# $\pi^+$ Photoproduction at angles from 50° to 165° c.m. and energies from 500 to 1350 MeV

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#### ABSTRACT

The cross section for the reaction  $\gamma + p \rightarrow \pi^+ + n$  was measured at the Caltech synchrotron. The  $\pi^+$  was detected in a multi-channel magnetic spectrometer, and the data were recorded in the memory of a pulse height analyzer. The results are presented in the form of energy distributions at 12 fixed laboratory angles from  $34^{\circ}$  to  $155^{\circ}$ . 378 cross section measurements are reported with photon energies between 500 MeV and 1350 MeV. No detailed fitting of the entire angular range was attempted; however, a narrow bump in the cross section at  $180^{\circ}$  is explained as the effect of a cusp at the eta meson threshold.

To Challis

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#### L INTRODUCTION

There is presently a considerable theoretical interest in photoproduction data. Several authors have used the data for evaluating sum rules. (1,2,3) For these purposes, a multipole and isotopic spin decomposition of the photoproduction amplitudes is desired. Similar decompositions are already available for the pion scattering data. (4, 5, 6, 7, 8) This experiment was designed to collect a large number of points of the cross section for  $y + p \rightarrow \pi^+ + n$  with sufficient resolution to extract the energy dependence of the cross section. When the data of this experiment are combined with the data of Ecklund and Walker, (9) a consistent set of cross sections is available for angles between 6° and 165° c.m. and photon energies between 589 MeV and 1269 MeV, with some additional data available between 500 and 1350 MeV. In particular, this experiment covered the angular range from  $50^{\circ}$  to  $165^{\circ}$  c.m. for the entire range of energies (see Section V-C for further details). These data are being combined with data from the other single pion photoproduction reactions and an attempt is being made to determine the decomposition of the photoproduction amplitudes. (10) However, it appears likely that much more data will be required on the polarization and the cross section in the other channels before a unique decomposition can be made for energies greater than 800 MeV.

A second important consideration in the design of this experiment was to set up a spectrometer which can be used simultaneously with the already existing High Energy Magnet. A 600 MeV/c spectrometer was constructed by modifying the former Low Energy Magnet, then the spectrometer was carefully calibrated and instrumented with several general purpose counters. This spectrometer is available

as a laboratory instrument, and an experiment is now in progress which uses both magnets simultaneously. (11)

Since this experiment and the experiment of Ecklund and Walker were done at approximately the same time, a considerable amount of work was saved by avoiding a duplication of effort. Thus the same computer programs were used in the data reduction of both experiments. In general, this author did most of the programming for magnet resolution, etc., while Stan Ecklund did the evaluation of the cross section integrals and a large amount of data fitting. In practice, a strict division of the work was not always possible, and many parts of this thesis are very similar to his thesis.

#### II. EXPERIMENTAL METHOD, GENERAL

The reaction  $\gamma + p - \pi^+ + n$  was studied at the Caltech 1.5 GeV Electron Synchrotron. The experimental method was very similar to that which was used in several past experiments (12, 13, 14, 15, 16, 17), namely, the photon beam irradiated a liquid hydrogen target and the positive pions produced were detected and momentum analyzed in a magnetic spectrometer.

The kinematics of the reaction relate the observed quantities,  $P_{\pi lab}$ ,  $\theta_{\pi lab}$ , to desired quantities, k,  $\theta_{\pi CM}$  (where k is the photon lab energy) under the assumption that only one pion was produced. If two or more pions are produced, as in the reactions,

$$\gamma + p \rightarrow \pi^{+} + n + \pi^{0}$$

$$\rightarrow \pi^{+} + p + \pi^{-}$$

$$\rightarrow \pi^{+} + N + (n\pi) \dots$$

then there will be a minimum photon energy,  $k_{2\pi}$ , required to produce a  $\pi^+$  with the observed angle and momentum. In general,  $k_{2\pi}$  will be greater than k. In the energy region of this experiment, it is possible to choose  $E_0$ , the maximum energy of the photon spectrum, to lie between k and  $k_{2\pi}$  so that the multiple pion reaction will not be observed.

The background of particles incident on the spectrometer includes protons, electrons, and muons. Protons are eliminated by velocity selection in a lucite Cerenkov counter, crude time-of-flight requirements, and dE/dx selection in two scintillation counters.

Electrons and muons are indistinguishable from pions in the electronics. This experiment relies on the fact that previous experiments have shown that electron contamination at large angles from the photon beam is small; several checks with magnet field reversed have been made to look for this kind of contamination. The major source of muons is the decay of the  $\pi^+$ ,  $\pi^+ \rightarrow \mu^+ + \nu$ , since typically 20% of the pions decay while passing through the spectrometer. Muon pair production,  $\gamma + p \rightarrow \mu^+ + \mu^- + p$ , is usually eliminated by the same kinematical requirement that eliminates pion pair production. In addition, the cross section for muon pair production should be down by a factor

 $e^4 = (\frac{1}{137})^2$  from pion pair production. Thus this source of events can be safely ignored.

The spectrometer, the 600 MeV/c Magnet, differs from those used in the earlier work in that it collects data in several momentum channels simultaneously. Because the kinematic transformation between lab and center-of-mass co-ordinate systems varies rapidly with  $p_{\Pi}$  and  $\theta_{\Pi lab}$ , it was not feasible to measure angular distributions at fixed values of k. Instead, the data were taken as energy scans at fixed lab angle. Several spectrometer momentum settings were required for each scan and an appropriate value of  $E_{0}$  was chosen for each spectrometer setting. Angular distributions were obtained by linear interpolation in the measured data.

The data were taken during two separate periods, May - August 1965, and December 1965 - March 1966. Each point was measured at least once during each period, and checks were made for consistency between runs.

#### III. APPARATUS

## A. The Photon Beam, Liquid Hydrogen Target, and Beam Monitoring Equipment

The photon beam was generated by bremsstrahlung in a 0.2 radiation length tantalum radiator in the Caltech 1.5 GeV Electron Synchrotron. At energies greater than 0.91 GeV, the synchrotron produced a nearly uniform 100 msec, beam spill once per second. For energies less than 0.91 GeV, it was possible to run the synchrotron twice per second with a beam spill time of 50 msec. At the lowest energy used in this experiment, 0.66 GeV, it was extremely difficult to obtain a uniform beam spill. The cause of this difficulty was not fully understood, but it is believed that the radio frequency control system was sensitive to noise from many sources when operated at the very low power levels required to make a uniform dump at this energy. The result of this difficulty was a large spike superimposed upon the normal spill. This spike, which was of about 200 µsec duration, contained on the order of 5% of the total energy of the dump. During the first data-taking period, this problem was eliminated by careful tuning, but during the second period it was not possible to eliminate this effect. Since an accidentals monitoring system was used continuously during the experiment, the 660 MeV points were repeated with this poor spill.

The liquid hydrogen target is the same one that has been used by the magnet group for all experiments since that of J. Boyden. (18) The liquid hydrogen is contained in a long 3 inch diameter cylinder ("appendix") with 0.005 inch mylar walls. The axis of this cylinder is perpendicular to the beam line and is coincident

with the axis of rotation of the spectrometer. The beam line was adjusted to intersect the axis of the cylinder and the beam was collimated to a rectangular cross section 1 1/2 inch horizontal by 1 3/4 inch vertical. Because it has been observed that after long use "ice" builds up on the walls of the appendix (19), the target was disassembled and cleaned at approximately monthly intervals. In addition, empty target runs were usually taken within a week of full target runs, so that a gradual accumulation of "ice" would be corrected by the empty target subtraction.

The beam area layout during the first data-taking period is shown in Figure 1. For the second data-taking period, the quantameter was relocated on the scraping wall immediately upstream of the hydrogen target. Otherwise, the setup was unchanged between the two data-taking periods.

Figure 1 shows the High Energy Magnet at an angle for which the beam line intercepted the magnet yoke. During the running period of this experiment, Mr. F. Wolverton was setting up another experiment to detect protons at small angles from the photon beam with the High Energy Magnet. Occasionally, Mr. Wolverton needed to make a test with the High Energy Magnet in the beam line. Under these circumstances, a careful check of the consistency of data taken with the High Energy Magnet in the beam line and data taken under normal circumstances showed no significant difference.

The beam monitoring equipment consisted of several different instruments which were used at various times during the run. The primary standard was a Wilson type quantameter. (20) An absolute calibration of this instrument against a Faraday Cup was made at the Stanford Mark III Linear Accelerator on 2 May, 1966.

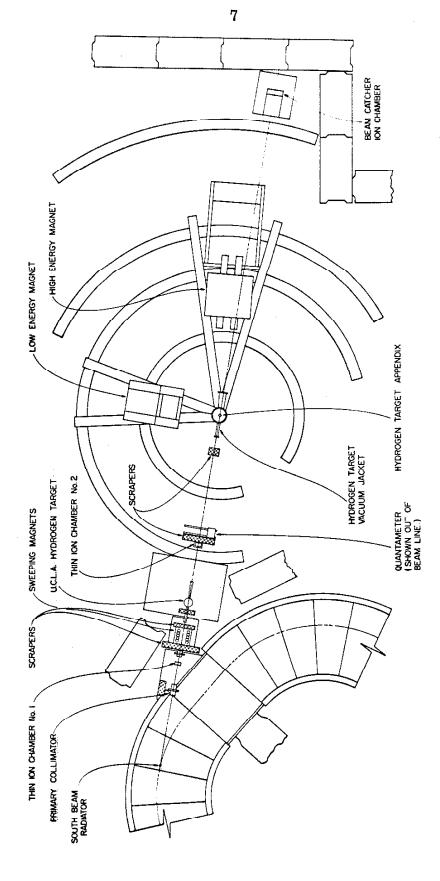


Figure 1. Beam Area Layout

This calibration differed from the previous absolute calibrations and the theoretical value by less than 1.5%. (21)

The secondary monitors consisted of two very thin ion chambers located upstream of the hydrogen target, a thick ion chamber located in the beam catcher, a 2-counter telescope which monitored particles produced at 90° from the hydrogen target, and a radio frequency monitor of the circulating beam which is commonly called the "40 mc. probe". The uses of these secondary monitors are described in Appendix I.

