is considered to be an Mtuple of processes  $[p_1, p_2, \ldots, p_M]$ , each  $p_i$  being defined over  $\mathfrak{M}_i$ , then equation (2.6.10) implies that  $E\{(p_i m_i)(p_j m_j)\} = 0$  if  $i \neq j$  for all  $m_i \in \mathfrak{M}_i$  and all  $m_j \in \mathfrak{M}_j$ . The component processes are thus uncorrelated.

An example of the type of smoothing operator that is useful in the practical applications of this theory (such as Chapter 5) can be obtained as the solution to a second-order inhomogeneous differential equation with homogeneous boundary conditions. Consider the problem of constructing a smoothing operator C on the space of functions real-valued and continuous on the interval [a,b],  $0 \le R \le R \le 12$ 

Let  $\Lambda(r)$  be a differential operator of the Sturm-Liouville type;  $\Lambda(r) = \frac{d}{dr} \left[ p(r) \frac{d}{dr} \right] - q(r), r \in [a,b]$ . The differential equation with homogeneous boundary conditions

(2.6.11) 
$$\begin{aligned} & \Lambda(\mathbf{r}) \mathbf{s}(\mathbf{r}) + \mathbf{k}^2 \mathbf{w}(\mathbf{r}) \mathbf{s}(\mathbf{r}) = 0, \\ & \left[ \frac{\mathrm{d}}{\mathrm{d}\mathbf{r}} \mathbf{s}(\mathbf{r}) + \alpha \mathbf{s}(\mathbf{r}) \right]_{\mathbf{r}=\mathbf{a}} = 0, \end{aligned}$$

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<sup>&</sup>lt;sup>12</sup> The interval [a,b] is used instead of [0,R] to allow the construction of autocorrelation operators for functions (processes) expected to be piecewise-continuous. See Chapter 5.

(2.6.11 cont.) 
$$\left[\frac{d}{dr} s(r) + \beta s(r)\right]_{r=b} = 0$$

generates a set of eigenfunctions  $\{s_n: n = 1, 2, ...\}$ , taken to be normalized, that is complete on the interval [a,b] [Morse and Feshbach, 1953]. The eigenvalues  $k_n^2$ , n = 1, 2, ..., can be ordered as a continuously increasing sequence with  $k_1^2 < k_2^2 < \cdots < k_n^2 < \cdots$ . With this ordering the number of nodes in the eigenfunctions on the interval [a,b] also forms a continuously increasing sequence [Morse and Feshbach, 1953, p.722]. We specify the kernel of C in the following form:

(2.6.12) 
$$C(r,r') = \sum_{n=1}^{\infty} \kappa_n^2 s_n(r) s_n(r').$$

For C to be a smoothing operator the sequence of spectral coefficients  $\{\kappa_1^2, \kappa_2^2, \ldots, \kappa_n^2, \ldots\}$  should be continuously decreasing. This will be true if, for a given scalar value of the parameter k,

(2.6.13) 
$$\kappa_n^2 = \frac{k^2}{k^2 + k_n^2}$$
.

Particularized in this way C has the desirable properties that a) its norm is less than or equal to 1, and b) it converges in quadratic mean to the identity operator as k goes to infinity. That is,

 $(2.6.14a) ||C|| \le 1,$ 

(2.6.14b) 
$$\lim_{k \to \infty} ||(I - C) \cdot f \cdot || = 0.$$

The parameter k is simply the mean wave-number of C. It can be easily verified that for this choice of spectral coefficients the kernel of C satisfies the inhomogeneous system

$$[w(r) - k^{-2} \Lambda(r)] C(r,r') = \delta(r-r')$$

$$\left[\frac{d}{dr} C(r,r') + \alpha C(r,r')\right]_{r=a} = 0,$$

$$\left[\frac{d}{dr} C(r,r') + \beta C(r,r')\right]_{r=b} = 0.$$

As an example we solve this system for the special case  $w(r) = p(r) = r_{,}^{2}$ q(r) = 0. In this case (2.6.15) has a regular singular point at r = 0. Solutions to the equations (2.6.11) are the spherical Bessel functions of angular order zero. Solving (2.6.15) we find

(2.6.16) 
$$C(r,r') = \frac{k}{2rr'} \left\{ e^{-k|r-r'|} + D^{-1}[A e^{-k(b-a)}\cosh k(r-r') + B \cosh k(a+b-r-r') + C \sinh k(a+b-r-r')] \right\},$$

where  $A = [1 - a(k+\alpha)][1 + b(k-\beta)],$   $B = \alpha a + \beta b - [k^{2} - k(\alpha+\beta) + \alpha\beta]ab - 1,$  C = k(b-a),  $D = [1 - \alpha a - \beta b + (\alpha\beta-k^{2})ab]sinh k(a-b)$  $- k[b - a + (\beta-\alpha)ab]cosh k(a-b).$ 

Fig. 2.1 shows C(r,r') given by (2.6.16) on the interval (0,1] centered at r' = 0.5 for the case  $\alpha^{-1} = \beta^{-1} = 0$ . In this figure the kernel is displayed for k values of 5, 20, and 50.

2.7 <u>The tradeoff curve</u>. The Backus-Gilbert theory of linear estimation [Backus and Gilbert, 1970] suggests that for the problem described in §2.5 - the estimation of a function given the values of a set of linear data functionals corrupted by noise - there exists a tradeoff between the ability to resolve detail and the reliability of the estimate. In

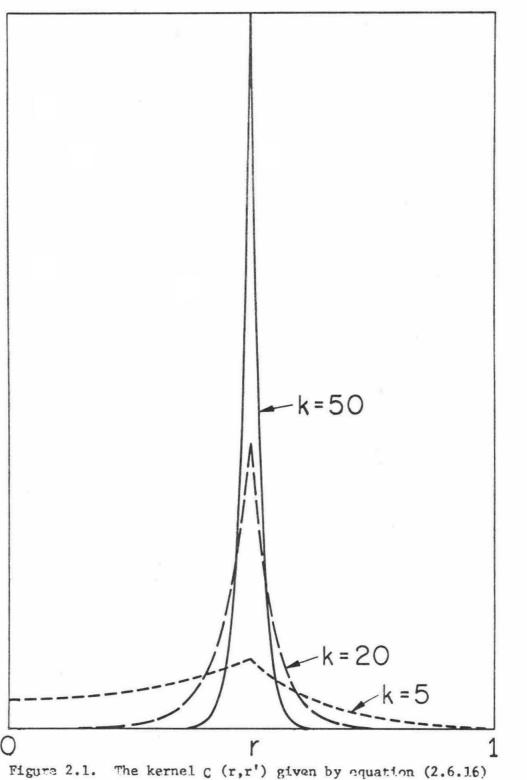


Figure 2.1. The kernel C (r,r') given by equation (2.6.16) on the interval (0,1] centered at r'=1/2 for the case  $\alpha^{-1}=\beta^{-1}=0$ .

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this section we construct a Backus-Gilbert-type tradeoff curve on which the generalized inverse (§2.4) and the stochastic inverse (§2.5) are represented as discrete points. It is shown that the stochastic inverse is an optimal point. The generalized inner product  $\sim \frac{L}{2} \sim$  and norm  $||\sim||_{L}$  introduced in §2.6 are retained throughout the analysis and are assumed to be dimensionless quantities.

An estimate  $\overline{\delta \mathbf{m}}$  of the function  $\delta \mathbf{m}_0$  satisfying

$$(2.7.1) A_{L}^{L} \delta m_{0} + n = \delta d$$

is sought given  $A_L^{\Lambda}$ ,  $\delta d$ , and the statistics of a Gaussian noise process  $p_n$  from which n is a sample. The process  $p_n$  is assumed to have zero expectation and a positive definite autocorrelation operator  $C_{nn}^{\Lambda}$ . The null space  $\mathfrak{N}(A)$  is populated by those members h of  $\mathfrak{M}_L$  for which  $A_L^L h = 0$ . Since the data contain no information about the components of  $\delta m_0$  in  $\mathfrak{N}(A)$ , the estimate  $\overline{\delta m}$  is required to belong to the range space  $\mathfrak{R}(A^*) = \mathfrak{M}_L - \mathfrak{N}(A)$ . This is equivalent to constraining  $\overline{\delta m}$  to be a linear combination of the data kernels:

(2.7.2) 
$$\overline{\delta m} = A_L^* b$$
, for some  $b \in E^N$ .

The vector **b** is to be determined by minimizing an appropriate scalar measure of the error of estimation.

One obvious measure of the error of estimation of  $\delta m_0$  is the norm of the difference between  $\delta m_0$  and  $\overline{\delta m}$ . Define

(2.7.3) 
$$\varepsilon_1^2(b) = ||\delta m_0 - A_L^* b||_L^2$$

The subspaces  $\mathfrak{N}(\mathbf{A})$  and  $\mathfrak{l}(\mathbf{A}^*)$  are orthogonal, so it is clear that the projection of  $\delta \mathbf{m}_0$  onto  $\mathfrak{N}(\mathbf{A})$  contributes to  $\varepsilon_1^2$  its full squared norm regardless of the choice of **b**. In fact,  $\varepsilon_1^2$  is minimized at the value  $||\mathbf{P}_{\mathfrak{N}(\mathbf{A})}^{\mathrm{L}} \circ \mathbf{m}_0||_{\mathrm{L}}^2$  for  $\mathbf{b} = (\mathbf{A}_{\mathrm{L}}^{\mathrm{L}} \mathbf{A}_{\mathrm{L}}^*)^{\dagger} \mathbf{A}_{\mathrm{L}}^{\mathrm{L}} \circ \mathbf{m}_0$ . This is the solution (2.6.6).

Therfore, if the data were perfectly accurate, the best linear estimate of the vector  $\delta \mathbf{m}_0$  would result from the application of the generalized inverse  $\mathbf{A}_L^{\dagger} = \mathbf{A}_L^{\star} (\mathbf{A}_L^{\dagger}, \mathbf{A}_L^{\star})^{\dagger}$  to the data sample vector  $\delta \mathbf{d}$ . However  $\mathbf{n} \neq 0$  implies an uncertainty in  $\delta \mathbf{d}$  and, correspondingly, in  $\overline{\delta \mathbf{m}}$ . A measure of the uncertainty of any estimate of the form (2.7.2) due to noise in the data is the variance  $\varepsilon_2^2$  of the projection of  $\mathbf{p}_n$  onto **b**. By definition,

(2.7.4) 
$$\epsilon_2^2(b) = b C_{nn} b$$
.

Minimizing this error with respect to a variation of  $\mathbf{b}$  yields the trivial solution  $\mathbf{b} = 0$ .

In general the two measures of error  $\varepsilon_1^2$  and  $\varepsilon_2^2$  compete:  $\varepsilon_1^2$  is minimized when  $\varepsilon_2^2$  is largest and vice versa. To explore the possibilities for some sort of compromise, we consider the quadratic measure of error

(2.7.5) 
$$\varepsilon^2(\theta, \mathbf{b}) = \varepsilon_1^2(\mathbf{b}) \cos \theta + \varepsilon_2^2(\mathbf{b}) \sin \theta$$

composed of a weighted sum of the two measures of error. The weighting is parameterized by an angle  $\theta$  that will be allowed to vary on the interval [0, $\pi/2$ ], so that  $\varepsilon^2(0, b) = \varepsilon_1^2(b)$  and  $\varepsilon^2(\pi/2, b) = \varepsilon_2^2(b)$ . For a fixed  $\theta > 0$ ,  $\varepsilon^2(\theta, \mathbf{b})$  can be minimized with respect to a variation of the vector **b**. The first and second variations are

$$\delta(\varepsilon^{2}) = 2[b A_{L}^{L} A_{L}^{*} \delta m_{0}^{L} A_{L}^{*}] \delta b \cos \theta + 2 b C_{nn} \delta b \sin \theta,$$

$$\delta^{2}(\varepsilon^{2}) = [\delta b A_{L}^{L} A_{L}^{*} \delta b + 2(b A_{L}^{L} A_{L}^{*} - \delta m_{0}^{L} A_{L}^{*}) \delta^{2} b] \cos \theta$$

$$+ [\delta b C_{nn} \delta b + 2 b C_{nn} \delta^{2} b] \sin \theta.$$

For the functional  $\epsilon^2(\theta, \mathbf{b})$  to be stationary it is required that

(2.7.7) 
$$(A_{L}^{L}, A_{L}^{*} + \tan \theta C_{nn}) b = A_{L}^{L} \delta m_{0}.$$

If  $\theta > 0$ , then  $A_L^L A_L^* + \tan \theta C_{nn}$  is positive definite, and the unique b that makes  $\varepsilon^2(\theta, b)$  stationary is

(2.7.8) 
$$b(\theta) = (A_{L}^{L} A_{L}^{*} + \tan \theta C_{nn})^{-1} A_{L}^{L} \delta m_{0}.$$

This stationary point is a minimum because the second variation reduces to the positive definite quadratic form

(2.7.9) 
$$\delta^{2}(\epsilon^{2}) = \delta b (A_{L}^{L} A_{L}^{*} \cos \theta + C_{nn} \sin \theta) \delta b.$$

If  $\theta = 0$  and  $A_L$  has rank K < N, then there exists an (N-K)-dimensional manifold of solutions to (2.7.7), and the stationary point is not unique. To obtain a unique solution we may constrain b and its variations to lie in the subspace  $\mathfrak{K}(A_L^L, A_L^*) = \mathfrak{K}(A) \subset E^N$ . Then the choice of b that minimizes (2.7.5) is given by the generalized inverse

(2.7.10) 
$$b(0) = (A_L^L A_L^*)^{\dagger} A_L^L \delta m_0.$$

This choice is the natural one, because, as was shown in §2.6, the

estimate (2.7.2) substituting for b using (2.7.8) regularizes the computation of the generalized inverse solution obtained from (2.7.10) along the path  $\theta \rightarrow 0$ . Realizing that the generalized inverse of a positive definite operator is just its ordinary inverse, we can write

(2.7.11) 
$$b(\theta) = (A_{L}^{L} A_{L}^{*} + \tan \theta C_{nn})^{\dagger} A_{L}^{L} \delta m_{0},$$

for any  $\theta \in [0, \pi/2]$ .

Replacing the vector  $A_L^L \delta m_0$  by its best estimate  $\delta d$  and substituting (2.7.11) into equation (2.7.2) yields for the best linear estimate of  $\delta m_0$  the equation

(2.7.12) 
$$\overline{\delta m}(\theta) = A_{L}^{*}(A_{L}^{L} A_{L}^{*} + \tan \theta C_{nn})^{\dagger} \delta d.$$

Special cases of (2.7.12) include the generalized inverse ( $\theta = 0$ ) and the stochastic inverse ( $\theta = \pi/4$ ).

The estimate  $b(\theta)$  can be put into (2.7.3) and (2.7.4) to obtain  $\varepsilon_1^2$  and  $\varepsilon_2^2$  as functions of  $\theta$ :

(2.7.13) 
$$\varepsilon_1^2(\theta) = ||\delta \mathbf{m}_0 - \mathbf{R}(\theta) \stackrel{\mathbf{L}}{\cdot} \delta \mathbf{m}_0||_{\mathbf{L}}^2,$$
$$\varepsilon_2^2(\theta) = \delta \mathbf{m}_0 \stackrel{\mathbf{L}}{\cdot} \mathbf{V}(\theta) \stackrel{\mathbf{L}}{\cdot} \delta \mathbf{m}_0.$$

The operators  $\mathbf{R}(\theta)$  and  $\mathbf{V}(\theta)$  appearing in these expressions are defined by the equations

$$R(\theta) = A_{L}^{*} Q^{\dagger}(\theta) A_{L},$$

$$V(\theta) = A_{L}^{*} Q^{\dagger}(\theta) C_{nn} Q^{\dagger}(\theta) A_{L},$$

$$Q(\theta) = A_{L}^{L} A_{L}^{*} + \tan \theta C_{nn}.$$

Both  $\mathbf{R}(\theta)$  and  $\mathbf{V}(\theta)$  are positive semi-definite, symmetric operators mapping III onto  $\mathfrak{k}(\mathbf{A}^*)$ .

For  $\delta \mathbf{m}_0$  fixed, equations (2.7.13) determine a curve in the positive quadrant of the  $\varepsilon_1^2 - \varepsilon_2^2$  plane that is parameterized by the angle  $\theta$ . Backus and Gilbert [1970] have termed such graphs <u>tradeoff</u> <u>curves</u>. They have constructed tradeoff curves for the problem of estimating the scalar quantity  $\delta \mathbf{m}_0(\mathbf{r})$  (r fixed). The tradeoff curve given by equations (2.7.13) is for the problem of estimating the vector quantity  $\delta \mathbf{m}_0$ . Nevertheless, the qualitative features of these curves are essentially the same. For any  $\theta \in (0, \pi/2)$ , the expressions for  $\varepsilon_1^2$  and  $\varepsilon_2^2$  can be differentiated with respect to  $\theta$ :

(2.7.15) 
$$\frac{d\varepsilon}{d\theta}^{2} = 2 \delta \mathbf{m}_{0} \stackrel{\mathbf{L}}{\cdot} \frac{d}{d\theta} \stackrel{\mathbf{L}}{\cdot} [\mathbf{R} - \mathbf{C}_{ss}] \stackrel{\mathbf{L}}{\cdot} \delta \mathbf{m}_{0},$$
$$\frac{d\varepsilon}{d\theta}^{2} = 2 \delta \mathbf{m}_{0} \stackrel{\mathbf{L}}{\cdot} \mathbf{A}_{L}^{*} \frac{d\mathbf{Q}}{d\theta} \stackrel{\mathbf{L}}{\cdot} \mathbf{C}_{nn} \mathbf{Q}^{-1} \mathbf{A}_{L} \stackrel{\mathbf{L}}{\cdot} \delta \mathbf{m}_{0}.$$

Now, since  $\frac{d}{d\theta} [QQ^{-1}] = \frac{d}{d\theta} [I] = 0$ , we can write (2.7.16)  $\frac{dQ^{-1}}{d\theta} = -Q^{-1} \frac{dQ}{d\theta} Q^{-1}$ .

The derivative of  $Q(\theta)$  can be computed from (2.7.14):

(2.7.17) 
$$\frac{\mathrm{d}\mathbf{Q}}{\mathrm{d}\theta} = \mathbf{C}_{\mathrm{nn}} \sec^2 \theta.$$

Using (2.7.14), (2.7.16), and (2.7.17) in (2.7.15), we find that

(2.7.18) 
$$\frac{d\varepsilon}{d\theta}^2 = 2 \, \delta \mathbf{m}_0 \stackrel{\mathrm{L}}{\cdot} \mathbf{V}(\theta) \stackrel{\mathrm{L}}{\cdot} \left[ \mathbf{C}_{ss} - \mathbf{R}(\theta) \right] \stackrel{\mathrm{L}}{\cdot} \delta \mathbf{m}_0 \, \sec^2 \theta,$$

and that

(2.7.19) 
$$\frac{d\varepsilon}{d\theta}^2 = -2 \ \delta m_0 \ \dot{L} \ A_L^* Q^{-1} \ C_{nn} \ Q^{-1} \ C_{nn} \ Q^{-1} \ A_L^* \ \delta m_0 \ \sec^2 \theta.$$

 $C_{nn}$  is assumed to be positive definite, and it will be shown in §2.8 that, for a finite number of data, the operator  $[C_{ss} - R(\theta)]$  is positive definite. Therefore, for any  $\delta m_0 \notin \mathfrak{N}(A)$ ,

$$\frac{d\varepsilon}{d\theta} 1^{2} > 0,$$

$$\frac{d\varepsilon}{d\theta} 2^{2} > 0.$$

Now,

$$V(\theta) \stackrel{L}{\bullet} [C_{ss} - R(\theta)] = A_{L}^{*} Q^{-1}(\theta) C_{nn} Q^{-1}(\theta) [Q(\theta) - A_{L}^{*L} A_{L}] Q^{-1}(\theta) A_{L} = A_{L}^{*} Q^{-1}(\theta) C_{nn} Q^{-1}(\theta) C_{nn} Q^{-1}(\theta) A_{L} \tan \theta .$$

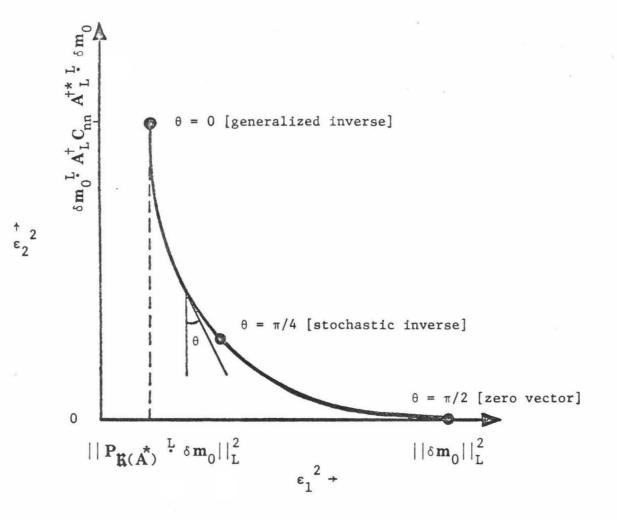
Using this equation in equation (2.7.18) and dividing the results into (2.7.19), we obtain

(2.7.21) 
$$\frac{d[\epsilon_2^2]}{d[\epsilon_1^2]} = -\cot \theta .$$

Equation (2.7.21) can be differentiated with respect to  $\epsilon_1^2$  to yield

(2.7.22) 
$$\frac{d^2[\varepsilon_2^2]}{d[\varepsilon_1^2]^2} = \csc^2 \theta \left[\frac{d \theta}{d[\varepsilon_1^2]}\right].$$

The inequality (2.7.20) implies that this derivative is positive.



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From (2.7.20), (2.7.21), and (2.7.22), we infer that the tradeoff curve between  $\varepsilon_1^2$  and  $\varepsilon_2^2$  is monotonically decreasing and convex towards the origin and that  $\theta$  is the acute angle between the tangent to the tradeoff curve and the  $\varepsilon_2^2$  axis. Therefore,

$$\inf_{\substack{0 < \theta < \pi/2 \\ 0 <$$

A schematic diagram of this tradeoff curve is pictured in Figure 2.2. The qualitative features of this diagram are essentially identical to those of Figure 3 of Backus and Gilbert [1970, p.144].

Backus and Gilbert [1970] point out that it is best to avoid solutions corresponding to extremal values of  $\theta$ . Clearly, the generalized inverse solution [eq.(2.6.4)] is a poor choice on the tradeoff curve. According to Gilbert [1972, p.146], " the place to be is down at the corner." This optimal point can be defined by the equation

(2.7.24) 
$$\frac{d[\epsilon_2^2]}{d[\epsilon_1^2]} = -1.$$

We see from equation (2.7.21) that this point corresponds to the solution (2.5.10) obtained from the stochastic inverse.

2.8 <u>The response operator</u>. For the estimate  $\delta \mathbf{m}(\theta)$  to be useful, we must be able to evaluate how successfully it approximates the desired solution  $\delta \mathbf{m}_0$ . Substituting equation (2.7.11) into equation (2.7.2) we obtain

(2.8.1) 
$$\overline{\delta \mathbf{m}}(\theta) = \mathbf{R}(\theta) \stackrel{\mathrm{L}}{\cdot} \delta \mathbf{m}_{0}.$$

This result is a generalization of equation (2.4.4). The operator  $\mathbf{R}(\theta)$  represents the filter through which we "see"  $\delta \mathbf{m}_0$ . It is optimal in the sense that it minimizes the quadratic form  $\epsilon^2$ . We shall call  $\mathbf{R}(\theta)$  the <u>response operator</u>. For  $\theta = 0$ , the response operator reduces to the projection operator  $\mathbf{P}_{\mathbf{K}}^{\mathbf{L}}(\mathbf{A}_{\mathbf{L}}^{*})$  defined in §2.6. For  $\theta = \pi/4$ , the response operator equals the autocorrelation operator of the process  $\overline{\mathbf{p}_s}$  given by (2.5.7).

Given  $\mathbf{R}(\theta)$  and any  $\mathbf{g} \in \mathbb{M}_{L}$ , we define the <u>relative success</u> of <u>estimation</u>  $\eta_{L}^{2}$  of the vector  $\mathbf{g}$  at  $\theta$  by the equation

(2.8.2) 
$$\eta_{L}^{2}(\theta,g) = \frac{g^{L} R(\theta) \overset{L}{\cdot} g}{g^{L} g}.$$

It can be easily seen that  $0 \leq n_L^2(\theta, g) \leq 1$  for all g. Let  $f = (A_L \stackrel{L}{\cdot} A_L^*)^{\dagger} A_L \stackrel{L}{\cdot} g$ , so that  $g = A_L^* f + P_{\Pi(A_L)}^L \stackrel{L}{\cdot} g$ . Since  $R(\theta)$  is positive semi-definite,  $n_L^2 \geq 0$ . Furthermore, since  $\Pi(R) = \Pi(A_L)$ , it is clear that  $n_L^2 \leq f A_L \stackrel{L}{\cdot} A_L^* Q^{\dagger} A_L \stackrel{L}{\cdot} A_L^* f / f A_L \stackrel{L}{\cdot} A_L^* f$ . Now the term on the right of this expression will be always less than or equal to 1 if  $||Q^{\dagger} A_L \stackrel{L}{\cdot} A_L^* f|| \leq ||f||$ . This inequality holds because  $||A_L \stackrel{L}{\cdot} A_L^*|| \leq ||Q||$ , and we can therefore replace  $A_L \stackrel{L}{\cdot} A_L^*$  by Q.

Thus we conclude that  $\eta_L^2 \leq 1$ . This implies that  $C_{ss}$ -  $R(\theta)$  is a positive semi-definite operator, a fact we used in the previous section.

Suppose that  $R(r,r_0)$  is the kernel of  $R(\theta)$ . From (2.8.1) we see that that this kernel with  $r_0$  fixed is an averaging kernel in  $\mathfrak{M}_L$ ; that is, defines a vector in  $\mathfrak{M}_L$  whose L-product with  $\delta m_0$  is the estimate  $\overline{\delta m}(r_0)$ . In the limit of infinite resolution this kernel will approach the kernel  $C_{ss}(r,r_0)$ . Equivalent averaging kernels in the space  $\mathfrak{M}$  are obtained by applying  $\mathbf{R}$  to the operator  $\mathbf{I}$ . Define

In the limit of infinite resolution the kernel of  $\mathscr{A}$  approaches the kernel I(r,r<sub>0</sub>) which consists of delta functions.  $\mathscr{A}$  and  $\mathbf{R}(\theta)$  are equivalent in the sense that

(2.8.4) 
$$\mathscr{I} \cdot \delta \mathbf{m}_0 = \mathbf{R}(\theta) \stackrel{\mathrm{L}}{\cdot} \delta \mathbf{m}_0.$$

It is usually more convenient to work with  $\mathscr{A}$ , since it does not require comparison with  $C_{ss}$ . We note that  $\mathscr{A}$  is not symmetric.

2.9 <u>The variance operator</u>. In the previous section we saw that the response operator  $\mathbf{R}(\theta)$  is a representation of the inverse filter used to calculate the estimate  $\overline{\delta \mathbf{m}}$ . Examination of this operator (or, equivalently, the operator  $\mathscr{A}$ ) allows one to judge the nature of the averaging required in the estimation of the solution  $\delta \mathbf{m}_0$ . Any features of the solution lost in this averaging are said to be unresolvable. The components in the null space of  $\mathbf{A}$  will obviously be

unresolvable, and, due to the fact that the data are contaminated by errors, it is possible that a component of the solution in the range space of A is unresolvable as well.

A simple quantitative criterion for the resolvability of any vector in the model space can be established in terms of the operator  $V(\theta)$  defined in (2.7.14). This operator represents a transformation of the error autocorrelation operator  $\,C_{\,nn}\,$  into the model space. The eigenvalues of  $V(\theta)$  represent the variances of the errors induced on the model space by errors in the data along directions given by its eigenvectors, motivating us to call  $V(\theta)$  the variance operator. If  $\xi^2$  is an eigenvalue of  $V(\theta)$  associated with the eigenvector v, then the probability that the errors in the data will give rise to an error in the estimate along the direction  ${f v}$  with a magnitude less than 1.96  $\xi$ is 95%. This follows from the fact that the errors are normally distributed and that, for a normal distribution, the integrated probability in the interval [-1.96 × the standard deviation, +1.96 × standard deviation] about the mean is 95%. In general, let k(c) be the factor associated with the confidence coefficient c, so that k(95%) = 1.96.

Now, since the errors are normally distributed, the question of the resolvability of vectors in  $\mathbb{M}$  can be posed as the problem of deciding between two simple hypotheses. Let  $\mathbf{m}$  and  $\mathbf{m}$ ' be two vectors in  $\mathbb{M}$ , and let us ask, are these two vectors resolvable by the observations? Quite obviously, they will not be if the difference between them  $\delta \mathbf{m} = \mathbf{m} - \mathbf{m}$ ' is the zero vector. In the usual fashion of statistical inference [Freeman, 1963] we set up a null hypothesis:

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the vector  $\delta \mathbf{m}$  is the zero vector, and an alternative hypothesis: the vector  $\delta \mathbf{m}$  is not the zero vector. If, on the basis of some criterion, we can reject the null hypothesis, then we shall say that  $\delta \mathbf{m}$  is resolvable.

The most obvious criterion is the following: we reject the null hypothesis if the projection of  $\delta m$  onto  $\mathfrak{k}(A^*)$  lies outside the hyperellipse  $\mathscr{C}[V(\theta)] \subset \mathfrak{k}(A^*)$  whose principal axes are along the eigenvectors  $\mathbf{v}_n$  of  $V(\theta)$  and have lengths  $k(c) \xi_n$ , where c is some chosen confidence coefficient. Translating this geometrical criterion into an algebraic statement, we say that  $\delta m$  is resolvable with a confidence c if

(2.9.1) 
$$\delta \mathbf{m} \cdot \mathbf{V}^{\dagger}(\theta) \cdot \delta \mathbf{m} > \mathbf{k}^{2}(\mathbf{c}).$$

The form of the resolvability criterion given in equation (2.9.1) requires that the error autocorrelation operator  $C_{nn}$  be nonsingular. In fact, because the generalized inverse of  $V(\theta)$  appears in this expression, the computation will be unstable if the error induced on the model space is very small.

#### Chapter 3

# SPHERICALLY SYMMETRIC AVERAGES OF THE EARTH'S VELOCITY AND DENSITY DISTRIBUTIONS

3.1 <u>Introduction</u>. For most seismological purposes, wave propagation in the Earth can be adequately described by specifying the compressional and shear velocities and density at each point in the Earth's interior. At the present time, however, the inverse problem of modeling these three quantities from the observations of wave propagation becomes feasible only if the distributions are taken to be spherically symmetric. For models involving more than one spatial dimension, the foward computation of such data functionals as travel times and eigenperiods is difficult and incredibly laborious. More importantly, the available observations do not contain enough usable information about aspherical variations of velocity and density to warrant inversion. For these reasons we restrict our attention to Earth models that are spherically symmetric.

Approximate spherical symmetry is to be expected. For an isolated, stationary, self-gravitating fluid in its equilibrium configuration, surfaces of constant density, pressure, and therefore velocity are spherical and concentric about its center of mass. Because the strength of the Earth is much less than the hydrostatic pressure throughout most of its interior, its state of stress is very nearly hydrostatic. If the state of the Earth's interior is close to equilibrium, then the density distribution should be approximately spherically symmetric, since the other body forces are small compared to the force of self-

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gravity. Realizing that velocity variations are intimately related to density variations through their dependence on pressure, we should expect approximate spherical symmetry in the velocities as well.

In the early years of seismology, spherical symmetry proved to be an adequate assumption for the purposes of modeling the velocities and density. Indeed, it was not until the 1930's that the errors in travel time observations were reduced to the point that corrections for the Earth's ellipticity were warranted. These corrections, up to four seconds for some phases, were published in the form of tables by Bullen in 1937. Apart from the Earth's ellipticity of figure, which was sufficiently well predicted by hydrostatic theory, aspherical variations for the most part appeared to be confined to the Earth's crust. The existence of lateral differences in the uppermost layers explained reasonably well the fluctuations in travel times at short distances and the differences in surface wave dispersion. The consistency of travel times at distances greater than 20°, evidenced by the similarity of the Jeffreys-Bullen and Gutenberg-Richter tables, provided a strong argument for the spherical symmetry of velocities in the lower mantle and core.

Predictably, modern refinements and diversification of seismic techniques have reduced the standard error of one observation to where most of the scatter in travel times can be attributed to lateral heterogeneity. This is also true for many of the eigenperiods greater than 300 seconds. It now appears that the entire upper mantle is laterally variable and that heterogeneities persist at least to the

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depth of the core-mantle interface. In the light of these facts, we must reexamine the appropriateness of requiring a spherically symmetric representation of the Earth to satisfy data contaminated by the effects of lateral heterogeneities.

Most authors working on the radial variations of velocity using travel times have tried to eliminate lateral effects either by averaging the data or by applying direct corrections for them. The latter procedure is exemplified by the use of station corrections [Herrin and Taggart, 1968]. Unfortunately, this method is limited; it only accounts for anomalies in the vicinity of the receiver - usually only in the form of a constant correction for all distances and azimuths. Some work has progressed on correcting for source anomalies underneath the Aleutian arc using nuclear explosion data and three-dimensional ray tracing techniques [Sorrells <u>et al</u>.,1971; Jacob,1972], but the wide application of this method has been prevented by its complexity and a lack of data.

Applying direct corrections to free oscillation data is even more tedious. McGinley [1968] has treated the effect of some lateral structures on torsional oscillations using perturbation theory, and Dahlen [1968, 1969] has formulated the general first-order perturbation theory for both spheroidal and torsional oscillations using Rayleigh's principle. However, the calculations are too complex and the regional structure of the Earth is too unknown to permit any simple correction to be made to the eigenperiod data.

A more reasonable procedure is to treat the fluctuations due to

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lateral variations as another source of error and simply eliminate them by averaging. This has been the procedure of most investigators since the early work of Jeffreys. It is clear that averaged data contain information about some sort of spherically averaged representation of the Earth. For any estimates to be useful we must know the approximate nature of the spherical averaging, as well as the kind of data distribution required to insure that the sample averages estimate without bias data functionals of this spherically symmetric representation.

Two averaging theorems which provide this information exist, one for eigenfrequencies, due to Gilbert, and one for travel times. The purpose of this chapter is to state these theorems.

3.2 <u>The Terrestrial Monopole</u>. Suppose  $v_p(r,\theta,\phi)$  is the compressional velocity,  $v_s(r,\theta,\phi)$  is the shear velocity, and  $\rho(r,\theta,\phi)$  is the density in the Earth expressed in spherical coordinates with an origin at the Earth's center of mass. Then the spherically symmetric distributions

(3.2.1) 
$$\begin{bmatrix} v_{p0}(r) \\ v_{s0}(r) \\ \rho_{0}(r) \end{bmatrix} = \frac{1}{4\pi} \int_{0}^{2\pi} \int_{0}^{\pi} \begin{bmatrix} v_{p}(r,\theta,\phi) \\ v_{s}(r,\theta,\phi) \\ \rho(r,\theta,\phi) \end{bmatrix} \sin \theta \, d\theta \, d\phi$$

constitute what Gilbert [1972] has termed the Terrestrial Monopole. The velocity and density distributions in the Earth can each be written as the sum of two terms:

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(3.2.2) 
$$\begin{bmatrix} v_{p}(r,\theta,\phi) \\ v_{s}(r,\theta,\phi) \\ \rho(r,\theta,\phi) \end{bmatrix} = \begin{bmatrix} v_{p0}(r) \\ v_{s0}(r) \\ \rho_{0}(r) \end{bmatrix} + \begin{bmatrix} \delta v_{p}(r,\theta,\phi) \\ \delta v_{s}(r,\theta,\phi) \\ \delta \rho(r,\theta,\phi) \end{bmatrix} .$$

The terms  $\delta v_p$ ,  $\delta v_s$ , and  $\delta \rho$  represent the departures from spherical symmetry and average to zero on spheres of constant radius r. If the Earth is nearly spherically symmetric, then these terms will be small compared to  $v_p$ ,  $v_s$ , and  $\rho$ .

3.3 <u>Gilbert's averaging theorem for eigenfrequencies</u>. Because of rotational symmetry, an eigenfrequency of angular order  $\ell$  belonging to to the Terrestrial Monopole is  $(2\ell + 1)$ -fold degenerate. The effect of adding aspherical perturbations as in equation (3.2.2) is to remove this degeneracy. Gilbert [1972] has shown that, to first order in  $\delta v_p$ ,  $\delta v_g$ , and  $\delta \rho$ , the arithmetic average of singlet eigenfrequencies in a mode multiplet split by lateral heterogeneities is the degenerate multiplet eigenfrequency of the Terrestrial Monopole. This result is a direct consequence of the zero sum rule of degenerate perturbation theory and is true for all first-order aspherical perturbations, including those due to rotation and ellipticity.<sup>1</sup>

As Gilbert [1972] points out, this implies that, if the distribution of source and receiver parameters is such that the probability of picking a particular frequency as the "peak frequency" of a mode multiplet has a density equal to the density of singlets at that fre -

<sup>1</sup> Dahlen [1968, p.364] had shown this for ellipticity.

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quency, then the average of many observed peaks is an unbiased estimate of the eigenfrequency belonging to the Terrestrial Monopole.

Because of this averaging theorem, the construction of the Terrestrial Monopole is a logical goal of gross Earth inversion studies that use mode data.

3.4 <u>An averaging theorem for travel times</u>. At the present time, the body of reliable eigenperiod data samples only sparsely those modes with periods less than 300 seconds. Below 300 seconds the normal mode spectrum of the Earth is densely populated, and the identification of individual lines is difficult. Until this deficiency is remedied,<sup>2</sup> better estimates of the density and seismic velocities in the Earth will be obtained by the simultaneous inversion of both eigenperiod and travel-time data. However, for the results of any inversion to have meaning, the sets of averaged eigenperiod data and averaged traveltime data must be consistent in the sense that they average the velocity distributions in roughly the same way.

Most seismologists have seemed contented to define the "average" radial velocity distribution in the Earth to be the one obtained by the inversion of travel-time averages. Quotes are often used around the word <u>average</u> to indicate that the nature of the averaging depends on the distribution of sources and receivers [e.g. Freedman, 1968, p.1270]; there is the general realization that often regions of high seismicity (tectonic regions) and high station density (continental

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<sup>&</sup>lt;sup>2</sup> Dziewonski and Gilbert (personal communication) have turned their attention to this problem and have met with some success.

platforms) receive undue weight and bias this averaging. Intuitively, the average velocity distribution corresponds to the travel-time curve obtained by averaging many observations, each measured from a sourcereceiver pair located at random on the Earth's surface.

These intuitive notions have a solid basis in the following theorem: To first order in  $\delta v$  (P or S), the ray-theoretical surfacefocus travel times between source-receiver pairs at constant angular distance  $\Delta$  are distributed with a mean equal to the travel time  $T_0$  at distance  $\Delta$  through the Terrestrial Monopole, provided the distributions of sources and receivers on the surface of the Earth are uniform.

This result follows directly from Fermat's principle of stationary time. To first order, perturbations of the travel times due to variations in the path are negligible. As a consequence, an integration over all source-receiver geometries to get the mean yields  $T_0(\Delta)$ plus terms containing areal averages of  $\delta v$ , which are zero. A more complete discussion of the proof is given in Appendix 1.

To a good approximation, unbiased estimates of both the travel times and eigenperiods of the Terrestrial Monopole are attainable, making their simultaneous inversion feasible. In practice, the hypothesis of this averaging theorem is difficult to satisfy for absolute travel times - the distributions of sources and receivers on the Earth's surface are certainly not uniform. This motivates the use of differential travel times, discussed in Chapter 4.

Importantly, since no equivalent averaging theorems exist at this

time for amplitude,  $dT/d\Delta$ , and group velocity data functionals, the averages of their observations cannot be as simply interpreted as the averages of travel-time and eigenperiod data. For these reasons we have excluded them from the data sets used in our calculations.

3.5 Other spherically symmetric representations. Abrupt discontinuities are well-established features of the Earth's velocity and density distributions. The Earth's surface and core-mantle interface are the most obvious examples. Since the radii of these discontinuities are variable due to the effects of rotation, lateral heterogeneities, and non-hydrostatic stress differences, averaging over spheres of constant radius to obtain the Terrestrial Monopole " smears them out "; sharp discontinuities become zones of transition. For example, it is observed that the core-mantle boundary reflects considerable compressional energy propagating at periods as low as 1 second. Kanamori [1967] estimates from the spectral amplitudes of PcP phases that a major transition must occur in a layer less than 1 kilometer thick. Now, the ellipticity of the core-mantle interface is about 0.003, so that spherical averaging [equation (3.2.1)] yields a transition region approximately 10 km thick. Large amplitude lateral variations in the radius of this boundary would yield a correspondingly thicker transition zone. This sort of spherically symmetric representation can be inconvenient in theoretical and numerical calculations.

If the variations in the radii of discontinuities are small compared to the radius of the Earth, spherically symmetric averages can

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be defined which preserve these discontinuities and still allow one to make use of the first-order averaging theorems. The prescription is simple: the radii of the discontinuities are first averaged over the sphere, and the resulting distributions are averaged as in equation (3.2.1). Of course, we expect that the difference between this averaged representation and the Terrestrial Monopole will be negligible, at least to first order.

#### Chapter 4

### DIFFERENTIAL TRAVEL TIMES AS GROSS EARTH DATA

4.1 <u>Introduction</u>. A differential travel time is simply the difference between the times of arrival of any two body phases radiated from the same source and recorded at the same station. For example, if the travel time of the phase PcP at distance  $\Delta$  is  $T_{PcP}(\Delta)$  and if the time of P is  $T_{p}(\Delta)$ , then the differential travel time of the phase combination PcP-P equals  $T_{PcP}(\Delta) - T_{p}(\Delta)$  and is denoted  $T_{PcP-P}(\Delta)$ .

Differential travel times have been used for some time by seismologists for locating earthquakes. The differential times of certain phase combinations yield directly good first approximations to the origin time (S-P), the depth (pP-P,sP-P), and the distance (PcP-P, PKKP-P) of an earthquake, and they are often tabulated for use at observatories.

