## APPENDIX A

X-ray Crystallographic Data for:
4,4-Difluoro-3-(trifluoromethyl)-tricyclo[4.2.1.0 $0^{2,5}$ ]non-7-ene-3-carboxylic acid (2.10)

## X-ray Experimental for Compound 2.10:

The crystal was cut from a larger crystal and had approximate dimensions: $0.48 \times 0.24 \times 0.19$ mm . The data were collected on a Nonius Kappa CCD diffractometer using a graphite monochromator with $\mathrm{MoK} \alpha$ radiation $(\lambda=0.71073 \AA$ ). A total of 347 frames of data were collected using $\omega$-scans with a scan range of $1^{\circ}$ and a counting time of 39 seconds per frame. The data were collected at $-120^{\circ} \mathrm{C}$ using an Oxford Cryostream low temperature device. Details of crystal data, data collection, and structure refinement are listed in Table 1. Data reduction were performed using DENZO-SMN. ${ }^{1}$ The structure was solved by direct methods using SIR92 ${ }^{2}$ and refined by full-matrix least-squares on $\mathrm{F}^{2}$ with anisotropic displacement parameters for the non- H atoms using SHELXL-97. ${ }^{3}$ The hydrogen atom positions were located in a $\Delta \mathrm{F}$ and refined with isotropic displacement parameters. The function, $\mathrm{\Sigma w}\left(\left|\mathrm{~F}_{0}\right|^{2}-\left|\mathrm{F}_{\mathrm{c}}\right|^{2}\right)^{2}$, was minimized, where $\mathrm{w}=$ $1 /\left[\left(\sigma\left(\mathrm{F}_{0}\right)\right)^{2}+\left(0.0455^{*} \mathrm{P}\right)^{2}+\left(0.4828^{*} \mathrm{P}\right)\right]$ and $\mathrm{P}=\left(\left|\mathrm{F}_{0}\right|^{2}+2\left|\mathrm{~F}_{\mathrm{c}}\right|^{2}\right) / 3 . \mathrm{R}_{\mathrm{w}}\left(\mathrm{F}^{2}\right)$ refined to 0.102 , with $\mathrm{R}(\mathrm{F})$ equal to 0.0455 and a goodness of fit, $\mathrm{S}=0.998$. Definitions used for calculating $\mathrm{R}(\mathrm{F})$, $\mathrm{R}_{\mathrm{w}}\left(\mathrm{F}^{2}\right)$, and the goodness of fit, S , are given below. ${ }^{4}$ The data were corrected for secondary extinction effects. The correction takes the form: $\mathrm{F}_{\text {corr }}=\mathrm{kF}_{\mathrm{c}}\left[1+\left(6(4) \times 10^{-6}\right) * \mathrm{~F}_{\mathrm{c}}{ }^{2} \lambda^{3} /(\sin 2 \theta)\right]^{0.25}$ where k is the overall scale factor. Neutral atom scattering factors and values used to calculate the linear absorption coefficient are from the International Tables for X-ray Crystallography (1992). ${ }^{5}$ All figures were generated using SHELXTL/PC. ${ }^{6}$ Tables of positional and thermal parameters, bond lengths and angles, figures and lists of observed and calculated structure factors are located in Tables 1 through 6 .