#### B. Magnetic Spectrometer and Counters

The magnetic spectrometer used for this experiment, designated the 600 MeV/c Magnet, was constructed by modifying the former Low Energy Magnet. The magnet is of the wedge-shaped, uniform field type and is very similar in design to the magnets which have been used by Professor R. L. Walker and his students for many years. An elevation view of the spectrometer is shown in Figure 2.

The calibration of the spectrometer is the subject of a separate report (22), and only a few important results will be summarized here. The solid angle of the spectrometer is 3.3 × 10<sup>-3</sup> sr. and the total momentum acceptance is 10.3%. The momentum interval is divided into seven smaller channels. With the beam size typically used in this experiment (1.5 inch horizontal by 1.8 inch vertical) the r.m.s. momentum resolution obtained is 1.10%, when no scattering or other similar resolution degrading effects are included. (Note that the full width at half maximum is 2.2 times the r.m.s. width for a Gaussian resolution function). A graph of these basic resolution functions is presented as Figure 3.

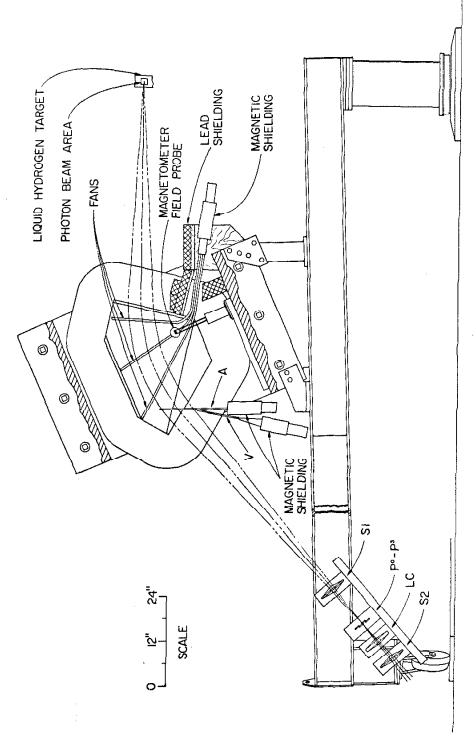
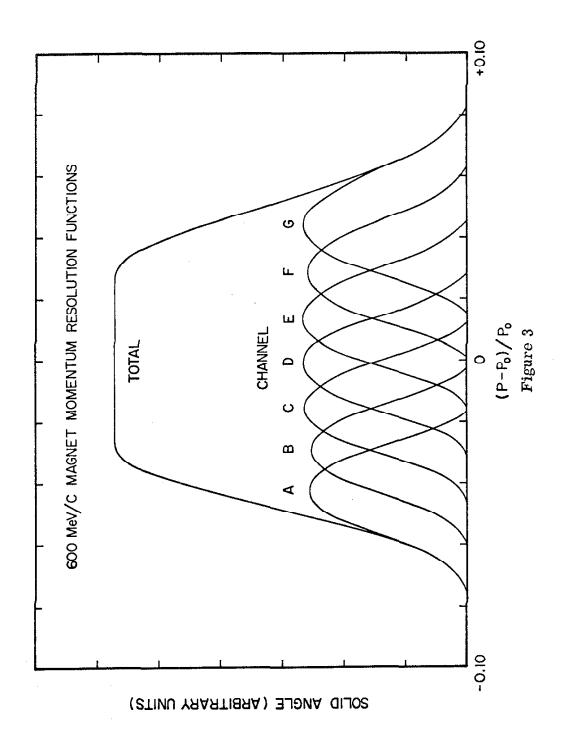


Figure 2. 500 MeV/c Magnet and Counters



A graphic display of the results of the magnet calibration measurements is presented in Figure 4. In this drawing, a contour map of the magnetic field is superimposed on a drawing of the pole tip structure. Three particle trajectories calculated by the ray tracing program (23) are shown. In addition, the effective edges (for a model with uniform field and zero fringe fields) computed by the same ray tracing program are shown. The accuracy of  $\Delta\Omega$   $\Delta P/P$  calculated from ray traces is expected to be  $\pm$  1% when a small correction for the variation with central field is included. (22)

The uniform field of the spectrometer is monitored with a nuclear resonance magnetometer. The central momentum of the spectrometer has been calibrated against the magnetometer by floating wire techniques. This calibration has an absolute accuracy of  $\pm$  0.2% for a fixed location of the beam centroid. Because the beam centroid seems to wander slowly for fixed synchrotron energy, and because there is a systematic movement of the beam centroid with the synchrotron energy, the total error in the momentum calibration is taken to be  $\pm$  0.5%. The counters used with the 600 MeV/c Magnet are very similar in design and function to those which are in use on the High Energy Magnet. (9) The location of the counters is shown on Figure 3. The physical characteristics and use of each counter are given in Table 1.

The fan counters were designed so that no charged particle originating in the hydrogen target can undergo a single scattering from the pole tips and be counted in S2 without also being counted by one of the arms of the fan counters. In retrospect, it might have been useful to strengthen the specifications to include provision for vetoing neutrals which convert in the pole tips. The fan counters of the present design veto all events generated in the

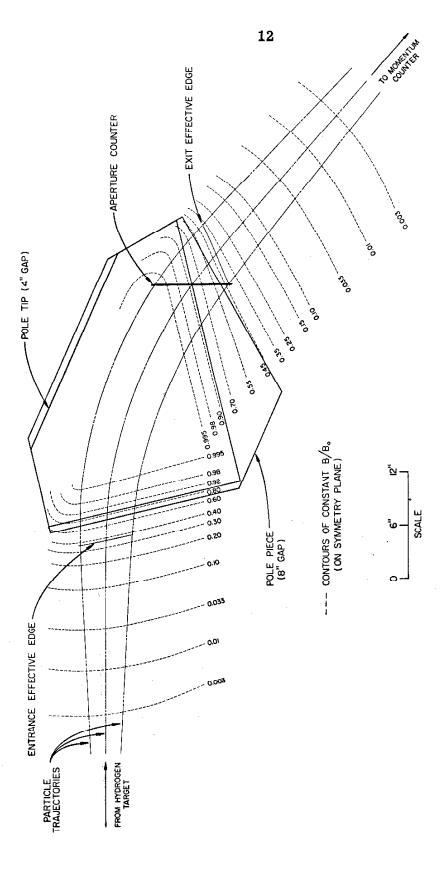


Figure 4, 600 MeV/C MAGNET OPTICS AT 10 KILOGAUSS

TABLE 1. Characteristics of 600 MeV/c Magnet Counters

	Comments	Particles pass through at 42°. Ends cut at 45°. Defines solid angle of spectrometer. Mounted on long, thin lucite light pipe.	Used for particle definition and rejection of protons by dE/dx.	Defines momentum (see EFigure 5).	Cerenkov counter which rejects particles with velocity less than $\sim 0.8$ c.	Time-of-flight (A·S2) and dE/dx rejection of protons.	Veto scattering from pole faces.	Veto events with particle passing through light pipe of A.
	Phototube	I-6810A	2-6655A	6655A	2-6810A	2-6655A	2-6810A	6655A
	$\mathbf{Typc}$	NE 102 Scintillator	NE 102 Scintillator	NE 102 Scintillator	UVT Lucite	NE 102 Scintillator	NE 102 Scintillator	NE 102 Scintillator
Mass (including) wrapping)	$gm/cm^2$	0.54	0.74	" 1, 08	2.84	0.74	not in normal path	not in normal path
() Dimension		<b>2.</b> 75 $\times$ 9, 50 $\times$ 0, 125	7. $50 \times 15$ , $00 \times 0$ , $250$	"0, 75 $\times$ 15, 00 $\times$ 0, 375" 1, 08	7. $50 \times 15$ , $00 \times 1$ , $00$	7.50 $\times$ 15.00 $\times$ 0.250	$3-1/2 \times 1/2$ rods bent as shown in Figure 2.	$8.00 \times 12.00 \times 0.250$
	Counter	<b>4</b>	SI	Average P Channel	IC	S2	Fans	>

TABLE 2. Properties of Momentum Channels of 600 MeV/c Magnet

Channel	Width (inches)	$(\overline{P}-P_0)/P_0 \times 10^2$	ΔΩ ΔΡ/Ρ <sub>ο</sub> × 10 <sup>5</sup>	Logical Definition
A	0.759	-4. 29	4.314	$\mathbf{P}^{0}$ . $\mathbf{\bar{P}}^{1}$ . $\mathbf{\bar{P}}^{2}$ . $\mathbf{\bar{P}}^{3}$
В	0.734	<b>-2.</b> 96	4. 324	$\mathbf{p}^{0}$ . $\mathbf{p}^{1}$ . $\mathbf{\overline{p}}^{2}$ . $\mathbf{\overline{p}}^{3}$
C	0.756	-1.58	4.612	$\overline{\mathbf{p}}^{0}$ . $\mathbf{p}^{1}$ . $\overline{\mathbf{p}}^{2}$ . $\overline{\mathbf{p}}^{3}$
D	0.753	-0.13	4. 800	$\overline{\mathbf{p}}^{0}$ . $\mathbf{p}^{1}$ . $\mathbf{p}^{2}$ . $\overline{\mathbf{p}}^{3}$
E	0.758	1.38	4. 976	$\overline{\mathbf{p}}^{0}$ . $\overline{\mathbf{p}}^{1}$ . $\mathbf{p}^{2}$ . $\overline{\mathbf{p}}^{3}$
F	0.734	2, 92	5.000	$\bar{\mathbf{p}}^0$ . $\bar{\mathbf{p}}^1$ . $\mathbf{p}^2$ . $\mathbf{p}^3$
G	0.759	4. 52	5, 359	$\bar{\mathbf{p}}^{0}$ . $\bar{\mathbf{p}}^{1}$ . $\bar{\mathbf{p}}^{2}$ . $\mathbf{p}^{3}$
H = TOTAL	5.253	0, 19	33. 65	Sum of events satisfying logic for each of above channels. (Note that this definition is not the same as $P^0+P^1+P^2+P^3$ .)