Use has been made of differential times in the construction and verification of absolute travel-time curves. Gutenberg and Richter [1934] used PKKP-P, P'P'-P, and P'P'P'-P times to get the absolute times of PKKP, P'P', and P'P'P'. These phases were recorded only after deep events with poorly constrained hypocenters, and the differential times were relatively insensitive to the depth of focus. In more recent studies, Hales and Roberts [1970 b, 1971] used the differential times of SKS-S, SKKS-SKS, and SKKKS-SKKS to construct travel-time curves for S and K. Bolt [1968] presented some readings of the time  $T_{P'(AB)-P'(DF)}$  to check his determination of the absolute times for the phase P'(AB).

Although differential times have been employed in the study of absolute travel times, the direct use of them to infer the velocity structure has been limited to locating reflectors. If the velocity distribution above a discontinuity is known, then the time between the arrivals of the direct and reflected waves yields an estimate of the depth of the discontinuity. Hales and Roberts [1970 b] used a shear velocity model for the mantle and the differential times of ScS-S to estimate the depth of the core-mantle boundary.

The purpose of this chapter is 1) to demonstrate that the differential travel times of particular phase combinations are an excellent source of gross Earth data and are relatively uncontaminated by the systematic errors that corrupt absolute travel time data, and 2) to present some observations of  $T_{PCP-P}$ ,  $T_{SCS-S}$ ,  $T_{P'(AB)-P'(DF)}$ , and  $T_{P'(BC)-P'(DF)}$ . The observations are included in the data sets used in Chapter 5 to derive estimates of the radial variation of seismic velocities and density. We begin with a general discussion on the inversion of travel-time data.

4.2 <u>Inversion of travel-time data</u>. The classical work of Herglotz [1907] and Wiechert [1910] established a constructive existence and uniqueness theorem for the solution of the travel-time inverse problem in a radially stratified medium, subject to certain assumptions. Their method has been used extensively in seismology to construct profiles of elastic-wave velocities in the Earth from the observations of travel times. A number of authors [Slichter, 1932; Gerver and Markushevich,

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1967; Backus and Gilbert, 1969; Johnson, 1971] have pointed out the various inadequacies of this theory in its application to real data and the real Earth. To be strictly valid, the Herglotz-Wiechert procedure requires that the velocity gradient dv/dr be everywhere less than v/r and that the ray-parameter - distance relationship be perfectly well known at almost all distances. Of course, in practice neither requirement can be realized. Only a finite number of data can be obtained, and both shadow zones in the Earth and errors in the data do exist.

These reasons motivate the use of a linear theory, such as the one in Chapter 2, to solve the inverse problem. The linear formulation, equation (2.3.3), utilizes the spherically symmetric Fréchet kernels to relate changes in the model to changes in the data functionals. For travel times the spherically symmetric Fréchet kernel is given by equation (Al.2.5). Using (Al.1.4) and (Al.2.3), we see that this kernel can be written

(4.2.1) 
$$a(r) = \sum_{i=1}^{n+1} \frac{-\eta(r)}{v_0^2(r) (\eta^2(r) - p^2)^{1/2}} H[\varepsilon_i(r - \rho_{i-1})]$$
$$\cdot H[\varepsilon_i(\rho_i - r)], \quad 0 \le r \le R,$$

where  $\eta(r) = r/v_0(r)$  and p is the parameter of the ray. If any of the turning radii  $\rho_i$ , i = 1,2,...,n, equal the classical turning radius  $\rho = p v_0(\rho)$ , then the kernel has a square-root singularity at  $r = \rho$ .

We can easily show that this singularity is integrable. That

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is, it can be shown

(4.2.2) 
$$I[a] \equiv \int_0^R a(r) dr < \infty$$
.

The integral I[a] is an improper integral of the second kind, and according to Gradshteyn and Ryzhik [1965], the integral is bounded if there exists a scalar  $\alpha < 1$  such that

(4.2.3) 
$$\lim_{r \to 0} [(r - \rho)^{\alpha} a(r)] < \infty.$$

Now,  $a(r) \propto (r - [v_0(r)/v_0(\rho)] \rho)^{-1/2}$ , the other factors being always bounded, so that (4.2.3) is true if  $\alpha \ge 1/2$  and if  $v_0$  is continuous at  $\rho$ . Therefore, the integral exists at all but isolated values of p.

Although a(r) is integrable, its square obviously is not. This means that the Fréchet kernel relating changes in velocity to firstorder changes in travel time is not a member of the Hilbert space of square-integrable functions, a fact that is the source of some theoretical difficulty. The linear theory requires that the Fréchet kernels belong to the space of Earth models. Since Backus and Gilbert [1967] take this to be the Hilbert space of square-integrable functions, travel time data cannot be inverted directly for velocity using their procedure. To avoid this difficulty, Backus and Gilbert [1969] and Johnson [1971] integrate the perturbation equation [equation (2.3.2)] by parts, yielding an equation relating a change in a <u>derivative</u> of velocity to a change in travel-time. The Fréchet kernel in this new equation is an integral of a(r) and is square-integrable. As Johnson [1971] points out, this procedure is an example of what Backus [1970b] has called a linear quelling by integration.

The fact that a(r) is not square-integrable presents no difficulty if the inner product on the model space is suitably chosen.<sup>1</sup> The Fréchet kernel a(r) relates a spherically symmetric velocity variation  $\delta v(r)$  to its corresponding first-order perturbation  $\delta T$  in travel time by the equation

(4.2.4) 
$$\int_0^R a(r) \, \delta v(r) \, dr = \delta T.$$

If the inner product on the model space is defined as the bilinear form associated with the positive definite symmetric kernel L(r,r'), then we noted in §2.6 that the Fréchet kernel is

(4.2.5) 
$$a_{L}(r) = \int_{0}^{R} L^{-1}(r,r') a(r') dr',$$

so that the perturbation equation (4.2.4) becomes

(4.2.6) 
$$\int_0^R \int_0^R a_L(r) L(r,r') \delta v(r') dr dr' = \delta T.$$

Now, the kernel  $a_{I}(r)$  belongs to the model space if

(4.2.7) 
$$\int_0^R \int_0^R a_L(r) L(r,r') a_L(r') dr dr' < \infty$$

This inequality is satisfied if the integral

(4.2.8) 
$$\int_{0}^{R} \int_{0}^{R} a(r) C(r,r') a(r') dr dr'$$

is bounded, where  $C(r,r') \equiv L^{-1}(r,r')$ . It is easy to show that

<sup>&</sup>lt;sup>1</sup> Generalization of the inner product on the model space is discussed in Chapter 2. The notation used in this section is compatible with the notation used in Chapter 2 if M = 1 and w(r) = 1.

(4.2.8) is bounded if we specify C(r,r') by the expansion

(4.2.9) 
$$C(r,r') = \sum_{n=1}^{\infty} \frac{k^2}{k^2 + n^2 \pi^2} s_n(r) s_n(r'),$$

where  $s_n(r) = 2^{-1/2} \sin n\pi r$  for all positive integers n.<sup>2</sup> Substituting (4.2.9) into (4.2.8), we obtain

(4.2.10) 
$$\sum_{n=1}^{\infty} \frac{k^2}{k^2 + n^2 \pi^2} \left[ \int_0^R a(r) s_n(r) dr \right]^2,$$

which we assert is bounded. The assertion is verified by noting that the integral in the brackets is always less than or equal to  $2^{-1/2}$  I[a], a constant for all n. Therefore, (4.2.10) converges as  $n^{-2}$ , and  $a_{L}(r)$ belongs to the model space.

Since the characteristic wave-number  $k_n$  of the system (2.6.11) is always proportional to n, the travel-time Fréchet kernel (4.2.1) will belong to any model space for which C(r,r') (=  $L^{-1}(r,r')$ ) satisfies the system (2.6.15). In the terminology of Backus [1970b], equation (4.2.5) is a linear quelling by convolution.

Travel-time data can thus be inverted using the theory developed in Chapter 2.

## 4.3 A comparison of systematic errors in absolute and differential

travel times. Because a differential travel time is a linear combination of absolute travel times, the theory presented in the previous section and the averaging theorem for travel times given in §3.4 for

<sup>&</sup>lt;sup>2</sup> It can be shown that C(r,r') satisfies (2.6.15) with p(r) = w(r) = 1, q(r) = 0. Since  $f_0(r) = (\sin r)/r$ , C(r,r') equals the product of the kernel given in (2.6.16) and the factor rr'.

absolute times can be applied <u>verbatum</u> to differential times. In this section we argue that the systematic errors in particular differential travel times are generally much less than the systematic errors in the corresponding absolute travel times. For this reason differential travel-time data will be used in lieu of absolute travel-time data in the numerical inversions presented in Chapter 5.

The statistical uncertainties in estimating mean travel times calculated from sample dispersion are generally small, as low as ±0.06 seconds (standard error in the mean) for direct teleseismic P waves in the 1968 Tables [Arnold, 1968]. For Gaussian processes the standard error in the mean is inversely proportional to the square-root of the sample size, and it can be arbitrarily reduced simply by increasing the number of measurements. But statistics of this type adequately measure the error only if the error process has zero mean - the sample averages of existing travel-time data are severely biased by systematic errors introduced in the mislocation of earthquakes, incorrect identification of arrival times, poor sampling of lateral heterogeneities, the inadequacies of ray theory, etc.

Because we cannot easily account for their effect on model estimates, these systematic errors must be reduced to insignificance. Obviously, systematic errors are not reduced simply by increasing the sample size. If independently estimated, they can be subtracted. For travel times this procedure involves estimating source and station anomalies, calculating corrections for ellipticity, and the like.

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The difficulties involved with this approach were mentioned in §3.1. An alternative is to use differential travel times. The idea is the following: A differential travel time is the difference between two absolute travel times. If the absolute times are systematically in error by the same amount, their difference will be an unbiased quantity.

The relative effect of some systematic errors on the differential times of PcP-P, ScS-S, P'(AB)-P'(DF), and P'(BC)-P'(DF) and on their corresponding absolute times for an earthquake 600 km deep can be evaluated using Table 4.1. (Further discussion of these phase combinations and some observations of their differential travel times are presented in the next section.) We consider the following sources of systematic error:

Origin time and location errors. Before the use of nuclear explosions as sources and before the advent of the WWSSN, origin time and location errors were the most serious concern of seismologists. These errors are now much reduced. However, locating earthquakes and modifying travel-time tables is still a "bootstrap" procedure and is susceptible to bias. Of course, for differential travel times, origin time errors cancel uniquely. The difference in travel time  $\delta T$  resulting from a mislocation  $\delta \Delta$  in angular distance and  $\delta h$  in depth is given approximately by the formula

(4.3.1) 
$$\delta T = \begin{bmatrix} \frac{\partial T}{\partial \Delta} \end{bmatrix} \delta \Delta + \begin{bmatrix} \frac{\partial T}{\partial h} \end{bmatrix} \delta h .$$

The values of the derivatives in (4.3.1) have been computed for several

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Parameters for estimating the sensitivity of travel times to bias

|                                  | 1    |       |                 |                 |                     |                  |                  |                  |
|----------------------------------|------|-------|-----------------|-----------------|---------------------|------------------|------------------|------------------|
| 600 km<br> X-Y                   | 30   | 14    | 52              | 9               | 2                   | 5                | 0                | Ч                |
| above<br>Y                       | 102  | 90    | 182             | 143             | 72                  | 11               | 72               | 71               |
| seconds above 600 km<br>X Y  X-Y | 72   | 76    | 130             | 137             | 74                  | 76               | 72               | 72               |
| 00km)<br>X-Y                     | 5.3  | 0     | 8.3             | 1.0             | -0.6                | -1.1             | -0.2             | -0.2             |
| aT/ah (sec/100km)<br>X Y X-Y     | 6.9  | 8.6   | 8.8             | 14.5            | 9.6                 | 6°6              | 9.6              | 9.7              |
| ат/ан<br><b>х</b>                | 9.2  | 8.6   | 17.1            | 15.5            | 0.0                 | 8.8              | 9.4              | 9.5              |
| /deg)<br>X-Y                     | -5.9 | -1.6  | -10.5           | -1.7            | 2.2                 | 4.3              | 0.9              | 0.9              |
| ∂T/∂∆ (sec/deg)<br>Y X-)         | 8.5  | 5.9   | 15.4            | 10.0            | 1.7                 | 0.1              | 1.7              | 1.3              |
| ле<br>Х                          | 2.6  | . 4.3 | 4.9             | 8.3             | 3.9                 | 4.4              | 2.6              | 2.2              |
| ∆<br>(deg)                       | 300  | 700   | 30 <sup>0</sup> | 80 <sup>0</sup> | 145 <sup>0</sup>    | 175 <sup>0</sup> | 145 <sup>0</sup> | 155 <sup>0</sup> |
| Х                                | ٩    | Ļ     | S               |                 | P <sup>†</sup> (DF) |                  | P' (DF)          |                  |
| x                                | PcP  |       | ScS             |                 | P'(AB)              |                  | P' (BC)          |                  |
|                                  |      |       |                 |                 |                     |                  |                  |                  |

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phases from the Jeffreys-Bullen Tables and listed in Table 4.1. With few exceptions, these values are less for the differential times. For example, at 70° the error in  $T_p$  due to an epicentral mislocation of 0.1° is about 0.6 seconds  $[\partial T_p/\partial \Delta = 5.9 \text{ sec/deg}]$ , whereas the corresponding error in  $T_{pcP-P}$  is only about 0.2 seconds  $[\partial T_{PcP-P}/\partial \Delta = -1.6$ sec/deg]. At the same distance the error in  $T_p$  due to a 10 km error in the depth of focus is 0.9 seconds  $[\partial T_p/\partial h = 8.6 \text{ sec/100 km}]$ . The corresponding error in the time of PcP-P is less than .01 seconds. For differential times, the greatest absolute values of  $[\partial T/\partial \Delta]$  and  $[\partial T/\partial h]$  given in the table are those of ScS-S at 30° (10.5 sec/deg and 8.3 sec/100 km, respectively). Even so, both of these values are less than the corresponding values for S at the same distance (15.4 and 8.8).

Sampling bias. Because seismic sources are generally in tectonic regions and because most receivers are on continental platforms, the uniform distributions of sources and receivers required by the firstorder averaging theorem [§3.4] are not available. In particular, there is a paucity of observations that sample the upper mantle under ocean basins. This sampling bias is now probably the most serious source of systematic errors in the measurements of absolute travel times. Fortunately, severe lateral heterogeneity seems for the most part confined to the crust and upper mantle. Phases with high apparent velocities travel along nearly vertical paths through this region, so that for some range of (low) dT/dA's sampling bias will appear in the travel time curve as approximately a constant term. This constant error is termed the baseline error. Of course, the baseline error for phases propagating as compressional waves through the upper mantle will be different (generally smaller) than for shear phases. We observe that differential travel times of high apparent velocity phases travelling through the upper mantle in the same mode of propagation are relatively insensitive to variations in upper mantle structure. Quite obviously, simple baseline errors cancel. Table 4.1 gives some indication of how insensitive several phase combinations are. For example, the phase PcP arriving at an angular distance of  $30^{\circ}$  from a source 600 km deep spends about 72 seconds traversing the upper 600 km of the mantle; at the same distance the phase P spends about 102 seconds. Therefore, a 1% variation in velocity averaged over the upper mantle will change the travel time by about 0.7 seconds for PcP and 1.0 second for P. However, the same variation will affect their differential travel time by only 0.3 seconds. This reduction is even more dramatic for the other combinations and distances listed in the table.

<u>Reading errors</u>. Much of the art of seismology involves extracting signals from a background of noise. In this task, no substitute has yet been found for the seismologist's eye. However, every seismologist is aware that picking emergent arrivals late, especially phases that are not first arrivals, can be a source of considerable bias in travel-time measurements. If two phases have the same waveform, then their differential travel time can be measured between any two correlatable features of the signal, such as peaks or zero-crossings. This advantage of differential travel times has been used to reduce

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reading errors and improve time resolution. Hales and Roberts [1970b], for instance, read the differential times of ScS-S by correlating peaks. However, this procedure must be used with caution since unknown effects due to propagation and source can distort one signal relative to another and introduce systematic errors.

We have established in the discussion above that the susceptibility of a differential travel-time datum to bias will be small if

- the difference between the ray parameters of the two phases is small,
- ii) the modes of propagation through the upper mantle are the same,
- iii) the ray paths through the upper mantle are similar,
  - iv) the waveforms are similar and well recorded on the same instrument.

4.4 <u>Observations of differential travel times</u>. In this section five sets of differential travel-time data are presented. These are listed in Table 4.2. Surface focus differential travel times of PcP-P were reduced from the published absolute travel times of PcP and P recorded from nuclear explosions and reported by Kogan [1960], Buchbinder [1965], Kanamori [1968], and Lambert <u>et.al</u>. [1968]. Differential travel times of core phases (relative to P'(DF)) were obtained from the data sets of Hai [1963] and Engdahl [1968] and supplemented by new readings from three deep-focus events in the Sunda Arc. In addition, two new sets of differential travel times for the phase combinations PcP-P and ScS-S were read from long-period records of the World Wide Standardized Seismographic Network using eleven deep-focus

Observed sets of differential travel times

| Phase combination | Distance ran                      | ige Events used  |
|-------------------|-----------------------------------|------------------|
| PcP-P             | 25° - 80°                         | Explosions       |
| PcP-P             | $25^{\circ} - 70^{\circ}$         | Deep earthquakes |
| ScS-S             | 25 <sup>°</sup> - 85 <sup>°</sup> | Deep earthquakes |
| P'(AB)-P'(DF)     | $145^{\circ} - 180^{\circ}$       | Deep earthquakes |
| P'(BC)-P'(DF)     | $145^{\circ} - 160^{\circ}$       | Deep earthquakes |

earthquakes.

The earthquakes used in this study were restricted to events with focal depths greater than 500 km and magnitudes between 5.5 and 6.5. The reasons for this were several. Deep earthquakes in this magnitude range write exceptionally sharp seismograms, making them ideal for travel time studies.<sup>3</sup> Secondly, the ray paths for these events include only one transit through the heterogeneous upper mantle, reducing a source of possible bias. Thirdly, the records are uncontaminated by surface waves. This allows one to read the times of ScS-S at short distances. For normal-focus events, surface waves preceed ScS at distances less than 45°, and the reading of ScS-S is difficult [Hales and Roberts, 1970b]. Finally, simple geometrical considerations imply that these events will be well located [Mitronovas and Isacks, 1971].

<sup>3</sup> This fact was first noticed by Zoeppritz.

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Table 4.3

Earthquakes used in the travel-time study

| Designation   | Date     | Origin Time GMT  | Latitude                              | Longitude   | Depth                                      | Mag        | Source                        |  |
|---------------|----------|--|---------------------------------------|---|--|------------|-------------------------------|--|
| Fiji A        | 4/10/65  | 22 32 46.0 ± .12<br>22 32 46.6                             | 17.84 ± .028 S<br>17.8                | 17.84 ± .028 S 178.70 ± .032 W<br>17.8 178.8                                    | 535 ± 4.5<br>543<br>554 (pP-P)             | 5.7        | ISS<br>USCGS<br>ISS           |  |
| New Hebrides  | 4/10/65  | 22 53 04.5 ± .11<br>22 53 04.8                             | 13.45 ± .023 S 170.30 ±<br>13.4 170.3 | 170.30 ± .026 E<br>170.3  | 641<br>644                                 | 5.3<br>6.2 | ISS<br>USCGS                  |  |
| Mindanao      | 7/15/65  | 18 33 31.8 ± .10<br>18 33 30.7                             | 7.64 ± .023 N<br>7.7                  | 7.64 ± .023 N 123.76 ± .031 E<br>7.7 123.8                                      | 605 ± 4.3<br>590<br>592 (pP-P)             | 5.7        | -6<br>DSCGS -<br>ISS -<br>ISS |  |
| Peru-Brazil A | 11/03/65 | 01 39 03.2 ± .09<br>01 39 03.1<br>01 39 03.3               | 9.04 ± .022 S<br>9.1<br>9.05          | 71.32 ± .032 W 587<br>71.4· 593<br>71.34 590<br>589                             | 587 ± 4.4<br>593<br>590 ± 11<br>589 (pP-P) | 5.9        | ISS<br>USCGS<br>*<br>ISS      |  |
| Fiji B        | 3/17/66  | 15 50 32.3 ± .26<br>15 50 33.1<br>15 50 33.0<br>15 50 33.0 | 21.08 ± .024 S<br>21.1<br>21.12       | 21.08 ± .024 S 179.15 ± .026 W 627<br>21.1 179.2 639<br>21.12 179.24 639<br>633 | 627 ± 3.6<br>639<br>639 ± 12<br>633 (pP-P) | 5.9        | ISS<br>USCGS<br>*<br>ISS      |  |
| Argentina     | 12/20/66 | 12 26 53.6 ± .29<br>12 26 54.6                             | 26.06 ± .020 S<br>26.1                | 26.06 ± .020 S 63.10 ± .032 W 571<br>26.1 63.2 586<br>582                       | 571 ± 3.8<br>586<br>582 (pP-P)             | 5.8        | ISS<br>USCGS<br>ISS           |  |

\* Engdah1 [1968] Table 4.3 (cont.)

| Designation    | Date     | Origin Time GMT                              | Latitude                         | Longitude                           | Depth                                       | Mag        | Source                   |
|----------------|----------|--|----------------------------------|-------------------------------------|---|------------|--------------------------|
| Peru-Brazil B  | 2/15/67  | 16 11 11.8 ± .25<br>16 11 11.5               | 9.05 ± .020 S<br>9.07            | 71.34 ± .024 W<br>71.38             | 598 ± 3.6<br>595 <sup>±</sup><br>597 (pP-P) | 6.1<br>6.1 | ISS<br>USCGS<br>ISS      |
| Java Sea A     | 3/24/67  | 09 00 20.0 ± .45<br>09 00 19.1               | 6.01 ± .025 S<br>5.99            | 112.33 ± .027 E<br>112.33           | 606 ± 6.2<br>595<br>596 (pP-P)              | 5.9        | ISS<br>USCGS<br>ISS      |
| Fiji C         | 10/09/67 | 17 21 48.7<br>17 21 49.5<br>17 21 46.2 ± .33 | 21.07 S<br>21.08<br>21.10 ± .022 | 179.27 W<br>179.35<br>179.18 ± .019 | 643<br>654<br>605 ± 4.6<br>633 (pP−P)       | 7.0        | +<br>USCGS<br>ISS<br>ISS |
| Java Sea B     | 1/30/68  | 03 44 24.8 ±<br>03 44 24.4                   | 6.10 ± .020 S 113.36 ± 6.1 113.4 | 113.36 ± .022 E<br>113.4            | 599 ± 5.2<br>594<br>591 (pP-P)              | 6.0        | ISS 80                   |
| Flores Sea     | 5/24/68  | 15 43 54.8 ± .53<br>15 43 54.2               | 6.84 ± .023 S<br>6.8             | 118.91 ± .028 E<br>118.9            | 618 ± 7.3<br>609<br>618 (pP-P)              | 5.8        | ISS<br>USCGS<br>ISS      |
| China          | 4/10/69  | 14 54 03.9                                   | 42.0 N                           | 130.9 E                             | 555   | 5.6        | USCGS                    |
| Marianas       | 5/10/70  | 20 05 15.9                                   | 18.6 N                           | 145.2 E                             | 602   | 5.6        | USCGS                    |
| Sea of Okhotsk | 9/05/70  | 07 52 27.9                                   | 52.2 N                           | 151.4 E                             | 580   | 5.7        | USCGS                    |

+ Mitronovas and Issacs [1971]

The thirteen deep-focus earthquakes used in this study are listed in Table 4.3. For the purposes of comparison, both ISS and USCGS locations are given, if available. In all cases the epicentral locations agree within 0.1°, and for all but one event the focal depths agree within 10 km. It can be judged from Table 4.1 that location errors of this magnitude will introduce errors in the differential travel times no greater than 1 second (for the extreme case of ScS-S at  $30^{\circ}$ ). One event (Fiji C, 10/9/67) shows anomalous disagreement in the ISS and USCGS locations; the discrepancy in focal depth is nearly 50 km. Fortunately, this earthquake has been one subject of an intensive study by Mitronovas and Isacks [1971]. On the basis of their work, this anomaly can be attributed to the effect of including readings from certain anomalous stations for which the ray paths lie within the high-velocity lithospheric slab. The location we have used for this event is theirs, obtained by deleting these anomalous readings. They claim an accuracy of about ±5 km. For the other events we have used the ISS location if available and the USCGS location if not. In all cases we have used the location given in the top line of Table 4.3. All distances have been computed using geocentric coordinates.

We discuss below each data set individually: <u>PcP-P (surface focus)</u>. Observations of the travel times of PcP and P from nuclear explosions have been published by Kogan [1960] (South Pacific events), Buchbinder [1965] (BILBY event), Kanamori [1968] (LONGSHOT event), and Lambert <u>et.al</u>. (LONGSHOT event). All readings were made from records of short-period vertical seismometers. From

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these published values the differential times of PcP-P were computed, no corrections being applied. The data were residualed with respect to the Jeffreys-Bullen times, the residuals were divided into  $5^{\circ}$  cells, and the sample means and standard errors in the means were computed for cells centered at  $30^{\circ}$ ,  $35^{\circ}$ ,  $40^{\circ}$ , ...,  $75^{\circ}$  (from here on, a series of distances such as this will be abbreviated  $30^{\circ}(5^{\circ})75^{\circ}$ ). The distribution of residuals is given in Table 4.4. For every cell except

# Table 4.4

Distribution of PcP-P residuals (surface focus)

| Cell              | -   | 3 | -2 II | -1 |   | ec)<br>+1 | +2 | +3 |
|-------------------|-----|---|-------|----|---|-----------|----|----|
| 30 <sup>°</sup>   | 1   | 0 | 2     | 8  | 4 | 0         | 0  | 0  |
| 35 <sup>°</sup>   | 0   | 4 | 9     | 7  | 1 | Q         | 0  | Q  |
| 40 <sup>°</sup>   | Q   | 1 | 8     | 6  | 3 | ۵         | 2  | 0  |
| 45 <sup>°</sup>   | 1   | 2 | 16    | 13 | 3 | 2         | 1  | 0  |
| 50 <sup>0</sup> . | 0   | 1 | 6     | 10 | 6 | 3         | 0  | 0  |
| 55 <sup>0</sup>   | . 0 | 0 | 1     | 2  | 5 | 1         | 1  | Q  |
| 60 <sup>0</sup>   | 1   | 0 | 0     | 5  | 4 | 0         | 2  | ۵  |
| 65 <sup>0</sup>   | 1   | 1 | 1     | 2  | 3 | 3         | 0  | 1  |
| 70 <sup>0</sup>   | 2   | 1 | 0     | 0  | 1 | 1         | 1  | 1  |
| 75 <sup>0</sup>   | 1   | 1 | 1     | 1  | 0 | 1         | 0  | 0  |

the last two, the residuals had a well-defined mode. Readings beyond  $65^{\circ}$  were few and showed considerable scatter. The sample mean and standard error in the mean were computed using the following formulae:

(4.4.1) 
$$\overline{T} = \frac{\Sigma w_i T_i}{\Sigma w_i}$$
,  $s_m^2 = \frac{\Sigma w_i^2 (T_i - T)^2}{(\Sigma w_i)^2}$ 

In these expressions the w<sub>i</sub>'s are weights. It was decided to weight the readings given in Lambert <u>et.al</u>. only half as much as those in the other studies, because these readings showed appreciably more scatter. The means and standard errors in the means are given in Table 4.5.

#### Table 4.5

Observed surface focus PcP-P times

| Distance Mean res<br>(deg.) (sec.) |      | S.E.M.<br>(sec.) | J.B.time<br>(sec.) | Obs.time<br>(sec.) |
|------------------------------------|------|------------------|--------------------|--------------------|
| 30                                 | -0.5 | 0.18             | 182.4              | 181.9              |
| 35                                 | -1.1 | 0.14             | 152.5              | 151.4              |
| 40                                 | -0.7 | 0.22             | 125.8              | 125.1              |
| 45                                 | -0.9 | 0.22             | 101.6              | 100.7              |
| 50                                 | -0.4 | 0.19             | 80.3               | 79.9               |
| 55                                 | +0.7 | 0.45             | 61.6               | 62.3               |
| 60                                 | +0.2 | 0.33             | 45.9               | 46.1               |
| 65                                 | +0.1 | 0.43             | 32.9               | 33.0               |
| 70                                 | -0.3 | 1.11             | 22.4               | 22.1               |
| 75                                 | -0.7 | 0.76             | 14.1               | 13.4               |

Figure 4.1 displays the observed residuals and the  $5^{\circ}$  cell means. The error bars represent one standard error in the mean. <u>PcP-P (deep focus)</u>. Records of fifteen deep-focus earthquakes from WWSSN stations in the distance range  $25^{\circ} - 75^{\circ}$  from the source were examined for PcP phases. Two of the earthquakes were discarded because the P phases showed evidence of precursors, indicating a complex source function. PcP-P differential times were read exclusively from longperiod, vertical components. Long-period records were used to insure

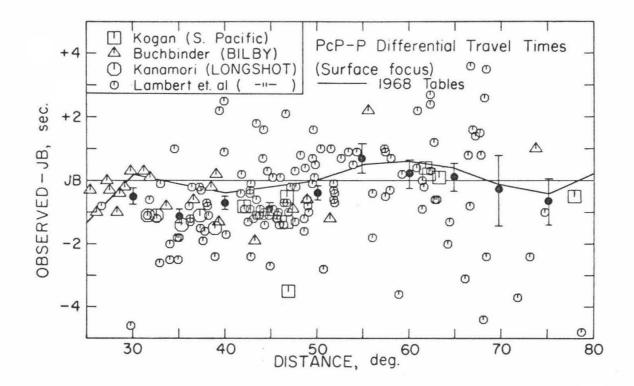


Figure 4.1. PcP-P differential travel times from nuclear explosion sources.

proper identification of the PcP phase. All readings were assigned a "quality", an integer between 0 and 5 inclusive, on the basis of sharpness of the onsets. The readings assigned a zero quality were dropped, eliminating all readings from three of the earthquakes. The measured PcP-P times from the remaining ten events are listed (with all the other data presented in this section) in Appendix 2. Figure 4.2 shows several records from the event designated Peru-Brazil B.

The procedure used to reduce these data was similar to the one described for the surface-focus PcP-P times: the times were residualed with respect to the appropriate J.B. travel time, the residuals were grouped into  $5^{\circ}$  cells, and means and standard errors in the means were computed. The distribution of residuals is given in the following table:

# Table 4.6

Distribution of PcP-P residuals (deep focus)

| Cell            | - | 4 - | Inter<br>3 - |   |    | 0 + | 1 |
|-----------------|---|-----|--------------|---|----|-----|---|
| 30 <sup>°</sup> | 1 | 0   | 0            | 2 | 3  | 0   | 0 |
| 35 <sup>°</sup> | 1 | 1   | 1            | 0 | 1  | 1   | 0 |
| 40 <sup>°</sup> | 0 | 1   | 0            | 0 | 2  | 0   | 0 |
| 45 <sup>°</sup> | 0 | 1   | 1            | 2 | 7  | 3   | 0 |
| 50 <sup>°</sup> | 0 | 0   | 0            | 0 | 13 | 6   | 0 |
| 55 <sup>0</sup> | 0 | 0   | 0            | 1 | 2  | 2   | 0 |
| 60 <sup>°</sup> | 1 | 0   | 1            | 7 | 7  | 2   | 0 |
| 65 <sup>°</sup> | 0 | 0   | 2            | 7 | 1  | 3   | 0 |
| 70 <sup>°</sup> | 0 | 1   | 0            | 1 | 5  | 1   | 0 |

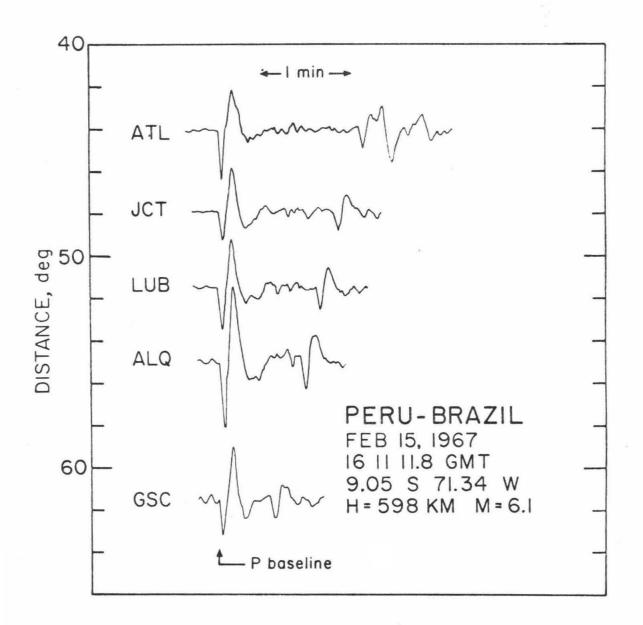


Figure 4.2. Examples of records from which PcP-P differential travel times have been measured.

The weighted means and standard errors in the means were computed for each cell using the formulae (4.4.1), the weights being set equal to the "quality" assigned to each reading. The results are given in Table 4.7.

#### Table 4.7

|                    | For a 600 km        |                  |                    |                    |
|--------------------|---------------------|------------------|--------------------|--------------------|
| Distance<br>(deg.) | Mean res.<br>(sec.) | S.E.M.<br>(sec.) | J.B.time<br>(sec.) | Obs.time<br>(sec.) |
| 30                 | -0.9                | 0.27             | 163.1              | 162.2              |
| 35                 | -2.2                | 0.78             | 135.3              | 133.1              |
| 40                 | -1.2                | 0.81             | 110,3              | 109,1              |
| 45                 | -0.9                | 0.28             | 88,2               | 87,3               |
| 50                 | -0.1                | 0.06             | 68,9               | 68,8               |
| 55                 | +0.1                | 0.19             | 52.4               | 52,5               |
| 60                 | -1.0                | 0.23             | 38,5               | 37,5               |
| 65                 | -1.1                | 0.27             | 27,0               | 25.9               |
| 70                 | -0.7                | 0.25             | 17.9               | 17,2               |
|                    |                     |                  |                    |                    |

The observed residuals and the cell means are displayed in Figure 4.4. For a focal depth of 600 km, the travel-time curves of the phases PcP, pP, and PP intersect at about 40°. Thus there are few observations and correspondingly large uncertainties in mean travel times in . the distance range  $35^{\circ} - 40^{\circ}$ .

Comparison of the mean PcP-P travel times for the two depths of focus shows that they are mutually consistent at a confidence level of 90%. The 1968 tables show the same general trend, although they are

Observed deep-focus PcP-P times

| QUALITY |            |            |             |                | EVENT          |
|---------|------------|------------|-------------|----------------|----------------|
| 1       | 2          | 3          | 4           | 5              |                |
| x       | X          | X          | X           | X              | Fiji A         |
| ×       | ×          | Ă          | Ă           | Ħ              | New Hebrides   |
| +       | Ŧ          | 4          | $\clubsuit$ | 4              | Mindinao       |
| •       | $\diamond$ | $\diamond$ | $\diamond$  | $\diamondsuit$ | Peru–Brazil A  |
| ×       | ×          | Х          | X           | $\times$       | Fiji B         |
| Ø       | O          | $\bigcirc$ | $\bigcirc$  | $\bigcirc$     | Argentina      |
| ۵       |            |            |             |                | Peru-Chile B   |
| *       | ж          | Ж          | Ж           | Ж              | Java Sea A     |
| x       | X          | X          | X           | $\mathbb{X}$   | Fiji C         |
| Ŕ       | ¢          | 文          | 文           | 众              | China          |
| +       | +          | +          | +           | +              | Marianas       |
|         | ▲          | ▲          | ⚠           | $\triangle$    | Sea of Okhotsk |

Figure 4.3. Legend for figures 4.4 and 4.6

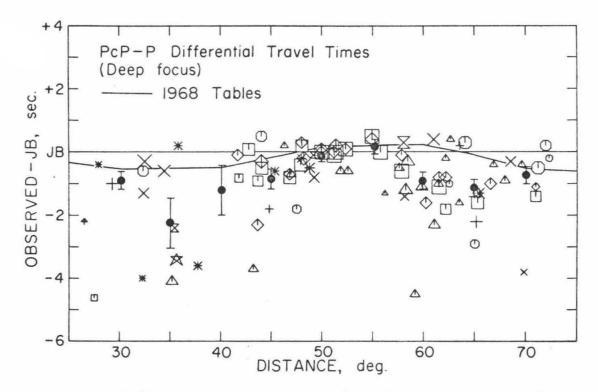


Figure 4.4. PcP-P residuals from deep-focus events. Black dots are the 5° cell means; error bars represent one standard error in the mean. Legend of events given in Figure 4.3.

up to one second later than the observed surface-focus times at distances in the range  $30^{\circ} - 50^{\circ}$ .

<u>ScS-S (deep focus)</u>. Eleven of the deep-focus earthquakes listed in Table 4.3 (all except Java Sea B and Flores Sea) were used in the ScS-S study. All available records from WWSSN stations in the distance range 25° to 80° were read. The readings were assigned qualities ranging from 0 to 5 on the basis of the sharpness of the arrival, the similarities of the waveforms, and instrument polarization. Although both horizontal long-period instruments were used, SH polarization was prefer<sup>r</sup>ed. This eliminates possible contamination by such SV polarized arrivals as SKS. Records of the Argentina event (12/20/66) from stations in the United States are reproduced in Figure 4.5. As before, all readings assigned a zero quality were discarded. There remained 193 observations. These are listed in Appendix 2.

Distributions of the residuals in  $5^{\circ}$  cells centered at the distances  $30^{\circ}(5^{\circ})80^{\circ}$  are listed in Table 4.8. Cell means and their computed standard errors can be found in Table 4.9, and they are plotted with the raw observations in Figure 4.6. Again, there are complications in the travel-time curve near  $40^{\circ}$  which make reading of the differential time difficult (in this case, due to the interference of sS and SS with ScS). The cell mean centered at  $40^{\circ}$  is displaced by about 1 1/2 seconds from the value obtained by interpolating nearby means, and this behavior can be attributed to these complications. In the inversion computations (Chapter 5) the standard error of this point was doubled.

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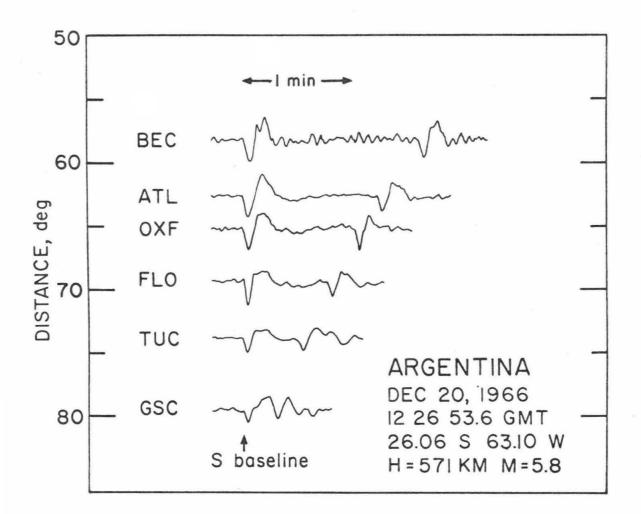


Figure 4.5. Examples of records from which ScS-S differential travel times have been measured.

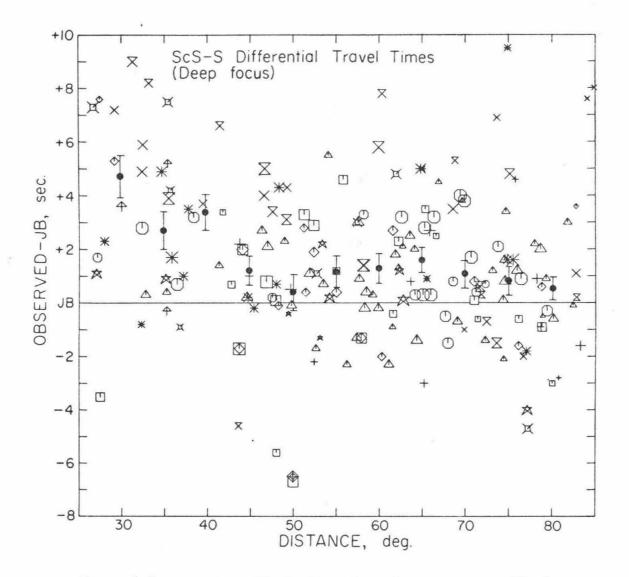


Figure 4.6. ScS-S residuals from deep-focus events. Black dots are the 5° cell means; error bars represent one standard error in the mean. Legend of events given in Figure 4.3.

| Ce  | e11 |    |    | I  | interv | val (s | sec) |    |    |   |
|-----|-----|----|----|----|--------|--------|------|----|----|---|
|     |     | -6 | -4 | -2 | 0      | +2     | +4   | +6 | +8 |   |
|     | 30° | 0  | 0  | 0  | 1      | 0      | 3    | 3  | 1  | 1 |
| ~   | 35° | 0  | 0  | 0  | 2      | 6      | 1    | 3  | 1  | 1 |
| Z   | 40° | 0  | 0  | 0  | 0      | 2      | 4    | ٥  | 1  | Ω |
| L   | 45° | 0  | 1  | 0  | 3      | 5      | 5    | 2  | 0  | 0 |
|     | 50° | 3  | 1  | 1  | 3      | 6      | 6    | 2  | 0  | 0 |
|     | 55° | 0  | 0  | 1  | 3      | 5      | 3    | 2  | 1  | 0 |
| . ( | 60° | 0  | 0  | 2. | 6      | 8      | 3    | 2  | 1  | 0 |
| (   | 65° | 0  | 0  | 1  | 1      | 7      | 9    | 3  | 0  | Q |
| 1   | 70° | 0  | 0  | 0  | 7      | 9      | 3    | 2  | 0  | Q |
|     | 75° | 0  | 2  | 2  | 4      | 8      | 2    | 2  | 1  | 1 |
| ł   | 80° | 0  | 0  | 2  | 6      | 4      | 3    | ۵  | ρ  | ۵ |

Distribution of ScS-S residuals (deep focus)

All cell means are positive J.B. residuals, indicating that either the shear velocity in the mantle is slower than the J.B. model, or else the depth to the core is greater. Several recent studies on the absolute travel times of PcP [Kogan, 1960; Taggart and Engdahl, 1968], as well as the differential times of PcP-P given here, require that the core radius be increased on the order of 10 km over the J.B. value of 3473 km. The latter possibility must therefore be rejected in favor of the former. More will be said about this in Chapter 5.