## References

1) DENZO-SMN. (1997). Z. Otwinowski and W. Minor, Methods in Enzymology, 276: Macromolecular Crystallography, part A, 307-326, C. W. Carter, Jr. and R. M. Sweets, Editors, Academic Press.
2) SIR92. (1993). A program for crystal structure solution. Altomare, A., Cascarano, G., Giacovazzo, C. \& Guagliardi, A. J. Appl. Cryst. 26, 343350.
3) Sheldrick, G. M. (1994). SHELXL97. Program for the Refinement of Crystal Structures. University of Gottingen, Germany.
4) $\quad \mathrm{R}_{\mathrm{w}}\left(\mathrm{F}^{2}\right)=\left\{\Sigma \mathrm{w}\left(\left|\mathrm{F}_{\mathrm{o}}\right|^{2}-\left|\mathrm{F}_{\mathrm{c}}\right|^{2}\right)^{2 / \Sigma \mathrm{w}}\left(\mid \mathrm{F}_{\mathrm{o}}\right)^{4}\right\}^{1 / 2}$ where w is the weight given each reflection.
$\left.\mathrm{R}(\mathrm{F})=\Sigma\left(\left|\mathrm{F}_{\mathrm{o}}\right|-\left|\mathrm{F}_{\mathrm{c}}\right|\right) / \Sigma\left|\mathrm{F}_{\mathrm{o}}\right|\right\}$ for reflections with $\mathrm{F}_{\mathrm{o}}>4\left(\sigma\left(\mathrm{~F}_{\mathrm{o}}\right)\right)$.
$\mathrm{S}=\left[\Sigma \mathrm{w}\left(\left|\mathrm{F}_{\mathrm{o}}\right|^{2}-\left|\mathrm{F}_{\mathrm{c}}\right|^{2}\right)^{2 /(n-p)}\right]^{1 / 2}$, where n is the number of reflections and p is the number of refined parameters.
5) International Tables for X-ray Crystallography (1992). Vol. C, Tables 4.2.6.8 and 6.1.1.4, A. J. C. Wilson, editor, Boston: Kluwer Academic Press.
6) Sheldrick, G. M. (1994). SHELXTL/PC (Version 5.03). Siemens Analytical X-ray Instruments, Inc., Madison, Wisconsin, USA.

Table 1. Crystal data and structure refinement for 1.

Empirical formula
Formula weight
Temperature
Wavelength
Crystal system
Space group
Unit cell dimensions

Volume
Z
Density (calculated)
Absorption coefficient
F(000)
Crystal size
Theta range for data collection
Index ranges
Reflections collected
Independent reflections
Completeness to theta $=27.49^{\circ}$
Absorption correction
Refinement method
Data / restraints / parameters
Goodness-of-fit on $\mathrm{F}^{2}$
Final $R$ indices [ $I>2$ sigma $(\mathrm{I})$ ]
R indices (all data)
Extinction coefficient
Largest diff. peak and hole

C11 H9 F5 O2
268.18

153(2) K
0.71073 A

Monoclinic
P21/n
$a=6.7504(2) \dot{A} \quad \alpha=90^{\circ}$.
$\mathrm{b}=19.0686(5) \dot{\mathrm{A}} \quad \beta=110.485(2)^{\circ}$.
$\mathrm{c}=8.9486(2) \dot{\AA} \quad \gamma=90^{\circ}$.
1079.03(5) $\AA^{3}$

4
$1.651 \mathrm{Mg} / \mathrm{m}^{3}$
$0.169 \mathrm{~mm}^{-1}$
544
$0.48 \times 0.24 \times 0.19 \mathrm{~mm}$
3.29 to $27.49^{\circ}$.
$-8<=\mathrm{h}<=8,-22<=\mathrm{k}<=24,-11<=1<=11$
4338
$2414[\mathrm{R}($ int $)=0.0188]$
97.6 \%

None
Full-matrix least-squares on $\mathrm{F}^{2}$
2414 / 0 / 200
0.998
$R 1=0.0392, w R 2=0.0915$
$R 1=0.0585, w R 2=0.1016$
$6(4) \times 10 \times 10^{6}$
0.382 and -0.251 e. $\AA^{-3}$

Structure 1. View of $\mathbf{2 . 1 0}$ showing the atom labeling scheme. Thermal ellipsoids are scaled to the $30 \%$ probability level. Hydrogen atoms are drawn to an arbitrary size.


Structure 2. View of the H -bound dimers formed by $\mathbf{2 . 1 0}$. The dimer lies around a crystallographic inversion center at $0,1 / 2,1 / 2$. The geometry of the interaction is: O13H13 $\cdots$. O12 (related by -x, 1-y, 1-z), O $\cdots$ O 2.697(2) $\AA, \mathrm{H} \cdots \mathrm{O} 1.85(3) \AA$, O-H $\cdots \mathrm{O}$ $174(2)^{\circ}$. Thermal ellipsoids are scaled to the $30 \%$ probability level. Hydrogen atoms are drawn to an arbitrary size.