 $<sup>\</sup>overline{P}$  = mean momentum of particles accepted by a given channel

 $P_{o}$  = central momentum of magnet

pole tips by charged particles, but approximately 1/3 of the area of the pole tips is not shielded against events generated by neutrals.

The momentum-defining counter consisted of four scintillators which were mounted in the form of a seven channel hodoscope. A drawing of this counter is shown in Figure 5. The important parameters defined by the seven channels of this hodoscope are presented in Table 2. The decoding of the output of this hodoscope was done by the IBM 7094 computer. The logical definition used for this decoding is also given in Table 2.

#### C. Electronics

The electronics system for this experiment was broken down into three independent subblocks: a fast logic system containing the coincidence circuits; a pulse-height analysis system containing linear gates and discriminators; and a data storage system making use of a Nuclear Data 1024 channel pulse-height analyzer. The relationship between these three subsystems is shown in Figure 6.

The block diagrams of the fast logic system and the pulse-height analysis system are given in Figure 7. The modules from which these two systems were constructed have been described in the literature. (24, 25) Some of these modules were upgraded by installing more modern transistors on already existing circuit boards; otherwise these modules were the same ones which were used in the Groom-Marshall K<sup>+</sup> telescope experiment. (26)

The particle signature in this experiment consisted of a fast (10 nanosecond) triple coincidence, A·S1·S2, with coincidence circuit input biases of approximately 1/4 minimum ionizing. The basic trigger generated by the fast logic was

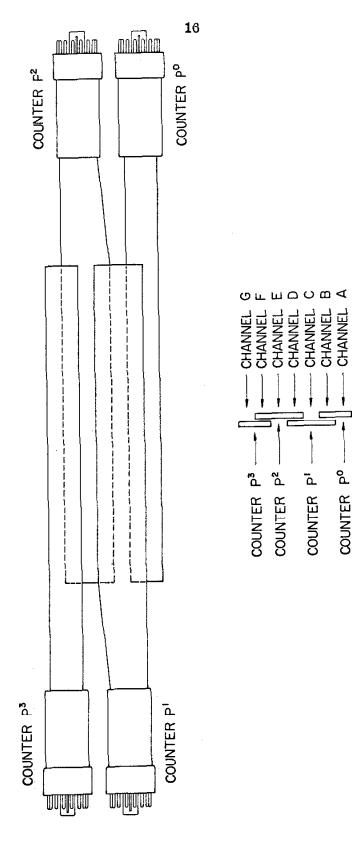


Figure 5. Momentum Hodoscope Counters P<sup>1</sup>

COUNTER P° -

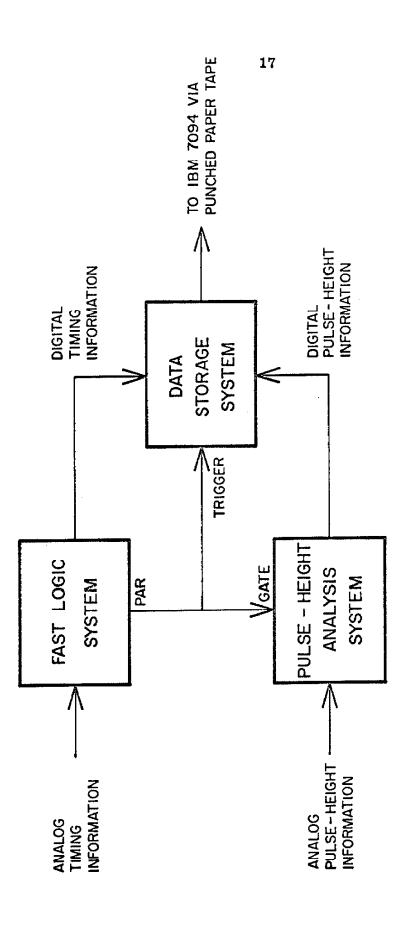
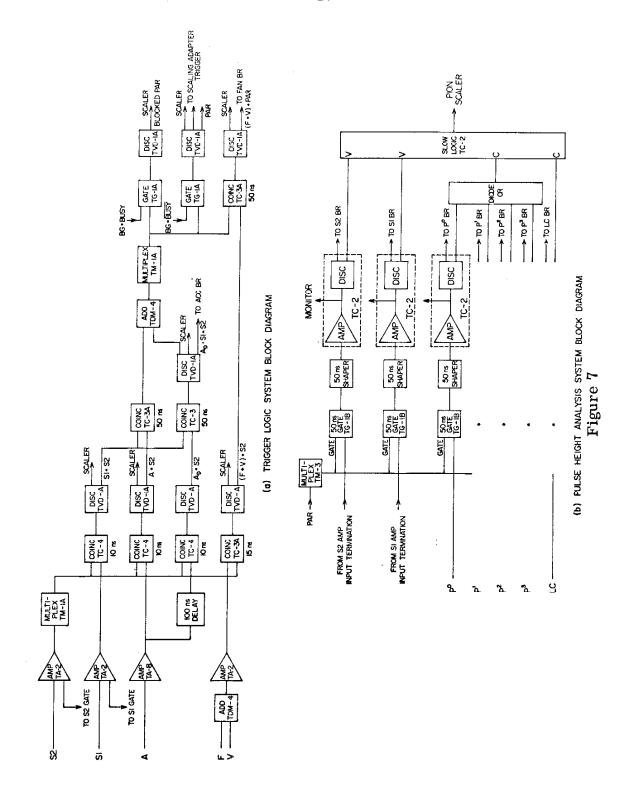


Figure 6
SYSTEM BLOCK DIAGRAM
600 MeV/C MAGNET ELECTRONICS



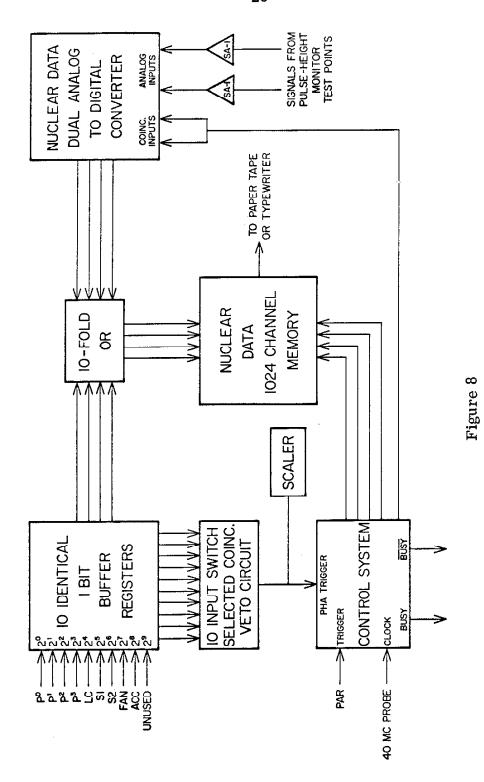
$$PAR = A \cdot S1 \cdot S2 + A_d \cdot S1 \cdot S2$$

where  $A_d$  indicates that the A signal was delayed by 100 nanoseconds from the correct timing. The signal PAR was used to operate the linear gates of the pulse-height analysis system and to trigger the data storage system.

Several scalers were used in the fast logic system. These scalers were extremely useful for diagnostic purposes, but they did not record numbers which could be used directly in cross section calculations. The final data were recorded only by the data storage system.

The data storage system was a new feature of this experiment. This system operated on the principle that each event could be represented by a 9 bit binary number. Each bit of this binary number was controlled by a digital output from either the fast logic system or the pulse-height analysis system. For each event, a count was added to the channel whose address was the same as this binary number. After a data-taking run, the contents of the memory were punched on paper tape. The IBM 7094 computer was then used to sort the 512 possible types of events into physically useful classes. (27) A block diagram of the data storage system is presented in Figure 8. For further details of the electronics, the reader should refer to the SCALING ADAPTER instruction manual. (28)

The correspondence between digital signals and the various bits of the binary number which defines the address is explained more fully in Table 3. Note that the 2<sup>9</sup> bit is always set to 1 so that the result will be stored in the second half of the memory. As an example of how the address for each event is generated, consider the event



DATA STORAGE SYSTEM BLOCK DIAGRAM

TABLE 3. Coding of Address Register Bits

Address Bit	Signal Source	Requirement
20	$^{\mathbf{p}_{0}}$	1/2 x minimum ionizing
2 <sup>1</sup>	$\mathtt{P}^1$	1/2 x minimum ionizing
$\mathbf{2^2}$	$_{ m P}^{f 2}$	1/2 x minimum ionizing
$2^3$	$_{ m P}^{3}$	1/2 x minimum ionizing
24	LC	$\sim$ 1 photoelectron or $\beta$ $\gtrsim$ 0.8
$\mathbf{2^{\bar{5}}}$	S1	~ 2.5 x minimum ionizing
<b>2</b> <sup>6</sup>	S2	~ 2.5 x minimum ionizing
27	(F+V)· PAR=FAN	F or V count within = 8 ns of PAR
28	$A_{d} \cdot S1 \cdot S2 = ACC$	PAR generated by accidental event in A
$2^{9}$	unused	always "1" so that all events are stored in second half of memory

## $\overline{\text{ACC}} \cdot \overline{\text{FAN}} \cdot \overline{\text{S2}} \cdot \overline{\text{S1}} \cdot \text{LC} \cdot \overline{\text{P}}^3 \cdot \text{P}^2 \cdot \overline{\text{P}}^0$

where S1 and S2 represent the high biases ( $\sim 2.5 \times \text{minimum}$  ionizing) on these two counters. This event is a typical pion in the central momentum channel. The address corresponding to this event is 1000010110 binary, or 534 decimal.

Because only 512 of the 1024 available channels of memory were needed for storage of the data, provision was built into the control system to allow the pulse-height analyzer to go through a normal pulse-height analysis cycle before storing the digital data for each event. The result of the pulse-height analysis was always recorded in the first half of the memory. Since the pulse-height analysis cycle did not interfere with the normal data storage cycle, the pulse-height analyzer was free for use as a diagnostic tool during data taking. Using this feature, the pulse-height distribution in each counter was checked on a daily basis.