Hales and Roberts [1970b] have presented times of ScS-S corrected

| Distance<br>(deg.) | Mean res.<br>(sec.) | S.E.M.<br>(sec.) | J.B.time<br>(sec.) | Obs.time<br>(sec.) |
|--------------------|---------------------|------------------|--------------------|--------------------|
| 30                 | +4.7                | 0.80             | 306.6              | 311.3              |
| 35                 | +27                 | 0.71             | 256.7              | 259.4              |
| 40                 | +3.3                | 0.66             | 212.4              | 215.7              |
| 45                 | +1.2                | 0.52             | 173.1              | 174.3              |
| 50                 | +0.5                | 0.69             | 138.1              | 138.6              |
| 55                 | +1.2                | 0.58             | 107.3              | 108.5              |
| 60                 | +1.3                | 0.52             | 80.7               | 82.0               |
| 65                 | +1.6                | 0.44             | 58.1               | 59.7               |
| 70                 | +1.1                | 0.46             | 39.5               | 40.6               |
| 75                 | +0.8                | 0.60             | 24.7               | 25.5               |
| 80                 | +0.5                | 0.37             | 13.5               | 14.0               |

Observed deep-focus ScS-S times

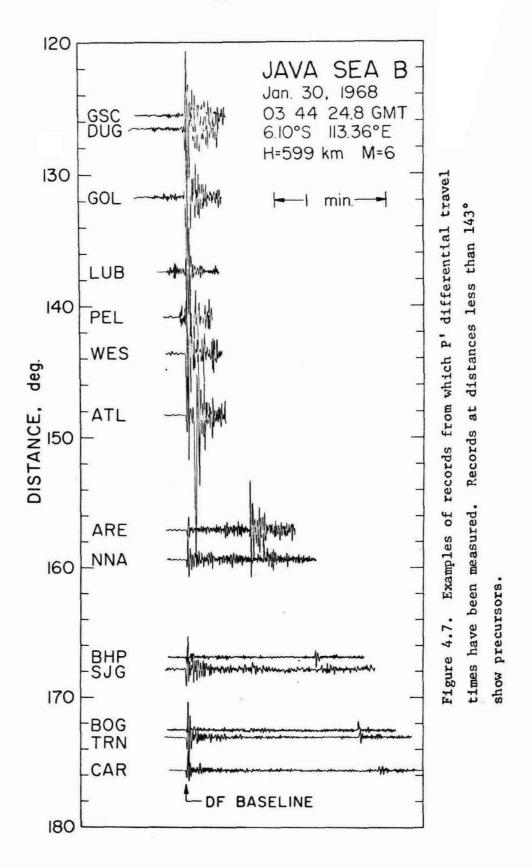
to a surface focus. From their observations they obtained 3486 km as the radius of the core. Comparison of our observations with theirs is difficult, since they list no travel times or J.B. residuals.

As can be seen from Table 4.8 or Figure 4.6, the differential travel times of ScS-S show a large scatter; the spread of the distribution at some distances exceeds 5 seconds. The scatter seems to be a genuine propagation effect; it does not correlate highly with the assigned qualities of the readings. A similarly large scatter was noted by Hales and Roberts [1970b]. They suggested the possibility that this scatter is due to lateral heterogeneity near or on the coremantle boundary. To account for the observed scatter of 5 seconds or so by fluctuations of the core-mantle interface itself would require "bumps" on the order of 15 km in amplitude. Variations of this magnitude have been suggested by Hide [1966] and Hide and Horai [1968] to explain certain geomagnetic peculiarities and geoidal topography of low angular order. Phinney and Alexander [1966] found evidence from their observations of diffracted P waves of lateral heterogeneity at the core-mantle interface. Since several lines of independent evidence support this hypothesis, the possibility that lateral structure in this transition zone accounts for some of the scatter in the ScS-S data seems to be reasonable.

<u>P'(AB)-P'(DF)</u> and <u>P'(BC)-P'(DF)</u>. It can be seen from an examination of Table 4.1 that the differential travel times of P' phase combinations are especially insensitive to the types of bias discussed in the previous section, a property which follows from the fact that these core phases are characterized by low values of  $dT/d\Delta$ . Since they also provide severe constraints on the possible variations of velocity in the core, the differential times of P' make excellent gross Earth data.

Several phase combinations were considered. The phase P'(DF) was chosen as the reference phase because it is a strong, clear arrival at all distances that other P' phases are observed  $(125^{\circ} - 180^{\circ})$ . For the Jeffreys model, there are two other branches of the P' travel-time curve, the AB branch and the BC branch. The AB branch represents the travel times of rays which bottom in the outer core and is well observed; it is a receding branch (has positive curvature) and terminates at the caustic B located at a distance of  $143^{\circ}$ . At distances greater than  $143^{\circ}$ , at least one other branch is observed. Jeffreys has labeled

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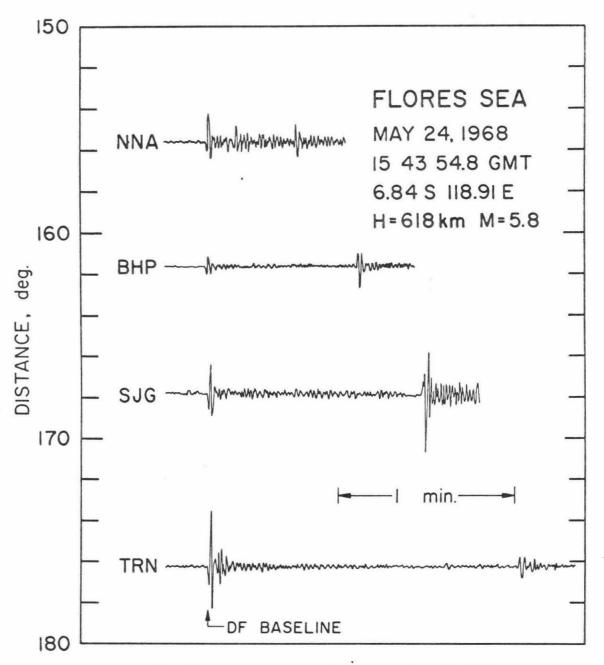


Figure 4.8. Examples of records from which P' differential travel times have been measured.

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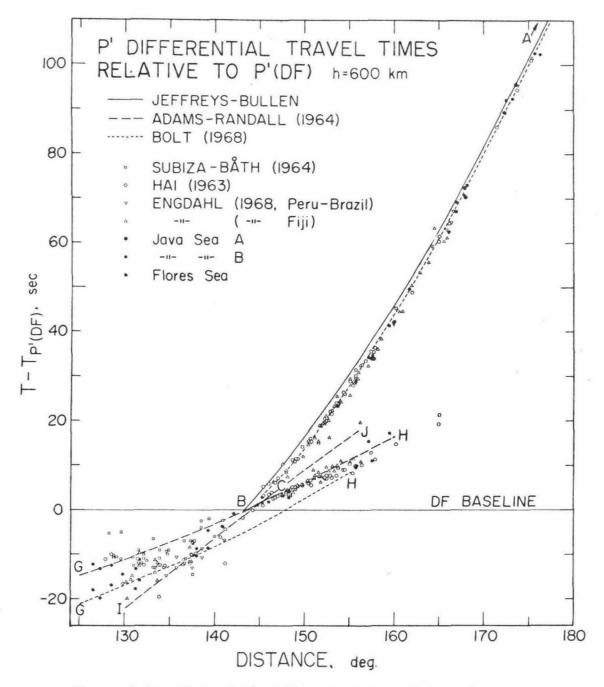


Figure 4.9. Plot of P' differential travel-time data.

this branch BC; in his model it represents rays bottoming below the B-caustic ray and above the inner core. Bolt [1959] has re-interpreted the arrivals beyond the caustic as members of a family constituting what he calls the GH branch. In his model there exists a transition region between the inner and outer cores in which these rays bottom, and it is separated from the outer core by a discontinuity. His interpretation was motivated by a series of small arrivals preceding P'(DF) at distances less than 143°. These precursors, originally studied by Gutenberg [1957], would, in Bolt's model, be refracted by the transition region - outer core discontinuity to distances near 125°. Recently, however, Haddon [1972] has proposed that these precursors might result from scattering off lateral heterogeneities in the vicinity of the core-mantle boundary. His arguement has been motivated by the anomalous curvature of this branch, pointed out by Buchbinder [1971], and the predominance of high frequencies in the precurors. Examples of these precursors from an event in the Sunda arc (Java Sea B) are shown in Figure 4.7.

To test Haddon's hypothesis, a simple model experiment was performed. Rays were traced through a two-dimensional Earth model consisting of a homogeneous mantle ( $v_p = 13 \text{ km/sec}$ ) surrounding a homogeneous core ( $v_p = 10 \text{ km/sec}$ ) separated by a "bumpy" boundary. The equation used to specify the radius of the boundary was  $R_c = 3473 + \frac{A}{2} \sin n\pi\theta$ . The rays were traced and the travel times computed for various values of the parameters n and A. The results for n = 20 and A = 0, 10, 20 km are pictured in Figure 4.10. It can be seen that the effect on the P'

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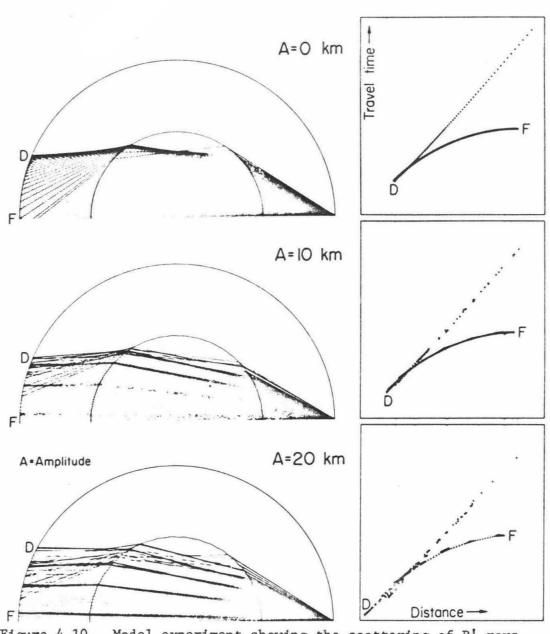


Figure 4.10. Model experiment showing the scattering of P' rays from bumps on the core-mantle boundary. Parameter A is the amplitude of bumps.

travel times is to introduce a number of arrivals as precursors to P'(DF) at distances less than the distance to the B caustic. Although the calculation is extremely crude, the resulting travel-time curve for A = 20 km looks surprisingly like the observations (compare with Figure 4.9 for example). This qualitative experiment confirms the plausibility of Haddon's hypothesis and lends further support to the speculation that the transition region between the mantle and core is laterally heterogeneous.

The observations of P' differential travel times shown in Figure 4.9 were computed from the raw readings of Engdahl [1968], who used the events designated Peru-Brazil A and Fiji B in Table 4.3, as well as Engdahl's [1968] compilation of Hai's [1963] times for a 600 km focal depth. Additional readings of precursor phases at distances less than 143<sup>°</sup> were taken from Subiza and Båth [1964]. To further supplement this data, times were read for three deep-focus earthquakes in the Sunda Arc from records written by short-period vertical component seismometers of the WWSSN. This geometry was advantageous because it provided a number of good readings of P'(AB)-P'(DF) near the antipode from stations situated in the Caribbean. Most of the readings were of very high quality. Examples of seismograms are shown in Figures 4.7 and 4.8.

All P' differential times were reduced to a 600 km focal depth using the J.B. Tables. Beyond 143° two branches are well delineated. The precursors to P'(DF) at distances less than 143° show their characteristic scatter. Neither the interpretaion of Bolt [1968] nor the more complex model of Adams and Randall [1964], plotted with the obser-

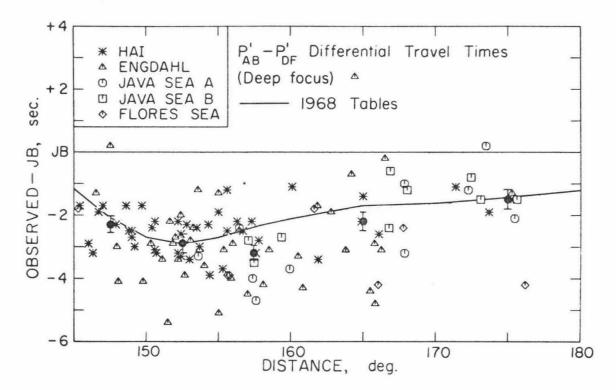


Figure 4.11. P'(AB) - P'(DF) residuals from deep-focus events. Black dots are cell means; error bars represent one standard error in the mean.

Distribution of P'(AB)-P'(DF) residuals (deep focus) Cell Interval (sec) -5 -4 -3 -2 -1 .0 +1 147.5° 152.5° 157.5° 165.0° 175.0° 

vations in Figure 4.9, adequately explain these arrivals. Because of the possibility that the precursors arise from scattering off lateral heterogeneities and therefore are not gross Earth data, we have assumed that the PKP curve is of the Jeffreys type and have computed cell means only for the combinations P'(AB)-P'(DF) and P'(BC)-P'(DF).

The distribution of residuals for these two phase combinations are given in Tables 4.10 and 4.12. Residuals for P'(BC)-P'(DF) were

Table 4.11

| Distance<br>(deg.) | Mean res.<br>(sec.) | S.E.M,<br>(sec.) | J.B.time<br>(sec.) | Obs.time<br>(sec.) |
|--------------------|---------------------|------------------|--------------------|--------------------|
| 147.5              | -2.3                | 0.24             | 10.0               | 7.7                |
| 152.5              | -2.9                | 0.28             | 23.5               | 20.6               |
| 157.5              | -3.2                | 0.19             | 38.3               | 35.1               |
| 165.0              | -2.2                | 0.31             | 63.0               | 60.8               |
| 175.0              | -1.5                | 0.31             | 101.6              | 100.1              |

Observed deep-focus P'(AB)-P'(DF) times

Distribution of P'(BC)-P'(DF) residuals (deep focus)

| Cell        | ell Interval |   | erval | (sec) |    |    |
|-------------|--------------|---|-------|-------|----|----|
|             |              | 0 | +1    | +2    | +3 | +4 |
| <br>146.25° | 1            | 6 | 0     | 1     | 0  | 0  |
| 148.75°     | 1            | 0 | 15    | 6     | 0  | 0  |
| 151.25°     | 0            | 0 | 5     | 10    | 3  | 2  |
| 153.75°     | 0            | 0 | 8     | 3     | 4  | 1  |
| 156.25°     | 0            | i | 5     | 1     | 3  | 0  |

computed by extending the BC branch in the Jeffreys model with a ray parameter of 2.2 sec/deg. In computing the cell means listed in Tables 4.11.and 4.13 all observations were given equal weight.

From Figure 4.11, which displays the observations of P'(AB)-P'(DF), we see that Bolt's [1968] times are in good agreement with the data. Figure 4.12 shows the residuals for P'(BC)-P'(DF). The point C is not well defined by these data but lies somewhere near 155°. The cell means centered at 153.75° and 156.25° may be biased by spurious arrivals.

# Table 4.13

Observed deep-focus P'(BC)-P'(DF) times

| Distance<br>(deg.) | Mean res.<br>(sec.) | S.E.M.<br>(sec.) | J.B.time<br>(sec.) | Obs.time<br>(sec.) |  |
|--------------------|---------------------|------------------|--------------------|--------------------|--|
| 146.25             | +0.7                | 0.30             | 1.8                | 2.5                |  |
| 148.75             | +1.7                | 0.11             | 3.2                | 4.9                |  |
| 151.25             | +2.8                | 0.20             | . 4.8              | 7.6                |  |
| 153.75             | +2.2                | 0.24             | 6.8                | 9.0                |  |
| 156.25             | +1.8                | 0.34             | 9.0                | 10.8               |  |

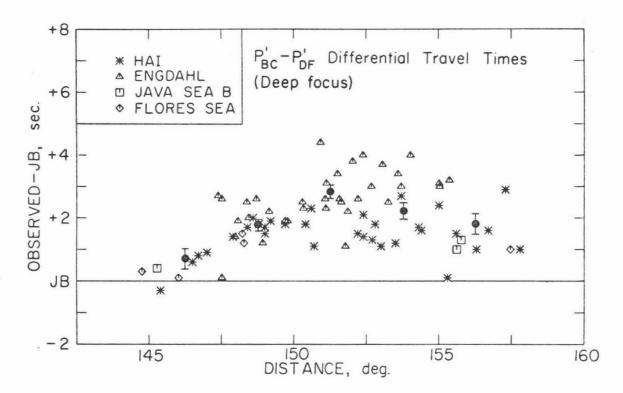


Figure 4.12. P'(BC) - P'(DF) residuals from deep-focus events. Black dots are cell means; error bars represent one standard error in the mean.

#### Chapter 5

#### NUMERICAL MODELING OF THE RADIAL VARIATIONS

5.1 <u>Introduction</u>. This chapter is concerned with actual numerical modeling of the radial distributions of velocity and density in the Earth. The data we shall attempt to fit are the Earth's mass and moment of inertia, the observed eigenperiods of oscillation, and the differential travel times presented in Chapter 4. The algorithm that we shall employ was outlined in Chapter 2: a starting model is constructed and tested against the data, a correction is computed by solving the linear perturbation equations, the data functionals are reevaluated, and the procedure is iterated until the fit is satisfactory.

Because the inverse problem is nonlinear and has no unique solution, interpretation of any numerical results is a tricky business. A common mistake is to infer that because a certain model satisfies the data some feature of that model actually exists in the Earth, when in reality the data do not require this feature. To guard against this kind of breach of scientific method, one must insure that the calculated perturbations are resolvable - are really required by the data. The resolving power of the data in a linear neighborhood of any model can be judged by examining the averaging kernels given in equation (2.8.3). To calculate the perturbations we shall use equation (2.7.12); it provides an approximate solution which has been filtered of any linearly unresolvable components.

As we emphasized in §2.3, the success of an algorithm based on

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linear estimation depends critically on the model used to "start" the computation. In the design of the starting model we must strike a balance between two opposing considerations. On the one hand, because the eigenperiods and travel times are nonlinear functionals, the starting model should be as linearly close as possible to the sought representation of the Earth. Otherwise, the model that results from successive perturbations may end up in a local minimum far removed from this representation, and resolving power computations may be deceptive. Generally speaking, the starting model should include any major discontinuities that exist in the Earth. A starting model in which the velocities and density are taken to be constants is an example of an inadequate representation. On the other hand, we desire that the starting model be "simple" - devoid of any features that might not exist in the spherically averaged Earth. For this reason published models generally make poor starting models.

The procedure we shall adopt is to construct starting models based on a series of reasonable but "simple" physical assumptions. These will be detailed in section 5.4. Since the inversion algorithm provides the minimum deviations (in a norm sense) from these starting models necessary to fit the data, the resulting models will, in some sense, be as simple as possible.

We discuss in the next section the adaptation of the inversion theory given in Chapter 2. The data sets used in the inversions are presented in §5.3, and §5.4 is devoted to construction of the starting models. In §5.5 models are derived and evaluated. In section 5.6 the resolving kernels are displayed. The last section contains conclusions.

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5.2 <u>The inversion algorithm</u>. Estimates of the spherically averaged compressional velocity  $v_{p0}(r)$ , shear velocity  $v_{s0}(r)$ , and density  $\rho_0(r)$ , which constitute a spherically symmetric Earth model  $\mathbf{m}_0$ , were sought given the observed values of the Earth's mass and moment of inertia and the sample means of available sets of eigenperiod and differential travel-time data. The data values were arranged in a vector  $\mathbf{d}_0$ . The errors in the data were assumed to be samples of independently distributed, Gaussian random variables with zero means and known variances. The vector  $\delta \mathbf{m}_0$  was defined to be equal to the difference between  $\mathbf{m}_0$  and some initial guess  $\mathbf{m}_s$ , and the vector  $\delta \mathbf{d}_0$  were assumed to be related by equation (2.5.1), where  $\mathbf{n}$  is the vector containing the noise components and  $\mathbf{A}$  is the linear operator whose ith row is the Fréchet kernel of the ith datum in  $\mathbf{d}_0$ . Under these assumptions the theory presented in Chapter 2 was applicable.

The inner product between any two vectors m and m' in the space of Earth models was defined by the equation

(5.2.1) 
$$\mathbf{m} \cdot \mathbf{m}' = \int_{0}^{R} [v_{p}(r)v_{p}'(r)w_{p}(r) + v_{s}(r)v_{s}'(r)w_{s}(r) + \rho(r)\rho'(r)w_{o}(r)] dr.$$

The measure on the interval [0,R] was chosen to be linear in r, so that the weighting functions  $w_p$ ,  $w_s$ , and  $w_p$  in the integral (5.2.1) are simply constants. These constants were chosen to render the inner product dimensionless. The velocities were expressed in units km/sec, and the density was expressed in units of gm/cm<sup>3</sup>. We write

(5.2.2) 
$$[v_p] = [v_s] = km/sec$$
,  
 $[\rho] = gm/cm^3$ .

The inner product is dimensionless if

(5.2.3) 
$$[w_{p}] = [w_{g}] = \sec^{2}/km^{3},$$
$$[w_{p}] = cm^{6}/gm^{2} km,$$

where the units of radius are taken to be kilometers. We specified the weighting functions to be numerically equal to  $R^{-1}$ . This specification implies that unit perturbations of both velocities and density are of equal weight. Although arbitrary, this decision was motivated by the near numerical equality of  $v_{p0}$ ,  $v_{s0}$ , and  $\rho_0$  when expressed in the units given in (5.2.2).

The four types of data functionals which compose a data vector d are the mass of the model, denoted M; its moment of intertia I; spheroidal and toroidal eigenperiods of radial order n and angular order  $\ell$ , denoted  ${}_{n}t_{\ell}^{\sigma}$  and  ${}_{n}t_{\ell}^{\tau}$  respectively; and the ray-theoretical travel times  $T_{x}(\Delta,h)$  of a phase x at angular distance  $\Delta$  from a source with focal depth h. The functionals M and I were normalized by their observed values (given in §5.3) and thus are dimensionless. The eigenperiods and travel times were expressed in seconds. The scale factors for these functionals appearing in the inner product on the data space were set equal to 1 sec<sup>-2</sup>.

With these conventions, a computer program was written to calculate the best linear estimate  $\overline{\delta m}$  given by equation (2.7.12) and the averaging kernels appearing in equation (2.8.3). Rewriting (2.7.12) and

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(2.8.3) in terms of the inner product (5.2.1), we find that

(5.2.4) 
$$\overline{\delta m} = C_{ss} \cdot A^* (A \cdot C_{ss} \cdot A^* + \tan \theta C_{nn})^{-1} \delta d_0,$$

and that

(5.2.5) 
$$\mathscr{A} = C_{ss} \cdot A^* (A \cdot C_{ss} \cdot A^* + \tan \theta C_{nn})^{-1} A$$
,

the angle  $\theta$  being the parameter of the tradeoff curve.

The foward calculation of the eigenperiods and the calculation of their Fréchet kernels was performed in subroutines written by Mr. Martin Smith. The travel-time routines were kindly provided by Dr. Bruce Julian.

Since the error components are assumed to be uncorrelated, the form of the noise autocorrelation operator  $C_{nn}$  is given by equation (2.5.12). This form was used with the variances along the diagonal set equal to the squares of the standard errors in the means estimated from the scatter in the data.

Specification of the operator  $C_{ss}$  requires some discussion. We saw in §2.6 that the meaning attached to  $C_{ss}$  in the stochastic formulation, where it plays the role of an autocorrelation operator, makes sense only if we impose on the model space an <u>a priori</u> probability distribution. This is because sample ensembles for the solution process are unavailable, and probabilities cannot be interpreted as the limits of sample frequencies. In §2.6 we also saw that, if quadratic convergence is sufficient to identify vectors, then choosing  $C_{ss}$  is equivalent to specifying the norm on the space of models. With this

realization we chose  $C_{ss}$  in the following manner: for each of the model functions  $v_{p}(r)$ ,  $v_{s}(r)$ , and  $\rho(r)$ , the interval [0,R] was partitioned into several sub-intervals, each bounded by radii at which discontinuities are known or thought to exist. Considering only one model function for a moment, let us label these radii a, where  $p = 1, 2, \dots, P$ . We define  $a_0 = 0$  and assume that  $a_p \equiv R$ , so that on the pth interval the radius varies between  $a_{p-1}$  and  $a_p$ ,  $p = 1, 2, \dots, P$ . On each of these sub-intervals we defined a smoothing operator  $C_{p}(r,r')$ by the equation

(5.2.6) 
$$C_{p}(r,r') = k_{p}/2 \left\{ e^{-k_{p}|r-r'|} + D^{-1}[A e^{-k_{p}(a_{p}-a_{p-1})] \times \cosh k_{p}(r-r') + B \cosh k_{p}(a_{p}+a_{p-1}-r-r')] + C \sinh k_{p}(a_{p}+a_{p-1}-r-r')] \right\},$$
where  $A = [1 - a_{p-1}(k_{p}+\alpha_{p})][1 + a_{p}(k_{p}-\beta_{p})],$ 

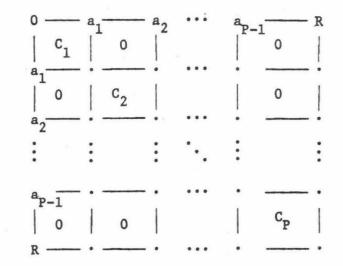
$$A = [1 - a_{p-1}(k_{p} + \alpha_{p})][1 + a_{p}(k_{p} - \beta_{p})],$$
  

$$B = \alpha_{p}a_{p-1} + \beta_{p}a_{p} - [k_{p}^{2} - k_{p}(\alpha_{p} + \beta_{p}) + \alpha_{p}\beta_{p}]a_{p-1}a_{p} - 1,$$
  

$$C = k_{p}(a_{p} - a_{p-1}),$$
  

$$D = [1 - \alpha_{p}a_{p-1} - \beta_{p}a_{p} + (\alpha_{p}\beta_{p} - k_{p}^{2})a_{p-1}a_{p}]\sinh k_{p}(a_{p-1} - a_{p})$$

 $-k_{p}[a_{p-1} + (\beta_{p-\alpha})a_{p}a_{p-1}] \cosh k_{p}(a_{p-1}-a_{p}).$ Equation (5.2.6) is similar to equation (2.6.16); in fact,  $C_p(r,r')$ satisfies the system (2.6.15) with w(r) = p(r) = 1,  $a = a_{p-1}$ ,  $b = a_p$ ,  $\alpha = \alpha_p$ , and  $\beta = \beta_p$ . Having done this for each of the three model functions, we specify  $\boldsymbol{C}_{_{\boldsymbol{\mathrm{SS}}}}$  to be a block-diagonal operator as in equation (2.6.10) with each of the three blocks in the form



(5.2.7)

This block-diagonal form of the operator  $C_{ss}$  expresses the conviction that between the radii of discontinuities the solution  $\delta m_0$  behaves smoothly. The estimation is therefore weighted in favor of this behavior. The parameter  $k_p$  is simply the mean wavenumber of the smoothing operator  $C_p$ . In the minimization to obtain the best linear estimate  $\delta m$ , components with unit amplitude and wavenumber  $k_p$  measure twice as much as components with unit amplitudes and wavenumbers near zero. Since the minimization seeks out the "smallest" solution that satisfies the data, low-wavenumber components; i.e., smoother components, are preferred.

The parameters  $\alpha_p$  and  $\beta_p$  specify the boundary conditions applied at the radii  $a_{p-1}$  and  $a_p$ . If they are set equal to zero, the derivatives of the solution will vanish at these radii (inside the interval); whereas if they are set equal to infinity, the values of the solution itself will vanish.

This form of the solution autocorrelation operator is quite

versatile. By its manipulation, one can introduce information about the solution not contained in the data or search for solutions with specified constraints. Often this is a convenient way to test hypotheses; e.g., does a solution to the inverse normal mode problem exist with a density at the top of the mantle equal to 3.33 gm/cm<sup>3</sup>?

We return now to a discussion of the numerical algorithm. Because the computer available to us was fairly small (an IBM 370/155 with 320 kilobytes = 80 K words of core), it was not feasible to invert all three functions,  $v_p$ ,  $v_s$ , and  $\rho$ , simultaneously. Instead, a FORTRAN program was written to invert either compressional velocity and density or shear velocity and density simultaneously. The iteration scheme employing the estimate given in (5.2.4) was designed to alternate between these two possiblities. At each step, up to eighty data could be inverted. Convergence was always rapid as long as tan  $\theta$  was kept at a value greater than 5; no model presented in this chapter required more than eight iterations. Typically, a run involving one iteration on a data set consisting of 50 normal modes and 30 travel times required about twenty minutes on the 370/155 and cost about fifty dollars. Over eighty per cent of this time was devoted to calculating the mode periods and Fréchet kernels. Calculation of the operator A took an additional five minutes.

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5.3 <u>The data set</u>. The basic data set comprised a total of 219 data. Of these, 178 were normal mode periods, 39 were differential travel times, and the remaining two were mass and moment of inertia. We devote this section to a discussion of each of these three subsets. <u>The normal mode data</u>. Gilbert [1972] observed that the average period of singlets in a mode multiplet split by disturbing influences such as rotation, ellipticity of figure, and the presence of lateral heterogeneities equals, to a first-order approximation, the degenerate eigenperiod of a spherically averaged Earth model.<sup>1</sup> Unfortunately, resolution of the multiplet structure of an eigenperiod is, with the exceptions of only the very gravest modes, impossible at the present time. Instead, we must rely on averages of many observations to give periods that can be interpreted in terms of an average Earth structure.

Averages of observed free oscillation periods were given by Pekeris in 1966. However, the wide variations in the quality of the early recordings (mainly from the Chilian earthquake of 1960) and the procedure used to reduce the data largely negated the advantage of using these averages; much of the early inversion work was done with values obtained from single records. Anderson [1967], who also presented averages, picked "best values" to evaluate various Earth models. As investigators have set themselves to the task of gleaning from existing records information about the mode spectrum, the situation

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<sup>&</sup>lt;sup>1</sup> This will be true as long as the disturbing influences leave the linear system describing small oscillations Hermitian.

has improved considerably. Derr [1969] averaged the observations available through 1968 using a complex, somewhat arbitrary system of weights to enhance the importance of high-resolution recordings. Although the great majority of the more than 1500 data he used were of the fundamental mode, he attempted to obtain averages of some of the higher modes as well. Backus and Gilbert [1968] had shown inclusion of higher modes greatly improves the resolving power of the normal mode data set.

Recently, a major contribution to the study of the normal mode spectrum has been made by Dziewonski and Gilbert [1972]. Using a comprehensive series of criteria to identify modes, they have analyzed 84 long-period seismograms of the great Alaskan earthquake of 1964 and tentatively identified all but 30 of the 136 theoretically predicted multiplets in the normal mode spectrum with periods greater than 300 seconds, as well as a number of modes in the period range 200 - 300 seconds. Besides their extensive listing of higher-mode periods, they also give cumulative averages of fundamental mode data for periods greater than 176 seconds ( $_0S_3 - _0S_{50}$ ,  $_0T_3 - _0T_{46}$ ).

Their averages, listed with standard errors in the means in Tables 2-5 of their paper, formed the basis of our normal mode data set. They did not list averages of the modes  $_0S_2$  and  $_0T_2$ , and the period they give for  $_0S_3$  (2140.57 sec, at the limit of their resolution) is evidently too large; for these modes we have used the periods given by Derr [1969]. In addition, we included in our data set the average periods of the modes  $_0S_{51}$  to  $_0S_{63}$  given in Table 2 of Dziewonski and

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Landisman [1970]. These data are listed with fits to the models derived in §5.5 in Table A3.1. The consistency of this data set is indicated by the precision with which these models satisfy the data. One model, model B1, has eigenperiods which differ from the observed values by no more than 0.4% in the extreme; generally, the fit is much better. This strongly suggests (but, of course, does not prove) that these data are representative of the averaged Earth.

The travel-time data. Because of the problem of baseline errors, we used only differential travel times in the inversion. Included in the data set were the 39 differential travel-time averages listed in Tables 4.5, 4.7, 4.9, 4.11, and 4.13 for the phase combinations PcP-P (surface focus), PcP-P (deep focus), ScS-S (deep focus), P'(AB)-P'(DF) (deep focus), and P'(BC)-P'(DF) (deep focus). These data along with the fits to the models are summarized in Table A3.2.

The mass and moment of inertia. The mass M and normalized moment of inertia I/MR<sup>2</sup> used in the inversion are given by Jeffreys [1970]. These are

(5.3.1)  $M = 5.977 \pm 0.0006 \times 10^{27} \text{ gm},$  $I/MR^2 = 0.330841 \pm 0.00018$ 

<u>Partitioning of the data sets</u>. Two subsets of the basic data set were formed. These were designated data set I and data set II. Data set I, used in the inversion of compressional velocity and density, consisted of the eigenperiods of the following modes and the differential travel times of the following phase combinations:  $_{0-4}$  S<sub>0</sub>,  $_{0}$ S<sub>2</sub>,  $_{0}$ S<sub>3</sub>,  $_{0}$ S<sub>5</sub>,  $_{0}$ S<sub>7</sub>,  $_{0}$ S<sub>9</sub>,  $_{0}$ S<sub>12</sub>,  $_{0}$ S<sub>15</sub>,  $_{1}$ S<sub>2</sub>,  $_{1}$ S<sub>7-10</sub>,  $_{2}$ S<sub>1-4</sub>,  $_{2}$ S<sub>6</sub>,  $_{2}$ S<sub>15</sub>,  $_{3}$ S<sub>2-9</sub>,  $_{3}$ S<sub>11</sub>,

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4S1-10, 5S2, 5S3, 6S1, 6S4, 6S5, 7S2, 7S3, 7S5, 8S1, 8S2, PCP-P [Tables 4.5 and 4.7], P'(AB)-P'(DF) [Table 4.11], P'(BC)-P'(DF) [Table 4.13]. Data set I included all modes observed by Dziewonski and Gilbert [1972] with greater than 25% compressional energy or greater than 5% compressional energy in the outer core (as given in their Table B2).

Data set II, used in the inversion of shear velocity and density, consisted of the following modes and travel times:  $_{0}S_{2}$ ,  $_{0}S_{3}$ ,  $_{0}S_{5-9}$ ,  $_{0}S_{12}$ ,  $_{0}S_{15}$ ,  $_{0}S_{18}$ ,  $_{0}S_{21}$ ,  $_{0}S_{25}$ ,  $_{0}S_{30}$ ,  $_{0}S_{37}$ ,  $_{0}S_{45}$ ,  $_{0}S_{54}$ ,  $_{0}S_{63}$ ,  $_{1}S_{2}$ ,  $_{1}S_{4}$ ,  $_{1}S_{5}$ ,  $_{1}S_{7-10}$ ,  $_{1}S_{14-17}$ ,  $_{2}S_{2}$ ,  $_{2}S_{8-14}$ ,  $_{3}S_{4-11}$ ,  $_{4}S_{1-3}$ ,  $_{4}S_{10}$ ,  $_{5}S_{2}$ ,  $_{8}S_{2}$ ,  $_{0}T_{3-6}$ ,  $_{0}T_{8}$ ,  $_{0}T_{10}$ ,  $_{0}T_{11}$ ,  $_{0}T_{13}$ ,  $_{0}T_{16}$ ,  $_{0}T_{21}$ ,  $_{0}T_{23}$ ,  $_{0}T_{25}$ ,  $_{0}T_{29}$ ,  $_{0}T_{35}$ ,  $_{0}T_{41}$ ,  $_{0}T_{46}$ ,  $_{5}CS-S$  [Table 4.9]. This data set provided good coverage of the fundamental mode as well as the higher modes sensitive to variations in shear velocity and density. 5.4 <u>Construction of the starting models</u>. Two starting models, designated model A and model B, were constructed. In this section we describe their derivation.

The central idea behind the construction was the assumption that discontinuities in density and shear velocity are associated with discontinuities in compressional velocity. For density, this assumption is well-motivated; available laboratory data on the behavior of mantletype materials indicates that the compressional velocity - density systematics are very regular over wide ranges of temperature and pressure. Birch [1961] proposed that, for materials of constant mean atomic weight, v and p are related by a linear law. The invariance of this relationship to temperature and pressure variations has been discussed by Anderson et.al. [1971]. Such a linear relationship was used to construct the upper mantle density profiles in the starting models. Densities in the lower mantle and core were derived using the Adams-Williamson integration procedure [Williamson and Adams, 1923]. By fixing the density at the base of the crust and fitting the mass and moment of inertia, construction of the density profile was made deterministic, once the velocities were chosen. This was exactly the procedure used by Birch [1964] to construct his model II.

We review the construction of the velocity models region by region:

The crust (Bullen's region A). The crust was modeled as a layer 21 km thick with  $v_p = 6.2$  km/sec and  $v_s = 3.4$  km/sec. This roughly corresponds to an areal average of the six crustal types listed by

-106-

Brune [1969] (oceanic, shield, ridge, alpine, basin and range, and island arc) taken in proportion to their surface areas.

The upper mantle and the transition zone (regions B and C). The presence of large velocity gradients and the existence of strong lateral heterogeneity complicate the interpretation of seismic data sensitive to the upper mantle and transition zone. Evidence from surface waves has confirmed Gutenberg's hypothesis that a low-velocity channel exists for shear waves 100 km or so below the base of the crust [Anderson, 1967]. Structure in the transition zone between 400 km and 700 km has been illuminated by  $dT/d\Delta$  studies using large seismic arrays [Niazi and Anderson, 1965; Johnson, 1967]. These have confirmed the presence of at least two major discontinuities at depths near 400 and 650 kilometers (corresponding to breaks in  $dT/d\Delta$  at distances of about 20 and 25 degrees). However, lateral variation of these structures is great, and currently available data sample only a small fraction of the Earth's surface.

Because the average structure of these regions is in doubt, we have used simple representations as starting models. The compressional velocity below the crust was fixed at 8.0 km/sec and increased linearly with depth to a value of 8.8 km/sec at 420 km. The shear velocity in the upper mantle was taken to be a constant 4.55 km/sec. Thus, the starting models have no low-velocity zone in this region.

The transition region was modeled by two discontinuities at depths of 420 km and 671 km with the velocities varying linearly in between. Only in this region do the starting models A and B differ. Model A is characterized by discontinuities of second-order. In this model, the compressional velocity rises from 8.80 km/sec at 420 km to a value of 10.86 km/sec at 671 km. In the same region shear velocity varies linearly between values of 4.55 km/sec and 6.13 km/sec.

In model B the discontinuities were chosen to be of first-order. At 420 km the compressional velocity jumps from 8.80 km/sec to 9.5 km/sec, and the shear velocity jumps from 4.55 km/sec to 5.33 km/sec. Between this depth and the discontinuity at 671 km, the compressional velocity increases at a rate of 0.27 km/sec per 100 km, and the shear velocity is constant.

Although the variation of velocities in these regions is somewhat ad hoc, the values chosen were designed to give the same baseline for teleseismic P as the 1968 Tables and the same baseline for teleseismic S as Hales and Roberts [1970 a].

<u>The lower mantle (region D)</u>. The Earth's lower mantle is a region characterized by relatively uniform increases in the velocities with depth. The models of lower mantle velocities derived from travel-time studies have changed very little since the early work of Jeffreys and Gutenberg. The travel times through this region show very little azimuthal dependence [Jeffreys, 1962], and it may be inferred that the lateral heterogeneity is small, at least in comparison with the upper mantle.<sup>2</sup>

The velocities in the lower mantle we have used in our starting models were taken from the studies of Herrin et.al. [1968] (compres-

<sup>&</sup>lt;sup>2</sup> A recent study of ISS P times by Sengupta and Julian [in preparation] indicates, however, some lateral variation in the lowermost 600 km.

## Table 5.1

Positions of the major discontinuities

| Region |                 | Radius | (km) |
|--------|-----------------|--------|------|
|        |                 | 6371   |      |
| A.     | Crust           | 6350   |      |
| В      | Upper mantle    | 5951   |      |
| С      | Transition zone | 5700   |      |
| D      | Lower mantle    | 3485   |      |
| E,F    | Outer core      |        |      |
| <br>G  | Inner core      | 1215   |      |
|        |                 | 0      |      |

sional velocity) and Randall [1971] (shear velocity). Both of these studies used ISS times from the same set of sources.

The radius of the core-mantle boundary. Since the radius of this discontinuity was fixed during the inversion, its accurate determination for the starting models was critical. The procedure we followed was to fit the differential travel times of PcP-P given in Tables 4.5 and 4.7 by varying this radius. The times were calculated for both depths of focus using the mantle and crustal velocities for model A described above. The differences between the observed times  $(5^{\circ}$  cell means) and the computed times were minimized with an RMS of 0.4 seconds for the radius 3485 km. Since differential times were used, this determination is essentially independent of the upper mantle model we assumed. The radius we obtained is 12 km greater than Jeffrey's value and 7 km greater than the value obtained by Taggart and Engdahl [1968].