Table 2. Atomic coordinates ( $\times 10^{4}$ ) and equivalent isotropic displacement parameters ( $\AA^{2} \times 10^{3}$ ) for $1 . U(e q)$ is defined as one third of the trace of the orthogonalized $U^{i j}$ tensor.

|  | x | y | z | $\mathrm{U}(\mathrm{eq})$ |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| $\mathrm{C}(1)$ | $2305(2)$ | $3607(1)$ | $3784(2)$ | $23(1)$ |
| $\mathrm{C}(2)$ | $4730(2)$ | $3586(1)$ | $4102(2)$ | $26(1)$ |
| $\mathrm{C}(3)$ | $4345(3)$ | $3470(1)$ | $2335(2)$ | $28(1)$ |
| $\mathrm{C}(4)$ | $4800(3)$ | $4081(1)$ | $1362(2)$ | $32(1)$ |
| $\mathrm{C}(5)$ | $3661(3)$ | $3859(1)$ | $-365(2)$ | $38(1)$ |
| $\mathrm{C}(6)$ | $1613(3)$ | $3916(1)$ | $-667(2)$ | $38(1)$ |
| $\mathrm{C}(7)$ | $1299(3)$ | $4179(1)$ | $847(2)$ | $30(1)$ |
| $\mathrm{C}(8)$ | $1891(3)$ | $3531(1)$ | $1956(2)$ | $26(1)$ |
| $\mathrm{C}(9)$ | $3263(3)$ | $4642(1)$ | $1510(2)$ | $33(1)$ |
| $\mathrm{C}(10)$ | $1379(2)$ | $4246(1)$ | $4334(2)$ | $24(1)$ |
| $\mathrm{C}(11)$ | $1523(3)$ | $2961(1)$ | $4411(2)$ | $31(1)$ |
| $\mathrm{O}(12)$ | $-191(2)$ | $4541(1)$ | $3460(1)$ | $33(1)$ |
| $\mathrm{O}(13)$ | $2395(2)$ | $4413(1)$ | $5826(1)$ | $32(1)$ |
| $\mathrm{F}(14)$ | $-595(2)$ | $2961(1)$ | $3925(1)$ | $42(1)$ |
| $\mathrm{F}(15)$ | $2237(2)$ | $2922(1)$ | $6001(1)$ | $44(1)$ |
| $\mathrm{F}(16)$ | $2084(2)$ | $2362(1)$ | $3878(1)$ | $41(1)$ |
| $\mathrm{F}(17)$ | $5809(1)$ | $4172(1)$ | $4781(1)$ | $33(1)$ |
| $\mathrm{F}(18)$ | $5764(2)$ | $3050(1)$ | $5069(1)$ | $37(1)$ |
|  |  |  |  |  |
|  |  |  |  |  |

Table 3. Bond lengths $[\dot{A}]$ and angles $\left[{ }^{\circ}\right]$ for 1.