An additional provision built into the control system permitted the use of the normal clock channel of the memory, channel zero, for recording beam monitoring information. This feature proved to be of only marginal value, however, for no single beam monitor was considered to be stable enough for use in cross section computations. This subject is discussed further in Appendix I.

#### IV. EXPERIMENTAL TECHNIQUE

#### A. Particle Identification

The major problems to be solved by the particle identification scheme were elimination of proton contamination and correction for accidentals. The proton contamination problem was most serious at small angles and high momenta where the time-of-flight requirements did not completely eliminate protons and the ratio of  $\pi^+$  to protons incident on the spectrometer was 1:3. The efficiencies of the various devices which eliminated protons are given in the following table:

Typical Pion and Proton Efficiency at 570 MeV/c

Technique	ε π	$\epsilon_{ m P}$
Time-of-flight	1. 00	0.1
S1 (high bias)	0.05	0.98
S2 (high bias)	0.05	0.98
LC	0, 98	0.03

The time-of-flight requirement in conjunction with any two of the other counters was more than sufficient to eliminate protons under the worst conditions. The redundancy provided by LC permitted a continuous monitoring of the efficiencies of each counter for pions and protons.

The definition of  $\pi^+$  used in this experiment was

$$\pi^+ = PAR \cdot (\overline{S1 \cdot S2})$$

where S1 and S2 indicate the high biases on counters S1 and S2. The IBM 7094 computer automatically corrected each run for the inefficiency of the pion definition and any residual proton contamination. Both of these corrections were less than 1.0% in the worst case.

The counter system of the 600 MeV/c Magnet was designed for minimum mass in the particle trajectories in order to minimize the effects of multiple scattering on the resolution of the spectrometer. Since only one aperture counter was used, this system was particularly sensitive to events produced by an accidental in counter A and a real event in the rear counter system. Since the data recording system was triggered by A·S1·S2 +  $A_d$ ·S1·S2, the IBM 7094 automatically corrected the observed number of pions for this type of accidental by subtracting the events with an  $A_d$  = ACC pulse from those events with no ACC pulse.

A correction for accidentals in the momentum defining counters was also made. This correction was based on the observed number of events with counts in the momentum hodoscope which could be generated only by accidentals or two particles passing through the hodoscope within the 50 ns. gate. An example of such an event is  $P^0 \cdot \overline{P}^1 \cdot \overline{P}^2 \cdot P^3$ . Eight of the sixteen possible kinds of event in the momentum hodoscope fell into this category, and these events were used to compute the corrections for each channel on the assumption that there was no correlation between the location of the true event and the second particle. The magnitude of this correction to the sum channel (H) was typically 0.5%, while the correction to individual channels was less than 2%. It is important to note that events in which a second particle passes through the channel adjacent to the true particle cannot be distinguished from single particle

events. However, such events were counted only once and were counted in either the correct channel or the channel adjacent to the correct channel.

Several checks were made of the efficiency of the fast electronics. For counters A, S1, S2, and V a separate small counter was used to define a beam and test the efficiency of the coincidence circuit. In each case the efficiency was greater than 99%. The 1% of inefficient events were observed on an oscilloscope and most of these were found to have no pulse at all in the counter being tested. These events were assumed to be events due to nuclear absorption or photon conversion in the counters and the electronic efficiency was taken to be 1.00 in each case. The A·S1·S2 and  $\boldsymbol{A_{d^{*}}S1^{*}S2}$  systems were checked by installing an extra 100 ns. length of cable in the A input. The result was that the two systems gave the same number of counts to within 5%. The fan counter efficiency was tested and found to be greater than 95% for minimum ionizing particles passing through the tip of the longest arm of each counter (see Figure 2). Fan accidentals in the F + V system were found to be less than 1% under normal operating conditions. On the basis of these measurements, it was believed that the overall efficiency of the electronic system was  $1.00 \pm 0.01$ .

#### B. Empty Target Background

The empty target background was measured on two or more occasions for each data point. In general, empty target runs were taken within a few days of full target runs to correct for any possible buildup of solid substances on the mylar cup. For those cases in which the high energy magnet yoke was in the beam line for a full

target run, an empty target run was taken under the same conditions. Typically, one-fifth of the total running time was spent measuring the empty target background.

For illustrative purposes, the observed ratios of empty target to full target rates are presented in Table 4. The data have been summed over the seven channels and averaged over the several runs taken at each point. However, the cross section computing program did not average the empty target runs; instead, it associated each full target run with a particular empty target run and calculated the cross sections independently. Only in this way would a varying empty target rate be correctly treated.

#### C. Negative Field Background

Since no electron detector was used in this experiment, a series of tests was made to look for possible  $e^+$  contamination in the  $\pi^+$  events. These tests were made with the normal magnet and synchrotron settings, but with the magnet field reversed. Under these conditions, the only single pion photoproduction process which can contribute is the reaction

$$\gamma + n \rightarrow \pi^{-} + p$$

Since neutrons are found only in the target structure, these events should be removed by an empty target subtraction. If we assume that e<sup>-</sup> and e<sup>+</sup> are produced in equal numbers, as in pair production, then the e<sup>-</sup> yield in the field reversed run should be equal to the e<sup>+</sup> contamination in the normal runs.

TABLE 4. Fractional Empty Target Rates Summed Over 7 Channels (See Table 6 for Point No. Definition)

Point No.	Empty/Full	Point No.	Empty/Full
34-1	$5.2 \pm 0.3\%$	84-1	$7.8 \pm 1.1\%$
34-2	$4.7 \pm 0.4\%$	84-2	$6.0 \pm 0.8\%$
34-3	$6.1 \pm 0.4\%$	84-3	$3.9 \pm 0.6\%$
0.7 0	30 4 ± 30 4/0	84-4	$2.9 \pm 0.5\%$
40-1	$3.9 \pm 0.3\%$	85-5	$5.4\pm0.5\%$
40-2	$3.8 \pm 0.3\%$	84-6	$4.9 \pm 0.5\%$
40-3	$4.6 \pm 0.6\%$		
		94-1	$7.8 \pm 1.0\%$
48-1	$3.6 \pm 0.4\%$	94-2	$5.2\pm0.7\%$
<b>4</b> 8- <b>2</b>	$3.4\pm0.3\%$	94-3	$4.5 \pm 0.7\%$
48-3	$4.6 \pm 0.5\%$	94-4	$2.8 \pm 0.5\%$
48-4	$4.9\pm0.5\%$	94-5	$6.0 \pm 0.7\%$
53-1	4.8 + 0.5%	106-1	$8.0 \pm 0.8\%$
56- <b>2</b>	$\frac{1}{4.6 \pm 0.5\%}$	106-2	$5.8 \pm 0.7\%$
56-3	$4.5 \pm 0.5\%$	106-3	4.9 + 0.7%
56-4	$3.6 \pm 0.5\%$	106-4	$4.9 \pm 0.7\%$
<b>Q</b>	_ , ,	106-5	$5.6 \pm 0.7\%$
64-1	$4.7 \pm 0.5\%$		
64-2	$4.6 \pm 0.3\%$	120-1	$8.2 \pm 1.2\%$
64-3	$3.6 \pm 0.5\%$	120-2	$4.7 \pm 0.9\%$
64-4	$4.6 \pm 0.5\%$	120-3	$5.9 \pm 0.7\%$
64-5	$6.4 \pm 0.5\%$	120-4	$5.3 \pm 0.7\%$
		120-5	$6.8 \pm 0.8\%$
74-1	$5.6 \pm 0.8\%$		<b></b>
74-2	$4.7 \pm 0.7\%$	134-1	$6.2 \pm 0.6\%$
74-3	$4.3 \pm 0.5\%$	134-2	$6.0 \pm 0.9\%$
74-4	$4.6 \pm 0.5\%$	134-3	$4.9 \pm 0.6\%$
74-5	$4.5 \pm 0.7\%$	134-4	$5.6 \pm 0.7\%$
74-6	$3.7\pm0.5\%$	450 1	10 7 . 1 907
		156-1 156-2	10. $7 \pm 1.2\%$ 5. $7 \pm 0.8\%$
		156-2 156-3	7. 4 ± 1.0%
		156-3 156-4	$10.5 \pm 1.1\%$
		T90-4	10.0 ± 1.1%

The field reversed runs were taken at several points which scanned the entire range of angles and energies used in this experiment. In order to improve the statistics, the results were summed over the seven momentum channels. The total amount of synchrotron time used for each of these points was approximately equal to half the amount of time used at each of the normal points. The results of these negative field tests are presented in Table 5. These results indicate that approximately two thirds of the observed events are produced in the target structure, but that the remainder of the events are produced in the hydrogen. Except for the points taken at the highest energies and most backwards angles, neglecting these events would result in errors which were small compared with the statistical errors of this experiment.