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## Table 5.2

| The starting models | The |
|---------------------|-----|
|---------------------|-----|

|                |          | Model A                    |                              |                            |                            |             |
|----------------|----------|----------------------------|------------------------------|----------------------------|----------------------------|-------------|
| Radius<br>(km) | (km/sec) | v <sub>s</sub><br>(km/sec) | $\rho$ (gm/cm <sup>3</sup> ) | v <sub>p</sub><br>(km/sec) | v <sub>s</sub><br>(km/sec) | $(gm/cm^3)$ |
| 0              | 11.20    | 3.50                       | 12.57                        | sam                        | e as model                 | A           |
| 600            | 11.20    | 3.50                       | 12.50                        |                            |                            |             |
| 1215           | 11.20    | 3.50                       | 12.28                        |                            |                            |             |
| 1215           | 10.12    | 0.00                       | 12.28                        |                            |                            |             |
| 1600           | 10,07    | 0.00                       | 12.05                        |                            |                            |             |
| 2000           | 9.85     | 0.00                       | 11.76                        |                            |                            |             |
| 2400           | 9,50     | 0.00                       | 11.40                        |                            |                            |             |
| 2800           | 9.06     | 0.00                       | 10.95                        |                            |                            |             |
| 3200           | 8,51     | 0.00                       | 10.42                        |                            |                            |             |
| 3485           | 8.10     | 0.00                       | 9.98                         |                            |                            |             |
| 3485           | 13.67    | 7.30                       | 5,51                         |                            | •                          |             |
| 3700           | 13,57    | 7.23                       | 5.41                         |                            | ,                          |             |
| 4000           | 13.22    | 7.11                       | 5.26                         |                            |                            |             |
| 4300           | 12.87    | 6.97                       | 5.11                         |                            |                            |             |
| 4600           | 12.51    | 6.81                       | 4.95                         |                            |                            |             |
| 4900           | 12.15    | 6.66                       | 4.79                         |                            |                            |             |
| 5200           | 11.71    | 6.48                       | 4.63                         |                            |                            |             |
| 5500           | 11.22    | 6.29                       | 4.45                         |                            |                            |             |
| 5700           | 10.86    | 6.13                       | 4.33                         |                            |                            |             |
| 5700           | 10.86    | 6.13                       | 4.33                         | 10.71                      | 5.33                       | 4.09        |
| 5951           | 8.80     | 4.55                       | 3.61                         | 9.50                       | 5.33                       | 3.85        |
| 5951           | 8.80     | 4.55                       | 3.61                         | sam                        | e as model                 | А           |
| 6350           | 8.00     | 4.55                       | 3.33                         |                            |                            |             |
| 6350           | 6.20     | 3.40                       | 2.79                         |                            |                            |             |
| 6371           | 6.20     | 3.40                       | 2.79                         |                            | •                          |             |

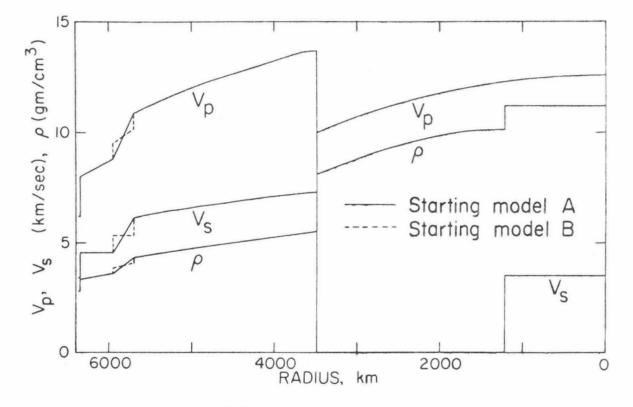


Figure 5.1. The starting models A and B.

The core (regions E, F, and G). A simple model of compressional velocity in the core was designed which fits most of the well-observed features of the PKP travel-time curve. It consists of an inner core and outer core separated by a discontinuity located at 1215 km. The velocity at the core-mantle boundary was taken to equal Jeffrey's value of 8.10 km/sec. The velocities in the outer core varied smoothly from this value to a value of 10.12 km/sec at the inner core - outer core boundary. Below this discontinuity, a constant velocity of 11.20 km/sec was assumed. For this model, the point A of the PKP travel-time curve occurred at a distance of 176°, the point B at 145°, the point C at 158°, and the point D at 111°. It fits Bolt's [1968] absolute times for the AB and DF branches within 2 seconds.

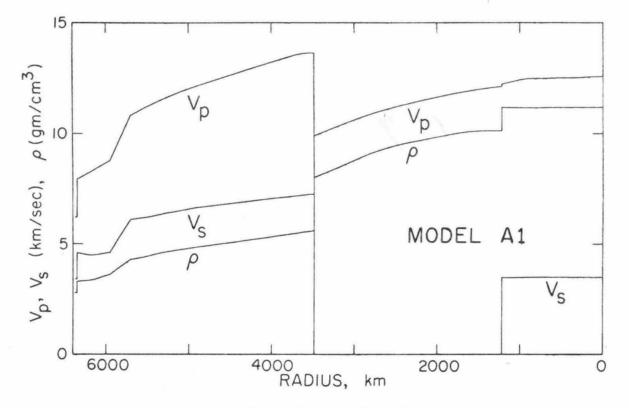
The shear velocity in the outer core was assumed to be zero. The shear velocity in the inner core was taken to equal to 3.5 km/sec, the value determined by Dziewonski and Gilbert [1972].

Once the velocity models had been constructed, it was possible to determine a unique density distribution from the observed values of the Earth's mass and moment of inertia using the method of Birch [1964]. The density in the crust was assumed to equal 2.79 gm/cm<sup>3</sup>. In the upper mantle and in the transition zone the density was assumed to obey the Birch law  $\rho = a v_p + b$ . The density at the top of the mantle was fixed at 3.33 gm/cm<sup>3</sup>, yielding a value of 1.54 gm/cm<sup>3</sup> for the constant b. Below the discontinuity at 671 km, density was determined by integrating the Adams-Williamson equations [Bullen, 1963, p.229]. At the top of the core these equations were re-initiated with a new value of the density (call it  $\rho_c$ ), and the solution was continued to the center. The values of the free parameters a and  $\rho_c$  were determined by fitting the mass and moment of inertia. For both models, the values obtained were 0.349 and 9.98, respectively. These can be compared with Birch's values of 0.379 and 9.96 for his solution II.

The starting models are listed in Table 5.2 and plotted in Figure 5.1.

5.5 <u>Inversion results</u>. We have used the inversion algorithm described in §5.2, the data sets presented in §5.3, and the starting models constructed in §5.4 to derive three estimates of the radial distributions of compressional velocity, shear velocity, and density in the Earth. These results are presented in this section.

<u>Model Al</u>. In this first experiment we were concerned with obtaining a model with a very simple structure in the upper mantle. Model A was used as the starting model. Initially, the fit to the eigenperiod data in data sets I and II was 0.3%, RMS relative deviation. The computed differential travel times deviated from the observed by at most 3 seconds (for ScS-S at  $30^{\circ}$ ). The autocorrelation operators for the functions v<sub>p</sub>, v<sub>s</sub>, and  $\rho$  were partitioned, or "decorrelated", at the radii of the discontinuities separating the inner and outer cores (1215 km), the outer core and mantle (3485 km), and the crust and mantle (6350 km). In each of these regions a correlation operator of the form given in equation (5.2.6) was used, and in all cases we assumed that  $\alpha_p = \beta_p = 0$ . For this experiment, the correlation wavelengths  $\lambda_p = 2/k_p$  were set





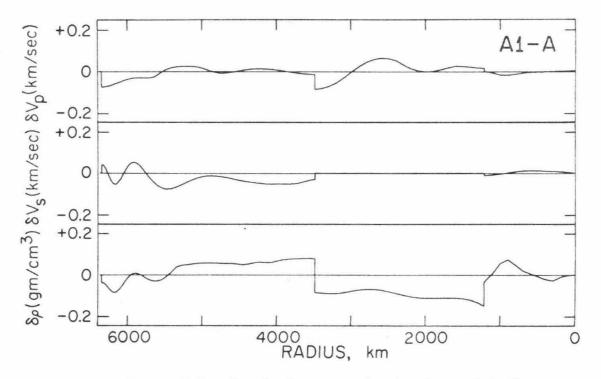


Figure 5.3. Cumulative perturbation for model Al.

equal to 1000 km. The diagonal components of the noise autocorrelation operator (the only nonzero components in the form we have assumed) were taken to equal the squares of the standard errors in the means of the data. In the algorithm we alternated between an inversion of  $v_p$ and  $\rho$  using data set I and an inversion of  $v_g$  and  $\rho$  using data set II. At each step the perturbation was computed from equation (5.2.4.). The perturbation was "overdamped" by setting tan  $\theta$  in this equation equal to 10. Although this value is ten times the "optimal" value of 1, doing this insured more rapid convergence.

For this model, convergence was achieved in six iterations. The final model is plotted in Figure 5.2, and the cumulative perturbation is plotted in Figure 5.3. A listing of the model and its fit to all of the data are given in Appendix 3.

As can be seen from Figure 5.3, the compressional velocity in model Al differs from the starting model by less than 0.05 km/sec everywhere except in the upper mantle and outer core. The value of the velocity at the top of the core is 8.01 km/sec, which is in agreement with Hales' and Roberts' [1971] conclusion that the velocities in this region are less than the values given by the Jeffreys model. Their study was based on the differential travel times of SKKS-SKS. The computed times of SKKS-SKS for model Al are listed along with times computed for equation 3 of their paper in Appendix 3. The agreement is excellent .

The times of P'(DF) are almost 0.3 seconds less than those given by Cleary and Hales [1971] and roughly one second greater than the times

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of Bolt [1968]. The times of P'(AB) computed for Al are a few tenths of a second greater than Bolt's.

The decrease of the compressional velocity in the upper mantle introduced in the inversion shifts the baseline of teleseismic P by about one second. If this amount is added to the P times given in the 1968 tables, then they agree with the times computed from model Al to within 0.2 seconds at distances greater than  $30^{\circ}$ .

The perturbation in the shear velocity distribution in going from model A to model Al is most dramatic in the lower mantle. In this region the perturbation is negative and averages about 0.03 km/sec in magnitude. The effect on the S times is to introduce a "drift" of nearly 5 seconds in the distance range  $30^{\circ}$  to  $80^{\circ}$ . Most responsible for this net decrease in shear velocity are the eigenperiods of the fundamental mode torsional oscillations of low angular order. The incompatibility of torsional oscillation eigenperiods with travel-time data has been evident since the early work of MacDonald and Ness [1961]. However, there seems to be no significant incompatibility between the oscillation data and the ScS-S travel-time data; for model Al all of this data (except for  $T_{ScS-S}(40^{\circ})$  which, due to interference with sS and SS, is poorly determined) is fit to within their 95% confidence intervals.

Because the solution was tightly correlated throughout the upper mantle, model Al has almost no low-velocity zone for shear waves. The need for this feature is evident from the fit of this model to the fundamental torsional mode data. At periods near 200 seconds, the

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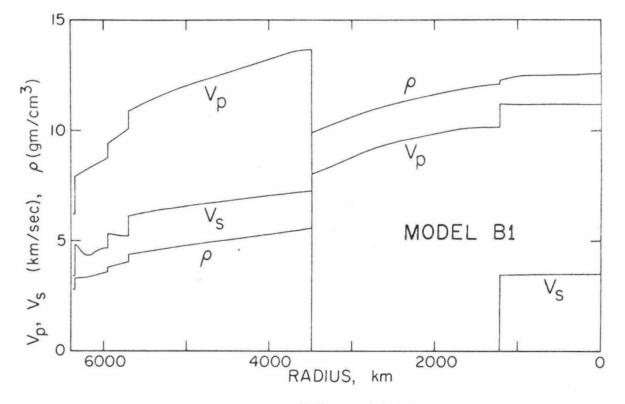
periods computed from the model deviate from the observations by as much as 0.5%, beyond the limits of probable error.

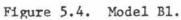
The perturbations to shear velocity in the inner core are very small, confirming the correctness of Dziewonski's and Gilbert's [1972] determination of 3.5 km/sec as the mean velocity of this region. The high phase velocity arrival seen at LASA by Julian, Davies, and Sheppard [1972] and identified by them as PKJKP implies, with this identification, a shear velocity in the inner core of about 2.8 km/sec. This value is incompatible with the mode data.

The cumulative perturbations to the density in the upper mantle are negative. In the resulting model the average density in the upper two hundred kilometers of the mantle is only about 3.33gm/cm<sup>3</sup>. In the lower mantle the perturbations are positive, and in the outer core they are again negative. The inversion introduces a small jump in the density at the boundary between the inner and outer cores, but the significance of this feature is very doubtful.

<u>Model B1</u>. In this second experiment, model B was used as the starting model. The inversion procedure was essentially the same as we used to derive model A1, the principal difference being a different specification of the solution autocorrelation operator. For this inversion, the distributions in the inner core, the outer core, and the lower mantle were decorrelated and assigned correlation wavelengths of 1000 km, as before. In addition, the transition region and the upper mantle were decorrelated. For the former, the correlation wavelengths for each of the three distributions were chosen to be 200 km. For the latter, the

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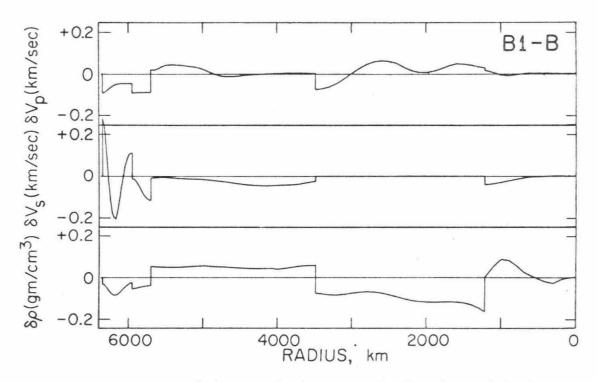


Figure 5.5. Cumulative perturbation for model B1.

correlation wavelengths for the velocities were chosen to be 100 km, and the correlation wavelength for the density was chosen to be 300 km. As before, the distributions in the crust were not inverted.

Convergence was achieved in eight iterations. The final iterate, designated model B1, is listed in Appendix 3 and is plotted in Fig. 5.4. The cumulative perturbations are pictured in Figure 5.5.

The fit of this model to the fundamental spheroidal and torsional mode data sets (given in Table A3.1) is considerably improved over model A1. This improvement results from the introduction of a more profound shear wave low-velocity zone in the upper mantle, made possible by relaxing the smoothing in the upper mantle.

A second feature which distinguishes this model from model Al is that the strong negative perturbation, centered at about 5600 km radius and broadly spread over the upper part of the lower mantle in model Al, is localized in the transition zone in model Bl. Examination of the averaging kernels for this perturbation confirms that this difference is indeed due to localization of the averaging. As a result, the transition zone of model Bl is characterized by a decrease in shear velocity with depth. A similar localization can be observed in the density in this region.

Other than these features, the models A1 and B1 are essentially the same.

<u>Model B2</u>. A second experiment using model B as the starting model was attempted. The purpose of the experiment was to see if modifications in the velocities at the very base of the mantle had any significant

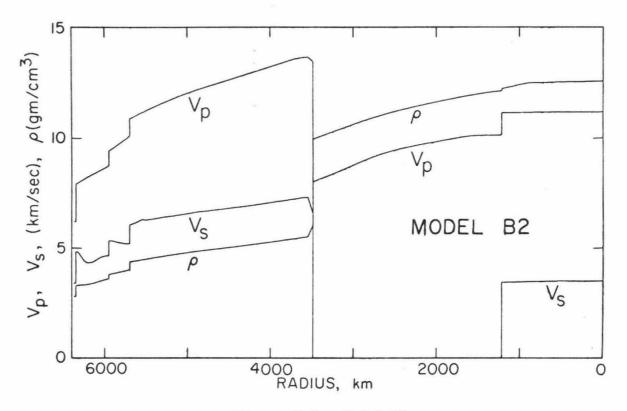


Figure 5.6. Model B2.

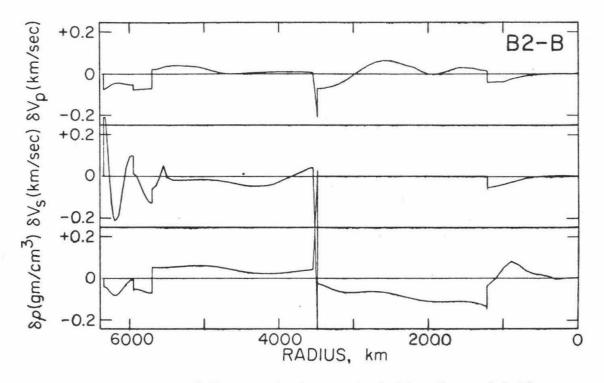


Figure 5.7. Cumulative perturbation for model B2.

effect on the inversion results and to attempt to further localize the averages of shear velocity at the top of the lower mantle by decorrelating at a radius of 5500 km. The existence of a transition zone at the base of the mantle has been the subject of some debate among seismologists since the paper of Dahm in 1936, and the recent observations by Cleary [1966] of so-called diffracted S which indicate a significant decrease in the velocity of S waves in this region, have heightened the speculation. This motivated us to modify the model B in the following way: The compressional velocity at the base of the mantle was decreased to 13.40, the shear velocity was decreased to 6.50, and the density was increased to 6.0. Linear gradients were used to connect these values to the unmodified values for model B at a radius of 3510 km.

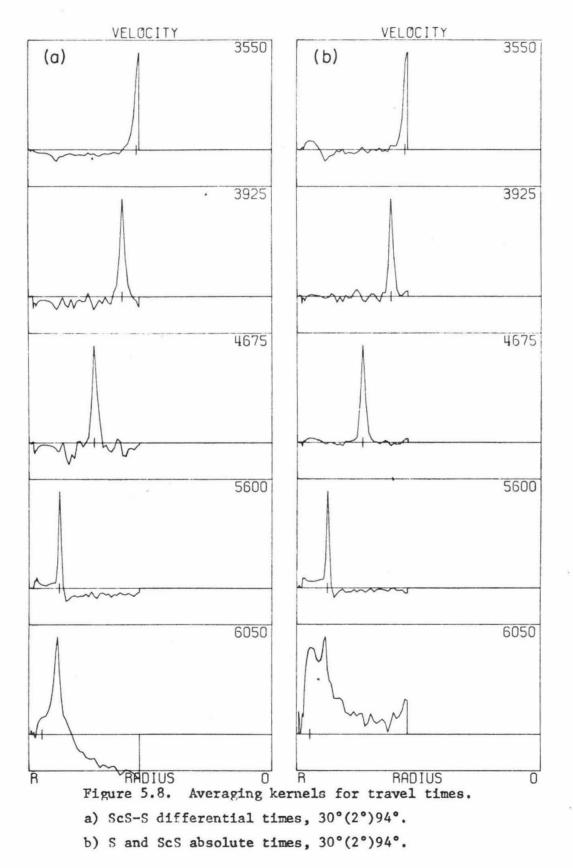
The resulting model was inverted as before, except that the shear velocity was decorrelated at a radius of 5500 km. This was done to localize the averages of shear velocity in this region and to test the hypothesis that a discontinuity in shear velocity exists at this radius. This has been suggested by Hales and Roberts [1970a], among others, on the basis of a discontinuity in the  $dT/d\Delta$  of shear waves at 42°. The correlation wavelength assumed in the region from 5500 km to 5700 km was 100 km.

The results of this inversion, which took eight iterations, was the model B2 plotted in Figure 5.6. Like the other models, it is listed in Appendix 3 along with the fits to the data. The cumulative perturbation for this model sequence is plotted in Figure 5.7.

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The inversion was successful; out of the 166 modes listed in Table A3.1, this model fit 114 of them with a relative error of less than 0.1%. The inversion introduced a region of negative velocity gradient between the depths of 821 and 851 kilometers and a corresponding break in the travel-time curve of S near  $42^{\circ}$ . However, the somewhat simpler model B1 fit the data better; it had 121 of the 166 modes fit with relative errors less than 0.1%. It cannot be argued on the basis of this experiment that the additional features appearing in model B2, in particular the negative gradients in shear velocity in the mantle, are warranted by the data used in the inversion.

5.6 Averaging kernels. We present in this section the averaging kernels, rows of the operator A given by equation (5.2.5), for various data sets and choices of the solution autocorrelation operator  $\mathrm{C}^{}_{\mathrm{ss}}.$ Six figures are presented. In each, the kernels of A corresponding to several radii for a given function,  $v_p$ ,  $v_s$ , or  $\rho$ , are plotted. The radii are indicated by the numbers in the corners of the plot; the function to which the kernel corresponds is indicated by whether the radius is plotted on the left or the right hand side of the graph: the left hand side indicates velocity, and the right hand indicates density. Figure 5.8. This plot shows the results of an experiment to compare the resolving power of absolute versus differential travel times. Two data sets were used. Panel (a) of this figure shows several kernels computed from a data set consisting of 32 ScS-S differential travel times in the distance range 30° to 94°. Panel (b) shows kernels centered at the same radii for a data set consisting of 64 S and ScS absolute times. All data were assumed to have errors of 1 second.



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The model used is Al, and the solution autocorrelation is 100 km. For all radii in the lower mantle, both sets of data yield highly peaked kernels with half-widths of about 75 km, roughly the spacing between the bottoming depths of the S rays. The absolute travel times give somewhat more localized averaging kernels, but the difference is not appreciable. We conclude that not much resolution is lost by using the more precisely observed differential travel times. Of course, since neither data set contains rays which have turning points in the upper mantle, neither yields localized kernels in this region, as can be seen from examination of the kernels centered at 6050 km.

Figure 5.9. Shown in this figure are averaging kernels computed from model Al for compressional velocity using the Fréchet kernels of data set I. The averaging is reasonably localized, although some tradeoff exists between perturbations in compressional velocity and density in the outer core beyond the radii at which P'(AB) rays bottom. Note the localization in the vicinity of the inner core - outer core boundary. This results from using the differential travel times of P'(BC)-P'(DF) The correlation operator used in this computation was the same as was used in the derivation of model Al.

Figure 5.10. This figure displays the averaging kernels for density using the same model, data set, and correlation operator as for Figure 5.9. The averaging in the inner core is extremely poor and unlocalized. We infer that our estimates of density in this region are correspondingly poor. In particular, we doubt that the jump in the density at the inner core - outer core boundary, present in all three models, is significant.

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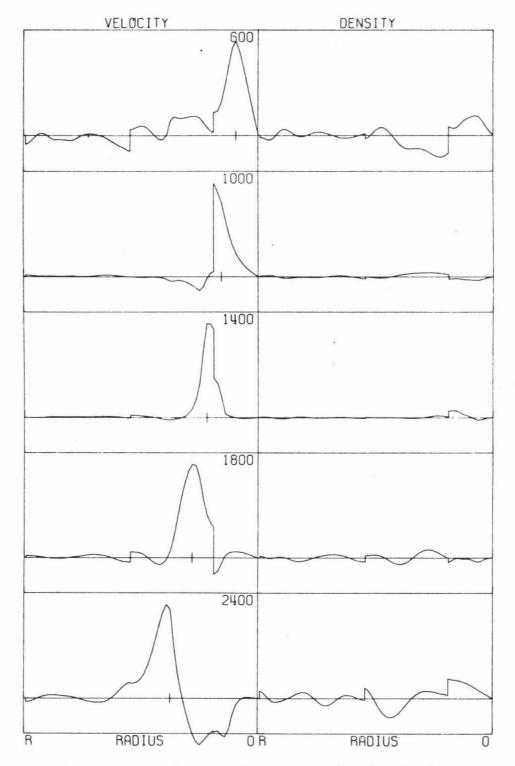


Figure 5.9. Averaging kernels for compressional velocity computed using data set I and the correlation operator for model Al. Functions inverted are compressional velocity and density.

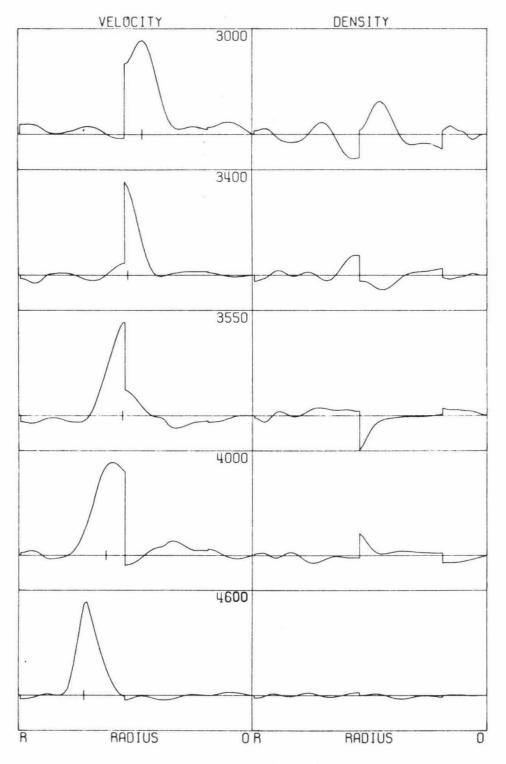


Figure 5.9. (cont.)

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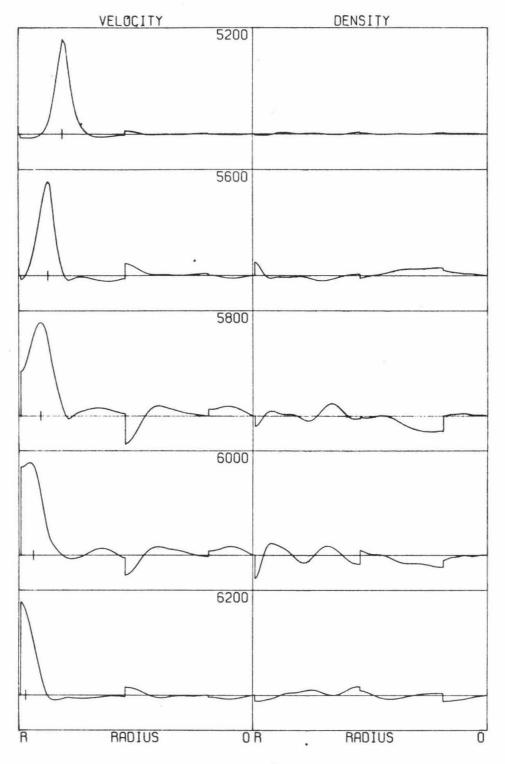


Figure 5.9. (cont.)

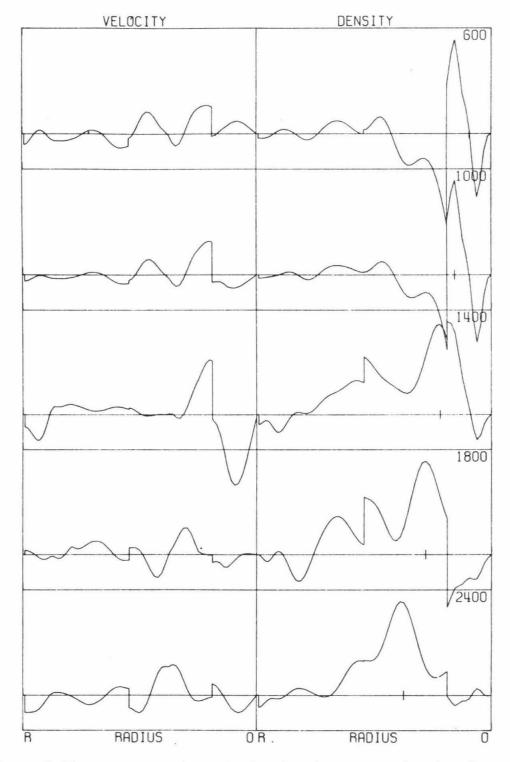


Figure 5.10. Averaging kernels for density computed using data set I and the correlation operator for model Al. Functions inverted are compressional velocity and density.

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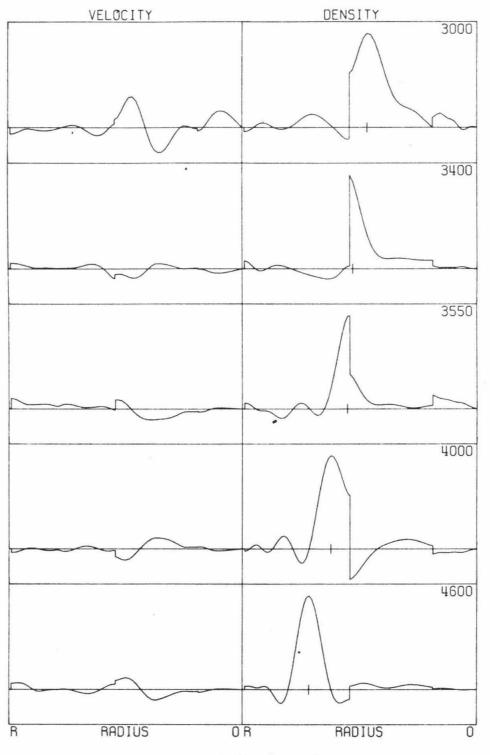


Figure 5.10. (cont.)

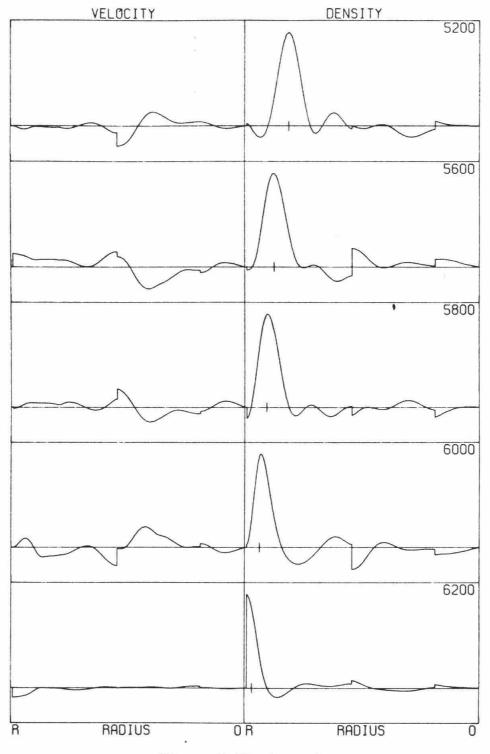


Figure 5.10. (cont.)

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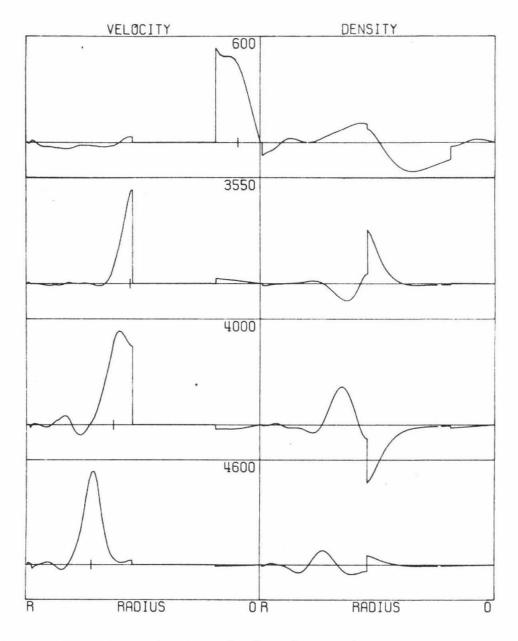


Figure 5.11. Averaging kernels for shear velocity computed using data set II and the correlation operator for model Al. Functions inverted are shear velocity and density.

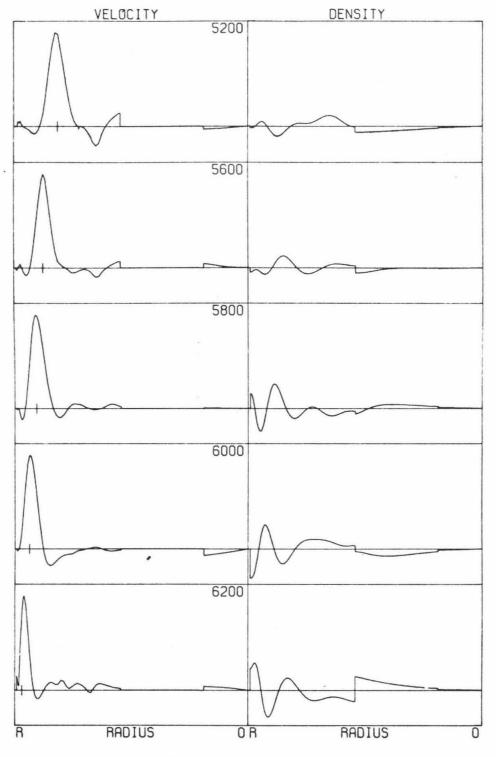


Figure 5.11. (cont.)

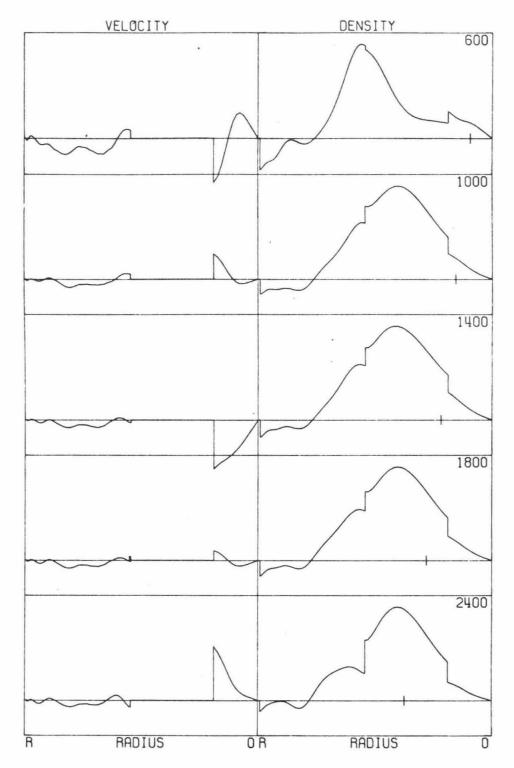
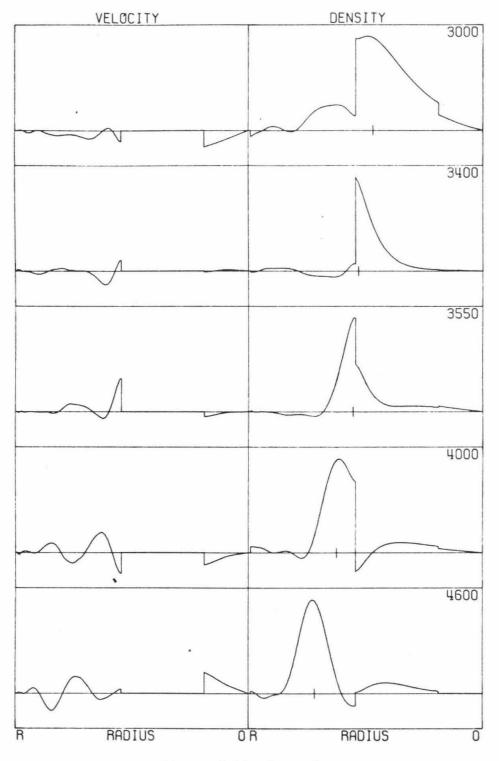
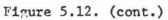


Figure 5.12. Averaging kernels for density computed using data set II and the correlation operator for model Al. Functions inverted are shear velocity and density.





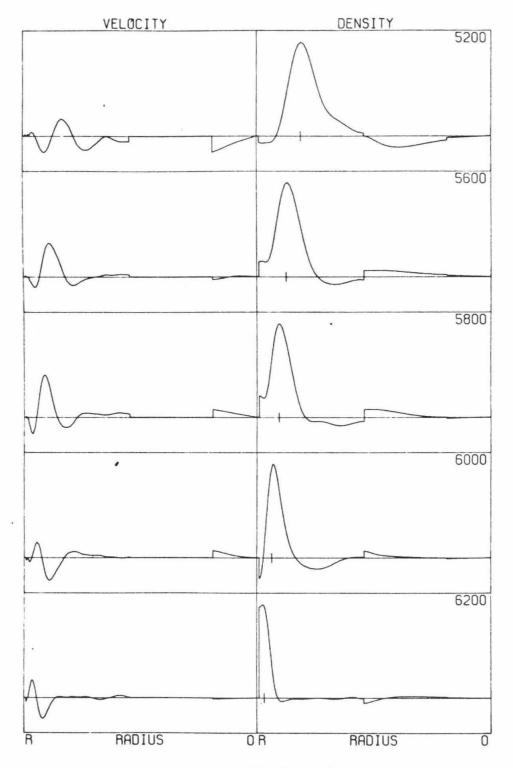


Figure 5.12. (cont.)

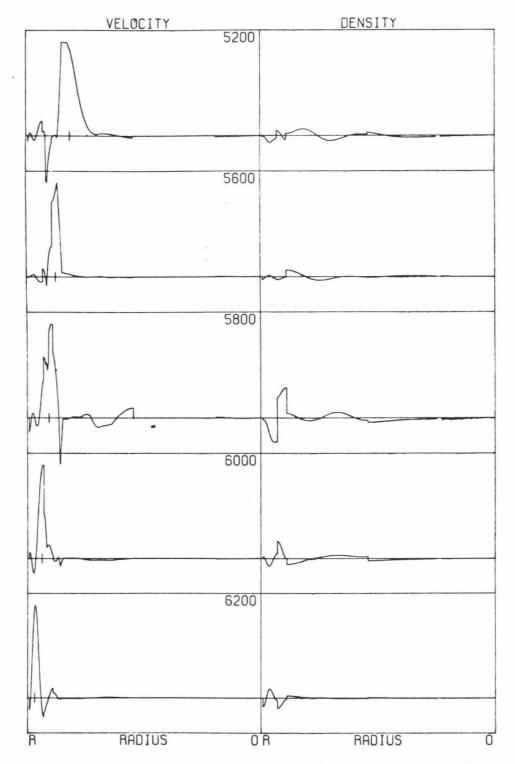


Figure 5.13. Averaging kernels for shear velocity computed using data set II and the correlation operator for model B2. Functions inverted are shear velocity and density.

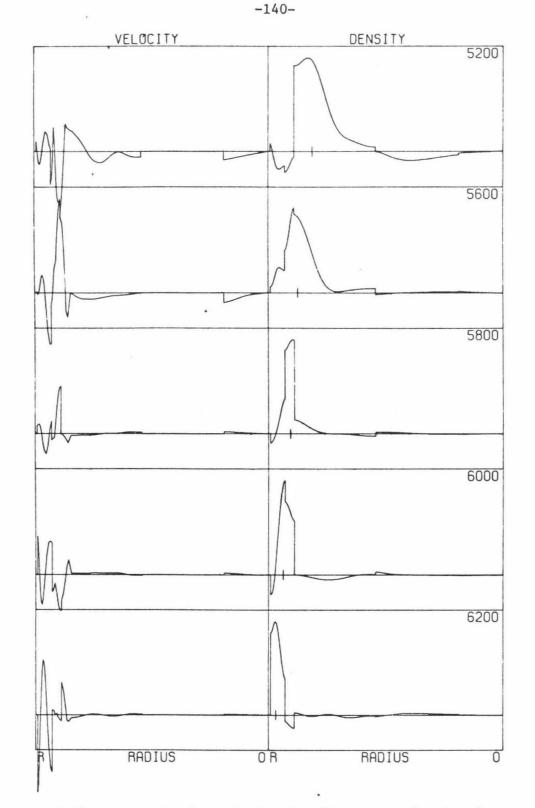


Figure 5.14. Averaging kernels for density computed using data set II and the correlation operator for model B2. Functions inverted are shear velocity and density.

<u>Figure 5.11</u>. We show in this figure the averaging kernels for shear velocity computed from model Al using data set II. The correlation operator is the same as before, although naturally shear velocity in the outer core has been fixed. Most interestingly, we see that the averages of shear velocity in the inner core are reasonably localized, resulting from the inclusion of modes such as  $_{0}S_{2}$ ,  $_{2}S_{2}$ ,  $_{5}S_{2}$ , and  $_{8}S_{2}$  in the data set. It can be inferred that the average shear velocity in the inner core is near the value 3.5 km/sec given by Dziewonski and Gilbert [1972]. As the radius is increased, the averaging kernels become progessively more peaked. However, for kernels centered in the upper mantle and transition zone the tradeoff between shear velocity and density is considerable.

Figure 5.12. This figure corresponds to Figure 5.11, except here the kernels for density are displayed. As we might expect, the averages of density in the core given by this data set are very broad. In fact they are not even localized for radii below about 2400 km. However, at the very top of the core the averaging kernels narrow considerably. The kernels centered in the mantle are similar to those for shear velocity.

Figures 5.13 and 5.14. The averaging kernels shown in these figures correspond to some of the averaging kernels given in Figures 5.11 and 5.12, except that here we use model B2 and its corresponding correlation operator. By comparison of the kernels used in the derivations of these two models, the effect of changing the autocorrelation operator can be seen. Comparison of the kernels for shear velocity centered

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at 6200 km radius in Figure 5.11 and 5.13, for example, illustrates how manipulation of the solution autocorrelation operator can be used to localize the averaging.

5.8 Summary. In this section we summarize our conclusions.

An inversion procedure has been developed to estimate the radial variation of compressional velocity, shear velocity, and density in the Earth. The radial distributions are defined as spherically symmetric averages of the actual distributions in the laterally heterogeneous Earth, and the nature of this averaging implied by averaging certain sets of eigenperiod and travel-time data has been examined. For travel-time data, the spherical averaging is simple if the data sample a distribution which results from a uniform distribution of sources and receivers. Since this is difficult to obtain for absolute times, we have used differential travel times to derive our estimates. It has been shown that the inherent bias in available sets of differential travel-time data. Observations have been presented for the phase combinations PcP-P, ScS-S, P'(AB)-P'(DF), and P'(BC)-P'(DF).

The inversion algorithm developed, based on a linear approximation to the perturbation equations, has been shown to provide a stable method for estimating the radial variations from a finite set of gross Earth data. One advantage of this approach is that it allows one to estimate the resolving power of the data and the resolvability of specified features in the Earth.

Three estimates of the radial distributions have been derived using

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an extensive set of eigenperiod and differential travel-time data, each representing a different level of complexity. Besides satisfying the data used in the inversion, these models also satisfy extensive sets of auxillary data.

The resolving power of the various data sets used in the inversions has been examined by computing their corresponding averaging kernels. It has been shown from this analysis that little resolving power is lost by using differential times in place of absolute times. It has demonstrated that the nature of the averaging for given sets of gross Earth data can be manipulated and improved by a judicious specification of the norm on the space of models.

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APPENDICES

## Appendix 1

## Al.1 Ray-theoretical travel times in a spherically symmetric body.

Suppose that in a sphere S(R) of radius R a signal propogates along a ray with parameter p at a velocity  $v_0(r)$  that varies with radius only. Let  $P_0 = (r_0, \Omega_0)$  be the position of the source and  $P_s = (r_s, \Omega_s)$  be the position of the station, where  $r_0, r_s \in [0, R]$  and  $\Omega_0, \Omega_s \in \partial S(1)$ , the surface of S(1). The ray-theoretical travel time of this signal is

(A1.1.1) 
$$T_0 = \int_{P_0}^{P_s} \frac{ds}{v_0}$$
,

where ds is a differential element of arc length along the ray path between  $P_0$  and  $P_s$ . Fermat's principle states that the permissible paths are those for which  $T_0$  is stationary with respect to path variations.

The travel time  $T_0$  depends on  $v_0$ ,  $P_0$ , and  $P_s$ . We assume that the station is located on  $\partial S(R)$ , the surface of S(R), so that  $r_s = R$ . Then, because the velocities are spherically symmetric,  $T_0$  depends only on  $v_0$ ,  $\Delta$ , and h, where  $\Delta$  is the angular distance between the source and receiver, and h is the focal depth.  $\Delta$  and h are assumed to be fixed, and dependence of  $T_0$  on these quantities will usually be suppressed.