| $\mathrm{C}(1)-\mathrm{C}(11)$ | 1.523(2) | $\mathrm{C}(6)-\mathrm{C}(7)$ | 1.527(3) |
| :---: | :---: | :---: | :---: |
| $\mathrm{C}(1)-\mathrm{C}(10)$ | 1.526(2) | $\mathrm{C}(6)-\mathrm{H}(6)$ | 1.01(2) |
| $\mathrm{C}(1)-\mathrm{C}(2)$ | $1.561(2)$ | C(7)-C(9) | 1.529(3) |
| $\mathrm{C}(1)-\mathrm{C}(8)$ | 1.567(2) | $\mathrm{C}(7)-\mathrm{C}(8)$ | 1.548(2) |
| C(2)-F(17) | $1.3563(19)$ | $\mathrm{C}(7)-\mathrm{H}(7)$ | 0.95(2) |
| $\mathrm{C}(2)-\mathrm{F}(18)$ | 1.3632(18) | $\mathrm{C}(8)-\mathrm{H}(8)$ | 0.981(19) |
| $\mathrm{C}(2)-\mathrm{C}(3)$ | 1.526(2) | $\mathrm{C}(9)-\mathrm{H}(9 \mathrm{~A})$ | 0.98(2) |
| $\mathrm{C}(3)-\mathrm{C}(4)$ | 1.549(2) | $\mathrm{C}(9)-\mathrm{H}(9 \mathrm{~B})$ | 1.00(2) |
| $\mathrm{C}(3)-\mathrm{C}(8)$ | 1.574(2) | $\mathrm{C}(10)-\mathrm{O}(12)$ | $1.2125(19)$ |
| $\mathrm{C}(3)-\mathrm{H}(3)$ | 0.96(2) | $\mathrm{C}(10)-\mathrm{O}(13)$ | 1.3094(19) |
| $\mathrm{C}(4)-\mathrm{C}(5)$ | 1.525(3) | $\mathrm{C}(11)-\mathrm{F}(15)$ | $1.335(2)$ |
| $\mathrm{C}(4)-\mathrm{C}(9)$ | 1.529(3) | $\mathrm{C}(11)-\mathrm{F}(14)$ | $1.341(2)$ |
| $\mathrm{C}(4)-\mathrm{H}(4)$ | 0.988(19) | $\mathrm{C}(11)-\mathrm{F}(16)$ | $1.341(2)$ |
| $\mathrm{C}(5)-\mathrm{C}(6)$ | 1.317(3) | $\mathrm{O}(13)-\mathrm{H}(13)$ | 0.85(3) |
| $\mathrm{C}(5)-\mathrm{H}(5)$ | 1.03(2) | - |  |
| $\mathrm{C}(11)-\mathrm{C}(1)-\mathrm{C}(10)$ | 107.03(13) | $\mathrm{C}(5)-\mathrm{C}(4)-\mathrm{C}(9)$ | 99.51(14) |
| $\mathrm{C}(11)-\mathrm{C}(1)-\mathrm{C}(2)$ | 112.84(13) | $\mathrm{C}(5)-\mathrm{C}(4)-\mathrm{C}(3)$ | 103.46(15) |
| $\mathrm{C}(10)-\mathrm{C}(1)-\mathrm{C}(2)$ | 118.94(13) | $\mathrm{C}(9)-\mathrm{C}(4)-\mathrm{C}(3)$ | 101.77(13) |
| $\mathrm{C}(11)-\mathrm{C}(1)-\mathrm{C}(8)$ | 110.56 (13) | $\mathrm{C}(5)-\mathrm{C}(4)-\mathrm{H}(4)$ | 118.8(11) |
| $\mathrm{C}(10)-\mathrm{C}(1)-\mathrm{C}(8)$ | 117.86(13) | $\mathrm{C}(9)-\mathrm{C}(4)-\mathrm{H}(4)$ | 118.6(12) |
| $\mathrm{C}(2)-\mathrm{C}(1)-\mathrm{C}(8)$ | 88.86(11) | $\mathrm{C}(3)-\mathrm{C}(4)-\mathrm{H}(4)$ | 112.2(11) |
| $\mathrm{F}(17)-\mathrm{C}(2)-\mathrm{F}(18)$ | 104.97(12) | $\mathrm{C}(6)-\mathrm{C}(5)-\mathrm{C}(4)$ | 107.82(16) |
| $\mathrm{F}(17)-\mathrm{C}(2)-\mathrm{C}(3)$ | 117.02(13) | $\mathrm{C}(6)-\mathrm{C}(5)-\mathrm{H}(5)$ | 127.3(13) |
| $\mathrm{F}(18)-\mathrm{C}(2)-\mathrm{C}(3)$ | $114.35(14)$ | $\mathrm{C}(4)-\mathrm{C}(5)-\mathrm{H}(5)$ | 124.3(13) |
| $\mathrm{F}(17)-\mathrm{C}(2)-\mathrm{C}(1)$ | 115.12(13) | $\mathrm{C}(5)-\mathrm{C}(6)-\mathrm{C}(7)$ | 107.84(16) |
| $\mathrm{F}(18)-\mathrm{C}(2)-\mathrm{C}(1)$ | 113.99(13) | $\mathrm{C}(5)-\mathrm{C}(6)-\mathrm{H}(6)$ | 127.9(12) |
| $\mathrm{C}(3)-\mathrm{C}(2)-\mathrm{C}(1)$ | 91.57(11) | $\mathrm{C}(7)-\mathrm{C}(6)-\mathrm{H}(6)$ | 124.0(12) |
| $\mathrm{C}(2)-\mathrm{C}(3)-\mathrm{C}(4)$ | 118.56(15) | $\mathrm{C}(6)-\mathrm{C}(7)-\mathrm{C}(9)$ | 99.42(15) |
| $\mathrm{C}(2)-\mathrm{C}(3)-\mathrm{C}(8)$ | 89.86(12) | $\mathrm{C}(6)-\mathrm{C}(7)-\mathrm{C}(8)$ | 102.78(14) |
| $\mathrm{C}(4)-\mathrm{C}(3)-\mathrm{C}(8)$ | 102.91(13) | $\mathrm{C}(9)-\mathrm{C}(7)-\mathrm{C}(8)$ | 102.60(13) |
| $\mathrm{C}(2)-\mathrm{C}(3)-\mathrm{H}(3)$ | 112.1(12) | $\mathrm{C}(6)-\mathrm{C}(7)-\mathrm{H}(7)$ | 118.1(11) |
| $\mathrm{C}(4)-\mathrm{C}(3)-\mathrm{H}(3)$ | 113.6(12) | $\mathrm{C}(9)-\mathrm{C}(7)-\mathrm{H}(7)$ | 116.6(12) |
| $\mathrm{C}(8)-\mathrm{C}(3)-\mathrm{H}(3)$ | 117.6(11) | $\mathrm{C}(8)-\mathrm{C}(7)-\mathrm{H}(7)$ | 114.9(11) |