Several possibilities for the source of the negative field events have been considered.  $\pi^{O}$  photoproduction with conversion of the decay photons in the target structure could result in a source of high energy electrons. However, this process can be calculated from known  $\tau^0$  cross sections and gives an upper limit of 0.2% of the  $\pi^+$  rate. If photons were converted in the aperture counter at the rear of the magnet, then low energy electrons could be counted. To check this effect, a 1/8" copper radiator was placed on the hydrogen target side of the aperture counter. This radiator had a thickness in radiation lengths of 29 times that of the aperture counter. For point number 134-4, the full target negative field yield was  $0.17 \pm 0.02$  counts/QBIP, while with the radiator in place this rate increased to  $0.55 \pm 0.07$  counts/QBIP. If we assume that half the full target events are due to  $\pi^-$  produced in the target walls, we would have expected an increase of a factor of 15 if all the remaining events were due to photons converting in the radiator, whereas a

TABLE 5. Summary of Negative Field Runs

Point	Full Target <sup>*</sup> π -/QBIP**	Empty Target* π /QBIP**	Difference* π / QBIP**	π <del>-</del> π+
34-1	$0.950 \pm 0.07$	$0.620 \pm 0.06$	$0.330 \pm 0.09$	0.012 ± 0.003
48-2	$0.400\pm0.04$	$0.340 \pm 0.04$	$0.060 \pm 0.06$	0.003 ± 0.003
64-3	$\textbf{0.330} \pm \textbf{0.03}$	$0.200\pm0.02$	0.130 $\pm$ 0.04	0.008 ± 0.002
84-1	$0.110 \pm 0.013$	$0.049 \pm 0.009$	$0.061 \pm 0.015$	$0.007 \pm 0.002$
84-4	$0.205 \pm 0.017$	$0.110 \pm 0.015$	$0.095 \pm 0.023$	$0.012 \pm 0.003$
106-1	$0.113 \pm 0.014$	$0.064 \pm 0.010$	$\textbf{0.049} \pm \textbf{0.017}$	$0.049 \pm 0.017$
106-4	$0.187 \pm 0.017$	$0.125 \pm 0.016$	$0.062 \pm 0.023$	$0.015 \pm 0.005$
134-1	$0.111 \pm 0.015$	$0.052 \pm 0.009$	$0.059 \pm 0.017$	$0.055 \pm 0.017$
134-3	$0.119 \pm 0.011$	$0.100 \pm 0.012$	$0.019 \pm 0.019$	$0.007 \pm 0.007$

<sup>\*</sup> summed over momentum channels so that  $\Delta\Omega \Delta P/P = 3.4 \times 10^{-4}$ 

<sup>\*\* 1</sup> QBIP =  $1.2 \times 10^{13}$  MeV

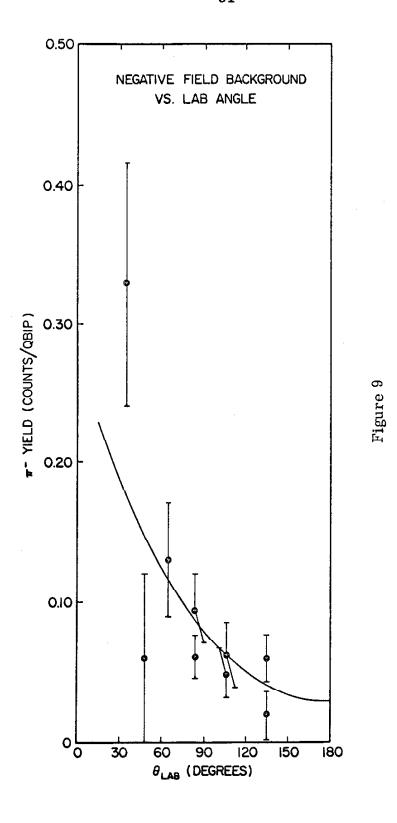
factor of 3.2  $\pm$  0.4 was observed. Thus this process can only account for a small fraction of the observed events. The contribution of multiple pion photoproduction was also checked. Using the known shape of the tails of the resolution functions due to decay and multiple scattering and data on  $\pi^-$  photoproduction at 84° lab<sup>(11)</sup>, we find that at most 10% of the observed events can be due to this process.

The negative field events can also be due to low energy pions or electrons which have the wrong momentum but can be counted because of wide-angle scattering processes, or the events may be due to conversion of photons in portions of the magnet iron which are not guarded by veto counters. Neither of these possibilities was investigated in any detail.

The conclusion drawn from the negative field runs was that an unexplained background exists and must be subtracted from the  $\pi^+$  data. To make this subtraction, it was necessary to extrapolate to angles and energies at which no negative field runs were taken. For the purposes of this extrapolation, the negative field yield was assumed to be a function only of lab angle. The empirical formula

$$\pi^{-}/\text{QBIP} = 0.03 + 0.05 \left(\frac{\theta - 180^{\circ}}{90^{\circ}}\right)^{2}$$

was found to give a good fit to the data. This function and the data of Table 5 are plotted in Figure 9. In order to indicate the expected errors in this correction, an rms error of 1/2 the correction has been included in the error bars of all the cross sections measured in this experiment.



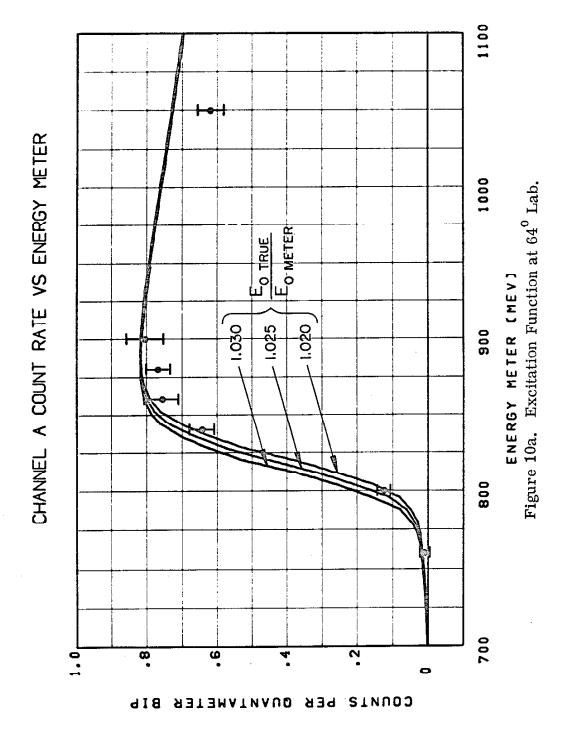
Experimental evidence for a small positron contamination at large angles is lacking in previous experiments. For experiments at small angles, the positron detection system usually showed a large ratio  $e^+/\pi^+$  which decreased rapidly to zero near  $15^0$  lab. For angles between 15 and  $45^0$ ,  $e^+/\pi^+$  was found to be small and neither Dixon (12) nor Kilner (13) used electron detection systems for lab angles greater than  $55^0$ . One bit of evidence is available from the present experiment. The excitation curve taken at  $\theta_{lab} = 64^0$  near K = 880 showed a background of events in the below threshold region. This background was  $0.15 \pm 0.02$  counts/QBIP in seven channels before correction for negative field contamination. The correction used in this experiment gives  $0.10 \pm 0.05$  counts/QBIP. By comparison, the  $\pi^+$  yield was 5.0 counts/QBIP for the normal point. Thus it appears that the correction used gives a reasonable but crude approximation to the true background.

## D. Excitation Functions as Proof of Particle and Reaction Identification

Two excitation functions were measured during this experiment. The first was taken near  $\theta_{\rm cm}=95^{\rm O}$  and K = 900 MeV, and the second near  $\theta_{\rm cm}=150^{\rm O}$  and K = 750 MeV. For each measurement, the magnet was set at constant momentum and lab angle while the synchrotron energy was varied. The counting rate in each channel was measured as a function of the synchrotron beam energy meter reading. The expected values of these rates were computed from the cross sections measured in this experiment and the resolution function used in reducing all the data. This resolution function includes the effects of multiple scattering, pion

decay, and angular resolution. The data and the expected yields are plotted in Figures 10a - 10n. The plotted data were corrected for empty target and negative field background.

Several important conclusions can be obtained from these data. The first conclusion is that in the off kinematics region (where the expected yields were less than 3% of the peak yields), there is a background of  $1.0 \pm 1.0\%$ , and most of the uncertainty comes from the negative field correction. The second conclusion is that the resolution function calculation gives a reasonable approximation to the true resolution of this experiment. Finally, the best fit to the data gives a value for the energy meter calibration constant,  $E_0 \text{ true} = 1.025 \pm 0.005. \text{ This calibration agrees satisfactorily with the measurements of Stan Ecklund} = 1.025 \pm 0.005.$ 



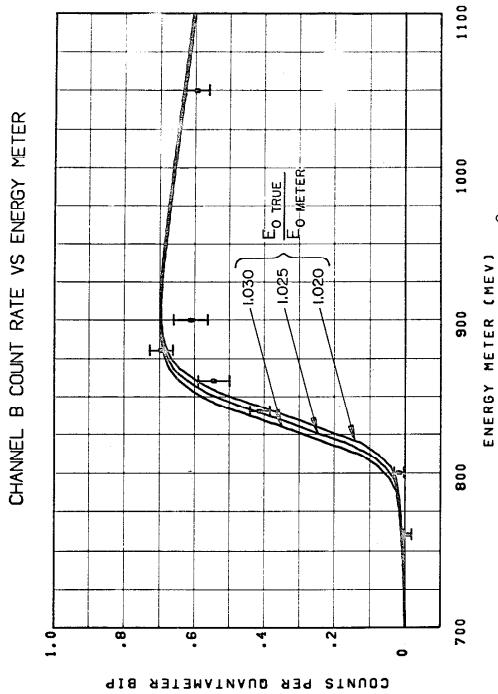


Figure 10b. Excitation Function at 64° Lab.

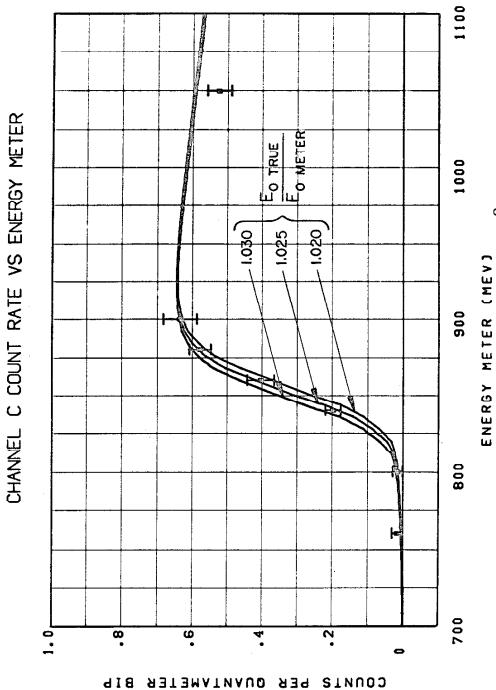


Figure 10c. Excitation Function at 64° Lab.