Spherical symmetry implies there exists a function K(r),  $r \! \in \! [0,R],$  such that

(A1.1.2) 
$$T_0 = \int_0^R \frac{K(r)}{v_0(r)} dr.$$

Because s(r) is a multi-valued function, the kernel K(r) is the sum of n+1 terms, n being the number of turning points of the ray generalized to include reflections from and transmissions through discontinuities:

The function s<sub>i</sub>(r) represents arc length along the ith ray segment and is single-valued. From Bullen [1963],

(A1.1.4) 
$$\left| \frac{ds}{dr} i^{(r)} \right| = \frac{\eta(r)}{(\eta^2(r) - p^2)^{1/2}} H[\varepsilon_i(r - \rho_{i-1})] H[\varepsilon_i(\rho_i - r)].$$

Here  $\eta(\mathbf{r}) = \mathbf{r}/\mathbf{v}_0(\mathbf{r})$ ,  $\rho_i$  is the ith turning radius ( $\rho_0 \equiv \mathbf{r}_0 = \mathbf{R} - \mathbf{h}$ ,  $\rho_{n+1} \equiv \mathbf{r}_s = \mathbf{R}$ ),  $H[\sim]$  is the Heaviside function, and  $\varepsilon_i$  equals either +1 or -1 depending on whether the direction of propogation is upward or downward.

The path of the ray can be traced in the following manner. Let  $\Pi_{i-1} \equiv (\rho_{i-1}, \Omega_{i-1})$  be the position vector of the (i-1)th turning point. Then the position vector along the ith ray segment,  $P_i(r) \equiv (r, \Omega_i(r))$ , satisfies the following vector and scalar relationships:

(A1.1.5)  

$$P_{i}(r) \cdot P_{0} \times P_{s} = 0,$$

$$P_{i}(r) \cdot \Pi_{i-1} = r \rho_{i-1} \cos \gamma_{i}(r),$$

$$\gamma_{i}(r) = \int_{\rho_{i-1}}^{r} \frac{\varepsilon_{i} p}{r'(\eta^{2}(r')-p^{2})^{1/2}} dr',$$

$$\varepsilon_{i} \rho_{i-1} \leq \varepsilon_{i} r \leq \varepsilon_{i} \rho_{i}.$$

The first equation states that the ray path lies in the plane defined by the source, the station, and the origin of coordinates; the second defines  $\gamma_i(r)$ , and the third is from Bullen [1963].

Al.2 <u>The Fréchet kernel for travel times</u>. If the velocity distribution in S(R) is varied from  $v_0(r)$  by an amount  $\delta v(r, \Omega)$ , then Fermat's principle implies that the perturbation in the travel time, to first order in  $\delta v$ , is equal to an integral of the velocity perturbation along the ray path [Archambeau and Flinn, 1966; Backus and Gilbert, 1969]:

(A1.2.1) 
$$\delta T = \int_{P_0}^{P_s} \frac{-\delta v}{v_0^2} ds.$$

This expression can be written as an integral over  $(r, \Omega)$ :

(A1.2.2) 
$$\delta T(P_0, P_s) = \int_0^R \int_{\partial S(1)} a(P_0, P_s; r, \Omega) \, \delta v(r, \Omega) \, d\Omega \, dr.$$

The function  $a(P_0, P_s; r, \Omega)$  is the Fréchet kernel for the three-dimensional perturbation problem and is given by

(A1.2.3) 
$$a(P_0, P_s; r, \Omega) = \sum_{i=1}^{n+1} -v_0^{-2}(r) \left| \frac{ds}{dr} i^{(r)} \right| \delta[\Omega - \Omega_i(r)].$$

Here  $\delta[\sim]$  is the Dirac delta distribution on  $\partial S(1)$ , and  $\Omega_i(r)$  is determined by (Al.1.5). If the velocity perturbations are spherically symmetric, the equation (Al.2.2) can be written

(A1.2.4) 
$$\delta T = \int_0^R a(r) \, \delta v(r) \, dr ,$$

where

(A1.2.5) 
$$a(r) = \int_{\partial S(1)} a(P_0, P_s; r, \Omega) d\Omega$$

is the spherically symmetric Fréchet kernel for travel times.

Al.3 <u>Proof of the averaging theorem for travel times</u>. In §3.4 we stated a simple averaging theorem for travel times. Its proof is a simple matter. Without loss of generality assume that all sources and receivers are located on the surface  $\partial S(R)$ . To first order, the travel time  $T(P_0,P_s)$  between a source located at  $P_0$  and a station located at  $P_s$  can be written as the sum of two terms:

(A1.3.1) 
$$T = T_0 + \delta T$$
.

The first term on the right-hand side of this expression is the travel time through the spherically symmetric Terrestrial Monopole, defined by equation (3.2.1). The second term is the first-order perturbation in the travel time due to an aspherical perturbation  $\delta v$  in the velocity. The first term depends only on the angular distance  $\Delta$  separating the source and receiver, while the second term depends only on P<sub>0</sub>,  $\Delta$ , and the azimuth  $\zeta$  from P<sub>0</sub> to P<sub>e</sub>.

The hypothesis of the existence of uniform distributions of sources and receivers implies that the probability that a source lies in the region  $d\Omega_0$  about the point  $P_0$  and that, for a fixed  $\Delta$ , a receiver lies between the azimuths  $\zeta$  and  $\zeta + d\zeta$  is constant. The averaging theorem is proved if we can show that the mean fluctuation  $\overline{\delta T}$ is zero. Because the distributions are uniform, we have

(A1.3.2) 
$$\overline{\delta T} \propto \int_{S(1)} \int_{0}^{2\pi} \delta T(\Omega_0, \zeta) d\zeta d\Omega_0$$

where  $\delta T(\Omega_0, \zeta)$  is given by equation (A1.2.2). Equation (A1.2.2) can be integrated immediately with respect to  $\Omega$ . This yields

(A1.3.3) 
$$\delta T(\Omega_0,\zeta) = \int_0^R \sum_{i=1}^{n+1} a_i(r) \, \delta v(r,\Omega_i) \, dr,$$

where  $a_i(r) \equiv -v_0^{-2}(r) |ds_i(r)/dr|$ . In equation (A1.3.3)  $\Omega_i$  will depend on r,  $\Omega_0$ , and  $\zeta$  through the relations (A1.1.5).

Now, we substitute (A1.3.3) into (A1.3.2) and interchange the order of integration. We obtain that  $\overline{\delta T}$  is proportional to

(A1.3.4) 
$$\int_{0}^{R} \sum_{i=1}^{n+1} a_i(r) \int_{S(1)} \int_{0}^{2\pi} \delta v(r, \alpha_i) d\zeta d\alpha_0 dr.$$

At any specified radius r, the locus of the intersection of S(r) and the ith ray segment describes, for fixed  $\Omega_0$  as  $\zeta$  is varied, a circle on S(r). These circles cover S(r) uniformly, and, therefore,

(A1.3.5) 
$$\int_{S(1)} \int_{0}^{2\pi} \delta \mathbf{v}(\mathbf{r}, \Omega_{\mathbf{i}}) \, d\zeta \, d\Omega_{0} \propto \int_{S(1)} \delta \mathbf{v}(\mathbf{r}, \Omega) \, d\Omega.$$

By definition, however, aspherical perturbations average to zero when integrated over the sphere. Thus, the integral on the right-hand side of (A1.3.5) is zero, implying that  $\overline{\delta T}$  is zero. This proves the averaging theorem.

| - | 1 | 5 | 8 | - |
|---|---|---|---|---|
|---|---|---|---|---|

## Appendix 2

A2.1 PcP-P differential travel-time data [nuclear explosions].

| EVENT         | STATION    | ∆<br>(deg.) | TIME<br>(sec.) | OBS-JB<br>(sec.) |
|---------------|------------|-------------|----------------|------------------|
| KOGAN (S.     | PACIFIC)   |             |                |                  |
| (h = 0 km)    | UGL        | 42.05       | 114.7          | -0.8             |
| (n = 0  km)   | TEM        | 46.68       | 92.8           | -1.3             |
|               | TEM        | 46.72       | 93.4           | -0.5             |
|               | TEM        | 46.90       | 89.7           | -3.5             |
|               | KAB        | 61.75       | 40.7           | +0.4             |
|               | COL        | 62.10       | 40.0           | +0.2             |
|               | IRK        | 63.20       | 37.2           | +0.1             |
|               | SEM        | 77.88       | 10.5           | -0.5             |
| BUCHBINDE     | R (BILBY)  |             |                |                  |
| (h = 0 km)    | AAM        | 25.36       | 213.3          | -0.3             |
| (II - 0 KIII) | ATL        | 26.06       | 207.5          | -1.0             |
|               | LND        | 27.19       | 200.8          | +0.0             |
|               | BL-        | 27.48       | 198.6          | -0.3             |
|               | BLA        | 28.28       | 192.6          | -1.0             |
|               | CSC        | 28.57       | 191.4          | -0.4             |
|               | BR-        | 29.11       | 188.0          | -0.2             |
|               | SCP        | 29.75       | 184.3          | +0.3             |
|               | OTT        | 31.17       | 175.5          | +0.3             |
|               | DH-        | 31.86       | 171.0          | +0.1             |
|               | COL        | 33.61       | 159.8          | -0.8             |
|               | HN-        | 36.56       | 143.3          | -0.6             |
|               | HW-        | 38.48       | 133.5          | -0.2             |
|               | RES        | 39.03       | 130.9          | +0.2             |
|               | MBC        | 39.30       | 128.1          | -1.3             |
|               | NP-        | 39.32       | 128.0          | -1.3             |
|               | BHP        | 43.24       | 107.9          | -1.9             |
|               | SJG        | 47.36       | 90.4           | -0.9             |
|               | ALE        | 48.90       | 84.3           | -0.6             |
|               | CAR        | 51.40       | 73.7           | -1.2             |
|               | TRN        | 55.56       | 62.0           | +2.2             |
|               | KON        | 73.71       | 17.1           | +1.0             |
| KANAMORI      | (LONGSHOT) |             |                |                  |
| (h = 0 km)    | TSK        | 31.61       | 171.3          | -1.1             |
|               | MAT        | 32.56       | 165.5          | -1.1             |
|               | MYK        | 35.27       | 149.3          | -1.4             |
|               | SHK        | 37.28       | 138.8          | -1.1             |
|               | SEO        | 38.91       | 129.8          | -1.5             |

| EVENT       | STATION   | Δ      | TIME   | OBS-JB |
|-------------|-----------|--------|--------|--------|
| DYDRI       | SIRION    | (deg.) | (sec.) | (sec.) |
|             |           | (468.) | (300.) | (360.) |
| LAMBERT ET. | AL. (LONG | SHOT)  |        |        |
| (h = 0 km)  | WH-       | 26.60  | 204.0  | -0.8   |
| ()          | WL-       | 29.80  | 181.9  | -4.6   |
|             | MTJ       | 31.60  | 171.5  | -1.1   |
|             | SI -      | 31,80  | 168.7  | -0.6   |
|             | MAT       | 32.60  | 165.7  | -1.2   |
|             | PHC       | 32.90  | 151.9  | -2.6   |
|             | FL-       | 33.00  | 163.9  | -0.1   |
|             | MBC       | 34.00  | 155.6  | -2.5   |
|             | NP-       | 34.00  | 156.1  | -2.0   |
|             | PG-       | 34.50  | 156.2  | +1.0   |
|             | KIP       | 34.80  | 152.2  | -1.8   |
|             | HON       | 34.90  | 151.0  | -2.5   |
|             | CMC       | 35.00  | 150.8  | -1.8   |
|             | YKA       | 36.10  | 145.9  | -0.8   |
|             | VIC       | 36.20  | 144.7  | -1.3   |
|             | YKC       | 36.20  | 145.3  | -1.2   |
|             | KV-       | 36.40  | 145.0  | -0.2   |
|             | TUM       | 37.20  | 140.5  | -0.2   |
|             | SHK       | 37.30  | 139.2  | -1.5   |
|             | JP-       | 37.40  | 138.8  | -0.3   |
|             | HIL       | 37.60  | 137.5  | -1.9   |
|             | PAH       | 37.80  | 136.2  | -1.6   |
|             | LON       | 38.00  | 135.7  | -0.7   |
|             | PNT       | 38.10  | 135.2  | -0.8   |
| Ϋ́.         | COR       | 38.20  | 134.4  | -1.1   |
| 5           | SEO       | 38.90  | 129.5  | -2.4   |
|             | RM6       | 39.40  | 132.1  | +2.2   |
|             | EDM       | 39.90  | 127.4  | +0.9   |
|             | LD6       | 39.90  | 129.0  | +2.5   |
|             | YR-       | 40.10  | 123.2  | -1.7   |
|             | BMO       | 41.70  | 116.5  | -0.4   |
|             | ннм       | 41.80  | 116.6  | +0.2   |
|             | ORV       | 42.10  | 113.8  | -0.9   |
|             | BA6       | 42.50  | 112.1  | -1.3   |
|             | BKS       | 42.70  | 111.5  | -0.9   |
|             | BRK       | 42.70  | 112.5  | -0.3   |
|             | SW-       | 42.70  | 112.3  | -0.4   |
|             | ALE       | 42.80  | 109.7  | -2.4   |
|             | PCC       | 42.80  | 111.1  | -0.1   |
|             | NRR       | 43.10  | 109.2  | -1.2   |
|             | BLC       | 43.40  | 111.1  | +1.8   |
| :#          | GCC       | 43.40  | 108.5  | -1.1   |
|             | MHC       | 43.40  | 108.3  | -0.6   |
|             | UNN       | 43.70  | 106.6  | -1.1   |
|             |           |        | 20000  | * * *  |

|         | 8            |                |              |   |
|---------|--------------|----------------|--------------|---|
| EVENT   | STATION      | Δ              | TIME         | OBS-JB                                    |
|         |              | (deg.)         | (sec.)       | (sec.)                                    |
|         |              |                |              | and the second state in the second states |
| LAMBERT | ET.AL.(LONGS |                |              |   |
|         | JAS          | 43.80          | 106.3        | -0.9                                      |
|         | 'HL2         | 44.10          | 105.7        | +0.7                                      |
|         | HV-          | 44.20          | 106.8        | +1.6                                      |
|         | PRS          | 44.20          | 104.4        | -1.1                                      |
|         | SH6          | 44.20          | 104.8        | -1.0                                      |
|         | LLA          | 44.30          | 103.8        | -1.4                                      |
|         | BOZ          | 44.60          | 103.6        | +0.3                                      |
|         | PRI          | 44.80          | 102.0        | -1.1                                      |
|         | MN-          | 44.90          | 99.7         | -2.7                                      |
|         | CH6          | 45.20          | 100.3        | -0.9                                      |
|         | FFC          | 45.20          | 101.7        | +0.1                                      |
|         | EUR          | 45.60          | 97.8         | -1.2                                      |
|         | TIN          | 45.70          | 97.4         | -1.2                                      |
|         | TNP          | 45.70          | 97.5         | -1.1                                      |
|         | TF-          | 45.80          | 97.0         | -1.0                                      |
|         | KRC          | 45.90          | 96.7         | -1.4                                      |
|         | WU6          | 46.00          | 96.8         | +0.1                                      |
|         | ISA          | 46.40          | 94.6         | -0.7                                      |
|         | SBC          | 46.40          | 93.9         | -1.4                                      |
|         | PI6          | 46.60          | 97.0         | +2.1                                      |
|         | FTC          | 46.70          | 93.9         | -0.7                                      |
|         | CLC          | 46.90          | 92.8         | -1.0                                      |
|         | LAO          | 47.10          | 92.2         | -0.2                                      |
|         | MWC          | 47.60          | 90.3         | +0.3                                      |
|         | PAS          | 47.60          | 89.0         | -1.3                                      |
|         | GSC          | 47.70          | 89.6         | -0.2                                      |
|         | RVR          | 48.20          | 88.6         | +0.8                                      |
|         | BCN          | 48.60          | 85.9         | -1.2                                      |
|         | IRF          | 48.60          | 84.8         | -1.6                                      |
|         | FGU          | 48.70          | 86.0         | +0.4                                      |
|         | PLM          | 48.90          | 84.0         | -0.6                                      |
|         | UBO          | 49.00          | 84.0         | -0.8                                      |
|         | KN-          | 49.10          | 83.4         | -1.0                                      |
|         | BAR          | 49.50          | 82.2         | -0.1                                      |
|         | HAY          | 49.50          | 83.3         | +0.7                                      |
|         | RG-          | 49.60          | 83.6         | +1.6                                      |
|         | CP-          | 49.70          | 81.7         | +0.1                                      |
|         | GCA          | 49.80          | 81.0         | +0.5                                      |
|         | RCD          | 50.40          | 79.2         | +1.0                                      |
|         | RK-<br>LAR   | 51.50          | 75.9         | +1.0                                      |
|         | PA6          | 50.70          | 77.9         | -2.8                                      |
|         | TA6          | 51.80          | 73.3         | -0.3                                      |
|         | TFO          | 51.80<br>51.80 | 73.2<br>72.8 | -0.1<br>-0.6                              |
|         | 110          | 1.00           | 12.0         | -0.0                                      |

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| EVENT     | STATION      | ∆<br>(deg.) | TIME<br>(sec.) | OBS-JB<br>(sec.) |
|-----------|--------------|-------------|----------------|------------------|
| LAMBERT E | T.AL. (LONGS | HOT, CONT.) |                |                  |
|           | GOL          | 51.90       | 72.8           | -0.4             |
|           | SA6          | 51.90       | 72.8           | -0.7             |
|           | WN-          | 52.60       | . 70.6         | +0.7             |
|           | TUC          | 53.40       | 67.7           | +0.9             |
|           | TRG          | 53.90       | 66.1           | +0.5             |
|           | ALQ          | 54.30       | 64.5           | +0.9             |
|           | GWC          | 56.00       | 57.8           | -0.4             |
|           | LC-          | 56.00       | 56.9           | -1.8             |
|           | MHT          | 57.30       | 55.2           | +1.0             |
|           | HKC          | 57.40       | 54.0           | -0.5             |
|           | WW6          | 57.40       | 54.6           | +0.9             |
|           | BAG          | 57.90       | 52.5           | -0.3             |
|           | LUB          | 58.00       | 53.1           | +0.7             |
|           | MAN          | 58.90       | 48.2           | -3.6             |
|           | WMO          | 59.20       | 48.8           | +0.2             |
|           | SV3          | 60.80       | 44.6           | +0.4             |
|           | ROL          | 60.90       | 47.0           | +2.2             |
|           | GV-          | 61.40       | 42.2           | +0.0             |
|           | JCT          | 61.40       | 41.3           | -0.9             |
|           | DAL          | 61.60       | 41.8           | -0.2             |
|           | AAM          | 62.30       | . 42.3         | +2.4             |
|           | DAV          | 62.30       | 40.3           | +0.3             |
|           | EN-          | 62.30       | 42.3           | +2.7             |
|           | KJN          | 62.70       | 40.2           | +1.2             |
|           | LRA          | 62.80       | 38.0           | -0.6             |
|           | LND          | 63.00       | 37.4           | -0.6             |
|           | MLF          | 64.20       | 32.9           | -2.0             |
|           | SJ-          | 64.40       | 33.3           | -1.3             |
|           | CPO          | 66.10       | 27.4           | -3.1             |
|           | SCP          | 66.40       | 30.8           | +0.8             |
|           | PMG          | 66.60       | 28.6           | -0.8             |
|           | DH-          | 66.70       | 32.3           | +3.6             |
|           | HN-          | 66.90       | 30.0           | +1.6             |
|           | FN-          | 67.20       | 29.3           | +1.4             |
|           | BLA          | 67.70       | 28.2           | +1.5             |
|           | SFO          | 67.80       | 27.1           | +0.8             |
|           | NHA          | 68.10       | 26.9           | -4.4             |
|           | PAL          | 68.20       | 28.7           | +2.6             |
|           | ATL          | 68.40       | 29.3           | +3.5             |
|           | UDD          | 68.40       | 24.5           | -2.4             |
|           | STJ          | 71.80       | 15.5           | -3.7             |
|           | BE-          | 73.10       | 15.5           | -2.4             |
|           | RAR          | 74.70       | 14.0           | -1.0             |
|           | DOU          | 78.70       | 4.4            | -4.8             |

| EVENT         | STATION | Δ      | TIME   | OBS-JB | QUAL. |
|---------------|---------|--------|--------|--------|-------|
|               |         | (deg.) | (sec.) | (sec.) |       |
| MINDINAO      |         |        |        |        |       |
| (h = 605  km) | CHG     | 26.51  | 181.9  | -2.2   | 1     |
| PERU-BRAZIL   | A       |        |        |        |       |
| (h = 587  km) | BEC     | 41.67  | 102.9  | -0.1   | 4     |
|               | SOM     | 43.64  | 92.0   | -2.3   | 4     |
|               | ATL     | 44.01  | 92.4   | -0.3   | 5     |
|               | BLA     | 46.79  | 80.6   | -0.7   | 4     |
|               | GEO     | 47.99  | 76.9   | +0.3   | 4     |
|               | DAL     | 48.20  | 75.2   | -0.2   | 5     |
|               | OGD     | 49.94  | 96.4   | 0.0    | 4     |
|               | SCP     | 49.96  | 69.4   | +0.1   | 4     |
|               | WES     | 51.17  | 65.0   | 0.0    | 4     |
|               | LUB     | 51.37  | 64.6   | +0.2   | 5     |
|               | AAM     | 52.32  | 61.2   | +0.1   | 4     |
|               | ALQ     | 54.93  | 53.2   | +0.4   | 5     |
|               | GOL     | 57.85  | 44.2   | -0.1   | 4     |
|               | RCD     | 60.24  | 36.5   | -1.6   | 4     |
|               | GSC     | 61.53  | 34.1   | -0.8   | 4     |
|               | DUG     | 62.20  | 32.5   | -0.8   | 4     |
|               | BOZ     | 65.31  | 25.2   | -1.3   | 3     |
|               | BKS     | 66.58  | 23.1   | -1.0   | 4     |
|               | CDR     | 71.00  | 15.4   | -1.1   | 2     |
| FIJI B        |         |        |        |        |       |
|               | CTA     | 32.37  | 147.2  | -1.3   | 3     |
| (h = 627  km) | RAB     | 32.49  | 147.5  | -0.3   | 5     |
|               | PGM     | 34.42  | 136.8  | -0.6   | 4     |
|               | GUA     | 49.24  | 70.2   | -0.8   | 3     |
|               | MUN     | 58.14  | 41.5   | -1-4   | 2     |
|               | DAV     | 61.01  | 35.9   | +0.4   | 4     |
|               | MAN     | 68.55  | 19.8   | -0.3   | 3     |
|               | BAG     | 69.84  | 14.1   | -3.8   | 1     |
|               |         |        |        |        |       |
| ARGENTINA     | 0.00    |        |        |        | -     |
| (h = 571  km) | BOG     | 32.33  | 150.4  | -0.6   | 3     |
|               | SJG     | 44.01  | 93.7   | +0.5   | 3     |
|               | LPS     | 47.50  | 77.1   | -1.8   | 2     |
|               | ATL     | 62.54  | 31.8   | -1.0   | 1     |
|               | SPA     | 64.09  | 63.0   | +0.3   | 4     |
|               | BLA     | 65.03  | 24.4   | -2.9   | 2     |
|               | SOB     | 71-22  | 15.7   | -0.5   | 4     |
|               | WIN     | 71.97  | 15.3   | +0.2   | 3     |
|               | SBA     | 72.30  | 14.4   | -0.2   | 1     |

A2.2 PcP-P differential travel-time data [deep-focus events].

| EVENT                      | STATION  | ∆<br>(deg.)  | TIME<br>(sec.)   | OBS-JB<br>(sec.)   | QUAL.                      |
|----------------------------|--|--|--|--|----------------------------|
| PERU-BRAZIL                | В  |  |  |  |                            |
| (h = 598 km)               | SJG<br>BEC<br>SHA<br>SOM<br>ATL<br>BLA<br>JCT<br>GEO<br>OGD<br>WES<br>LUB<br>AAM<br>ALQ<br>TUC<br>GOL<br>GSC<br>DUG<br>BOZ | 27.47<br>41.68<br>42.68<br>43.63<br>44.01<br>46.79<br>47.87<br>48.00<br>49.95<br>51.18<br>51.37<br>52.32<br>54.92<br>55.75<br>57.85<br>61.53<br>62.19<br>65.31 | 173.9<br>101.8<br>98.3<br>93.1<br>91.9<br>80.2<br>76.4<br>76.5<br>69.1<br>64.7<br>64.1<br>61.0<br>53.1<br>50.1<br>43.6<br>33.6<br>31.4<br>24.8 | $ \begin{array}{r} -4.6 \\ -0.8 \\ +0.1 \\ -0.9 \\ -0.5 \\ -0.8 \\ -0.4 \\ +0.2 \\ 0.0 \\ -0.1 \\ 0.0 \\ +0.1 \\ +0.5 \\ 0.0 \\ -1.1 \\ -1.8 \\ -1.6 \end{array} $ | 12434445555555534          |
|                            | COR  | 71.00  | 15.0   | -1.4   | 3                          |
| JAVA SEA A<br>(h = 606 km) | CHG<br>ANP<br>CTA<br>GUA<br>RIV<br>TAU<br>MAT<br>WEL   | 27.94<br>32.26<br>35.79<br>37.73<br>45.36<br>47.99<br>48.78<br>65.47   | 174.8<br>146.0<br>131.2<br>117.5<br>85.9<br>76.0<br>72.7<br>24.7   | -0.4<br>-4.0<br>+0.2<br>-3.6<br>-0.6<br>-0.2<br>-0.5<br>-1.3   | 1<br>2<br>2<br>2<br>3<br>3 |
| FIJI C<br>(h = 643 km)     | TAU<br>GUA<br>MUN  | 35.44<br>49.15<br>58.04  | 129.0<br>70.8<br>43.2  | -2.4<br>-0.1<br>+0.3   | 2<br>1<br>4                |
| CHINA<br>(h = 555 km)      | CHG  | 35.63  | 130.2  | -3.4   | 4                          |
| MARIANAS<br>(h = 602 km)   | HKC<br>SNG<br>SHL<br>COL<br>NIL  | 29.28<br>44.79<br>49.62<br>63.59<br>65.17  | 166.3<br>87.2<br>70.1<br>30.2<br>24.5  | -1.0<br>-1.8<br>-0.1<br>+0.2<br>-2.2   | 4<br>2<br>2<br>4           |

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| EVENT | STATION   | ∆<br>(deg.) | TIME<br>(sec.) | OBS-JB<br>(sec.) | QUAL.            |
|-------|-----------|-------------|----------------|------------------|------------------|
| SEA O | F OKHOTSK |             |                |                  |                  |
|       | ANP       | 35.21       | 130.9          | -4.1             | 4                |
|       | BAG       | 43.23       | 92.6           | -3.7             | 3                |
|       | NOR       | 46.30       | 83.6           | +0.2             | 2<br>3<br>3<br>3 |
|       | KBS       | 46.95       | 80.2           | -0.7             | 3                |
|       | KEV       | 51.85       | 62.3           | -0.6             | 3                |
|       | CHG       | 52.56       | 59.9           | -0.6             | 3                |
|       | RAB       | 56.18       | 47.9           | -1.3             | 1                |
|       | KTG       | 57.61       | 44.6           | -0.5             | 3                |
|       | UME       | 58.23       | 42.1           | -1.2             | 5                |
|       | NDI       | 58.43       | 42.6           | -0.3             | 5                |
|       | BKS       | 59.17       | 34.4           | -4.5             | 3                |
|       | NUR       | 59.83       | 38.1           | -1.1             | 4                |
|       | SNG       | 61.06       | 34.1           | -2.3             | 4                |
|       | PMG       | 61.47       | 34.1           | -1.0             | 3<br>2<br>2<br>2 |
|       | AKU       | 62.18       | 32.3           | -0.2             | 2                |
|       | DUG       | 62.67       | 32.7           | +0.4             | 2                |
|       | QUE       | 63.52       | 28.8           | -1.6             | 2                |
|       | GOL       | 66.88       | 23.2           | -0.4             | 2<br>3           |
|       | P00       | 67.98       | 20.7           | -0.9             | 3                |
|       | TUC       | 69.62       | 18.3           | -0.4             | 2                |

| EVENT         | STATION | ۵<br>(deg.) | TIME<br>(sec.) | OBS-JB<br>(sec.) | QUAL.                      |
|---------------|---------|-------------|----------------|------------------|----------------------------|
| FIJI A        |         |             |                |                  |                            |
| (h = 535  km) | RIV     | 31.30       | 307.0          | +9.0             | 4                          |
|               | CTA     | 33.18       | 287.2          | +8.2             | 3                          |
|               | ADE     | 41.44       | 211.0          | +6.6             | 3<br>2<br>4<br>5<br>3<br>2 |
|               | KIP     | 43.57       | 182.8          | -4.6             | 2                          |
|               | GUA     | 47.55       | 161.3          | +3.4             | 4                          |
|               | MUN     | 59.91       | 89.1           | +5.8             | 5                          |
|               | DAV     | 60.33       | 89.0           | +7.8             | 3                          |
|               | BAG     | 68.80       | 50.3           | +5.3             | 2                          |
|               | LEM     | 72.44       | 32.3           | -0.7             | 3                          |
|               | SEO     | 75.14       | 30.2           | +4.8             | 4                          |
|               | BKS     | 76.69       | 19.5           | -2.0             | 2                          |
| NEW HEBRIDE   | S       |             |                |                  |                            |
| (h = 641  km) | RIV     | 26.72       | 345.6          | +7.3             | 5                          |
|               | TAU     | 35.42       | 257.3          | +7.5             | 4                          |
|               | ADE     | 35.66       | 251.7          | +4.2             | 3                          |
|               | GUA     | 36.76       | 236.7          | -0.9             | 2                          |
|               | MUN     | 52.65       | 120.5          | +1.1             | 4                          |
|               | BAG     | 57.40       | 95.5           | +3.0             | 3                          |
| -             | LEM     | 61.92       | 75.0           | +4.8             | 4                          |
|               | SEO     | 65.03       | 61.8           | +5.0             | i                          |
|               | HKC     | 65.48       | 55.9           | +0.9             | 2                          |
|               | CHG     | 77.22       | 13.9           | -4.7             | 4                          |
| MINDINAO      |         |             |                |                  |                            |
|               | SEO     | 20 02       | 210 5          | 12 6             | 4                          |
| (h = 605  km) | SHL     | 29.93       | 310.5          | +3.6             | 4                          |
|               | CTA     | 35.22       | 254.0          | -0.3             | 3                          |
|               | CIA     | 35.34       | 258.4          | +5.2             | 3                          |
| PERU-BRAZIL   |         |             |                |                  |                            |
| (h = 587  km) | SJG     | 27.45       | 342.6          | +7.6             | 2                          |
|               | LPS     | 29.16       | 321.8          | +5.3             | 3                          |
|               | SOM     | 43.64       | 182.4          | -1.7             | 4                          |
|               | ATL     | 44.01       | 183.2          | +2.0             | 5                          |
|               | DAL     | 48.20       | 150.7          | -0.1             | 3                          |
|               | OGD     | 49.94       | 132.6          | -6.5             | 5                          |
|               | SCP     | 49.96       | 132.5          | -6.5             | 5<br>3<br>5<br>2<br>3      |
|               | WES     | 51.17       | 133.9          | +2.8             | 3                          |
|               | LUB     | 51.37       | 130.2          | +0.4             | 3                          |
|               | AAM     | 52.32       | 125.8          | +1.9             | 4                          |
|               | ALQ     | 54.93       | 108.7          | +0.4             | 4                          |
|               | GOL     | 57.85       | 90.9           | -1.3             | 4                          |
| ×.            | RCD     | 60.24       | 36.5           | -2.0             | 3                          |

| A2.3 Sc | S-S differentia | 1 travel-times | [deep-focus | events] |  |
|---------|-----------------|----------------|-------------|---------|--|
|         |                 |                |             |         |  |

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| EVENT         | STATION  | ∆<br>(deg.) | TIME<br>(sec.) | OBS-JB<br>(sec.) | QUAL.            |
|---------------|----------|-------------|----------------|------------------|------------------|
| PERU-BRAZIL   | A (CONT. | .)          |                |                  |                  |
|               | GSC      | 61.53       | 71.1           | +2.7             | 4                |
|               | COR      | 71.00       | 37.3           | +0.8             | 4                |
|               | PTO      | 76.13       | 20.4           | -1.6             | 3                |
|               | TOL      | 78.81       | 16.6           | +0.6             | 3                |
|               | SDB      | 82.82       | 12.5           | +3.6             | 1                |
| FIJI B        |          |             |                |                  |                  |
| (h = 627  km) | RIV      | 29.18       | 319.1          | +7.2             | 3                |
| (n = 027  km) | CTA      | 32.37       | 285.0          | +4.9             | 4                |
|               | RAB      | 32.47       | 285.0          | +5.9             | 4                |
|               | ADE      | 39.44       | 219.0          | +3.7             | 3                |
|               | KIP      | 46.57       | 164.2          | +4.0             | 4                |
|               | GUA      | 49.24       | 137.5          | +4.3             | 3                |
|               | MUN      | 58.14       | 90.5           | +1.4             | 3<br>5           |
|               | MAN      | 68.55       | 47.3           | +3.5             | 4                |
|               | BAG      | 69.84       | 38.4           | -1.0             | 1                |
|               | ANP      | 73.68       | 34.6           | +6.9             | 1                |
|               | COR      | 82.78       | 9.9            | +1.1             | 3                |
|               | TUC      | 84.13       | 14.6           | +7.6             | 1                |
|               | LON      | 84.94       | 14.1           | +8.0             | 1                |
| ARGENTINA     |          |             |                |                  |                  |
|               | SOM      | 27.09       | 342.0          | +1.7             | 3                |
| (h = 571  km) | BOG      | 32.33       | 287.7          | +2.8             | 5                |
|               | GIE      | 36.40       | 246.5          | +0.7             | 5                |
|               | BHP      | 38.35       | 231.5          | +3.2             | 4                |
|               | LPS      | 47.50       | 156.7          | +0.2             | 3                |
|               | BEC      | 58.13       | 94.6           | +3.3             | 3                |
|               | ATL      | 62.54       | 72.8           | +3.2             | 5<br>4           |
|               | SPA      | 64.09       | 63.0           | +0.3             | 4                |
|               | BLA      | 65.03       | 59.1           | +0.3             | 5                |
|               | OXF      | 65.23       | 60.7           | +2.8             | 5                |
|               | GEO      | 65.94       | 55.3           | +0.3             | 5                |
| 3)            | JCT      | 66.33       | 56.7           | +3.2             | 5<br>4           |
|               | OGD      | 67.64       | 48.0           | -0.5             | 4                |
|               | SCP      | 67.94       | 45.8           | -1.5             | 4                |
|               | WES      | 68.53       | 46.0           | +0.8             | 3                |
|               | FLO      | 69.41       | 46.1           | +4.0             | 5                |
|               | LUB      | 69.87       | 44.3           | +3.8             | 3<br>5<br>5<br>3 |
|               | AAM      | 70.64       | 39.7           | +1.7             | 5                |
|               | SDB      | 71.22       | 36.5           | +0.4             | 3                |
|               | SBA      | 72.30       | 33.4           | +0.7             | 2                |
|               | TUC      | 73.77       | 30.6           | +2.1             |                  |
|               | GOL      | 76.42       | 22.5           | +0.9             | 5                |
|               | GSC      | 79.44       | 14.7           | -0.3             | 4                |
|               |          |             |                |                  |                  |

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| EVENT                      | STATION   | ∆<br>(deg.)   | TIME<br>(sec.)  | OBS-JB<br>(sec.)  | QUAL.                         |
|----------------------------|---|---|---|---|-------------------------------|
| PERU-BRAZIL                | . В   |   |   |   |                               |
| (h = 598 km)               | STG<br>BEC<br>SHA<br>SOM<br>ATL<br>BLA<br>JCT<br>GEO<br>OGD<br>WES<br>AAM<br>ALQ<br>TUC<br>GOL<br>GSC<br>DUG<br>BOZ<br>BKS<br>COR<br>LON<br>PTO<br>TOL<br>VAL | 27.47<br>41.68<br>42.68<br>43.63<br>44.01<br>46.79<br>47.87<br>48.00<br>49.95<br>51.18<br>52.32<br>54.92<br>55.75<br>57.85<br>61.53<br>62.19<br>65.31<br>66.58<br>71.00<br>71.40<br>76.15<br>78.83<br>80.04 | 343.1<br>202.2<br>191.6<br>181.8<br>182.6<br>161.0<br>152.7<br>146.1<br>131.8<br>133.8<br>123.3<br>109.1<br>107.8<br>90.4<br>73.0<br>72.7<br>60.4<br>54.3<br>36.4<br>34.4<br>21.2<br>14.9<br>10.5 | $\begin{array}{r} -3.5 \\ +3.4 \\ +0.7 \\ -1.7 \\ +2.0 \\ +0.8 \\ +0.1 \\ -5.6 \\ -6.7 \\ +3.3 \\ +2.9 \\ +1.2 \\ +4.6 \\ -1.3 \\ -0.4 \\ +2.3 \\ +3.5 \\ +2.5 \\ +0.1 \\ -0.6 \\ -0.6 \\ -0.9 \\ -3.0 \end{array}$ | 31254542444234232131231       |
| JAVA SEA A<br>(h = 606 km) | CHG<br>ANP<br>PMG<br>CTA<br>SHL<br>GUA<br>SHK<br>RIV<br>TAU<br>NDI<br>MSH<br>WEL<br>AAE<br>AFI<br>NAI<br>SBA  | 27.94<br>32.26<br>34.66<br>35.79<br>37.14<br>37.73<br>44.66<br>45.36<br>47.99<br>48.31<br>64.82<br>65.47<br>74.83<br>74.92<br>75.47<br>77.05  | 330.3<br>282.1<br>264.4<br>250.6<br>234.8<br>235.0<br>175.5<br>169.9<br>152.0<br>153.4<br>63.7<br>56.9<br>26.6<br>33.3<br>25.0<br>17.8  | +2.3-0.8+4.9+1.7+1.0+3.5+0.2-0.2+0.7+4.3+5.0+0.9+1.6+9.5+1.6-1.8  | 3 2 4 5 3 3 3 3 4 4 2 3 2 5 3 |

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| EVENT           | STATION    | ∆<br>(deg.)    | TIME<br>(sec.) | OBS-JB<br>(sec.) | QUAL. |
|-----------------|------------|----------------|----------------|------------------|-------|
| FIJI C          |            |                |                |                  |       |
| (h = 643  km)   | TAU        | 35.44          | 253.3          | +3.9             | 5     |
| (11 - 045 Km)   | KIP        | 46.62          | 163.9          | +5.0             | 5     |
|                 | GUA        | 49.15          | 144.6          | +3.1             | 4     |
|                 | MUN        | 58.04<br>71.66 | 90.4<br>33.9   | +1.4+0.6         | 4     |
|                 | SHK        | 71.84          | 33.0           | +0.3             | 2     |
|                 | ANP        | 73.59          | 26.2           | -1.5             | 4     |
|                 | COR        | 82.85          | 8.9            | +0.2             | 2     |
| CHINA           |            |                |                |                  |       |
|                 | BAG        | 27.00          | 343.7          | +1.1             | 4     |
| (h = 555  km)   | DAV        | 35.09          | 260.0          | +0.9             | 4     |
|                 | COL        | 49.38          | 143.9          | -0.4             | 1     |
|                 | LEM        | 53.05          | 119.5          | -1.3             | 1     |
|                 | PMG        | 53.29          | 121.5          | +2.2             | 3     |
|                 | MSH        | 54.13          | 114.4          | +0.2             | 4     |
|                 | TAB        | 62.29          | 72.4           | +1.2             | 3     |
|                 | SHI        | 62.72          | 69.4           | +0.1             | 5     |
|                 | IST        | 71.36          | 36.6           | +0.6             | 1 4   |
|                 | HLW        | 77.14          | 16.2           | -4.0             | 4     |
| MARIANAS        |            |                |                |                  |       |
| (h = 602  km)   | CHG        | 43.69          | 185.2          | +2.2             | 5     |
| (II - 002 KIII) | SNG        | 44.79          | 175.5          | +1.0             | 3     |
|                 | SHL        | 49.62          | 141.0          | +0.5             | 5     |
|                 | KIP        | 52.37          | 120.7          | -2.2             | 2     |
|                 | COL        | 63.59          | 64.8           | +0.8             | 3     |
|                 | NIL        | 65.17          | 54.3           | -3.0<br>+2.7     | 3     |
|                 | KOD<br>MSH | 65.82<br>75.79 | 57.4<br>27.2   | +4.6             | 2     |
|                 | COR        | 78.23          | 17.9           | +0.9             | 4     |
|                 | LON        | 78.69          | 15.2           | -0.9             | 2     |
|                 | BKS        | 80.78          | 9.3            | -2.8             | 1     |
|                 | SHI        | 83.28          | 6.6            | -1.6             | 4     |
| SEA OF OKHO     | атѕк       |                |                |                  |       |
| (1 - 500 1-)    | COL        | 32.77          | 280.1          | +0.3             | 4     |
| (h = 580  km)   | ANP        | 35.21          | 256.6          | +0.4             | 3     |
|                 | HKC        | 41.30          | 204.4          | +1.4             | 3     |
|                 | MAN        | 44.56          | 177.7          | +0.2             | 5     |
|                 | NOR        | 46.30          | 167.3          | +2.7             | 4     |
|                 | KBS        | 46.95          | 162.1          | +2.1             | 5     |
|                 | KIP        | 48.92          | 148.6          | +2.3             | 3     |
|                 | DAV        | 49.73          | 140.7          | -0.1             | 4     |