| $\mathrm{C}(7)-\mathrm{C}(8)-\mathrm{C}(1)$ | $120.45(14)$ | $\mathrm{H}(9 \mathrm{~A})-\mathrm{C}(9)-\mathrm{H}(9 \mathrm{~B})$ | $108.6(16)$ |
| :--- | :---: | :--- | :--- |
| $\mathrm{C}(7)-\mathrm{C}(8)-\mathrm{C}(3)$ | $102.34(13)$ | $\mathrm{O}(12)-\mathrm{C}(10)-\mathrm{O}(13)$ | $124.93(15)$ |
| $\mathrm{C}(1)-\mathrm{C}(8)-\mathrm{C}(3)$ | $89.55(11)$ | $\mathrm{O}(12)-\mathrm{C}(10)-\mathrm{C}(1)$ | $121.73(14)$ |
| $\mathrm{C}(7)-\mathrm{C}(8)-\mathrm{H}(8)$ | $113.0(11)$ | $\mathrm{O}(13)-\mathrm{C}(10)-\mathrm{C}(1)$ | $113.28(14)$ |
| $\mathrm{C}(1)-\mathrm{C}(8)-\mathrm{H}(8)$ | $111.1(11)$ | $\mathrm{F}(15)-\mathrm{C}(11)-\mathrm{F}(14)$ | $106.96(13)$ |
| $\mathrm{C}(3)-\mathrm{C}(8)-\mathrm{H}(8)$ | $118.4(11)$ | $\mathrm{F}(15)-\mathrm{C}(11)-\mathrm{F}(16)$ | $106.85(14)$ |
| $\mathrm{C}(4)-\mathrm{C}(9)-\mathrm{C}(7)$ | $94.83(14)$ | $\mathrm{F}(14)-\mathrm{C}(11)-\mathrm{F}(16)$ | $106.65(14)$ |
| $\mathrm{C}(4)-\mathrm{C}(9)-\mathrm{H}(9 \mathrm{~A})$ | $114.3(11)$ | $\mathrm{F}(15)-\mathrm{C}(11)-\mathrm{C}(1)$ | $113.28(14)$ |
| $\mathrm{C}(7)-\mathrm{C}(9)-\mathrm{H}(9 \mathrm{~A})$ | $115.1(11)$ | $\mathrm{F}(14)-\mathrm{C}(11)-\mathrm{C}(1)$ | $110.38(14)$ |
| $\mathrm{C}(4)-\mathrm{C}(9)-\mathrm{H}(9 \mathrm{~B})$ | $112.7(11)$ | $\mathrm{F}(16)-\mathrm{C}(11)-\mathrm{C}(1)$ | $112.35(13)$ |
| $\mathrm{C}(7)-\mathrm{C}(9)-\mathrm{H}(9 \mathrm{~B})$ | $110.8(11)$ | $\mathrm{C}(10)-\mathrm{O}(13)-\mathrm{H}(13)$ | $106.8(16)$ |