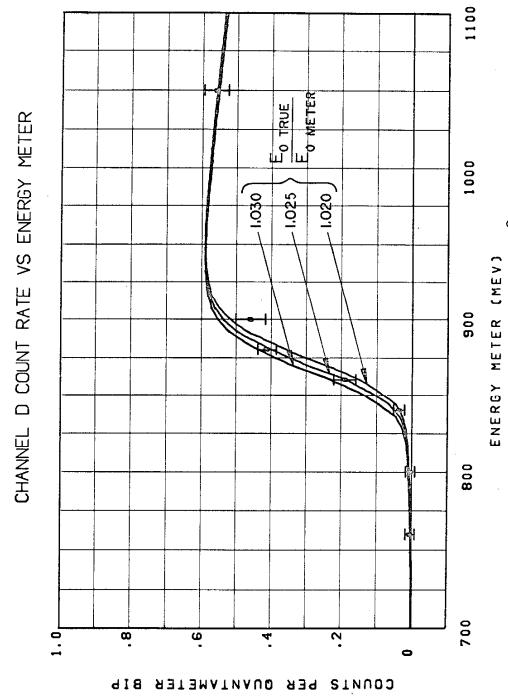
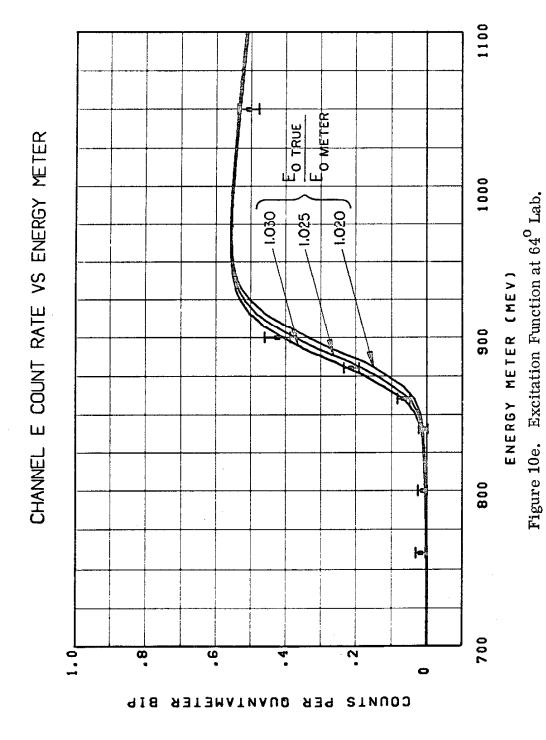


Figure 10d. Excitation Function at 64° Lab.



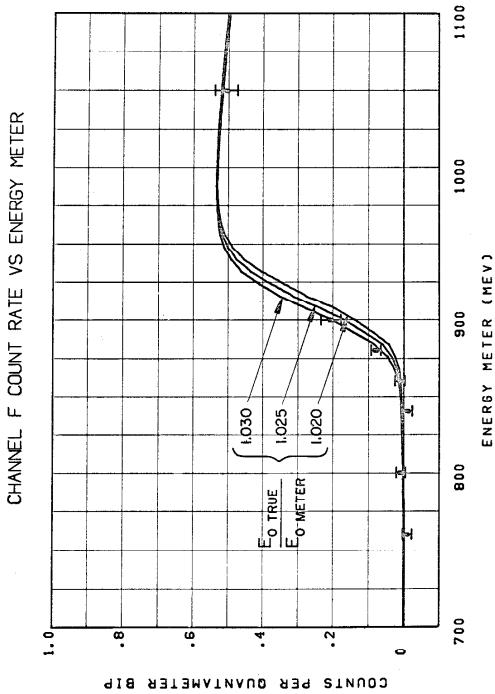


Figure 10f. Excitation Function at 64° Lab.

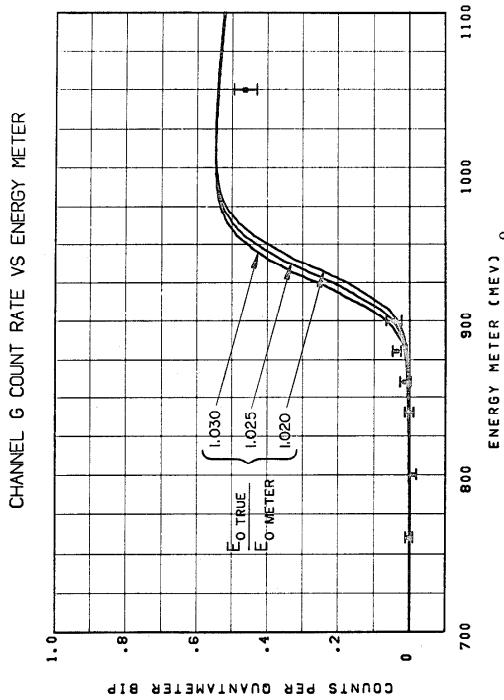


Figure 10g. Excitation Function at 64° Lab.

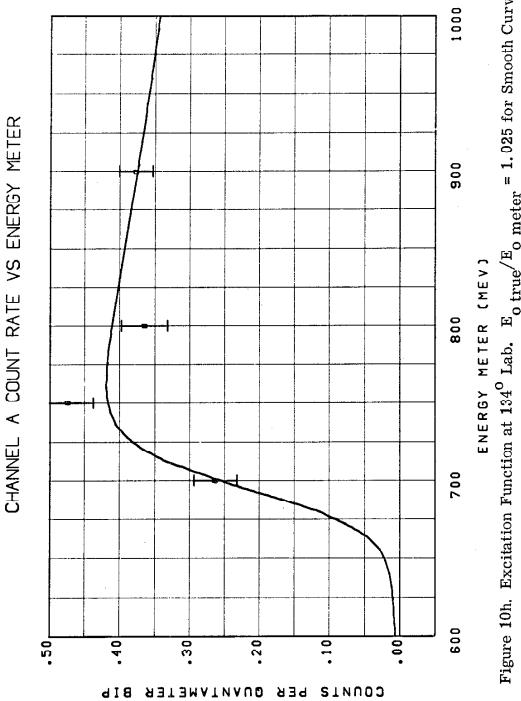


Figure 10h. Excitation Function at  $134^{\circ}$  Lab. E true/E meter = 1.025 for Smooth Curve

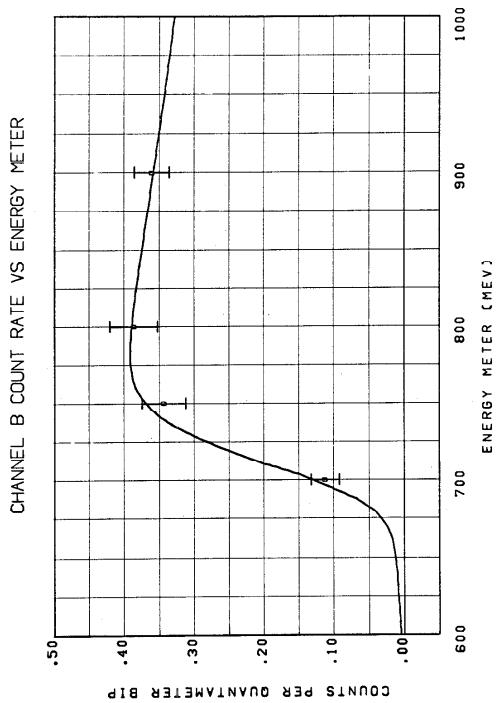


Figure 10i. Excitation Function at 134° Lab. E o true/E meter = 1.025 for Smooth Curve

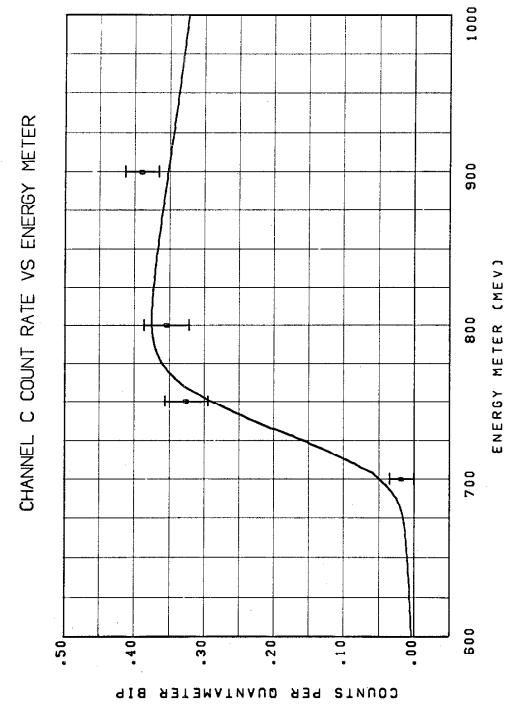
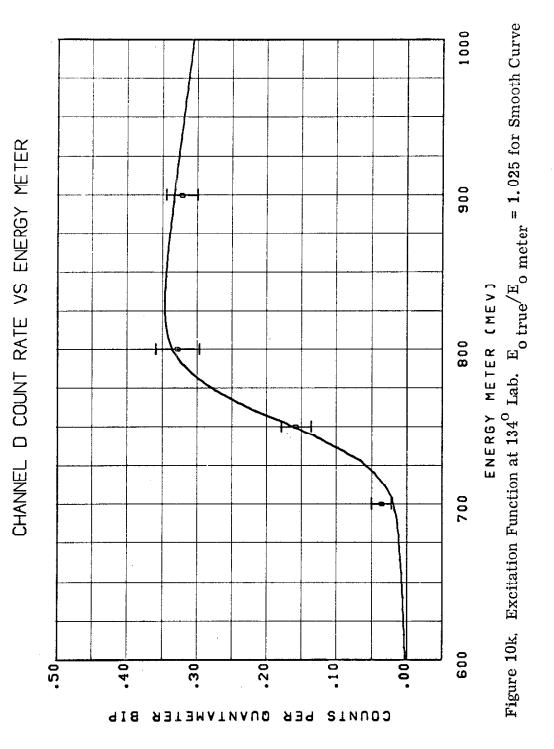