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| EVENT .                | STATION | ∆<br>(deg.) | TIME<br>(sec.) | OBS-JB<br>(sec.) | QUAL.       |  |  |  |
|------------------------|---------|-------------|----------------|------------------|-------------|--|--|--|
| SEA OF OKHOTSK (CONT.) |         |             |                |                  |             |  |  |  |
| JLA UI                 | KEV     | 51.85       | 128.2          | +1.1             | 5           |  |  |  |
|                        | ' CHG   | 52.56       | 121.0          | -1.7             | 3           |  |  |  |
|                        | LON     | 53.4?       | 118.1          | +0.7             | 4           |  |  |  |
|                        | COP     | 54.03       | 119.3          | +5.5             | 3           |  |  |  |
|                        | RAB     | 56.18       | 99.2           | -2.3             | 3           |  |  |  |
|                        | NIL     | 57.31       | 94.0           | -1.3             | 4           |  |  |  |
|                        | GDH     | 57.49       | 97.3           | +3.0             | 5           |  |  |  |
|                        | KTG     | 57.61       | 94.6           | +0.9             | 4           |  |  |  |
|                        | UME     | 58.23       | 90.2           | -0.2             | 5           |  |  |  |
|                        | NDI     | 58.43       | 89.8           | +0.4             | 5           |  |  |  |
|                        | BKS     | 59.17       | 85.9           | +0.3             | 3           |  |  |  |
|                        | NUR     | 59.83       | 32.0           | -0.2             | 4           |  |  |  |
|                        | SNG     | 61.06       | 73.9           | -2.3             | 4           |  |  |  |
|                        | PMG     | 61.47       | 73.4           | -0.9             | 2           |  |  |  |
|                        | HNR     | 61.82       | 74.5           | +1.8             | 4           |  |  |  |
|                        | AKU     | 62.18       | 72.3           | +1.3             | 3           |  |  |  |
|                        | DUG     | 62.67       | 70.8           | +2.1             | 2           |  |  |  |
|                        | QUE     | 63.52       | 67.5           | +2.5             | 4           |  |  |  |
|                        | GSC     | 64.05       | 64.7           | +2.0             | 3           |  |  |  |
|                        | KON     | 64.32       | 60.1           | -1.4             | 5           |  |  |  |
|                        | GOL     | 66.88       | 55.6           | +4.5             | 2           |  |  |  |
|                        | TAB     | 69.05       | 42.4           | -0.7             | 4           |  |  |  |
|                        | TUC     | 69.62       | 45.0           | +3.8             | 2           |  |  |  |
|                        | SHI     | 72.26       | 31.3           | -1.4             | 3           |  |  |  |
|                        | AFI     | 73.13       | 31.3           | +1.2             | 3           |  |  |  |
|                        | STU     | 74.36       | 26.8           | +0.1             | 4           |  |  |  |
|                        | VAL     | 74.40       | 24.5           | -2.1             | 2           |  |  |  |
|                        | AAM     | 74.52       | 27.9           | +1.6             | 4           |  |  |  |
|                        | IST     | 74.57       | 26.9           | +J.8             | 5           |  |  |  |
|                        | FLO     | 74.67       | 29.2           | +3.4             | 3           |  |  |  |
|                        | TRI     | 75.97       | 23.7           | +1.2             | 5           |  |  |  |
|                        | SCP     | 77.98       | 20.1           | +2.2             | 3           |  |  |  |
|                        | OXF     | 78.66       | 18.4           | +2.0             | 5<br>1<br>3 |  |  |  |
|                        | OGD     | 78.90       | 16.0           | -0.5             | 1           |  |  |  |
|                        | ATU     | 79.31       | 16.0           | +0.9             |             |  |  |  |
|                        | BLA     | 80.17       | 12.8           | -0.6             | 4           |  |  |  |
|                        | ATL     | 81.81       | 13.5           | +3.0             | 3           |  |  |  |
|                        | SHA     | 82.44       | 9.4            | -0.1             | 2           |  |  |  |

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|               |         |        | *      |  |
|---------------|---------|--------|--------|--|
| EVENT         | STATION | Δ      | TIME   | OBS-JB   |
|               |         | (deg.) | (sec.) | (sec.)   |
| HAI           |         |        |        | 1998 - Barlow F. Y. H. H. Harrison, B. H. Harrison, B. Ha |
| (h = 600  km) | CLL     | 145.40 | 3.2    | -1.7   |
| (11 - 000 Km) | JEN     | 146.00 | 3.4    | -2.9   |
|               | LWI     | 146.30 | 3.9    | -3.2   |
|               | BNS     | 146.70 | 6.1    | -1.9   |
|               | DUR     | 147.00 | 7.1    | -1.7   |
|               | CCP     | 147.90 | 8.7    | -2.3   |
|               | STU     | 148.60 | 11.2   | -1.7   |
|               | TUB     | 148.80 | 10.9   | -2.5   |
|               | STR     | 149.00 | 11.4   | -2.5   |
|               | HLE     | 149.00 | 11.2   | -2.7   |
|               | PAR     | 149.20 | 11.4   | -3.0   |
|               | PRU     | 149.70 | 14.1   | -1.7   |
|               | BNS     | 150.40 | 15.3   | -2.4   |
|               | VIE     | 150.60 | 16.0   | -2.2   |
|               | DUR     | 150.60 | 15.1   | -3.1   |
|               | GAR     | 150.70 | 15.3   | -3.2   |
|               | CFF     | 152.20 | 19.5   | -3.2   |
|               | STU     | 152.20 | 20.5   | -2.2   |
|               | TUB     | 152.40 | 20.7   | -2.6   |
|               | JEN     | 152.40 | 20.0   | -3.3   |
|               | MSS     | 152.80 | 22.1   | -2.3   |
|               | PAR     | 153.00 | 21.6   | -3.4   |
|               | BNS     | 153.50 | 24.0   | -2.4   |
|               | MCN     | 153.70 | 24.0   | -3.0   |
|               | NEU     | 154.30 | 26.4   | -2.3   |
|               | GAR     | 154.40 | 26.1   | -3.9   |
|               | STU     | 155.00 | 28.9   | -1.9   |
|               | PTO     | 155.30 | 28.0   | -3.7   |
|               | MSS     | 155.60 | 31.4   | -1.2   |
|               | STR     | 155.60 | 30.1   | -2.5   |
|               | PAR     | 156.30 | 32.5   | -2.2   |
|               | CHU     | 156.70 | 33.4   | -2.5   |
|               | MCN     | 157.30 | 35.5   | -2.2   |
|               | TCL     | 157.60 | 35.4   | -3.2   |
|               | GAR     | 157.80 | 36.4   | -2.8   |
|               | MON     | 160.10 | 45.3   | -1.1   |
|               | MBO     | 161.90 | 48.9   | -3.4   |
|               | ALG     | 164.90 | 60.4   | -2.2   |
|               | SET     | 165.00 | 61.6   | -1.4   |
|               | REL     | 166.10 | 64.4   | -2.6   |
|               | BAB     | 171.40 | 86.0   | -1.1   |
|               | TAM     | 173.70 | 94.4   | -1.9   |
|               | TAM     | 175.20 | 100.9  | -1.5   |
|               | 1.011   |        |        |  |

A2.4 P'(AB)-P'(DF) differential travel-time data [deep-focus events].

| EVENT         | STATION   | ∆<br>(deg.) | TIME<br>(sec.) | OBS-JB<br>(sec.) |
|---------------|-----------|-------------|----------------|------------------|
| ENGDAHL (PE   | ERU-BRAZI | A)          |                |                  |
| (1 500 1 )    | LEM       | 164.19      | 59.4           | -0.7             |
| (h = 590  km) | HKC       | 165.80      | 63.0           | -2.5             |
|               | BAG       | 166.27      | 64.5           | -3.1             |
|               | CHG       | 166.51      | 68.2           | -0.2             |
| ENGDAHL (F)   | IJI B)    |             |                |                  |
| LINDANC III   | KSA       | 146.53      | 6.3            | -1.3             |
| (h = 639  km) | CHZ       | 147.52      | 10.3           | +0.2             |
|               | RAC       | 147.98      | 8.3            | -3.0             |
|               | VAL       | 148.07      | 7.4            | -4-1             |
|               | BNS       | 149.79      | 11.9           | -4.1             |
|               | TNS       |             | 14.6           | -2.9             |
|               |           | 150.33      |                | -3.4             |
|               | WRM       | 151.11      | 16.2           | -5.4             |
|               | KRL       | 151.51      | 15.4           | -2.2             |
|               | PRK       | 151.64      | 18.9           |                  |
|               | TUB       | 151.86      | 18.8           | -2.5             |
|               | STR       | 152.03      | 19.5           | -2.7             |
|               | MSS       | 152.21      | 19.3           | -3.4             |
|               | ZAG       | 152.39      | 21.2           | -2.0             |
|               | FEL       | 152.67      | 20-1           | -3.9             |
|               | LJU       | 152.70      | 16-2           | -7.9             |
|               | ZUR       | 153.06      | 22.4           | -2.8             |
|               | TRI       | 153.25      | 23.3           | -2.4             |
|               | BES       | 153.59      | 25.5           | -1.2             |
|               | NEU       | 153.70      | 23.9           | -3.1             |
|               | ATH       | 154.02      | 24.3           | -3.6             |
|               | VAM       | 155.01      | 29.5           | -1.3             |
|               | RSL       | 155.03      | 25.8           | -5.1             |
|               | LNS       | 155.37      | 28.8           | -3.1             |
|               | MNY       | 155.88      | 29.4           | -4.0             |
|               | BNG       | 155.99      | 30.8           | -2.9             |
|               | ISO       | 156.41      | 32.5           | -2.5             |
|               | RCM       | 157.03      | 32.4           | -4.5             |
|               | BDB       | 158.11      | . 36.0         | -4.2             |
|               | PTO       | 158.52      | 38.3           | -3.1             |
|               | LIS       | 160.52      | 44.5           | -3.3             |
|               | TOL       | 160.85      | 44.6           | -4.3             |
|               | MBO       | 161.85      | 50.5           | -1.7             |
|               | ALI       | 162.79      | 53.4           | -1.9             |
|               | MAL       | 163.81      | 55.7           | -3.1             |
|               | SET       | 164.44      | 63.4           | +2.4             |
|               | RBA       | 165.51      | 60.4           | -4.4             |
|               | AVE       | 165.86      | 61.3           | -4.8             |
|               | TAM       | 175.28      | 101.5          | -1.3             |
|               |           |             |                |                  |

| EVENT                             | STATION  | ∆<br>(deg.)  | TIME<br>(sec.)  | OBS-JB<br>(sec.)   | QUAL.  |
|-----------------------------------|--|--|---|--|--|
| JAVA SEA A<br>(h = 606 km)        | BEC<br>GIE<br>ARE<br>LPB<br>NNA<br>BHP<br>SJG<br>TRN<br>BOG<br>CAR | 153.61<br>156.44<br>157.37<br>157.61<br>159.94<br>167.85<br>167.87<br>172.27<br>173.49<br>175.46 | 23.4<br>32.7<br>33.9<br>33.9<br>42.2<br>72.4<br>70.3<br>89.3<br>95.6<br>101.4 | -3.3<br>-2.4<br>-4.0<br>-4.7<br>-3.7<br>-1.0<br>-3.2<br>-1.2<br>+0.2<br>-2.1 | 2<br>2<br>4<br>5<br>4<br>3<br>2<br>2<br>2<br>5 |
| <b>JAVA SEA</b> B<br>(h = 599 km) | ARE<br>LPB<br>NNA<br>QUI<br>BHP<br>SJG<br>BOG<br>TRN<br>CAR        | 157.08<br>157.47<br>159.37<br>166.79<br>166.88<br>168.05<br>172.46<br>173.12<br>175.61           | 34.2<br>34.7<br>41.4<br>67.1<br>69.2<br>73.0<br>92.1<br>92.4<br>102.6         | -2.8<br>-3.5<br>-2.7<br>-2.4<br>-0.6<br>-1.2<br>-0.8<br>-1.5<br>-1.5         | 5<br>4<br>5<br>3<br>5<br>2<br>4<br>5<br>5      |
| FLORES SEA<br>(h = 618 km)        | SHA<br>NNA<br>LPB<br>BHP<br>ARE<br>SJG<br>TRN                      | 145.28<br>155.62<br>155.77<br>161.62<br>166.06<br>167.78<br>176.21                               | 2.8<br>28.7<br>29.2<br>49.6<br>62.6<br>70.7<br>102.5                          | -1.8<br>-3.9<br>-1.8<br>-4.2<br>-2.4<br>-4.2                                 | 3<br>4<br>5<br>2<br>4<br>5                     |

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| EVENT         | STATION | Δ      | TIME       | OBS-JB |
|---------------|---------|--------|------------|--------|
|               |         | (deg.) | (sec.)     | (sec.) |
| HAI           |         |        |            |        |
| (h = 600  km) | CLL     | 145.40 | 1.0        | -0.3   |
| (11 - 000 Km) | · KEW   | 146.50 | 2.5        | +0.6   |
| 2             | BNS     | 146.70 | 2.8        | +0.8   |
|               | DUR     | 147.00 | 3.1        | +0.9   |
|               | COP     | 147.90 | 4.0        | +1.4   |
|               | KRL     | 148.40 | 4.6        | +1.7   |
|               | STU     | 148.60 | 5.1        | +2.0   |
|               | TUB     | 148.80 | 5.0        | +1.8   |
|               | STR     | 149.00 | 4.8        | +1.5   |
|               | HLE     | 149.00 | 5.0        | +1.7   |
|               | CLL     | 149.00 | 5.0        | +1.7   |
|               | PAR     | 149.20 | 5.3        | +1.9   |
|               | PRU     | 149.70 | 5.5        | +1.8   |
|               | BNS     | 150.40 | 6.0        | +1.8   |
|               | VIE     | 150.60 | 6.6        | +2.3   |
|               | GAR     | 150.70 | 5.5        | +1.1   |
|               | CFF     | 152.20 | 7.0        | +1.5   |
|               | STU     | 152.70 | 7.2        | +1.3   |
|               | TUB     | 152.40 | 7.7        | +2.1   |
|               | JEN     | 152.40 | 7.0        | +1.4   |
|               | MSS     | 152.80 | 7.7        | +1.8   |
|               | PAR     | 153.00 | 7.2        | +1.1   |
|               | BNS     | 153.50 | 7.7        | +1.2   |
|               | MON     | 153.70 | 9.4        | +2.7   |
|               | NEU     | 154.30 | 9.0        | +1.7   |
|               | GAR     | 154.40 | 9.0        | +1.6   |
|               | STU     | 155.00 | 10.3       | +2.4   |
|               | PTO     | 155.30 | 8.3        | +0.1   |
|               | MSS     | 155.60 | 9.9        | +1.5   |
|               | PAR     | 156.30 | 10.0       | +1.0   |
|               | CHU     | 156.70 | 11.0       | +1.6   |
|               | MON     | 157.30 | 12.8       | +2.9   |
|               | GAR     | 157.80 | 11.3       | +1.0   |
| CN00114 451   |         |        |            |        |
| ENGDAHL (FI   |         | 1/7 20 | <b>c</b> . |        |
| (h = 639  km) | KRA     | 147.39 | 5.1        | +2.7   |
|               | JER     | 147.52 | 2.6        | +0.1   |
|               | CHZ     | 147.52 | 5.1        | +26    |
|               | RAC     | 147.98 | 4.1        | +1.4   |
|               | VAL     | 148.07 | 4.6        | +1.9   |
|               | CLL     | 148-38 | 5.4        | +2.5   |
|               | HLE     | 148.44 | 5.0        | +2.0   |
|               | CMP     | 148.71 | 5.7        | +2.6   |
|               | IST     | 148.93 | 4.5        | +1.2   |

A2.5 P'(BC)-P'(DF) differential travel-time data [deep-focus events].

| EVENT            | STATION   | ∆<br>(deg.) | TIME<br>(sec.) | OBS-JB<br>(sec.) | QUAL.  |
|------------------|-----------|-------------|----------------|------------------|--------|
| ENGDAHL (        | FLUI B. C | ONT.)       |                |                  |        |
| LITODATE I       | PRA       | 149.15      | 5.6            | +2.2             |        |
|                  | KEW       | 149.70      | 5.6            | +1.9             |        |
|                  | BNS       | 149.79      | 5.7            | +1.9             |        |
|                  | GG-       | 150.30      | 6.6            | +2.5             |        |
|                  | TNS       | 150.33      | 6.4            | +2.3             |        |
|                  | DOU       | 150.93      | 9.0            | +4.4             |        |
|                  | HEI       | 151.08      | 7.3            | +2.6             |        |
|                  | WRM       | 151.11      | 7.0            | +2.3             |        |
|                  | HLW       | 151.13      | 7.8            | +3.1             |        |
|                  | KRL       | 151.51      | . 8.4          | +3.4             |        |
|                  | STU       | 151.58      | 7.6            | +2.6             |        |
|                  | PRK       | 151.64      | 7.5            | +2.5             |        |
|                  | PDA       | 151.78      | 6.2            | +1.1             |        |
|                  | TUB       | 151.86      | 7.4            | +2.2             |        |
|                  | STR       | 152.03      | 9.1            | +3.8             |        |
|                  | MSS       | 152.21      | 8.1            | +2.6             |        |
|                  | ZAG       | 152.39      | 9.6            | +4.0             |        |
|                  | FEL       | 152.67      | 8.8            | +3.0             |        |
|                  | ZUR       | 153.06      | 9.9            | +3.7             |        |
|                  | TRI       | 153.25      | 8.8            | +2.5             |        |
|                  | BES       | 153.59      | 10.0           | +3.4             |        |
|                  | NEU       | 153.70      | 9.7            | +3.0             |        |
| 5                | ATH       | 154.02      | 11.0           | +4.0             |        |
|                  | VAM       | 155.01      | 11.0           | +3.1             |        |
|                  | RSL       | 155.03      | 10.9           | +3.0             |        |
|                  | LNS       | 155.37      | 11.4           | +3.2             |        |
| JAVA SEA         | В         |             |                |                  |        |
| $(h = 599 \ km)$ | n) SHA    | 145.28      | 1.6            | +0.4             | 3      |
|                  | NNA       | 155.62      | 9.5            | +1.0             | 3      |
| ÷                | LPB       | 155.77      | 9.9            | +1.3             | 2      |
| FLORES SE        | Δ         |             |                |                  |        |
| $(h = 618 \ km)$ |           | 144.76      | 1.1            | +0.3             | 5      |
| 010 10           | GED       | 146.02      | 1.8            | +0.1             | 5<br>1 |
|                  | ATL       | 148.22      | 4.3            | +1.5             | 5      |
|                  | SHA       | 148.28      | 4.1            | +1.2             | 4      |
|                  | LPB       | 157.47      | 11.0           | +1.0             | 2      |
|                  |           |             |                |                  |        |

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## Appendix 3

Tables A3.1 - A3.3 display the three final inversion models (A1, B1, and B2) derived in section 5.5. Besides listing the defining parameters  $v_p$ ,  $v_s$ , and  $\rho$ , we have also listed the values of the seismic parameter  $\Phi = v_p^2 - \frac{4}{3}v_s^2$ , the bulk modulus K, the shear modulus  $\mu$ , the modulus  $\lambda$ , the Poisson ratio  $\sigma$ , pressure, and gravity.

Tables A3.4 and A3.5 show the fit of the models to the basic data set described in section 5.3 of the text. The relative errors are computed as (computed - observed)/observed. For comparison we list the standard errors in the mean of the data and the associated symmetric 95% confidence intervals computed from critical t values of the student's t-distribution [Freeman, 1963]. This allows for the fact that the sample variances are only estimates of the true variances.

Of the 177 eigenperiods listed in Table A3.4, model Al fits 86 within their 95% confidence intervals, model Bl fits 127, and model B2 fits 115. We conclude that Bl is the most satisfactory model from this point of view.

Table A3.6 gives observed and computed absolute travel times for teleseismic distances useful in evaluating the inversion models. Comparing model B1 with P times from the 1968 Herrin Tables, we observe that the difference in baseline is approximately 0.8 seconds. The same comparison with Hales and Roberts [1970a] S times indicates a baseline shift of approximately 5 seconds.

Table A3.7 lists additional differential travel time data.

| 3  |  |
|----|--|
| A  |  |
| 0) |  |
| q  |  |
| d  |  |

MODEL A1

| 1   | RADIUS<br>(km). | DEPTH<br>(km) | VP<br>(km/sec) | VS<br>(km/sec) | RHO ( pm/cm <sup>3</sup> ) | PHI<br>(km <sup>2</sup> /sec <sup>2</sup> ) | K<br>(kb) | (q))<br>М | LAMBDA<br>(kb) | SIGAA      | PRESSURE<br>(kb) | GRAT<br>(cm/sec <sup>2</sup> ) |
|-----|-----------------|---------------|----------------|----------------|----------------------------|---|-----------|-----------|----------------|------------|------------------|--------------------------------|
| 1   | 1               | 6373          | 1.2            | 3.50           | 12.54                      | 11.901                                      | 13721     | 1540      | 12694          | 0.4459     | 3611             | 0                              |
| 2   | 001             | 6271          | 1.2            | 3.50           | 12.57                      | 10.05                                       | 13769     | 1543      | 12680          | 544        | 3608             | 52                             |
| ۲   | 200             | 6171          | 1.2            | 3.51           | 12.55                      | 108.99                                      | 13684     | 1544      | 12654          | 445        | 3633             | 73                             |
| \$  | 300             | 6071          | 1.2            | 3.51           | 12.53                      | 108.95                                      | 13648     | 1542      | 12620          | 45         | 3588             | 110                            |
| ν   | 400             | 1165          | 1.2            | 1.51           | 12.52                      | :08.92                                      | 13636     | 2961      | 12607          | 442        | 1512             | 144                            |
| 9   | 500             | 5871          | 1.1            | 3.51           | 12.52                      | 138.87                                      | 13625     | 1543      | 12596          | 44.7       | 2555             | 8/1                            |
| 1   | 600             | 1115          |                | 5              | 12.51                      | 108.82                                      | 13610     | 1543      | 18621          | 5 5 5      | 3521             | 212                            |
| 20  | 001             | 5671          | 11.19          | 15.6           | 12.49                      | 108.11                                      | 68561     | 1525      | 10552          | 0.4455     | 3444             | 147                            |
| 10  | 006             | 11.00         |                | 10.0           | 12.43                      | 108.62                                      | 13561     | 1530      | 12541          | 5 4 2      | 3428             | 316                            |
| 11  | 1000            | 5371          |                | 1 0            | 12.43                      | 108.71                                      | 13510     | 1518      | 12498          | 44         | 3347             | 35.0                           |
| 12  | 0011            | 5271          | 1.1            | 3.49           | 12.34                      | 108.96                                      | 13444     | 1504      | 12442          | 440        | 3341             | 384                            |
| 13  | 1215            | 5156          | 1.2            | 3.49           | 12.24                      | 109.16                                      | 13363     | 1489      | 12370          | - T        | 3284             | 422                            |
| 14  | 1215            | 5156          | 0.1            | c.c            | 12.13                      | 132.58                                      | 12438     | 0         | 12438          | 0. 5000    | 3234             | 422                            |
| 15  | 1300            | 5071          | 0.1            | 0.0            | 12.10                      | 102.42                                      | 12414     | c         | 12414          | ŝ          | 3239             | 450                            |
| 16  | 1400            | 1164          | 0.1            | 0.0            | 12.06                      | :02.62                                      | 12371     | 0         | 12371          | ŝ          | 3133             | 482                            |
| 17  | 1533            | 4871          | 0.1            | 0.0            | 12-03                      | 132.37                                      | 12287     | 0         | 12281          | n 1        | 3123             | 514                            |
| 18  | 0091            | 1115          | 0-0            | 0.0            | 11.94                      | 101.89                                      | 12168     | 0 0       | 89171          | n u        | 2005             | 040                            |
| 51  | 00/1            | 1194          |                | 0.0            | 11.88                      | $\mathbf{r}$                                | 15611     | 0 0       | 16611          | n v        | 2666             | 510                            |
| ~~  | C001            | 1104          |                | · · ·          | 08.11                      | 21.44                                       | 0111      | 0         | 11636          | <b>N U</b> | 3313             | 600                            |
| 17  | 0061            | 11 55         |                | 0.0            | 11.13                      | 98.38                                       | 05611     | 0         | 01011          |            | 6407             | 140                            |
| 27  | 0002            | 1144          | • 0            |                | 11.65                      | 66.96                                       | 16711     | 0         | 16211          |            | 2112             | 110                            |
| 52  | C012            | 1124          |                | 0.0            | 11.51                      | 95.46                                       | 11040     | 2         | 04011          | 0.000      | 76.07            | 101                            |
| 26  | 0022            | 1115          | •••            |                | 11.48                      | 44.44                                       | 5R/01     |           | 4010:          |            | 7636             | 141                            |
| ~~~ | 0076            | 1104          |                |                | 16.11                      | ****  |           | <b>,</b>  | CLEUI          | n ur       | 75.20            | 10.1                           |
| 27  | 0052            | 1796          | •              |                | 10 11                      | 22.11                                       | 7200.     |           | 45001          | 0.5000     | 2346             | 919                            |
| HC  | 0002            | 1775          | •              |                | 11 11                      | 47.19                                       | 1170      | 0.0       | 1179           | 1 5        | 2253             | 347                            |
| 29  | 2700            | 3671          | • •            | 0.0            | 11.00                      | 85.30                                       | 9384      | 0         | 9384           | C-5360     | 2157             | 874                            |
| 30  | 2600            | 3571          |                | C • C          | 10.84                      | 32.84                                       | 4014      | C         | 4106           | 0.5333     | 2363             | 505                            |
| 31  | 29.33           | 3471          |                | 0.0            | 10.75                      | 80.10                                       | 8614      | 0         | 4014           | 0.5000     | 1961             | 928                            |
| 32  | SOCE            | 3371          | •              | 0.0            | 10.62                      | 77.16                                       | 8192      | 0         | 3192           | 0.5000     | 1861             | 456                            |
| 55  | 100             | 3271          | ٠              | C. C           | 10.47                      | 74.24                                       | 1776      | 0         | 7776           | 0.5333     | 1759             | 619                            |
| 34  | 32.30           | 3171          | ٠              | 0.0            | 10.33                      | 71.44                                       | 1311      | 0         | 7377           | u. 5000    | 1656             | 1033                           |
| 35  | 3300            | 1706          |                | 0.0            | 10.18                      | 68.79                                       | 1002      | 0         | 2001           | 0.5000     | 1551             | 1026                           |
| 91  | 3400            | 1162          | •              | 0.0            | 10.03                      | 66.32                                       | 6653      | C I       | 6000           | 000000     | 1551             | 6401                           |
| 31  | 3485            | 2886          | 'n.            | 0.0            | 9.89                       | 64.16                                       | 6341      | 0         | 1450           | 0.000      | 1001             | 1003                           |
| 38  | 3485            | 2886          |                | 1.2.1          | 5.60                       | 115.57                                      | 6488      | 2955      | 4113           | 0. 1025    | 1651             | 1068                           |
| 34  | 1105            | 1997          | -              | 1.26           | 5.58                       | 115.94                                      | 2149      | 2443      | 0104           |            | 2451             | 1001                           |
| 10  | 3550            | 2821          | m e            | 7.25           | 5.56                       | 115.93                                      | 6449      | 2924      | 5555           |            | 1110             | 6501                           |
| 14  | 6295            | 2140          |                | 1.22           | 5.52                       | 115.78                                      | 6396      | 1182      | 11 55          |            | C171             | C601                           |
| 24  | 31.00           | 2611          | ÷.             | 1.13           | 5.49                       | 115.07                                      | 6312      | 1797      | 1755           |            | 1221             | 1401                           |
| 43  | 3115            | 2596          | ÷.             | 7.15           | 5.45                       | 113.58                                      | 6186      | 1812      | 2614           |            | 6811             | 10 14 N                        |
| 4.4 | 0696            | 1252          | ÷.,            | 11.1           | 15.61                      | 111.36                                      | 5509      | 2131      | 4224           | 4505.0     | 1611             | 9701                           |
| 4.7 | 3425            | 2440          | 'n             | 1.09           | 5.37                       | 110.13                                      | 1165      | 5697      | 6114           |            | 6011             | 2201                           |
| 40  | 4000            | 1162          | 'n,            | 1.06           | 5.33                       | 108.41                                      | 2115      | 2650      | 5004           |            | 1004             | 1 10 1                         |
| 1 5 | 5104            | 2296          | 'nr            | 1. 32          | 5.23                       | 136.12                                      | 5634      | 2634      | 1685           | 5          | 5701             | 5101                           |
| 84  | 0515            | 2221          | 'n,            | 66.9           | 5.24                       | 105.79                                      | 5509      | 5555      | 2066           | 867        | 505              | 6001                           |
|     | 6225            | 0412          | 12.95          | 65.9           | 5.23                       | 101.56                                      | 1416      | 1167      | 2111           | 0.00100    | 100              | 6001                           |
| 20  | 2005            | 1113          | •              |                | 01.0                       | 1.11.70                                     | 0070      | 2162      | 1100           | 11.7       | 22               |                                |

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|     |        | 140   |          |          |          | MODEL A1 (G                          | (cont.) |       |         |         |          |                        |
|-----|--------|-------|----------|----------|----------|--------------------------------------|---------|-------|---------|---------|----------|------------------------|
| I   | RADIUS | DEPTH | VP       | VS       | RHO      | IHd                                  | ×       | 2     | LAVBDA  | SIGMA   | PRESSIVE | GRAV                   |
|     | (km)   | (km)  | (km/sec) | (km/sec) | (pm/cm3) | (km <sup>2</sup> /sec <sup>2</sup> ) | (kb)    | (kb)  | (kb)    |         | (kb)     | (cn/sec <sup>2</sup> ) |
| 51  | 4375   | 1995  | 12.78    | 8.       | 5.12     | 100.2                                | 5131    | 1545  | 3512    |         | 567      | 0001                   |
| 52  | 4453   | 1921  | 12.69    | Ψ.       | 5.38     | 9.6                                  | 6993    | 2383  | 3404    |         | 62R      | 666                    |
| 53  | 4525   | 1846  | 12.60    | 6.81     | 5.04     | 96.8                                 | 4682    | 2341  | 3321    |         | 141      | 166                    |
| 54  | 6634   | 1771  | 12.51    | 6.73     | 10.2     | .96.                                 | 4767    | 2333  | 3233    | 2       | 153      | 966                    |
| 55  | 4675   | 1696  | 12.42    | 6.15     | 16.4     | 93.4                                 | 4644    | 2261  | 3136    | 0.29.15 | 116      | 566                    |
| 56  | 4750   | 1621  | 12.33    | 6.71     | 4.93     | 91.9                                 | 4535    | 2222  | £ 5 0 E | ~       | 619      | 766                    |
| 15  | 4825   | 1546  | 12.24    | 6.63     | 4.84     | 4.06                                 | 4422    | 2141  | 2367    | J.2831  | 542      | 566                    |
| 50  | 0065   | 1471  | 12.15    | 0.65     | 4.85     | 68.1                                 | 4306    | 2442  | 2977    | 0.2366  | 909      | 566                    |
| 59  | 4975   | 1395  | 12.06    | 6.54     | 4.81     | 87.3                                 | 4203    | 6402  | 5906    | $\sim$  | 613      | 566                    |
| 6.3 | 5353   | 1321  | 11.56    | 6.54     | 4.77     | 35                                   | 6504    | 2040  | 2134    | 0.2866  | 534      | 566                    |
| 61  | 5125   | 1246  | 11.85    | 6.4.9    | 4.72     | 8                                    | 3984    | 1987  | 2659    | ~       | 66.4     | 666                    |
| 62  | 5200   | 11 71 | 11.74    | 6.44     | 4.63     | 82.                                  | 3460    | 1937  | 2509    | ~       | 494      | 966                    |
| 63  | 5275   | 9601  | 11.62    | 6.33     | 4.63     | 80.                                  | 3727    | 1892  | 2466    | ~       | 429      | 966                    |
| 94  | 5350   | 1021  | 11.49    | 6.33     | 4.58     | ÷                                    | 3605    | 1832  | 2384    | $\sim$  | 368      | 166                    |
| 62  | 5425   | 946   | 11.36    | 6.25     | 4.51     | ;                                    | 3462    | 1763  | 22 43   | 0.2417  | 361      | 998                    |
| 65  | 5500   | 871   | 11.23    | 6.21     | 42.44    | 74.57                                | 3369    | 1712  | 2168    | 0.2793  | 327      | 666                    |
| 67  | 5550   | 821   | 11.13    | 6.18     | 4.40     | N                                    | 3205    | 1683  | 2085    | 0.2768  | 305      | 666                    |
| 6 8 | 5630   | 111   | 11.03    | 6.15     | 4.36     | 71.12                                | CC1E .  | 1651  | 2000    | 0.2739  | 233      | 666                    |
| 69  | 5650   | 721   | 10.52    | 0.13     | 4.33     |                                      | 2997    | 1524  | 1914    | 0.2705  | 261      | 1003                   |
| 10  | 5700   | 671   | 10.83    | 6.10     | 4. 3.0   |                                      | 2905    | 1602  | 1336    | 0.2570  | 240      | 1000                   |
| 11  | 5733   | 671   | 10.83    | 6.13     | 4.33     | 67.54                                | 2905    | 1632  | 1336    | 0.2670  | 240      | 1000                   |
| 72  | 5725   | 646   | 10.62    | 5.96     | 4.23     | 65.49                                | 2772    | 1502  | 1771    | C.27U5  | 522      | 1000                   |
| 14  | 5750   | 621   | 10.42    | 5.82     | 4.17     | 63.47                                | 2644    | 1041  | 17.36   | 0.2740  | 617      | 1001                   |
| 42  | 5115   | 596   | 12.01    | 5.67     | 4.10     | 61.47                                | 2521    | 1316  | 1643    | 0.2716  | 208      | 1001                   |
| 75  | 5800   | 571   | 10.01    | 5.52     | 4.04     | 9.5                                  | 2401    | 1229  | 1531    | 0.2412  | 148      | 1000                   |
| 16  | 5825   | 540   | 9.8.0    | 5.31     | 3.57     | -                                    | 2284    | 1146  | 1523    | J. 2351 | 133      | 1000                   |
| 11  | 5850   | 521   | 6.60     | 5.23     | 3.90     | 55.68                                | 2112    | 1065  | 1462    | 0.2392  | 178      | 1000                   |
| 13  | 5875   | 464   | 5.39     | 5.CB     | 1.83     | 3.3                                  | 2063    | 186   | 1405    |         | 164      | 666                    |
| 41  | 2003   | 114   | 9.19     | 4.92     | 3.76     | 52.35                                | 1958    | 912   | 1350    | J. 2984 | 159      | 666                    |
| 6.9 | 5925   | 440   | 8.98     | 4.77     | 3.69     | 0.3                                  | 1850    | 838   | 1297    |         | 150      | 966                    |
| d 1 | 5551   | 420   | 8.76     | 4.60     | 3. 51    | 5                                    | : 754   | 764   | 1244    |         | 140      | 166                    |
| 28  | 1565   | 420   | E. 76    | 4.63     | 3.61     | 8.5                                  | 1754    | 764   | 1244    |         | 140      | 166                    |
| 63  | 5155   | 396   | N.71     | 4.59     | 3.59     | -                                    | 1714    | 757   | 12.39   | C.3375  | 28:      | 166                    |
| 94  | 0009   | 115   | 8.66     | 4.53     | 3.50     | 47.01                                | 1673    | 143   | 1174    | 3.3355  | 123      | 966                    |
| 6.8 | 6353   | 321   | 6.56     | 4.55     | ٠        | ŝ                                    | 1594    | 725   | 1110    | 0.3324  | 105      | 566                    |
| 36  | 6100   | 271   | 8.45     | 4.52     | 3.44     | :                                    | 1517    | 201   | 1049    | 0.2946  | 99       | 266                    |
| 10  | 0619   | 127   | b = 34   | 4.50     | 3. 39    | 42.63                                | 2551    | 420   | 006     | 2662.0  | 1.       | 666                    |
| 0   | 6/10   | 061   | 67.8     |          | 3.31     | -                                    | 1403    | 10    | 166     | 1162.0  | 0        | 101                    |
| 50  | 0029   | 1/1   | 47°B     | 4.00     | CF . F   | : .                                  | 101     | 010   | 416     | 1182-0  | 50       | 200                    |
|     | 6773   | 145   | C. 18    | 16.4     | 3. 34    | 59.19                                | 1328    | 080   | 610     |         | 0.0      | 186                    |
| 16  | 6220   | 171   | 0.13     | 4.03     | 3.33     | 38.11                                | 1284    | 100   | 600     | •       | 55       | 186                    |
| 26  | 179    | 100   | 60.8     | CC . 4   | 4 · 4 4  | :                                    | 0621    | 0 8 8 | 161     |         | 15       | 996                    |
| 43  | 1179   | 100   | e. 3     | 44.55    | 3.33     | 31.17                                | 1256    | 200   | 161     | •       | 15       | 996                    |
| 76  | 0679   | 18    | E.05     | 4.57     | 3.32     | 36.94                                | 1221    | 692   | 501     |         | 52       | 586                    |
| 56  | 6410   | 19    | 8.01     | 4.58     | 16 . 4   | ÷                                    | 1156    | 649   | 133     | ٠       | 10       | 586                    |
| 96  | 6330   | 41    | 1.56     | 4.59     | 3.30     | 35.34                                | 1168    | 696   | 103     |         | 12       | 984                    |
| 16  | 6350   | 21    | 7.52     | 4.53     | 3.29     | *                                    | 1142    | 694   | 678     | 0.2471  | 5        | 686                    |
| 55  | 6350   | 21    | 6.23     | 3.40     | 2.74     | э.                                   | 642     | 322   | 421     | 0.2450  | n        | 696                    |
| 37  | 6360   | 11    | ¢.20     | 3.40     | 2.79     | 23.03                                | 642     | 322   | 421     | 0.2850  | m        | 982                    |
| 100 | 6371   | 0     | 6.20     |          | 2.79     | ÷                                    | 249     | 322   | 124     |         | 0        | 982                    |

MODEL A1 (cont.)