Table 4. Anisotropic displacement parameters $\left(\dot{A}^{2} \times 10^{3}\right)$ for 1 . The anisotropic displacement factor exponent takes the form: $-2 \pi^{2}\left[h^{2} a^{* 2} U^{11}+\ldots+2 h k a^{*} b^{*} U^{12}\right]$

|  | $\mathrm{U}^{\prime 1}$ | $\mathrm{U}^{22}$ | $\mathrm{U}^{33}$ | $\mathrm{U}^{23}$ | $\mathrm{U}^{13}$ | $\mathrm{U}^{12}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{C}(1)$ | $25(1)$ | $23(1)$ | $23(1)$ | $-1(1)$ | $10(1)$ | $0(1)$ |
| $\mathrm{C}(2)$ | $25(1)$ | $28(1)$ | $26(1)$ | $3(1)$ | $9(1)$ | $2(1)$ |
| $\mathrm{C}(3)$ | $30(1)$ | $30(1)$ | $28(1)$ | $2(1)$ | $13(1)$ | $7(1)$ |
| $\mathrm{C}(4)$ | $28(1)$ | $41(1)$ | $30(1)$ | $5(1)$ | $13(1)$ | $2(1)$ |
| $\mathrm{C}(5)$ | $45(1)$ | $46(1)$ | $28(1)$ | $4(1)$ | $18(1)$ | $7(1)$ |
| $\mathrm{C}(6)$ | $41(1)$ | $48(1)$ | $24(1)$ | $2(1)$ | $11(1)$ | $3(1)$ |
| $\mathrm{C}(7)$ | $28(1)$ | $35(1)$ | $26(1)$ | $5(1)$ | $10(1)$ | $8(1)$ |
| $\mathrm{C}(8)$ | $28(1)$ | $26(1)$ | $24(1)$ | $-4(1)$ | $11(1)$ | $-3(1)$ |
| $\mathrm{C}(9)$ | $40(1)$ | $30(1)$ | $29(1)$ | $5(1)$ | $13(1)$ | $-1(1)$ |
| $\mathrm{C}(10)$ | $24(1)$ | $26(1)$ | $24(1)$ | $-2(1)$ | $11(1)$ | $-2(1)$ |
| $\mathrm{C}(11)$ | $34(1)$ | $29(1)$ | $32(1)$ | $0(1)$ | $16(1)$ | $-2(1)$ |
| $\mathrm{O}(12)$ | $28(1)$ | $39(1)$ | $28(1)$ | $-8(1)$ | $6(1)$ | $9(1)$ |
| $\mathrm{O}(13)$ | $34(1)$ | $36(1)$ | $23(1)$ | $-5(1)$ | $7(1)$ | $8(1)$ |
| $\mathrm{F}(14)$ | $35(1)$ | $43(1)$ | $54(1)$ | $-1(1)$ | $23(1)$ | $-10(1)$ |
| $\mathrm{F}(15)$ | $60(1)$ | $41(1)$ | $33(1)$ | $9(1)$ | $21(1)$ | $-4(1)$ |
| $\mathrm{F}(16)$ | $54(1)$ | $23(1)$ | $53(1)$ | $-1(1)$ | $27(1)$ | $-2(1)$ |
| $\mathrm{F}(17)$ | $27(1)$ | $39(1)$ | $30(1)$ | $-2(1)$ | $7(1)$ | $-7(1)$ |
| $\mathrm{F}(18)$ | $33(1)$ | $42(1)$ | $36(1)$ | $13(1)$ | $12(1)$ | $13(1)$ |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |

Table 5. Hydrogen coordinates ( $\times 10^{4}$ ) and isotropic displacement parameters ( $\AA^{2} \times 10^{3}$ ) for 1 .

|  | $x$ | $y$ | $z$ | $U(e q)$ |
| :--- | ---: | ---: | ---: | ---: |
|  |  |  |  |  |
| $H(3)$ | $4880(30)$ | $3027(11)$ | $2140(20)$ | $35(5)$ |
| $H(4)$ | $6320(30)$ | $4195(10)$ | $1710(20)$ | $38(5)$ |
| $H(5)$ | $4390(40)$ | $3634(12)$ | $-1080(30)$ | $55(6)$ |
| $H(6)$ | $420(30)$ | $3772(11)$ | $-1660(30)$ | $43(6)$ |
| $H(7)$ | $-20(30)$ | $4390(10)$ | $750(20)$ | $34(5)$ |
| $H(8)$ | $1000(30)$ | $3121(10)$ | $1510(20)$ | $30(5)$ |
| $H(9 A)$ | $3560(30)$ | $4814(10)$ | $2600(20)$ | $37(5)$ |
| $H(9 B)$ | $3170(30)$ | $5056(11)$ | $800(20)$ | $40(5)$ |
| $H(13)$ | $1750(40)$ | $4764(14)$ | $6040(30)$ | $63(7)$ |