Figure 10j. Excitation Function at 134° Lab. E true/E meter = 1.025 for Smooth Curve



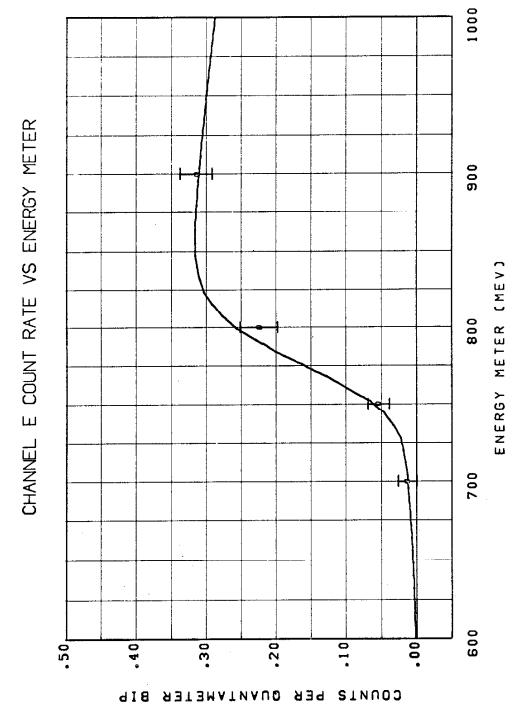
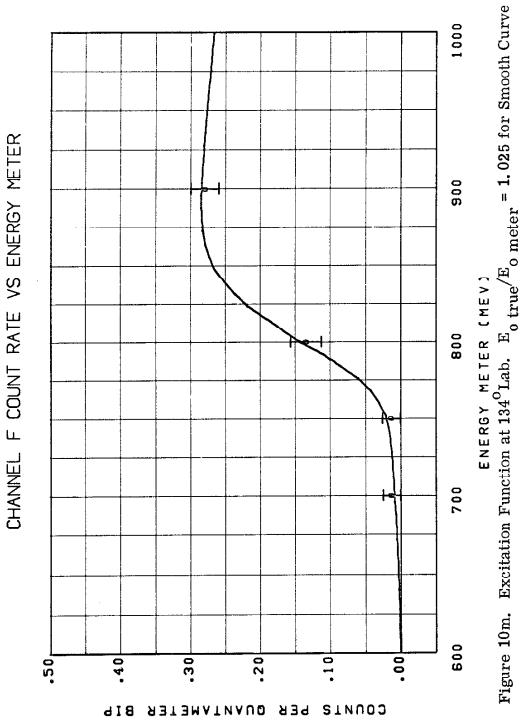


Figure 101, Excitation Function at 134° Lab. E true/E meter = 1.025 for Smooth Curve



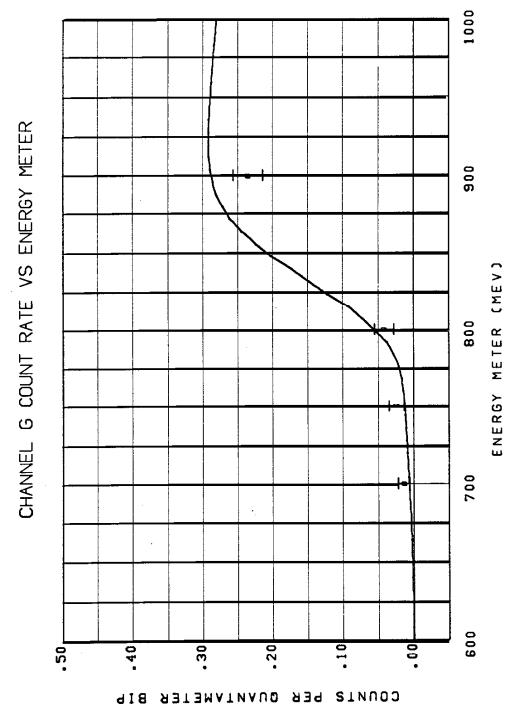


Figure 10n. Excitation Function at  $134^{0}$ Lab. E<sub>o true</sub>/E<sub>o meter</sub> = 1.025 for Smooth Curve

#### V. DATA AND DATA ANALYSIS

### A. Cross Section Calculation

The observed pion counting rate in the  $i^{th}$  spectrometer channel,  $C_i$ , may be written as a multiple integral over geometrical and kinematical quantities and the cross section  $\sigma(k, \theta^*)$ 

$$C_{i} = \iiint \int \int \int \sigma(k, \theta^{*}) G(\Omega, p) N(k, x, y) n_{H}(x, y, z)$$

$$\times A(p, \Omega) E_{i}(x, y, z, p, \Omega) d\Omega dp dx dy dz$$

where

- C = number of events/quantameter BIP satisfying the pion definition after subtraction of backgrounds,
- $\sigma(k, \theta^*)$  = differential cross section for single π<sup>+</sup> photoproduction from hydrogen by a photon of lab energy k producing a π<sup>+</sup> in dΩ\* at θ \* (\* refers to c. m. system),
- $G(\Omega, p)$  = the Jacobian of the transformation between the independent variables  $(k, \Omega^*)$  and  $(p, \Omega)$ ,
- N(k, x, y) = number of photons per BIP per cm<sup>2</sup> with energy between k and k + dk striking a plane perpendicular to the beam line at the hydrogen target at the point (x, y),

 $n_{H}(x, y, z)$  = number of protons/cm<sup>3</sup> at the point x, y, z where the origin is at the center of the hydrogen target and the z-axis is along the beam line,

 $A(p, \Omega)$  = a correction for nuclear absorption in the material in the path of particles passing through the spectrometer,

 $E_i(x, y, z, p, \Omega)$  = efficiency of the i<sup>th</sup> spectrometer channel for accepting an event originating at the point x, y, z with momentum p and at lab solid angle  $\Omega$ .

As this integral is defined here, the limits on the effective hydrogen target volume are contained in the functions  $n_H(x, y, z)$  and N(k, x, y) while the limits for the spectrometer acceptance are contained in the function  $E_s(x, y, z, p, \Omega)$ .

In order to simplify the evaluation of this multiple integral, several approximations were made. The first approximation involved averaging the bremsstrahlung spectrum over the target and collimator geometry. The spectrometer acceptance was taken outside of this integral and replaced with an average acceptance. This approximation may be schematically represented as follows:

$$\iiint dx dy dz \rightarrow \overline{E}_{i}(p, \Omega) \iiint dx dy dz \rightarrow \overline{E}_{i}(p, \Omega) \frac{W}{E_{o}} \frac{\overline{B}(k, E_{o})}{k}$$

where

 $\overline{E}_{i}(p, \Omega)$  = the spectrometer efficiency averaged over the origin of events,

W = total energy in the photon beam per quantameter BIP,

 $E_0 = \text{synchrotron end point energy,}$ 

 $\overline{B}(k, E_o)$  = bremsstrahlung spectrum averaged over target and collimator geometry (defined below),

N<sub>H</sub> = number of protons per square centimeter in a planar target of thickness equal to the diameter of the hydrogen target appendix.

This approximation allows the separation of the calculation of the spectrometer acceptance and the bremsstrahlung spectrum into two separate computer programs. The effect of averaging the spectrometer acceptance is a broadening of the momentum resolution, while the total volume of  $\mathfrak{p},\Omega$  phase space accepted remains constant. There is also a correlation between z and  $\Omega$  which has been neglected. Since the bremsstrahlung distribution in z (along the beam line) is uniform, neglecting this correlation will have no effect on  $\overline{B}(k,E_0)$ .

The average bremsstrahlung spectrum,  $\overline{B}(k, E_0)$ , was computed from the differential spectrum,  $BR(k, E_0, \theta_x, \theta_y)$ , given by the program BPAKI written by Mr. Frank Wolverton.  $\overline{B}$  is defined by the average of BR over the target and collimator geometry, namely

$$\overline{B}(k, E_{o}) = \int \int BR(k, E_{o}, \theta_{x}, \theta_{y}) \frac{d(\theta_{x}, \theta_{y})}{D} d\theta_{x} d\theta_{y}$$

$$\theta_{x \min} \theta_{y \min}$$

where

 ${}^{0}x$ ,  ${}^{0}y$  = the angle between the photon and the nominal beam line,

D = the diameter of the hydrogen target appendix,

 $d(\theta_x, \theta_y)$  = the thickness of the hydrogen target at an angle  $\theta_x, \theta_y$  to the nominal beam line,

 $^{\theta}$ x min,  $^{\theta}$ x max = limits on the photon beam angles defined by  $^{\theta}$ y min,  $^{\theta}$ y max the primary collimator.

Mr. Mike Hauser coded a program to tabulate the value of  $\overline{B}(k, E_0)$  for several values of k and  $E_0$ . A second short subroutine, also coded by Mr. Hauser, was able to compute  $\overline{B}(k, E_0)$  by interpolation on the tabular values. (31) This subroutine was used for all the data analysis of this experiment.

Using this first approximation, the counting rate integral was reduced from a six fold integral to a three fold integral over  $d\Omega$  dp. This integral contains the effects of the finite resolution of the spectrometer in the quantities k and  $\theta^*$ . Since the unfolding of two dimentional resolution is a difficult numerical analysis problem, an approximation was made to reduce the integral to an integral over a single variable, k. This approximation consisted of replacing  $\theta$ ,  $\varphi$ , and  $\theta^*$  by the mean values  $\overline{\theta}$ ,  $\overline{\varphi}$ , and  $\overline{\theta}^*$ , and may be schematically represented as follows

$$\iint d \Omega \to R_{i}(p, p_{O}, \overline{\theta}) G(p, \overline{\theta}) \sigma(k, \overline{\theta}^{*})$$

where

 $R_i(p, p_0, \overline{\theta}) =$  the effective momentum resolution function for the  $i^{th}$  spectrometer channel,

p<sub>o</sub> = the spectrometer central momentum.