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| 2     |       |
|-------|-------|
| A3.   | 81    |
| Table | MODEL |

| GRAV<br>(cm/sec <sup>2</sup> )              | 0      | 52     | 74       | 110    | 144        | 212      | 747    | 281    | 316    | 150    | 385    | 423    | 423    | 450    | 482    | 514    | 546    | 573    | 609    | 643    | 671      | 101     | 731     | 160    | 061    | 818     | 846    | 874     | 106    | 928    | 954     | 616    | 1003   | 1026   | 1349   | 1068  | 1068   | 1364     | 1059   | 1049    | 1041   | 1034   | 1327   | 1021   | 1016   | 1101   | 1008   | 1004 | 1001    |
|---|--------|--------|----------|--------|------------|----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------|---------|---------|--------|--------|---------|--------|---------|--------|--------|---------|--------|--------|--------|--------|-------|--------|----------|--------|---------|--------|--------|--------|--------|--------|--------|--------|------|---------|
| PRESSURE<br>(kb)                            | 3609   | 3606   | 3598     | 3586   | 0104       | 3525     | 3495   | 3463   | 3426   | 4984   | 3339   | 3281   | 3281   | 3236   | 3140   | 3120   | 3056   | 2990   | 5167   | 2846   | 2769     | 2690    | 2607    | 2522   | 2434   | 2343    | 2250   | 2155    | 2058   | 1959   | 1858    | 1756   | 1653   | 1549   | 1444   | 1354  | 1354   | 1340     | 1316   | 1272    | 1229   | 1187   | 1145   | 1104   | 1063   | 1323   | 984    | 556  | 915     |
| SIGNA                                       | 0.4459 | 0.4459 | 0.4458   | 0.4459 | 6684 °O    | 1444     | 0.4467 | 0.4464 | 0.4466 | 0.4469 | 0-4472 | 0.4475 | 0.5000 | 0-5000 | 0.5000 | 0.5333 | 0.5000 | 0.5000 | 0.5333 | 0.5000 | 0* 50 30 | 0. 5030 | 0. 5000 | 0.5333 | 0.5000 | 0. 5000 | 0.5333 | 0. 5000 | 0.5300 | 0.5333 | C. 5000 | 0.5000 | 0.5000 | 0.5000 | 0-5333 | 0.000 | 1201-0 | 0.3329   | 0.3033 | 0. 3045 | 0.3349 | 304    | 0.3029 | 30     | 3      | 3.2988 | NI.    | 0    | J. 2962 |
| LAMBDA<br>(kb)                              | 12694  | 12689  | 12674    | 12648  | 64071      | 01 24 39 | 26321  | 12632  | 12623  | 17610  | 12531  | 12513  | 12460  | 12444  | 12411  | 12334  | 12219  | 12042  | 118.05 | 11561  | 1011     | 11048   | 10785   | 13542  | 10309  | 10032   | 9718   | 9388    | 1206   | 8628   | 8209    | 1611   | 1400   | 7326   | 6676   | 6373  | 4523   | 4510     | 4498   | 4471    | 4412   | 4309   | 41 94  | 6104   | 3966   | 3863   | 3765   | 3674 | 3533    |
| MU<br>(kb)                                  | 1540   | 1541   | 1539     | 1535   | 1531       | 1528     | 1523   | 1517   | 1510   | 1459   | 1485   | 1467   | 0      | 0      | o      | °,     | 0      | 0      | C      | 0      | 0        | C       | 0       | 0      | 0      | 0       | 0      | 0       | 0      | c      | 0       | 2      | 0      | C      | C      | 0     | 2948   | 2934     | 2916   | 2871    | 2822   | 2775   | 2130   | 2686   | 2642   | 26.01  | 2555   | 2509 | 2465    |
| К<br>(kb)                                   | 13721  | 11     | 13700    | 13671  | 13665      | 1 3454   | 1 3640 | 13644  | 363    | 13604  | 13571  | 13492  | 12460  | 12444  | 12411  | 12334  | 12219  | 12042  | 11835  | 11561  | 12307    | 11343   | 10785   | 10542  | 10309  | 10032   | 9118   | 9388    | \$206  | 8628   | 82 C 9  | 1611   | CC+1   | 7026   | 6676   | 6373  | 6483   | 40       | 5 3    | 36      | 6294   | 6160   | 6014   | 5873   | 5727   | 5591   | 5469   | 5347 | 5227    |
| PHI<br>(km <sup>2</sup> /sec <sup>2</sup> ) | 11.901 | 109.11 | 1.6      | 1.6    | 109.15     | 100 20   |        | 21-601 | 0.6    | 0      | 139.57 | 105.87 | 102.91 | 132.99 | 103.06 | 102.45 | 102.39 | 101.47 | 100.08 | 98.65  | 97.14    | 55.59   | 00.46   | 52.57  | 91.23  | 85.51   | 87.49  | 85.35   | 82.92  | 82.21  | 17-30   | 14-41  | 71.62  | 68.99  | 66.52  | 64.36 | 116.38 | 116.35   | 116.32 | 116.09  | 115.28 | 113.67 | 111.84 | 139.59 | 108.16 | 6.3    | 104.68 | 3.1  | 1.5     |
| RHO<br>(gm/cm <sup>3</sup> )                | 12.53  | 12.57  | 12-56    | 12.53  | 12.52      | 12 21    | 10.21  | 12.53  | 12-49  | 12.46  | 12.39  | 12.28  | 12.11  | 12.38  | 12.04  | 11.99  | 11.93  | 11.87  | 11.80  | 11.72  | 11.64    | 11.56   | 11.47   | :1.39  | 11.30  | 11.21   | 11.11  | 00-11   | 1C.88  | 13.76  | 10-62   | 10.48  | 10.33  | 10.19  | 10.04  | 06*6  | 5.58   | <b>^</b> | 5.54   | 5.50    | 5.46   | 5.42   | 5.38   | 5.34   | 5. 30  | 5.26   | 5.22   | 5.19 | 5-15    |
| VS<br>(km/sec)                              | 10     | 5      | 5        | 5      | n v        |          | 1 1    | 2 3    | . +    | 3.47   | 3.46   | 3.46   | 0.0    | 0.0    | 0.0    | 0.0    | 0.0    | 0.0    | 0.0    | C.0    | c.0      | 0.0     | 0.0     | 0.0    | 0.0    | C.0     | C . O  | 0.0     | 0.0    | 0.0    | 0.0     | 0.0    | 0.0    | c•0    | C • C  | 0.0   | 7.27   | 7.27     | 7.20   | 7.22    | 7.19   | 7.16   | 7.13   | 1.04   | 7.05   | 7. 63  | 65-9   | 6.5b | 6.92    |
| VP<br>(km/sec)                              | 11.20  | ~      | ~        | ~      | 11-20      | 02-11    | • •    | 11-19  | 11.19  | 11.19  | 11.21  | 11.22  | 10.14  | 10.15  | 10.15  | 10.14  | 10.12  | 10.07  | CC-01  | 9.53   | 5.86     | 5.78    | 6.70    | 9.62   | 9°.55  | 5.46    | 9.35   | 5.24    | 9.11   | 8.96   | 8.79    | 8.63   | E.46   | 8.31   | 8.16   | 8.32  | 13.67  | 19-61    | ••     | 13.63   | 13.57  | 13.49  | 13.40  | 13.31  | 13.22  | F1.F.  | 12.03  | ٠    |         |
| DEPTH<br>(km)                               | 6373   | 6271   | 6171     | 1109   | 1160       | 1773     | 5671   | 5571   | 5471   | 5371   | 5271   | 5156   | 5156   | 1105   | 1154   | 4871   | 4771   | 4671   | 4571   | 1244   | 4371     | 4271    | 4171    | 4071   | 1795   | 3871    | 2775   | 3671    | 3571   | 3471   | 3371    | 1122   | 3171   | 3071   | 1162   | 2886  | 2886   | 2861     | 2821   | 2746    | 2671   | 2596   | 2521   | 2446   | 2371   | 2296   | 2221   | 2146 | 2071    |
| RADIUS<br>(km)                              | 1      | 100    | 007      | 300    | 004        | 000      | 2002   | 803    | 006    | 1000   | 1100   | 1215   | 1215   | 1333   | 1400   | 1500   | 1600   | 1760   | 1800   | 1900   | 2000     | 2100    | 2200    | 2300   | 2433   | 2500    | 2600   | 2733    | 2800   | 2900   | 3000    | 3160   | 32.33  | 3300   | 3400   | 3485  | 3485   | 0151     | 3550   | 3625    | 3700   | 3775   | 3850   | 3925   | 0004   | 40.75  | 4150   | 4225 | 4300    |
| I   | -      | 2      | <b>~</b> | 3 1    | <b>^</b> - | 0~       | - 1    |        | 10     | 11     | 12     | 13     | 4      | 15     | 16     | 2 2    | 18     | 14     | 02     | 21     | 22       | 23      | 54      | 25     | 26     | 27      | 28     | 29      | 30     | I.E    | 32      | 33     | 34     | 35     | 36     | 37    | 38     | 61       | 64     | 4 L     | 24     | 43     | 44     | ¢      | 46     | 47     | 4 8    | 54   | 50      |

| (cm/sec <sup>2</sup> )               | 100    | 966   | 566  | 566  | 666  | 666    | 666  | 166  | 666     | 566  | 566  | 566  | 946    | 166   | 266   | 666  | CCC1   | 1000 | 1001 | 1001  | 1001   | 1000 | 1000   | 0001  | 666    | 666  | 666  | 993   | 966  | 166  | 166   | 166     | 007    | 100     | 100   | 080  | 988    | 937   | 986    | 986  | 986  | 985   | 934  | 984  | 983  | 983     | 982    | 981   |
|--------------------------------------|--------|-------|------|------|------|--------|------|------|---------|------|------|------|--------|-------|-------|------|--------|------|------|-------|--------|------|--------|-------|--------|------|------|-------|------|------|-------|---------|--------|---------|-------|------|--------|-------|--------|------|------|-------|------|------|------|---------|--------|-------|
| (kb)                                 | 867    | 161   | 754  | 716  | 630  | 643    | 601  | 115  | 535     | 200  | 465  | 430  | 665    | 191   | 175   | 305  | 283    | 261  | 239  | 239   | 228    | 218  | 238    | 661   | 183    | 179  | 169  | 163   | 041  | 140  | C * 1 | 761     | 501    | 601     | 11    | 19   | 4 1    | 46    | 38     | 31   | 31   | 25    | 18   | 12   | 5    | 5       | 3      | 0     |
| N 010                                | 0.2951 | 293   | 262  | 290  | 290  | $\sim$ | 287  | ~ 1  | $\sim$  | N    | 292  | 2 r  | 1812.0 | Nr    | 213   | N    | 512    | N    | 268  | 317   | 0.3141 | OIL  | 0.3355 | . 300 | 0.2948 | .238 | .282 | .276  | 017. | ~ *  | 1000  | 0. 3046 | 106.7. | 202     | 115   | 111  | 0.3072 | .300  | -287   | .271 | 271  | . 253 | 282. | .213 | 02   | .235    | 0.2350 | 285   |
| (kb)                                 | 3487   | 3309  | 3226 | 3136 | 3058 | 2477   | 2888 | 5816 | 2743    | 2651 | 2549 | 2435 | 2340   | 1922  | \$612 | 2037 | 6262   | 1957 | 1061 | 1161  | 1946   | 1777 | 1736   | 1632  | 1558   | 1482 | 1408 | 1338  | 1212 | 1210 | 1180  | 1611    | 5111   | 2701    | 1001  | 1051 | 1009   | 962   | 389    | 310  | C18  | 730   | 643  | 568  | 524  | 427     | 427    | 103   |
| (kb)                                 | 2422   | 2336  | 2293 | 2253 | 2214 | 2174   | 2136 | 2089 | 2 3 4 4 | 1998 | 1956 | 1923 | 181    | 1824  | 1119  | 1746 | 1712   | 1677 | 1642 | 1398  | 1092   | 1088 | 1 386  | 1084  | 1084   | 1084 | 1084 | 1083  | 6101 | 1074 | 100   | 511     | 801    | 1 34    | 640   | EEY  | 689    | 637   | 656    | 681  | 681  | 708   | 738  | 762  | 769  | 322     | 322    | 322   |
| (kb)                                 | 51.02  | 4866  | 4755 | 4638 | 4535 | 4427   | 4313 | 4211 | 4103    | 3984 | 1354 | 3715 | 3554   | 1469  | 3340  | 3252 | 3162   | 3075 | 2956 | 2644  | 2575   | 2503 | 2433   | 2355  | 2280   | 2205 | 2131 | 2660  | 2661 | 1926 | 9011  | 1008    | 10101  | 2001    | 00071 | 5671 | 6671   | 1 388 | 1327   | 1264 | 1264 | 1202  | 1135 | 1376 | 1037 | 642     | 642    | 642   |
| (km <sup>2</sup> /sec <sup>2</sup> ) | 95.84  |       | 2.1  | 3.4  | 2.1  | :      | 6.   | 1.5  | 0       | 4.3  | 2.3  |      | 8.3    | 6.3   | 4 . 1 | 2.1  |        | 6.7  | 8.3  | 65.37 |        | 2.6  | 1.1    | 9.6   | 8.1    | • 2  | 2.0  | 3.5   | 2.1  | i.   |       | 0.      | ÷ .    | 5       | •••   |      | 11.07  | 1     | 0.00   | 8.0  | 0    | ~     |      | 5    | 1.4  | 23.03   |        |       |
| (gm/cm <sup>3</sup> )                | 11.5   | 5.04  | 5.00 | 4.56 | 76.4 | 4.89   | 4.85 | 4.81 | 4.77    | 4.72 | 4.68 | 4.54 | 4. 59  | 4.55  | 6. 50 | 4.47 | 4 . 44 | 4.41 | 4.38 | 4.05  | 4.02   | 4.00 | 3.97   | 3.95  | 3.92   | 3.90 | 3.87 | 3.85  |      | 3.80 |       |         |        |         | 33 °C |      | 11.15  |       |        |      |      |       |      |      |      |         |        | 2.74  |
| (km/sec)                             | 6.83   | 6. 81 | 6.77 | 6.74 | 6.71 | 6.67   | 0.64 | 6.59 | é.55    | 6.50 | 6.47 | 6.44 | 6.39   | 6. 33 | 0.28  | 6.25 | 6.21   | 6.17 | 6.12 | 5.21  | 5.21   | 5.22 | 5.23   | 5.24  | 5.26   | 5.27 | 5.29 | 5.32  | 5.32 | 5*32 | 10.4  | 00.4    | 00.4   | - u - + | 14 1  | 72.7 | 56.45  | 4.37  | 4 . 44 | 4.53 | 4.53 | 4.62  | 4.72 | 4.8. | 4.83 | C 7 * E | 3.4.)  | 1.4.1 |
| (km/sec)                             | 12.77  | 1     | ~    | ~    | ~    | 2      | N    | è.   | -       | -    | -    | ÷.   | -      | ÷.    | 4     | -    | -      | -    |      | 0     | :      | ٠    | ٠      | ٠     |        |      |      |       |      |      |       | •       |        | •       |       | •    | • •    |       |        |      |      |       |      |      |      |         | ٠      |       |
| (km)                                 | 1996   | 1846  | 1771 | 1696 | 1621 | 1546   | 1471 | 1396 | 1321    | 1246 | 1111 | 1096 | 1201   | 946   | 118   | 821  | 111    | 721  | 671  | 671   | 646    | 621  | 965    | 115   | 546    | 521  | 490  | 4 7 2 | 440  | 4 20 | 024   | 040     | 100    | 170     | 117   | 196  | 171    | 146   | 121    | 1 30 | 100  | 81    | 61   | 15   | 21   | 21      | 11     | 0     |
| (km)                                 | 4375   | 4525  | 4600 | 4675 | 4750 | 4825   | 0064 | 6155 | 5050    | 5125 | 5200 | 5275 | 0444   | 6236  | 0000  | 0444 | 2600   | 5650 | 5700 | 5700  | 5725   | 5750 | 5175   | 5800  | 5825   | 5853 | 5815 | 0065  | 6766 | 1686 | 1040  | C1 6C   | 0000   | 00.00   | 0010  | 6175 | 6200   | 6225  | 6253   | 6271 | 627: | 6230  | 6310 | 6333 | 6350 | 6350    | 6363   | 6371  |
|                                      | 15     | 53    | 54   | 55   | 56   | 57     | 58   | 54   | 60      | 61   | 62   | 10   | \$9    | \$9   | 00    | 19   | 68     | 69   | 10   | 11    | 12     | 13   | 14     | 15    | 76     | 11   | 18   | 51    | 5.5  | 18   | 70    | 25      | 1 0    |         | 90    | 88   | 68     | 06    | 16     | 92   | 593  | 46    | 95   | 96   | 16   | 98      | 66     | 100   |

•

MODEL B1 (cont.)

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| с.    |       |
|-------|-------|
| A3    | B2    |
| Table | MODEL |

| (km)    | (km) | vr<br>(km/sec) | (km/sec)            | (gm/cm <sup>3</sup> ) | $(km^{5n1}_{2/sec^2})$ | (kb)      | (kb)  | (kb)      |         | (kb)    | (cm/sec <sup>2</sup> ) |
|---------|------|----------------|---------------------|-----------------------|------------------------|-----------|-------|-----------|---------|---------|------------------------|
|         | 6370 | 11.20          | 3.50                | 12.58                 | 11.9.11                | 13721     | 1540  | 12594     | 0.4429  | 1613    | c                      |
| 00      | 6272 | 11.20          | 3.50                | 12.58                 | 10.621                 | 13715     | 1542  | 12585     | 0.4458  | 36.39   | 25                     |
|         | 6171 | 11.20          | 3.50                | 12.51                 | 10.9.07                | 13766     | 1542  | 12673     | 0.4453  | 3601    | 78                     |
| 300     | 6671 | 11.20          | 3.50                | 12.55                 | 10.001                 | 13683     | :539  | 14062     | 0.4458  | 1539    | 111                    |
|         | 1165 | 11.23          | 3.53                | 12.55                 | 139.38                 | 13683     | 1537  | 12663     | 0.4458  | 6766    | 144                    |
| 500     | 5871 | 11.20          | 3.50                | 12.54                 | 109.06                 | 13675     | 1535  | 12022     | 0.4459  | 3553    | 6/1                    |
|         | 1110 |                |                     | 26-21                 | 104.02                 | 1052      | 0101  | 21 62 1   |         |         | C12                    |
| 001     | 1195 | 11.19          | 14°                 | 12.21                 | 16.801                 | 13631     | 5761  | 61971     | 104440  | 2475    | 147                    |
|         | 1100 | 01-11          | 0. • • 0<br>• • • • | 12.21                 | 10.07                  | 1 3 5 5 0 | 1501  | 101071    | 4444    | 00.95   | 316                    |
|         | 1140 |                |                     | 55 ° 7 7              | 100 FO                 |           | 2001  | 10001     | 0044-00 | 1445    | 150                    |
|         |      | 01-11          | 0                   | 26.21                 | 00.001                 |           |       | 0         |         | 1766    |                        |
|         | 1176 | 01-11          |                     | 16.55                 | 100.00                 | 2 X C C T | 1400  | 0-1/1     | 7677 (  | 2465    | 101                    |
| C 1 2 1 | 0010 | 01-11          | \$ C<br>• C         | 57 ° 71               | 10.001                 | 1 2 4 4 4 | 1641  | 20021     |         | 3225    | 222                    |
|         | 0010 | <b>10.13</b>   | ວ ເ<br>ວ ເ          | 12.14                 | 102.00                 | 16421     | ۰ c   | 10421     |         | 070     | 202                    |
|         | 1105 | 10.13          | ٠                   | 12.11                 | 102.67                 | 12428     | r     | 12423     | 000000  | 0 4 7 4 | 104                    |
|         | 1164 | 10.14          | ٠                   | 12.36                 | 132.74                 | 12388     | C     | 12385     | 0.003.0 | 3143    | 482                    |
| 500     | 4071 | 10.12          |                     | 12.00                 | 132.50                 | 12303     | ſ     | 12333     | 0.5300  | 3123    | 514                    |
| 600     | 4771 | 10.13          |                     | 11.94                 | 102.02                 | . 12181   | 0     | 12:31     | 0.5000  | 3060    | 546                    |
| CCL     | 4671 | 10.05          |                     | 11.87                 | 101.08                 | 66611     | 0     | 66611     | C- 5000 | 2993    | P14                    |
| 800     | 4571 | 65°6           | 0.0                 | 11.80                 | 99.72                  | 11766     | n     | 11746     | 0.5000  | \$252   | 609                    |
| 200     | 1244 | 5.             | 0.0                 | 11.72                 | 98.36                  | 11531     | C     | 11531     | 3.5333  | 2849    | 643                    |
| CCC     | 4371 | 5.85           | 0.0                 | 11.65                 | 96.98                  | 11294     | 0     | 11294     | 0.5000  | 2112    | 119                    |
|         | 4271 | ~              |                     | 11.57                 | 95.68                  | 11067     | 0     | 1:061     | 0.5313  | 2633    | 101                    |
|         | 1 17 |                | C • 0               | 11.43                 | 94.32                  | 13833     | ſ     | 1 3 3 3 3 | 0.5333  | 2613    | 131                    |
|         | 1204 | 5.63           |                     | 11.40                 | 42.14                  | 10573     | 0     | 10573     | 0.5030  | 2525    | 761                    |
| 2400    | 3971 | 5.55           | 0*0                 | 16.11                 | 91.25                  | 10322     | c     | 10322     | 0004-0  | 2437    | 19.0                   |
|         | 3871 | 4.             | C • C               | 11.22                 | 89.55                  | 10045     | r     | 54001     | 0.5333  | 2346    | 814                    |
|         | 3771 | 9.35           | C * 0               | 11.12                 | 87.5C                  | 5726      | 0     | 9726      | 0.5000  | 2253    | 847                    |
| 2733    | 1671 | 2.             |                     | 11.01                 | 85.32                  | 9389      | C     | 9339      | 0.5000  | 2153    | 875                    |
| 2800    | 3571 | c1*5           | 0°0                 | 10.89                 | 82.83                  | 1106      | S     | 111.6     | 0.5303  | 2060    | 206                    |
|         | 3471 | E. 55          |                     | 10.76                 | 90.09                  | ė617      | 0     | 3617      | 0.5130  | 1961    | 928                    |
|         | 3372 | e.76           | C.0                 | 10.63                 | 77.16                  | 6618      | C     | 6616      | 3.5333  | 1961    | 954                    |
|         | 3271 | 8.62           |                     | 10.49                 | 74.24                  | 1794      | С     | 561L      | 0.5330  | 1759    | 619                    |
|         | 3171 | E.46           | C.0                 | 10.35                 | 71.55                  | 7409      | 0     | 1409      | U. 5030 | :655    | 1004                   |
| OUFF    | 101  | 6.31           |                     | 13.22                 | 68.58                  | 6401      | C     | 1.24.1    | 0.5000  | 1551    | 1327                   |
| -       | 2471 | 6.15           | 0.0                 | 10.08                 | 66.55                  | 6710      | 0     | 6110      | 0.5000  | 1445    | 1050                   |
|         | 2686 | £0.3           |                     | 9.95                  | 64.42                  | 6412      | 0     | 64:2      | U. 5033 | 1355    | 1069                   |
|         | 2030 | 13.46          | in                  | 6.34                  | 123.91                 | 1485      | 2589  | 6413      | 34      | 1355    | 1069                   |
|         | 2861 | 13.54          | 6.85                | 5.84                  | 120.73                 | 7652      | 2738  | 5226      | 0.3281  | 1339    | 1066                   |
|         | 292: | 12.66          | 1.33                | 5.52                  | 114.58                 | 0346      | 2955  | 4359      | J. 2979 | 1315    | 1901                   |
| 3625    | 2746 | 13.63          | 7.29                | 5.48                  | 114.86                 | 6294      | 2415  | 4350      | 6.2944  | 1221    | 1052                   |
|         | 2671 | 12.58          | 7.25                | 5.44                  | 114.23                 | 6214      | 2463  | 4337      | 1       | 1228    | 1043                   |
|         | 2596 | 24.49          | 1.21                | 5.40                  | 112.33                 | 2509      | 28.35 | 4222      |         | 1136    | 1335                   |
|         | 2521 | 13.40          | 7.17                | 5.35                  | 111.23                 | 1955      | 2012  | 4126      | ٠       | 1144    | 1029                   |
|         | 2440 | 13.31          | 7.12                | 5.32                  | 109.61                 | 5833      | 2693  | C-L0+     | ٠       | 1101    | : 023                  |
|         | 2371 | 13.22          | 7.00                | 5.28                  | 136.32                 | 5732      | 2647  | 3937      |         | 1063    | 1101                   |
|         | 2296 | 13.13          | 7.04                | 5.24                  | 106.43                 | 5577      | 2596  | 3345      | ~       | 1023    | 1013                   |
|         | 122  | 1 3.04         | 7.00                | 5.20                  | 104.96                 | 5454      | 2545  | 1215      |         | 443     | 4001                   |
| 225     | 2145 | 12.96          | ¢ . 56              | 5.10                  | 133.38                 | 5338      | 2493  | 3473      | 0.2476  | 555     | 1005                   |
|         |      |                |                     |                       |                        |           |       |           |         |         |                        |

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| (cm/sec <sup>2</sup> )                      | 1000   | 000            | 566   | 565   | 666   | 666      | 166   | 666   | 666    | 466    | 565    | 566     | 966    | 166    | 866    | 666    | 1000    | 1001   | 1001   | 1001   | 1001   | 1001   | 1000   | 1000   | 666    | 666    | 666   | 966    | 866   | 166   | 166    | 166    | 966   | 566       | 266   | 043   | 988    | 948   | 186     | 986   | 986   | 985    | 486   | 984    | 983   | 983   | 982   | . 186 |
|---|--------|----------------|-------|-------|-------|----------|-------|-------|--------|--------|--------|---------|--------|--------|--------|--------|---------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|--------|-------|-------|--------|--------|-------|-----------|-------|-------|--------|-------|---------|-------|-------|--------|-------|--------|-------|-------|-------|-------|
| PRESSURE<br>(kb)                            | 198    | 161            | 754   | 717   | 683   | 643      | 6.07  | 571   | 535    | 500    | 465    | CE 5    | 395    | 361    | 125    | 3.15   | 283     | 26J    | 238    | 238    | 228    | 213    | 503    | 661    | 189    | 179    | 169   | 16.0   | 150   | 140   | 140    | 132    | 123   | 105       | 11    | 14    | 54     | 46    | 33      | 31    | 11    | 25     | 18    | 12     | \$    | S     | 3     | 0     |
| SIGMA .                                     | 0.2958 | 503            | 293   | ~     | 53    | 0.2894 - | 10    | 9.7   | 0.2865 | 0.2354 | 0.2833 | U. 2802 | 0.2739 | 0.2772 | 0.2736 | 0.2659 | C. 2701 | 0.2737 | 0.2745 | 0.3198 | 3.3162 | 0.3120 | 0.3070 | 0.3315 | 0.2457 | 0.2890 | m     | 0.2753 | 9     | 23    | 0.3329 | 3.2998 | 2.    | 5162 C    |       |       | 0.3099 | -     |         | 2.    | .271  | 0.2513 | .227  | .207   | .232  |       | . 285 | 9 2   |
| LAYBDA<br>(kb)                              | 3492   | 2165           | 3238  | 3149  | 3.172 | 2989     | 2493  | 2325  | 2746   | 2658   | 2558   | 2444    | 2356   | 2262   | 6512   | 2323   | 2014    | 2000   | 1960   | 1922   | 1855   | 1765   | 1111   | 1637   | 1562   | 1483   | 14.38 | 1334   | 1266  | 1233  | 1197   | 1151   | 1120  | 1056      | 1042  | 5501  | 1325   | 976   | 669     | 811   | 119   | 721    | 626   | 549    | 524   | 427   | 427   | 427   |
| MU<br>(kb)                                  | 2410   | 2327           | 2287  | 2250  | 2213  | 2175     | 2139  | 1602  | 2045   | 5661   | 1956   | 1918    | 1868   | 6181   | 1776   | 1778   | 1714    | 1655   | 1191   | 1083   | 1076   | 1076   | 1075   | 1771   | 1079   | 1083   | 1586  | 1089   | 1084  | 1084  | 611    | 215    | 769   | 140       | 140   | 634   | 623    | 633   | 654     | 683   | 683   | 512    | 143   | 112    | C11   | 322   | 326   | 322   |
| K<br>(kb)                                   | 6505   | 4114           | 4764  | 4650  | 4548  | 4440     | 4324  | 4219  | 4109   | 1561   | 3863   | 3723    | 3602   | 3475   | 3335   | 3206   | 3153    | 3104   | 3034   | 2644   | 2574   | 2502   | 2429   | 2355   | 2282   | 2206   | 2132  | 2060   | 1991  | 1925  | 1717   | 1678   | 1634  | 51 61     | 1141  | 872   | 1444   | 1 358 | 1335    | 1266  | 1266  | 1194   | 1125  | 1064   | 1038  | 642   | 249   | 249   |
| PHI<br>(km <sup>2</sup> /sec <sup>2</sup> ) | 130.16 | 78.41<br>CA.CR | 95-47 | 93.82 | 92.41 | 90.86    | 39.16 | 61.69 | 86.13  | 84. 19 | 82.43  | 80.22   | 78.36  | 76.38  | 74.06  | 71.69  | 11.11   | 70.40  | 65.32  | 65.93  | 64.55  | 63.09  | 61.56  | 60.03  | 58.43  | 56.78  | 55.17 | 53.59  | 52.11 | 50.73 | 47.66  | 46.02  | 46.02 | 20.64     | 44.10 | 44.54 | 43-12  | 41.95 | 40.15   | 38.16 | 38.16 | 36.14  | 34.01 | 32.26  | 31.58 | 23.33 | 23.03 | 23.33 |
| RHO<br>(gm/cm <sup>3</sup> )                | 5.39   | 50 °C          | 66-5  | 4.56  | 56.4  | 4. P . 4 | 4.95  | 8     | ~      | 4.73   | 4.69   | 4.64    | 4.60   | 4.55   | 4.53   | 4.47   | 4 - 44  | 4 - 41 | 4.38   | 10.4   | 3. 39  | 3.51   | 3.55   | 3. 43  | 3.91   | 1.89   | 3.87  | 3.84   | 3. 32 | 3.93  | 3.6J   | 3.56   | 3.50  | 3.51      | 04 .6 | 75.5  | 3.35   | 3.33  | 1.23    | 3.32  | 3.32  | 3.32   | 3.31  | 3.30   | 3.24  |       | 61.2  | 2.79  |
| VS<br>(km/sec)                              | 6.88   | 6.50           | 6.77  | 6.74  | 6.71  | 6.67     | 6.64  | 6.59  | 6.55   | 6.53   | 4.     | 6.43    | 6.38   | 6.32   | 6.28   | 6.31   | 6.21    | 6.13   | 6.C7   | 5.20   | 5.20   | 5.21   | 5.22   | 5.24   | 5.26   | 5.20   | 5.3.3 | 5.32   | 5.34  | 5.34  | 4.65   | ÷.     | 0.    | 4.54      | 4.40  | 4.34  | 4.33   | 4.36  | 4 . 4 % | 4.54  | 5     | 69.4   |       | 4 - B4 | τ.    | 3.4.0 | 3.40  | 3.4.) |
| VP<br>(km/sec)                              | 12.73  |                | 12.51 | 12.42 | 12.34 | 12.26    | 12.16 | 12.07 | 11.97  | 11.86  | 11.75  | 11.63   | 12.11  | 11.39  | 11.26  | 11.17  | 11.67   | 10.97  | 10.84  | 10.13  | 10.03  | 6.96   | 5.90   | 5.63   | 9.76   | 5.69   | 5.63  | 5      | 64.5  | 5.42  | ~      | ~      | 01    | 66.9<br>2 | C. 40 | 21    | 10     | N     |         | 6.1.9 | e.10  | 8.C6   | 10.8  | 1.5.1  | Ch.   | ¢.20  | ٠     | 6.23  |
| DEPTH<br>(km)                               | 1996   | 1921           | 1711  | 1696  | 1621  | 1540     | 1471  | 1396  | 1321   | 1246   | 1111   | 1096    | 1021   | 946    | 871    | 821    | 111     | 721    | 671    | 671    | 646    | 621    | 596    | 57:    | 546    | 521    | 496   | 471    | 440   | 420   | 4 20   | 365    | 371   | 321       | 100   | 194   | 171    | 140   | 121     | 100   | 100   | 81     | 61    | 41     | 21    | 21    | 11    | c     |
| RADIUS<br>(km)                              | 4375   | 45.75          | 4633  | 4675  | 64753 | 4825     | 4910  | 4975  | 5050   | 5125   | 52 33  | 5275    | 5350   | 5425   | 5500   | 5550   | 5630    | 5650   | 57.00  | 5730   | 5125   | 5750   | 5115   | 5800   | 5d25   | 5850   | 5915  | 5900   | 5925  | 1565  | 1565   | 5165   | 6333  | 0000      | 0219  | 6175  | 6233   | 6225  | 6250    | £271  | 6271  | 6290   | (163  | 633J   | 6350  | 6350  | 6360  | 6371  |
| I   | 15     | 2.5            | 54    | 55    | 20    | 14       | 54    | 53    | 09     | 6.     | 62     | 63      | 49     | 65     | 99     | 67     | 6 8     | 69     | C1     | 11     | 22     | 13     | 14     | 15     | 16     | 11     | 18    | 61     | 30    | 81    | 82     | 10     | 34    | 0 4       | 27    |       | 84     | 0.6   | 16      | 26    | 55    | 37     | 56    | 96     | 15    | 60    | 65    | CC1   |

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Fit of the models to mode data

|                   | 0bsei           | Observed Data   |             | Mod             | Model Al                    | Mod             | Model Bl                    | Mode            | Model B2                    |
|-------------------|-----------------|-----------------|-------------|-----------------|-----------------------------|-----------------|-----------------------------|-----------------|-----------------------------|
| Mode              | Period<br>(sec) | S.E.M.<br>(sec) | 95%<br>C.I. | Period<br>(sec) | Period Rel.Error<br>(sec) % | Period<br>(sec) | Period Rel.Error<br>(sec) % | Period<br>(sec) | Period Rel.Error<br>(sec) % |
| 0.50              | 1227.65         | 0.683           | 1.44        | 1227.65         | 0.000                       | 1227.61         | -0.002                      | 1227.65         | 0.000                       |
| 1S0               | 613.57          | 0.236           | 0.54        | 614.63          | 0.172                       | 614.09          | 0.084                       | 614.85          | 0.205                       |
| 2 <sup>S0</sup>   | 398.54          | 0.084           | 0.16        | 399.22          | 0.170                       | 398.49          | -0.013                      | 398.65          | 0.027                       |
| 3S0               | 305.84          | 0.129           | 0.32        | 305.76          | -0.027                      | 305.53          | -0.102                      | 305.62          | -0.073                      |
| 4S0               | 243.59          | 0.067           | 0.15        | 243.70          | 0.043                       | 243.55          | -0.018                      | 243.69          | 0.042                       |
|                   |                 |                 |             |                 |                             |                 |                             |                 |                             |
| 052               | 3233.30         | 0.496           | 0.98        | 3231.50         | -0.056                      | 3232.45         | -0.026                      | 3232.34         | -0.030                      |
| 0 <sup>S</sup> 3  | 2133.56         | 0.380           | 0.86        | 2133.50         | -0,003                      | 2134.13         | 0.027                       | 2134.25         | 0.032                       |
| 0 S 4             | 1547.30         | 0.877           | 1.76        | 1545.42         | -0.121                      | 1545.82         | -0.096                      | 1546.07         | -0.080                      |
| 0 <sup>S</sup> 5  | 1190.12         | 0.432           | 0.86        | 1190.19         | 0.006                       | 1190.42         | 0.025                       | 1190.65         | 0.045                       |
| 0 <sup>S6</sup>   | 963.17          | 0.292           | 0.58        | 963.61          | 0.046                       | 963.72          | 0.057                       | 963.88          | 0.074                       |
| 0 <sup>S</sup> 7  | 811.45          | 0.246           | 0.50        | 812.25          | 0,099                       | 812.24          | 0.098                       | 812.32          | 0.107                       |
| 0 <sup>S</sup> 8  | 707.64          | 0.135           | 0.28        | 707.84          | 0.028                       | 707.70          | 600.0                       | 707.71          | 0.010                       |
| 0 <sup>S</sup> 9  | 633.95          | 0.102           | 0.20        | 633.94          | -0.005                      | 633.69          | -0.041                      | 633.66          | -0.046                      |
| 0 <sup>S</sup> 10 | 580.08          | 0.097           | 0.18        | 579.52          | -0.096                      | 579.89          | -0.154                      | 579.15          | -0.161                      |
| 0 <sup>S</sup> 11 | 536.56          | 0.105           | 0.22        | 537.21          | 0.121                       | 536.87          | 0.057                       | 536.83          | 0.051                       |
| 0 <sup>S</sup> 12 | 502.18          | 0.073           | 0.14        | 502.64          | 0.092                       | 502.34          | 0.032                       | 502.32          | 0.028                       |

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|                   | Obser           | Observed Data   | ~           | Mode            | Model Al       | Mode            | Model B1       | Mode            | Model B2       |
|-------------------|-----------------|-----------------|-------------|-----------------|----------------|-----------------|----------------|-----------------|----------------|
| Mode              | Period<br>(sec) | S.E.M.<br>(sec) | 95%<br>C.I. | Period<br>(sec) | Rel.Error<br>% | Period<br>(sec) | Rel.Error<br>% | Period<br>(sec) | Rel.Error<br>% |
| 0 <sup>S13</sup>  | 473.14          | 0.070           | 0.14        | 473.44          | 0.063          | 473.21          | 0.015          | 473.21          | 0,015          |
| 0 <sup>S</sup> 14 | 448.28          | 0.054           | 0.10        | 448.23          | -0.011         | 448.10          | -0.040         | 448.12          | -0.036         |
| 0 <sup>S15</sup>  | 426.24          | 0.053           | 0.10        | 426.19          | -0.017         | 426.16          | -0.018         | 426.20          | -0.009         |
| 0 <sup>S</sup> 16 | 406.77          | 0.050           | 0.10        | 406.74          | -0.008         | 406.79          | 0.005          | 406.85          | 0.020          |
| 0 <sup>S</sup> 17 | 389.31          | 0.068           | 0.14        | 389.44          | 0.032          | 389.56          | 0.064          | 389.64          | 0.083          |
| 0 <sup>S</sup> 18 | 373.89          | 0.071           | 0.14        | 373.93          | 0.011          | 374.10          | 0.055          | 374.20          | 0.083          |
| 0 <sup>S</sup> 19 | 360.20          | 0.064           | 0.12        | 359.96          | -0.066         | 360.14          | -0.017         | 360.26          | 0.015          |
| 0 <sup>S</sup> 20 | 347.82          | 0.067           | 0.14        | 347.30          | -0.150         | 347.47          | -0.102         | 347.59          | -0.066         |
| 0 <sup>S</sup> 21 | 336.00          | 0.056           | 0.12        | 335.75          | -0.075         | 335.88          | -0.036         | 336.02          | -0.005         |
| 0 <sup>S</sup> 22 | 325.31          | 0.060           | 0.12        | 325,15          | -0.048         | 325.23          | -0.024         | 325,38          | 0.020          |
| 0 <sup>S</sup> 23 | 315.43          | 0.044           | 0.08        | 315.38          | -0.016         | 315,38          | -0.016         | 315.53          | 0.031          |
| 0 <sup>S</sup> 24 | 306.25          | 0.050           | 0.10        | 306.33          | 0.026          | 306.24          | -0.002         | 306.40          | 0.047          |
| 0 <sup>S</sup> 25 | 297.71          | 0.048           | 0.10        | 297.90          | 0.064          | 297.72          | 0.004          | 297.87          | 0.055          |
| 0 <sup>S</sup> 26 | 289.69          | 0.047           | 0.10        | 290.02          | 0.114          | 289.74          | 0.019          | 289.90          | 0.071          |
| 0 <sup>S</sup> 27 | 282.34          | 0.066           | 0.14        | 282.62          | 0.098          | 282.25          | -0.033         | 282.39          | 0.019          |
| 0 <sup>S</sup> 28 | 275.06          | 0.052           | 0.10        | 275.64          | 0.210          | 275.18          | 0.042          | 275.32          | 0.095          |
| 0 <sup>S</sup> 29 | 268.44          | 0.049           | 0.10        | 269.04          | 0.222          | 268.49          | 0.018          | 268.63          | 0.071          |

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|                    |                 |                 |             | Tabl            | Table A3.4 (cont.) |                 |                |                 |                |
|--------------------|-----------------|-----------------|-------------|-----------------|--------------------|-----------------|----------------|-----------------|----------------|
|                    | 0bse            | Observed Data   |             | Model Al        | 1 Al               | Mod             | Model B1       | Mod             | Model B2       |
| Mode               | Period<br>(sec) | S.E.M.<br>(sec) | 95%<br>C.I. | Period<br>(sec) | Rel.Error<br>%     | Period<br>(sec) | Rel.Error<br>% | Period<br>(sec) | Rel.Error<br>% |
| 0 <sup>S</sup> 30  | 262.15          | 0.051           | 0.10        | 262.76          | 0.236              | 262.15          | -0.000         | 262.29          | 0.052          |
| 0 <sup>S</sup> 31  | 256.00          | 0,062           | 0.12        | 256.81          | 0.315              | 256.12          | 0.048          | 256.26          | 0.100          |
| 0 <sup>S</sup> 32  | 250.20          | 0.055           | 0.12        | 251.12          | 0.368              | 250.38          | 0.073          | 250.51          | 0.125          |
| 0 <sup>5</sup> 33  | 244.95          | 0.056           | 0.12        | 245.68          | 0.300              | 244.91          | -0.018         | 245.03          | 0.033          |
| 0 <sup>S</sup> 34  | 239.70          | 0.066           | 0.14        | 240.48          | 0.324              | 239.67          | -0.013         | 239.79          | 0.037          |
| 0 <sup>S</sup> 35  | 234.69          | 0.067           | 0.14        | 235.48          | 0.337              | 234.66          | -0.014         | 234.77          | 0.035          |
| 0 <sup>S</sup> 36  | 229.74          | 0,066           | 0.14        | 230.66          | 0.409              | 229.85          | 0.048          | 229.96          | 0.097          |
| 0 <sup>S</sup> 37  | 225.16          | 0.052           | 0.10        | 226.06          | 0.400              | 225.24          | 0.034          | 225.35          | 0.083          |
| 0 <sup>5</sup> 38  | 220.62          | 0.050           | 0.10        | 221.61          | 0.400              | 220.80          | 0.083          | 220.91          | 0.131          |
| .0 <sup>5</sup> 39 | 216.43          | 0.052           | 0.10        | 217.32          | 0.412              | 216.54          | 0.049          | 216.64          | 0.097          |
| 0 S4 0             | 212.31          | 0.090           | 0.18        | 213.18          | 0.410              | 212.43          | 0.056          | 212.53          | 0.103          |
| 0 S41              | 208.05          | 0.123           | 0.24        | 209.18          | 0.544              | 208.47          | 0.201          | 208.57          | 0.249          |
| 0 S42              | 204.57          | 0.072           | 0.14        | 205.32          | 0.364              | 204.65          | 0.038          | 204.75          | 0.086          |
| 0 S4 3             | 200.93          | 0.080           | 0.16        | 201.58          | 0.321              | 200.96          | 0.016          | 201.06          | 0.063          |
| 0 S4 4             | 197.19          | 0.077           | 0.16        | 197.96          | 0.389              | 197.40          | 0.105          | 197.49          | 0.153          |
| 0 S45              | 194.03          | 0.073           | 0.14        | 194.45          | 0.218              | 193.95          | -0.039         | 194.05          | 0.008          |
| 0 S46              | 190.59          | 0.085           | 0.18        | 191.06          | 0.246              | 190.62          | 0.017          | 190.71          | 0.064          |
| 0 S4 7             | 187.43          | 0.054           | 0.11        | 187.77          | 0.180              | 187.40          | -0.018         | 187.49          | 0.029          |

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|                   |                 |                 |             | Tab             | Table A3. 4 (cont.) | ~               |                |                 |                |
|-------------------|-----------------|-----------------|-------------|-----------------|---------------------|-----------------|----------------|-----------------|----------------|
|                   | Obse            | Observed Data   |             | Mod             | Model Al            | Mod             | Model B1       | Mode            | Model B2       |
| Mode              | Period<br>(sec) | S.E.M.<br>(sec) | 95%<br>C.I. | Period<br>(sec) | Rel.Error<br>%      | Period<br>(sec) | Rel.Error<br>% | Period<br>(sec) | Rel.Error<br>% |
| 0 <sup>S48</sup>  | 184.25          | 060.0           | 0.19        | 184.58          | 0.177               | 184.27          | 0.019          | 184.36          | 0.059          |
| 0 <sup>S49</sup>  | 181.30          | 0.106           | 0.23        | 181.48          | 0.101               | 181.24          | -0.031         | 181.33          | 0.017          |
| 0 <sup>S</sup> 50 | 178.35          | 0.118           | 0.25        | 178.48          | 0.072               | 178.83          | -0.023         | 178.39          | 0.025          |
| 0 <sup>S</sup> 51 | 175.42          | 0.030           | 0.06        | 175.56          | 0.082               | 175.46          | 0.023          | 175.54          | 0.071          |
| 0 <sup>S</sup> 52 | 172.64          | 0.030           | 0.06        | 172.73          | 0.054               | 172.70          | 0.033          | 172.78          | 0.082          |
| 0 <sup>S</sup> 53 | 169.97          | 0.030           | 0.06        | 169.98          | 0.008               | 170.01          | 0.026          | 170.10          | 0.074          |
| 0 <sup>S</sup> 54 | 167.38          | 0.030           | 0.06        | 167.31          | -0.041              | 167.41          | 0.016          | 167.49          | 0.065          |
| 0 <sup>S</sup> 55 | 164.85          | 0.030           | 0.06        | 164.71          | -0.082              | 164.87          | 0.015          | 164.95          | 0.063          |
| 0 <sup>S</sup> 56 | 162.41          | 0.030           | 0.06        | 162.19          | -0.135              | 162.41          | 100.01         | 162.49          | 0.050          |
| 0 <sup>S</sup> 57 | 160.01          | 0.030           | 0.06        | 159.74          | -0.172              | 160.02          | 0.004          | 160.09          | 0.053          |
| 0 <sup>5</sup> 58 | 157.70          | 0.040           | 0.08        | 157.35          | -0.224              | 157.69          | -0.009         | 157.76          | 0.040          |
| 0 <sup>S</sup> 59 | 155.45          | 0.040           | 0.08        | 155.02          | -0.275              | 155.42          | -0.021         | 155.49          | 0.028          |
| 0 <sup>S</sup> 60 | 153.24          | 0.040           | 0.08        | 152.76          | -0.313              | 153.21          | -0.020         | 153.28          | 0.029          |
| 0 <sup>561</sup>  | 151.12          | 0,040           | 0.08        | 150.56          | -0.371              | 151.06          | -0.041         | 151.13          | 0.008          |
| 0 <sup>S</sup> 62 | 149.07          | 0,040           | 0.08        | 148.42          | -0.439              | 148.96          | -0.072         | 149.04          | -0.020         |
| 0 <sup>5</sup> 63 | 147.09          | 0.050           | 0,11        | 146.33          | -0.519              | 146.92          | -0.115         | 146.99          | -0.067         |

Table A3. 4 (cont.)

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|                   |                 |                 |             | Ta              | Table A3.4 (cont.) | nt.)            |                             |                 |                |
|-------------------|-----------------|-----------------|-------------|-----------------|--------------------|-----------------|-----------------------------|-----------------|----------------|
|                   | Obse            | Observed Data   |             | Mo              | Model Al           | Mod             | Model B1                    | Mod             | Model B2       |
| Mode              | Period<br>(sec) | S.E.M.<br>(sec) | 95%<br>C.I. | Period<br>(sec) | Rel.Error<br>%     | Period<br>(sec) | Period Rel.Error<br>(sec) % | Period<br>(sec) | Rel.Error<br>% |
| 1 <sup>S</sup> 2  | 1470.85         | 1.227           | 2.60        | 1468.52         | -0.158             | 1469.05         | -0.122                      | 1469.39         | -0.099         |
| 1 <sup>S</sup> 3  | 1060.83         | 0.993           | 2.05        | 1062.41         | 0.149              | 1062.76         | 0.182                       | 1063.09         | 0.213          |
| $1^{S_4}$         | 852.68          | 0.374           | 0.74        | 851.48          | -0.140             | 851.75          | -0.109                      | 852.11          | -0.067         |
| 1 <sup>55</sup>   | 730.56          | 0.437           | 1.00        | 729.16          | -0.191             | 729.30          | -0.172                      | 729.67          | -0.122         |
| 1 <sup>56</sup>   | 657.61          | 0.201           | 0.41        | 656.99          | -0.094             | 656.94          | -0.102                      | 657.27          | -0.052         |
| 1 <sup>S</sup> 7  | 603.93          | 0.306           | 0.63        | 604.40          | 0.078              | 604.25          | 0.053                       | 604.54          | 0.100          |
| 1 <sup>5</sup> 8  | 555.83          | 0.156           | 0.16        | 556.37          | 0.098              | 556.22          | 0.070                       | 556.45          | 0.112          |
| 159               | 509.58          | 0.197           | 0.43        | 509.97          | 0.076              | 509.86          | 0.056                       | 510.03          | 0.088          |
| 1 <sup>5</sup> 10 | 465.45          | 0.287           | 0.63        | 466.23          | 0.169              | 466.20          | 0.161                       | 466.29          | 0.180          |
| 1 <sup>S</sup> 14 | 337.00          | 0.084           | 0,16        | 336.57          | -0.128             | 336.64          | -0.107                      | 336.55          | -0.135         |
| 1 <sup>5</sup> 15 | 316.06          | 0.076           | 0.17        | 315.55          | -0.162             | 315.59          | -0.150                      | 315.64          | -0.132         |
| 1 <sup>5</sup> 16 | 299.87          | 0.145           | 0.33        | 299.59          | -0.094             | 299.47          | -0.135                      | 299.63          | -0.079         |
| 1 <sup>S</sup> 17 | 285.97          | 0.129           | 0.29        | 286.38          | 0.142              | 286.10          | 0.044                       | 286.29          | 0.112          |
|                   |                 |                 |             |                 |                    |                 |                             |                 |                |
| 2 <sup>S</sup> 1  | 1058.09         | 0.892           | 2.06        | 1057.79         | -0.029             | 1057.92         | -0.016                      | 1057.75         | -0.032         |
| 2 <sup>S</sup> 2  | 904.23          | 0.487           | 1.04        | 903.92          | -0.034             | 904.50          | 0.029                       | 904.57          | 0.038          |
| 2 <sup>S</sup> 3  | 804.17          | 0.511           | 1.10        | 804.66          | 0.061              | 805.04          | 0.109                       | 805.21          | 0.130          |
| 2 S4              | 724.87          | 0.234           | 0.45        | 724.76          | -0.016             | 725.02          | 0.021                       | 725.20          | 0.045          |

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|                    | Model B2      | Period Rel.Error<br>(sec) % | 657.67 -0.112   | 594.82 0.018    | 487.90 -0.024   | 448.63 0.061    | 416.15 0.114     | 388.80 0.136      | 365.37 0.067 | 344.91 0.010      | 326.57 0.094 | 308.87 -0.106 | 580.47 -0.057 | 487.94 -0.227 | 438.90 -0.063 | 414.88 -0.055 | 392.36 0.010 | 372.38 0.090    | 354.80 0.064     |
|--------------------|---------------|-----------------------------|-----------------|-----------------|-----------------|-----------------|------------------|-------------------|--------------|-------------------|--------------|---------------|---------------|---------------|---------------|---------------|--------------|-----------------|------------------|
|                    | Model B1      | Period Rel.Error<br>(sec) % |                 | -0.018          | -0.076          | 0.002           | 0.052            | 0.071             | 0.002        | -0.050            | 0.056        | -0.081        | -0.054        | -0.215        | -0.088        | -0.059        | 0.025        | 0.108           | 0.083            |
| nt.)               | Mode          | Period<br>(sec)             |                 | 594.60          | 487.65          | 448.37          | 415.89           | 388.54            | 365.13       | 344.71            | 326.44       | 308.95        | 580.49        | 488.00        | 438.79        | 414.87        | 392.42       | 372.45          | 354.86           |
| Table A3.4 (cont.) | Model Al      | Period Rel.Error<br>(sec) X |                 |                 | -0.151          | -0.076          | -0.026           | 0.000             | -0.054       | -0.083            | 0.053        | -0.058        | -0.034        | -0.211        | -0.023        | 0.047         | 0.097        | 0.180           | 0.141            |
| Tal                | Mo            | Period<br>(sec)             |                 |                 | 487.28          | 448.02          | 415.56           | 388.27            | 364.92       | 344.59            | 326.43       | 309.02        | 580.61        | 488.02        | 439.08        | 415.17        | 392.70       | 372.72          | 355.07           |
|                    |               | 95%<br>C.I.                 | 0.23            | 0.29            | 0.33            | 0.29            | 0.33             | 0.55              | 0.40         | 0.44              | 0.25         | 0.15          | 1.40          | 0.82          | 1.05          | 0.51          | 0.22         | 0.28            | 0.23             |
|                    | Observed Data | S.E.M.<br>(sec)             | 0.111           | 0.137           | 0.151           | 0.133           | 0.163            | 0.229             | 0.188        | 0.186             | 0.i24        | 0.055         | 0.700         | 0.359         | 0.476         | 0.221         | 0.114        | 0.126           | 0.106            |
|                    | Obse          | Period<br>(sec)             | 660.41          | 594.71          | 488.02          | 448.36          | 415.67           | 388.27            | 365.12       | 344.88            | 326.26       | 309.20        | 580.80        | 489.05        | 439.18        | 415.11        | 392.32       | 372.05          | 354.57           |
|                    |               | Mode                        | 2 <sup>55</sup> | 2 <sup>56</sup> | 2 <sup>58</sup> | 2 <sup>59</sup> | 2 <sup>S10</sup> | 2 <sup>5</sup> 11 | 2 S12        | 2 <sup>S</sup> 13 | 2 S14        | 2 S1 5        | 3 S2          | 3 S3          | 3 S4          | 3 S 5         | 3 S6         | 3 <sup>57</sup> | 3 <sup>5</sup> 8 |

|                   |                 |                 |             | Tal             | Table A3.4 (cont.) | t.) .           |                             |                 |                |
|-------------------|-----------------|-----------------|-------------|-----------------|--------------------|-----------------|-----------------------------|-----------------|----------------|
|                   | Obser           | Observed Data   |             | Moc             | Model Al           | Mod             | Model B1                    | Mod             | Model B2       |
| Mode              | Period<br>(sec) | S.E.M.<br>(sec) | 95%<br>C.I. | Period<br>(sec) | Rel.Error<br>%     | Period<br>(sec) | Period Rel.Error<br>(sec) % | Period<br>(sec) | Rel.Frror<br>% |
| 3 <sup>5</sup> 9  | 339.14          | 0.145           | 0.32        | 339.15          | 0.004              | 339.02          | -0.034                      | 338.98          | -0.048         |
| 3 <sup>5</sup> 10 | 323.80          | 0.111           | 0.23        | 324.45          | 0.201              | 324.41          | 0.187                       | 324.39          | 0.181          |
| 3 <sup>5</sup> 11 | 310.77          | 0.075           | 0.20        | 310.64          | -0.043             | 310.68          | -0.029                      | 310.68          | -0.028         |
|                   |                 | ſ               |             |                 |                    |                 |                             |                 |                |
| 4S1               | 505.82          | 0.211           | 0.45        | 504.36          | -0.288             | 504.14          | -0.333                      | 504.47          | -0.267         |
| 4S2               | 479.33          | 0.186           | 0.38        | 478.11          | -0.255             | 478.00          | -0.277                      | 478.29          | -0.217         |
| 4S3               | 460.78          | 0.146           | 0.30        | 461.14          | 0.077              | 460.93          | 0.033                       | 461.14          | 0.077          |
| 4S4               | 420.10          | 0.089           | 0.19        | 420.19          | 0.021              | 420.22          | 0.029                       | 420.14          | 0.009          |
| 4S5               | 369.72          | 0.074           | 0.15        | 369.83          | 0.029              | 369.88          | 0.044                       | 369.80          | 0.022          |
| 4.S6              | 332.11          | 0.082           | 0.18        | 332.08          | -0.009             | 332.15          | 0.011                       | 332.09          | -0.005         |
| 4S7               | 303.97          | 0.091           | 0.19        | 303.87          | -0.033             | 303.95          | -0.006                      | 303.95          | -0.007         |
| 458               | 283.56          | 0,098           | 0.21        | 283,73          | 0,061              | 283.83          | 0.095                       | 283.87          | 0,011          |
| 4S9               | 269.66          | 0.058           | 0.13        | 269.81          | 0.054              |                 |                             |                 |                |
| 4S10              | 258.86          | 0.049           | 0.10        | 258.94          | 0.032              | 259.03          | 0.064                       | 258.96          | 0.038          |
|                   |                 |                 |             |                 |                    |                 |                             |                 |                |
| 5 <sup>52</sup>   | 397.36          | 0.157           | 0.36        | 396.48          | -0.221             | 396.78          | -0.147                      | 397.06          | -0.075         |
| 5 <sup>5</sup> 3  | 353.52          | 0.170           | 0.42        | 354.34          | 0.233              | 354.22          | 0.197                       | 354.33          | 0.228          |

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|                    | Model B2      | Period Rel.Error<br>(sec) % | -0.012           | 0.033            | 0,001           | -0.130           | -0.050           | 0.015           |    | -0.123           | 0.528            |
|--------------------|---------------|-----------------------------|------------------|------------------|-----------------|------------------|------------------|-----------------|----|------------------|------------------|
|                    | Mod           | Period<br>(sec)             | 348.37           | 293.29           | 273.52          | 309.67           | 281.23           | 240.00          | r. | 271.77           | 249.05           |
|                    | Model B1      | Period Rel.Error<br>(sec) % | -0.027           | -0.021           | -0.019          | -0.158           | -0.053           | -0.026          |    | -0.244           | 0.390            |
| 1t.)               | Mode          | Period<br>(sec)             | 348.32           | 293.13           | 273.35          | 309.58           | 281.22           | 239.90          |    | 271.44           | 248.71           |
| Table A3.4 (cont.) | Model Al      | Period Rel.Error<br>(sec) % | 0.119            | 0.006            | 0.009           | -0.031           | -0.014           | 0.103           |    | -0.194           | -0.393           |
| Tab                | Moc           | Period<br>(sec)             | 348.83           | 293.21           | 273.54          | 309.97           | 281.33           | 240.21          |    | 271.57           | 246.77           |
|                    |               | 95%<br>C.I.                 | 0.10             | 0.28             | 0.11            | 0.17             | 0.25             | 0.06            |    | 0.31             | 0.05             |
|                    | Observed Data | S.E.M.<br>(sec)             | 0.046            | 0.132            | 0.046           | 0.079            | 0.113            | 0.028           |    | 0.144            | 0.022            |
|                    | Obse          | Period<br>(sec)             | 348.41           | 293.19           | 273.52          | 310.07           | 281.37           | 239.96          |    | 272.10           | 247.74           |
|                    |               | Mode                        | 6 <sup>S</sup> 1 | 6 <sup>5</sup> 4 | 6 <sup>S5</sup> | 7 <sup>S</sup> 2 | 7 <sup>S</sup> 3 | 7 <sup>S5</sup> |    | 8 <sup>S</sup> 1 | 8 <sup>5</sup> 2 |

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|                  |                 |                 |             | Tab             | Table A3.4 (cont.) |                 |                |                 |                |
|------------------|-----------------|-----------------|-------------|-----------------|--------------------|-----------------|----------------|-----------------|----------------|
|                  | Obse            | Observed Data   |             | Mod             | Model Al           | Mod             | Model B1       | Mod             | Model B2       |
| Mode             | Period<br>(sec) | S.E.M.<br>(sec) | 95%<br>C.I. | Period<br>(sec) | Rel.Error<br>%     | Period<br>(sec) | Rel.Error<br>% | Period<br>(sec) | Rel.Error<br>% |
| 0 <sup>T</sup> 2 | 2640.63         | 10.104          | 23.84       | 2630.62         | -0.379             | 2630.81         | -0.372         | 2631.36         | -0.351         |
| 0 <sup>T</sup> 3 | 1705.83         | 2.529           | 5.47        | 1702.30         | -0.213             | 1702.43         | -0.205         | 1702.91         | -0.177         |
| 0T4              | 1305.45         | 0.926           | 1.91        | 1303.42         | -0.155             | 1303.53         | -0.147         | 1303.98         | -0.113         |
| 0 <sup>T</sup> 5 | 1075.97         | 0.820           | 1.68        | 1075.20         | -0.072             | 1075.30         | -0.062         | 1075.73         | -0.022         |
| $0^{T}6$         | 925.83          | 0.530           | 1.11        | 925.16          | -0.072             | 925.26          | -0.062         | 925.67          | -0.018         |
| 0T7              | 819.31          | 0.680           | 1.41        | 817.68          | -0.199             | 817.76          | -0.189         | 818.15          | -0.142         |
| 0T 8             | 736.86          | 0.339           | 0.68        | 736.06          | -0.109             | 736.13          | -0.099         | 736.48          | -0.051         |
| $0^{T}9$         | 671.80          | 0.369           | 0.74        | 671.48          | -0.047             | 671.53          | -0.040         | 671.86          | 0.008          |
| $0^{T}10$        | 618.98          | 0.294           | 0.58        | 618.82          | -0.026             | 618.84          | -0.023         | 619.13          | 0,025          |
| 0T11             | 574.62          | 0.469           | 0.96        | 574.84          | 0.039              | 574.82          | 0.035          | 575.09          | 0.082          |
| 0T12             | 536.84          | 0.337           | 0.70        | 537.44          | 0.112              | 537.37          | 0.099          | 537.62          | 0.145          |
| 0T13             | 504.94          | 0.411           | 0.84        | 505.15          | 0.041              | 505.02          | 0.016          | 505.24          | 0.060          |
| 0T14             | 475.73          | 0.363           | 0.75        | 476.91          | 0.247              | 576.73          | 0.209          | 576.92          | 0.251          |
| 0T 15            | 450.97          | 0.255           | 0.54        | 451.95          | 0.216              | 451.71          | 0.164          | 451.89          | 0.204          |
| 0T16             | 429.19          | 0.270           | 0.56        | 429.68          | 0.115              | 429.40          | 0.049          | 429.56          | 0.085          |
| 0T 17            | 407.95          | 0.195           | 0.42        | 409.68          | 0.424              | 409.35          | 0.342          | 409.48          | 0.376          |
| 0T 18            | 390.94          | 0.283           | 0.58        | 391.58          | 0.163              | 391.20          | 0.066          | 391.32          | 0.096          |
| 0T 19            | 374.75          | 0.168           | 0.36        | 375.10          | 0.093              | 374.68          | -0.019         | 374.78          | 0.008          |

Table A3.4 (cont )

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|                   | Obser           | Observed Data   |             | Mod             | Model Al       | Mode            | Model B1       | Mode            | Model B2       |
|-------------------|-----------------|-----------------|-------------|-----------------|----------------|-----------------|----------------|-----------------|----------------|
| Mode              | Period<br>(sec) | S.E.M.<br>(sec) | 95%<br>C.I. | Period<br>(sec) | Rel.Error<br>% | Period<br>(sec) | Rel.Error<br>% | Feriod<br>(sec) | Rel.Error<br>% |
| 0 <sup>T</sup> 20 | 359.59          | 0.291           | 0.62        | 360.03          | 0.121          | 359.57          | -0.007         | 359.65          | 0.017          |
| 0 <sup>T</sup> 21 | 345.82          | 0.296           | 0.65        | 346.17          | 0.100          | 345.67          | -0.042         | 345.74          | -0.022         |
| 0 <sup>T</sup> 22 | 332.57          | 0.220           | 0.49        | 333,38          | 0.242          | 332.85          | 0.086          | 332.91          | 0.102          |
| $0^{T_{23}}$      | 321.21          | 0.291           | 0.63        | 321.52          | 0.097          | 320.98          | -0.071         | 321.02          | -0.058         |
| 0 <sup>T</sup> 24 | 310.18          | 0.252           | 0.55        | 310.51          | 0.106          | 309.95          | -0.075         | 309,98          | -0.065         |
| 0 <sup>T</sup> 25 | 299.51          | 0.206           | 0.51        | 300.24          | 0.244          | 299.66          | 0.051          | 299.68          | 0.057          |
| 0 <sup>T</sup> 26 | 290.26          | 0.156           | 0.39        | 290.64          | 0.130          | 290.05          | -0.072         | 290.06          | -0.069         |
| 0 <sup>T</sup> 27 | 281.21          | 0.444           | 1.13        | 281.64          | 0.153          | 281.05          | -0.057         | 281.05          | -0.058         |
| 0 <sup>T</sup> 28 | 272.75          | 0.274           | 0.61        | 273.19          | 0.161          | 272.59          | -0.057         | 272.58          | -0.061         |
| $0^{T}29$         | 264.53          | 0.324           | 1.01        | 265.24          | 0.267          | 264.64          | 0.041          | 264.62          | 0.034          |
| 0 <sup>T</sup> 30 | 257.29          | 0.375           | 1.01        | 257.73          | 0.171          | 257.14          | -0.060         | 257.11          | -0.070         |
| 0 <sup>T</sup> 31 | 249.85          | 0.239           | 0.59        | 250.64          | 0.316          | 250.05          | 0.080          | 250.02          | 0.067          |
| 0 <sup>T</sup> 32 | 242.97          | 0.251           | 0.59        | 243.93          | 0.396          | 243.35          | 0.155          | 243.31          | 0.139          |
| 0 <sup>T</sup> 33 | 236.71          | 0.235           | 0.62        | 236.71          | 0.365          | 237.00          | 0.120          | 236.95          | 0.102          |
| 0 <sup>T</sup> 34 | 231.29          | 0.227           | 0.64        | 231.54          | 0.107          | 230.97          | -0.140         | 230.92          | -0.161         |
| 0 <sup>T</sup> 35 | 224.93          | 0.346           | 0.86        | 225.79          | 0.384          | 225.24          | 0.137          | 225.18          | 0.112          |
| 0 <sup>T</sup> 36 | 219.69          | 0.247           | 0.64        | 220.33          | 0.292          | 219.79          | 0.043          | 219.73          | 0.017          |
| 0 <sup>T</sup> 37 | 213.89          | 0.214           | 0.67        | 215.13          | 0.578          | 214.59          | 0.328          | 214.53          | 0.298          |

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|                   |                 |                 |             | Ta              | Table A3.4 (cont.) | t.)             |                |                 |                |
|-------------------|-----------------|-----------------|-------------|-----------------|--------------------|-----------------|----------------|-----------------|----------------|
|                   | 0bse            | Observed Data   |             | Mo              | Model Al           | Mod             | Model B1       | Mod             | Model B2       |
| Mode              | Period<br>(sec) | S.E.M.<br>(sec) | 95%<br>C.I. | Period<br>(sec) | Rel.Error<br>%     | Period<br>(sec) | Rel.Error<br>% | Period<br>(sec) | Rel.Error<br>% |
| 0 <sup>T38</sup>  | 209.83          | 0.593           | 2.54        | 210.16          | 0.157              | 209.65          | -0.087         | 209.57          | -0.124         |
| 0 <sup>T</sup> 39 | 204.27          | 0,098           | 0.43        | 205.42          | 0.561              | 204.92          | 0.316          | 204.85          | 0.282          |
| 0 <sup>T</sup> 40 | 199.96          | 0.381           | 1.06        | 200.88          | 0.460              | 200.39          | 0.216          | 200.32          | 0.180          |
| 0 <sup>T41</sup>  | 195.88          | 0.434           | 1.20        | 196.54          | 0.336              | 196.05          | 0.088          | 195.99          | 0.056          |
| 0 <sup>T42</sup>  | 191.26          | 0.254           | 0.70        | 192.38          | 0.585              | 191.91          | 0.338          | 191.83          | 0.297          |
| $0^{T_43}$        | 187.40          | 0.490           | 0.21        | 188.39          | 0.528              | 187.93          | 0.283          | 187.85          | 0.240          |
| $0^{T_{44}}$      | 183.78          | 0.270           | 0.75        | 184.57          | 0.431              | 184.12          | 0.182          | 184.03          | 0.138          |
| 0 <sup>T45</sup>  | 180.25          | 0.056           | 0.19        | 180.90          | 0.358              | 180.45          | 0.112          | 180.37          | 0.065          |
| $0^{T_{46}}$      | 176.85          | 0.056           | 0.19        | 177.36          | 0.289              | 176.93          | .0.046         | 176.84          | -0.003         |
|                   |                 |                 |             |                 |                    |                 |                |                 |                |
| $1^{T_2}$         | 756.57          | 0.625           | 1.36        | 757.47          | 0.118              | 756.80          | 0.030          | 756.99          | 0.055          |
| $1^{T_3}$         | 695.18          | 0.515           | 1.10        | 694.92          | 0.037              | 694.41          | -0.109         | 694.52          | -0.092         |
| $1^{T_4}$         | 629.98          | 0.627           | 1.74        | 630.87          | 0.014              | 630.50          | 0.083          | 630.56          | 0.092          |
| $1^{T_6}$         | 519.09          | 0.297           | 0.68        | 519.60          | 0.098              | 519.46          | 0.072          | 519.52          | 0.083          |
| $1^{\mathrm{T8}}$ | 438.50          | 0.230           | 0.59        | 438.94          | 0,099              | 438.89          | 0.088          | 439.01          | 0.117          |
| 1 <sup>T10</sup>  | 381.58          | 0.148           | 0.33        | 382.17          | 0.155              | 382.07          | 0.129          | 382.24          | 0.173          |
| $2 T_{4}$         | 421.81          | 0.363           | 0.78        | 420.29          | -0.359             | 420.62          | -0.283         | 421.05          | -0.180         |
| 2 T7              | 363.66          | 0.283           | 0.62        | 363.72          | -0.010             | 363.47          | -0.053         | 363.59          | -0.020         |
| 2 T8              | 343.46          | 0.219           | 0.50        | 343.75          | -0.085             | 343.48          | 0.004          | 343.49          | 0.010          |

Table A3.4 (cont

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|                    | Model B2   | T ∆T<br>(sec) (sec)  | 181.1 -0.8 | 151.3 -0.1 | 124.5 -0.6 | 100.7 -0.0 |       | 61.8 -0.5 |       | 33.0 -0.0 | 22.1 -0.0 | 13.6 0.2 | 161.7 -0.6 | 134.0 0.9 | 109.3 0.2 | 87.7 0.4 | 68.8 -0.0 | 52.4 -0.1 | 38.4 0.9 | 26.7 0.8 | 17.3 0.1 |
|--------------------|------------|----------------------|------------|------------|------------|------------|-------|-----------|-------|-----------|-----------|----------|------------|-----------|-----------|----------|-----------|-----------|----------|----------|----------|
| time data          | Model B1   | ΔT<br>(sec)          | -0.9       | -0.1       | -0.6       | 0.1        | 0.0   | -0.5      | 0.0   | -0.2      | -0.3      | -0.8     | -0.5       | 1.0       | 0.3       | 0.5      | 0.0       | -0.1      | 0.8      | 0.6      | -0.2     |
| travel time        | Mode       | T<br>(sec)           | 181.0      | 151.3      | 124.5      | 100.8      | 79.9  | 61.8      | 46.1  | 32.8      | 21.8      | 13.3     | 161.7      | 134.1     | 109.4     | 87.8     | 68.8      | 52.4      | 38.3     | 26.5     | 17.0     |
| ential             | el Al      | AT<br>(sec)          | -0.5       | -0.0       | -0.7       | -0.1       | -0.2  | -0.7      | -0.1  | -0.3      | -0.2      | 0.2      | -0.3       | 1.0       | 0.2       | 0.4      | -0.1      | -0.2      | 0.7      | 0.7      | 0.7      |
| el to differential | Model      | T<br>(sec)           | 181.5      | 151.4      | 124.5      | 100.6      | 79.8  | 61.6      | 46.0  | 32.8      | 22.0      | 13.6     | 161.9      | 134.1     | 109.3     | 87.7     | 68.7      | 52.3      | 38.2     | 26.6     | 17.3     |
| the rodel          |            | 95%<br>C.I.          | 0.39       | 0.30       | 0.46       | 0.43       | 0.39  | 1.02      | 0.99  | 0.95      | 2.72      | 2.12     | 0.69       | 2.17      | 2.58      | 0.61     | 0.13      | 0.53      | 0.49     | 0.59     | 0.59     |
| Fit of             | Data       | S.E.M.<br>(sec)      | 0,18       | 0.14       | 0.22       | 0.22       | 0.19  | 0.45      | 0.45  | 0.43      | 1.11      | 0.76     | 0.27       | 0.78      | 0.81      | 0.28     | 0.06      | 0.19      | 0.23     | 0.27     | 0.25     |
|                    | Observed I | T<br>(sec)           | 181.9      | 151.4      | 125.1      | 100.7      | 79.9  | 62.3      | 46.1  | 33.0      | 22.1      | 13.4     | 162.2      | 133.1     | 109.1     | 87.3     | 68.8      | 52.5      | 37.5     | 25.9     | 17.2     |
|                    | OF         | ∆<br>(deg)           | 30.00      | 35.00      | 40.00      | 45.00      | 50,00 | 55.00     | 60.00 | 65.00     | 70.00     | 75.00    | 30.00      | 35.00     | 40.00     | 45.00    | 50.00     | 55.00     | 60.00    | 65.00    | 70.00    |
|                    |            | Phase<br>combination | PcP - P    | surface    | focus      |            |       |           |       |           |           |          | PcP - P    | deep      | focus     |          |           |           |          |          |          |

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|                     | Model B2   | ΔT<br>(sec)                  | 0.7    | 0.3      | -0.1   | 0.4    | 1.1    | 0.5    | -0.1    | -0.0   | -1.1   | -1.6   |
|---------------------|------------|------------------------------|--------|----------|--------|--------|--------|--------|---------|--------|--------|--------|
| 2                   | Mode       | T<br>(sec)                   | . 7.0  | 20.3     | 35.2   | 60.4   | 0.06   | 2.1    | 5.0     | 7.6    | 10.1   | 12.4   |
|                     | Model B1   | ∆T<br>(sec)                  | -0.1   | -0.3     | -0.6   | 0.1    | Ī      | 0.0    | -0.4    | -0.3   | -1.3   | -1.8   |
|                     | Mode       | T<br>(sec)                   | 7.8    | 20.9     | 35.7   | 60.7   | 1.     | 2.5    | 5.3     | 7.9    | 10.3   | 12.6   |
| 1.00110-1           | Model Al   | ΔT<br>(sec)                  | 0.3    | 0.1      | -0.2   | 0.5    | I      | 0.1    | -0.4    | -0.4   | -1.4   | -1.9   |
| Tante VI - (COIIC.) | Mode       | T<br>(sec)                   | 7.3    | 20.5     | 35.3   | 60.3   | 1      | 2.4    | 5.3     | 8.0    | 10.4   | 12.7   |
| ÷                   |            | 95%<br>C.I.                  | 0.51   | 0.58     | 0.39   | 0.64   | 0.69   | 0.71   | 0.23    | 0.42   | 0.58   | 0.77   |
|                     | )ata       | S.E.M.<br>(sec)              | 0.24   | 0.28     | 0.19   | 0.31   | 0.31   | 0.30   | 0.11    | 0.20   | 0.24   | 0.34   |
|                     | Observed D | T<br>(sec)                   | 7.7    | 20.6     | 35.1   | 60.8   | 100.1  | 2.5    | 4.9     | 7.6    | 0*6    | 10.8   |
|                     | Ob         | ∆<br>(deg)                   | 147.50 | 152.50   | 157.50 | 165.00 | 175.00 | 146.25 | 148.75  | 151.25 | 153.75 | 156.25 |
|                     |            | Phase ∆<br>combination (deg) | P'(AB) | -P' (DF) | deep   | focus  |        |        | -P'(DF) | deep   | focus  |        |

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Model B2

Model B1

Model Al

Observed Data

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| ∆T<br>(sec)          | -1.9    | -0.3  | -1.3  | 0.3   | 0.6   | 0.2   | 0.3   | -0.2  | 0.0   | 0.2   | 1.0   |
|----------------------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| , T<br>(sec)         | 309.4   | 259.1 | 214.4 | 174.6 | 139.2 | 108.7 | 82.3  | 59.5  | 40.6  | 25.7  | 15.0  |
| ∆T<br>(sec)          | -3.0    | -0.4  | -1.1  | 0.7   | 0.8   | 0.2   | 0.2   | -0.3  | -0.0  | 0.1   | 0.4   |
| T<br>(sec)           | 308.3   | 259.0 | 214.6 | 175.0 | 139.4 | 108.7 | 82.2  | 59.4  | 40.6  | 25.6  | 14.4  |
| ∆T<br>(sec)          | -1.6    | -0.7  | -2.3  | -0.9  | -0.0  | 0.2   | 0.5   | 0.3   | 0.5   | 0.7   | 0.6   |
| T<br>(sec)           | 309.7   | 258.7 | 213.4 | 173.4 | 138.6 | 108.7 | 82.5  | 60.0  | 41.1  | 26.2  | 14.6  |
| 95%<br>C.I.          | 1.77    | 1.53  | 1.62  | 1.11  | 1.44  | 1.25  | 1.07  | 0.92  | 0.96  | 1.25  | 0.80  |
| S.E.M.<br>(sec)      | 0.80    | 0.71  | 0.66  | 0.52  | 0.69  | 0.58  | 0.52  | 0.44  | 0.46  | 0.60  | 0.37  |
| T<br>(sec)           | 311.3   | 259.4 | 215.7 | 174.3 | 138.6 | 108.5 | 82.0  | 59.7  | 40.6  | 25.5  | 14.0  |
| ∆<br>(deg)           | 30.00   | 35.00 | 40.00 | 45.00 | 50.00 | 55.00 | 60.00 | 65.00 | 70.00 | 75.00 | 80,00 |
| Phase<br>combination | ScS - S | deep  | focus | e.    |       |       |       |       |       |       |       |

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| Phase    | Fit of<br>∆<br>(deg) | the mode<br>J.B.<br>(sec) | ls to absolute<br>'68 Tables<br>(sec) | travel ti<br>Al<br>(sec) | me data<br>Bl<br>(sec) | B2<br>(sec)    |
|----------|----------------------|---------------------------|---------------------------------------|--------------------------|------------------------|----------------|
| Р        | 30                   | 372.5                     | 369.5                                 | 370.5                    | 370.9                  | 370.6          |
| (surface | 35                   | 416.1                     | 413.3                                 | 414.5                    | 414.4                  | 414.2          |
| focus)   | 40                   | 458.1                     | 455.7                                 | 456.8                    | 456.5                  | 456.4          |
|          | 45                   | 498.9                     | 497.4                                 | 497.3                    | 497.0                  | 496.8          |
|          | 50                   | 538.0                     | 535.2                                 | 536.0                    | 535.6                  | 535.5          |
|          | 55                   | 575.4                     | 572.2                                 | 573.0                    | 572.6                  | 572.5          |
|          | 60                   | 610.7                     | 607.4                                 | 608.3                    | 608.0                  | 607.7          |
|          | 65                   | 644.0                     | 640.9                                 | 642.0                    | 641.7                  | 641.4          |
|          | 70                   | 675.4                     | 672.7                                 | 673.7                    | 673.6                  | 673.2          |
|          | 75                   | 705.0                     | 702.6                                 | 703.5                    | 703.5                  | 703.1          |
|          | 80                   | 732.7                     | 730.6                                 | 731.4                    | 731.5                  | 731.0          |
|          | 85                   | 758.5                     | 756.6                                 | 757.4                    | 757.4                  | 756.9          |
|          | 90                   | 782.7                     | 780.7                                 | 781.7                    | 781.5                  | 781.1          |
|          | 95                   | 805.7                     | 803.9                                 | 804.9                    | 804.6                  | 804.2          |
| PcP      | 30                   | 554.9                     | 552.1                                 | 552.1                    | 551.9                  | 551.7          |
| (surface | 35                   | 568.6                     | 565.9                                 | 565.9                    | 565.7                  | 565.5          |
| focus)   | 40                   | 583.9                     | 581.1                                 | 581.2                    | 581.0                  | 580.8          |
|          |                      | 600.5                     |                                       |                          | 597.7                  | 597.5          |
|          | 45<br>50             | 618.3                     | 597.7<br>615.5                        | 597.9<br>615.8           | 615.6                  | 615.4          |
|          | 55                   | 637.0                     | 634.3                                 | 634.6                    | 634.4                  | 634.3          |
|          | 60                   |                           |                                       |                          | 654.1                  | 654.0          |
|          |                      | 656.6                     | 653.9                                 | 654.3                    | 674.5                  | 674.4          |
| *        | 65                   | 676.9                     | 674.2                                 | 674.7                    |                        |                |
|          | 70<br>75             | 697.8                     | 695.1<br>716.5                        | 695.7<br>717.1           | 695.5<br>716.9         | 695.3<br>716.7 |
|          | 80                   | 719.1                     | 716.5                                 | 738.8                    |                        |                |
|          | 85                   | 740.6                     | 738.0                                 |                          | 738.5                  | 738.5          |
|          |                      | 762.3                     | 759.9                                 | 760.8                    | 760.5                  | 760.5          |
|          | 90                   | 784.2                     | 781.9                                 | 782.9                    | 782.7                  | 782.7          |

Table A3.6

| Table | A3.6 | (cont.) |
|-------|------|---------|
|       |      | (d) /01 |

| Phase              | ∆<br>(deg)   | J.B.<br>(sec) | '68 Tables<br>(sec) | Al<br>(sec) | Bl<br>(sec) | B2<br>(sec) |  |
|--------------------|--------------|---------------|---------------------|-------------|-------------|-------------|--|
| PKP<br>(surface    | 180 A<br>170 | 1330.6        | 1327.8<br>1283.7    | -           | -           | 1328.5      |  |
| focus)             |              |               |                     |             |             | 1239.3      |  |
|                    | 160          | 1242.7        | 1239.7              | 1239.9      | 1239.3      | 1196.6      |  |
|                    | 150          | 1200.2        | 1196.9              | 1197.3      | 1196.8      |             |  |
|                    | 145 B        | 1180.4        | 1178.0              | 1178.0      | 1177.4      | 1177.3      |  |
|                    |              |               |                     |             |             |             |  |
|                    | 145 B        | 1179.3        | 1174.4              | 1178.0      | 1177.4      | 1177.3      |  |
|                    | 150          | 1190.7        | 1188.1              | 1192.7      | 1191.8      | 1192.0      |  |
|                    | 155 C        | 1201.7        | 1201.0              | 1205.3      | 1204.3      | 1204.6      |  |
|                    |              |               |                     |             |             |             |  |
|                    | 110 D        | 1113.2        | 1113.0              | 1114.8      | 1114.0      | 1114.9      |  |
|                    | 120          | 1132.7        | 1132.1              | 1133.6      | 1132.7      | 1133.0      |  |
|                    | 130          | 1152.0        | 1151.3              | 1152.3      | 1151.4      | 1151.8      |  |
|                    | 140          | 1170.5        | 1170.1              | 1170.4      | 1169.5      | 1170.0      |  |
|                    | 150          | 1187.4        | 1186.8              | 1187.2      | 1186.2      | 1186.8      |  |
|                    | 160          | 1200.8        | 1200.0              | 1200.9      | 1200.0      | 1200.4      |  |
|                    | 170.         | 1209.2        | 1208.4              | 1209.8      | 1208.9      | 1209.3      |  |
|                    | 180 F        | 1212.2        | 1211.0              | 1212.9      | 1212.1      | 1212.4      |  |
|                    | X            |               |                     |             |             |             |  |
|                    |              |               | *                   |             |             |             |  |
| PKiKP              | 10           |               | 996.9*              | 996.9       | 996.2       | 996.3       |  |
| (surface<br>focus) | 20           |               | 1000.1              | 1000.3      | 999.6       | 999.6       |  |
|                    | 30           |               | 1005.7              | 1005.8      | 1005.1      | 1005.1      |  |
|                    | 40           |               | 1013.2              | 1013.4      | 1012.7      | 1012.8      |  |
|                    | 50           |               | 1022.8              | 1023.0      | 1022.3      | 1022.4      |  |
|                    |              |               |                     |             |             |             |  |

\* Data for PKiKP from Engdahl et.al. [1970, Table 1].

Table A3.6 (cont.)

| Phase              | ∆<br>(deg) | J.B.<br>(sec) | H&R [1970a]<br>(sec) | Al<br>(sec) | Bl<br>(sec) | B2<br>(sec) |
|--------------------|------------|---------------|----------------------|-------------|-------------|-------------|
| S                  | 30         | 670.2         | 669.5                | 672.0       | 675.0       | 671.7       |
| (surface<br>focus) | 35         | 748.2         | 749.0                | 751.5       | 752.8       | 751.9       |
| 10000)             | 40         | 824.5         | 825.7                | 829.5       | 828.8       | 828.6       |
|                    | 45         | 897.9         | 899.5                | 704.2       | 902.5       | 903.1       |
|                    | 50         | 968.6         | 970.5                | 975.9       | 973.9       | 974.6       |
|                    | 55         | 1036.8        | 1038.7               | 1044.4      | 1043.2      | 1043.8      |
|                    | 60         | 1102.6        | 1104.1               | 1109.7      | 1109.2      | 1109.6      |
|                    | 65         | 1165.5        | 1166.7               | 1172.4      | 1172.5      | 1172.9      |
|                    | 70         | 1225.6        | 1226.4               | 1233.1      | 1233.2      | 1233.7      |
|                    | 75         | 1282.6        | 1283.2               | 1290.4      | 1290.6      | 1291.1      |
|                    | 80         | 1336.5        | 1337.3               | 1344.9      | 1344.8      | 1345.3      |
|                    | 85         | 1387.3        | 1388.5               | 1395.8      | 1395.7      | 1395.5      |
|                    | 90         | 1435.5        | 1436.9               | 1444.2      | 1443.7      | 1442.0      |
|                    | 95         | 1478.2        | 1482.4               | 1489.1      | 1488.6      | 1490.6      |
|                    |            |               |                      |             |             |             |
| ScS                | 30         | 1011.0        |                      | 1016.6      | 1016.4      | 1016.7      |
| (surface<br>focus) | 35         | 1036.4        |                      | 1042.2      | 1042.0      | 1042.4      |
|                    | 40         | 1064.6        |                      | 1070.6      | 1070.5      | 1070.8      |
|                    | 45         | 1095.1        |                      | 1101.7      | 1101.5      | 1101.9      |
|                    | 50         | 1127.8        |                      | 1135.1      | 1134.8      | 1135.2      |
|                    | 55         | 1162.5        |                      | 1170.2      | 1169.9      | 1170.3      |
|                    | 60         | 1198.8        |                      | 1207.0      | 1206.6      | 1207.1      |
|                    | 65         | 1236.4        |                      | 1245.1      | 1244.7      | 1245.2      |
|                    | 70         | 1275.2        |                      | 1284.2      | 1283.9      | 1284.5      |
|                    | 75         | 1315.0        |                      | 1324.2      | 1323.9      | 1324.5      |
|                    | 80         | 1355.5        |                      | 1364.9      | 1364.6      | 1365.4      |
|                    | 85         | 1396.5        |                      | 1406.3      | 1405.8      | 1406.8      |
|                    | 90         | 1437.8        |                      | 1447.9      | 1447.3      | 1448.5      |
|                    | 95         | 1479.2        | ,                    | 1489.5      | 1489.0      | 1490.6      |

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## Table A3.7

| Fit of                      | the models to | auxillary d  | ifferential | travel time | data        |
|-----------------------------|---------------|--------------|-------------|-------------|-------------|
| Phase<br>Combination        | ∆<br>(deg)    | H&R<br>(sec) | Al<br>(sec) | Bl<br>(sec) | B2<br>(sec) |
|                             |               | *            |             |             |             |
| SKKS-SKS                    | 85            | 8.2          | 6.4         | 6.4         | 6.3         |
| (surface<br>focus)          | 90            | 15.4         | 13.4        | 13.4        | 13.2        |
| and the second second get   | 95            | 23.9         | 23.0        | 22.8        | 22.7        |
|                             | 100           | 33.9         | 34.1        | 33.9        | 33.9        |
|                             | 105           | 45.2         | 46.7        | 46.2        | 46.1        |
|                             | 110           | 57.9         | 59.8        | 59.4        | 59.3        |
|                             | 115           | 72.0         | 73.9        | 73.5        | 73.6        |
|                             | 120           | 87.6         | 88.8        | 88.5        | 88.6        |
|                             | 125           | 104.8        | 104.7       | 104.5       | 104.2       |
|                             |               |              |             |             |             |
| SKS-S<br>(surface<br>focus) | 85            | 6.4          | 6.4         | 7.0         | 6.3         |
|                             | 90            | 22.0         | 24.8        | 24.9        | 22.7        |
|                             | 95            | 39.4         | 42.5        | 42.6        | 44.1        |
|                             |               |              |             |             |             |

\* SKKS-SKS data from Hales and Roberts [1971, Eqn.3].

<sup>†</sup> SKS-S data from Hales and Roberts [1970a, Table 4].