The effective resolution function defined here is normalized so that the integral over p gives  $\Delta\Omega$   $\Delta p$ , i.e.

$$\int_{0}^{\infty} \frac{R_{i}(p, p_{O}, \overline{\theta})}{p_{O}} dp = \left(\frac{\Delta \Omega \Delta p}{p_{O}}\right)_{i}$$

where

 $\left(\frac{\Delta\Omega\ \Delta p}{p_{_{\rm O}}}\right)_{\rm i}$  = the volume of  $\Delta\Omega\ \Delta p/p_{_{\rm O}}$  phase space accepted by spectrometer channel i.

The details of the calculation of the effective resolution function are described in Appendix V.

This second approximation results in ignoring any effects of finite resolution in  $\theta^*$ . Because the observed angular distributions were smooth and the resolution in angle was good (less than 1.5 degrees r.m.s.), these effects were expected to be small.

After changing the variable of integration from p to k, the counting rate integral may be written

$$\begin{split} C(\overline{k},\overline{\theta}^*) &= \int\limits_0^{\infty} \sigma(k,\overline{\theta}^*) \ R_i(p(k,\overline{\theta}),p_0,\overline{\theta}) \, \frac{d\Omega^*}{d\Omega}(k,\overline{\theta}) \ A(p(k,\overline{\theta}),\overline{\theta}) \ N_H \, \frac{W}{E_0} \\ &\times \, \frac{\overline{B}(k,E_0)}{k} \ dk \end{split}$$

where

 $C(\overline{k}, \overline{\theta}^*)$  = the pion counting rate per quantameter BIP explicitly labelled with  $\overline{k}$  and  $\overline{\theta}^*$ ,

and

 $\overline{k}$  = the photon lab energy calculated from  $\overline{\theta}$  and the mean momentum of particles accepted by the  $i^{th}$  spectrometer channel.

The equation was solved in two steps. First,  $\sigma$  was assumed to be slowly varying in the region for which R is non-zero and was taken outside the integral. This approximation to  $\sigma$ , which will be called  $\overline{\sigma}$ , is related to C by an easily calculable factor, namely

$$\overline{\sigma}(\overline{k}, \overline{\theta}^*) = \frac{C(\overline{k}, \overline{\theta}^*)}{\int\limits_{0}^{\infty} R_{i}(k, p_{o}, \overline{\theta}) \frac{d\Omega^*}{d\Omega}(k, \overline{\theta}) A p_{o}\overline{\theta}) N_{H} \frac{W}{E_{o}} \frac{B(k, E_{o})}{k} dk}$$

or

$$\overline{\sigma}(\overline{k},\overline{\theta}^*) = \frac{C(\overline{k},\overline{\theta}^*)}{\kappa}$$

The average cross section,  $\overline{\sigma}$ , was calculated for each point by evaluating  $\kappa$  numerically. The computer program which computed  $\overline{\sigma}$  was called CRØS, and was a joint effort of the author and Mr. Stan Ecklund. (9)

The second step in the process of calculating  $\sigma$  was to start with the measured values of  $\overline{\sigma}$  and correct for the effects of the finite resolution of the spectrometer. The details of this process, which is called unfolding, are the subject of Section V-B.

### B. Resolution Unfolding

The equation for  $\sigma$  may be rewritten in the form of a Fredholm equation of the first kind, namely

$$\overline{\sigma}(\overline{k},\overline{\theta}) = \int_{0}^{\infty} \sigma(k,\overline{\theta}) K(k,\overline{k},\overline{\theta}) dk$$

where the kernel is given by the normalized resolution function, i.e.,

$$K(k, \overline{k}, \overline{\theta}) = \frac{R_{i}(k, p_{o}, \overline{\theta}) \frac{d\Omega^{*}}{d\Omega}(k, \overline{\theta}) \frac{\overline{B}(k, E_{o})}{k}}{\int\limits_{\Omega}^{\infty} R_{i}(k, p_{o}, \overline{\theta}) \frac{d\Omega^{*}}{d\Omega}(k, \overline{\theta}) \frac{\overline{B}(k, E_{o})}{k} dk}$$

where  $\overline{k}$  is the photon energy corresponding to the mean momentum and angle accepted by the i<sup>th</sup> spectrometer channel. The limits of the integrals are not actually infinite as shown, for there were no photons of energy greater than the maximum possible energy of the synchrotron, namely, 1.5 GeV. This integral equation may be converted into a sum if an appropriate numerical quadrature method is used. The method chosen was to assume that  $\sigma$  could be sufficiently accurately represented by straight line segments connecting the

experimental points and then to use Simpson's rule to calculate the integrals. For regions in which no experimental data existed, namely, for energies below the lowest energy measured or energies above the highest energy measured,  $\overline{\sigma}$  was assumed to be constant and have the same value as  $\overline{\sigma}$  at the nearest measured point. We may then write a matrix equation in which  $\sigma$  and  $\overline{\sigma}$  represent vectors whose components are the values of  $\sigma$  and  $\overline{\sigma}$  at the measured points. This equation may be written as follows

$$\overline{\sigma}_{i}(\overline{\theta}) = \sum_{i} K_{ij}(\overline{\theta}) \sigma_{j}(\overline{\theta})$$

or in simplified notation

$$\overline{\sigma}(\overline{\theta}) = K(\overline{\theta}) \sigma(\overline{\theta})$$

The solution to this equation is

$$K^{-1}(\overline{\theta})\overline{\sigma}(\overline{\theta}) = \sigma(\overline{\theta})$$

A computer program was written to compute K and  $K^{-1}$ . The matrix inversion was computed in double precision and elements of the matrix E, where

$$E = K K^{-1} - 1$$

were typically of order  $10^{-12}$ . Then the vector  $\sigma$  was computed from the vector  $\overline{\sigma}$ . The resulting solution for  $\sigma$  was violently oscillatory. In a typical example,  $\overline{\sigma}$  was nearly constant at about

3 microbarns/steradian while  $\sigma$  would vary between  $\pm$  2000 microbarns/steradian.

There are three possible sources for errors which can build up into the observed violent oscillations. These sources include statistical errors in  $\overline{\sigma}$ , inaccuracy of the numerical integration method, and the near singularity inherent in the solution of the Fredholm equation. The statistical errors are much greater than the errors of the quadrature method, so that we may safely neglect this source of oscillations.

Gold  $^{(32)}$  has made extensive studies of a method which has shown some success in eliminating the singularities of the Fredholm equation. This method was tried, but it was found that the statistical errors in  $\overline{\sigma}$  were greatly magnified in computing  $\sigma$ . Twomey  $^{(33)}$  has invented a method which attempts to filter out the oscillations and obtain a smooth unfolded result. This method was also coded for the computer. However, the smoothing function required to eliminate the oscillations was as broad as the resolution functions of the spectrometer. Intuitively, no gain may be obtained by this method.

Some success was obtained when the response matrix, K, was written as the sum of a diagonal matrix and another "small" matrix. The diagonal matrix was associated with the normal part of the resolution functions and the "small" matrix was associated with the tails of the resolution functions which result from the  $\pi \to \mu + \nu$  decay process (see Appendix IV). In the integral equation, this approximation is equivalent to assuming that the normal part of the resolution function is a delta function. Using this approximation, the inverted response matrix gave reasonable results, and the error bars for  $\sigma$  came out about 10% greater than the error bars for  $\overline{\sigma}$ . Since the effects of the resolution function tails on the peaks and

valleys was about 2%, it was felt that this correction would be worthwhile. Because there may be objections to the details of the unfolding method used, both the values of  $\overline{\sigma}$  and  $\sigma$  were tabulated.

One may wonder why the method previously used by R. Diebold (34) was not tried. Diebold fit the data with a theory which was folded with the resolution. The parameters of the theory determined in this fit were used to compute the unfolded cross sections. Since any reasonable theory must also work for regions not measured in this experiment, all available data must be fit simultaneously, and the program which does this job must be more complicated than the phenomenological analysis programs presently used by S. Ecklund (9) and C. Clinesmith (10). Since the other data which are available at the present time have similar or worse resolution, it is unreasonable to attempt this task now.

If it is necessary to completely unfold the resolution at some later date, one may start with the unfolded data (in which the effects of the tails have been corrected) and approximate the resolution functions by Gaussians with standard deviations given by the values of  $\Delta k_{r.\,m.\,s.}$  from Table 7. A sample calculation has shown that a Gaussian will be within  $\pm$  10% of the exact resolution functions (without decay tails) for values of  $(k-\overline{k})$  less than  $2\Delta k_{r.\,m.\,s.}$ .

### C. Data Point Summary and Internal Consistency of Data

The data were obtained from 12 momentum scans at 12 lab angles. At each lab angle, from three to six spectrometer central momentum settings were required to cover the range of

## TABLE 6-a and 6-b

# Kinematic Parameters and Some Intermediate Results of the Cross Section Calculation

$^{ heta}$ lab	is the mean spectrometer lab angle in degrees.
f	is the nuclear resonance magnetometer frequency in mc.
P <sub>o</sub>	is the mean momentum of the seven momentum channels (taken as one channel) referred to pion momentum at the center of the hydrogen target.
0*	is the mean pion C. M. angle in degrees.
<sup>k</sup> min	is the mean photon lab energy in MeV accepted by Channel A.
kmax	is the mean photon lab energy in MeV accepted by Channel G.
$^{\mathrm{k}}2\pi$	is the photon energy threshold in MeV for double pion photoproduction in Channel A.
Eo	is the synchrotron end point energy in MeV.
π <sup>+</sup>	is the observed number of pions summed over the seven channels in a pair of full and empty target runs.
QAVG	is the number of Quantameter BIPS in each run determined by the average of the other monitors (see Appendix I).

X.

is the constant relating cross sections in microbarns per Steradian and pion yield in counts per Quantameter BIP (pions summed over all seven channels). The total energy/BIP was 1.  $214 \times 10^{13}$  MeV/BIP and the number of hydrogen atoms/cm<sup>2</sup> in one diameter of the hydrogen target was 3.  $138 \times 10^{23}$  for all the runs shown in this table.

CCORR

is the correction for the field reversed background in units of microbarns/steradian.

 $\bar{\sigma}_{1}$ 

is the cross section in microbarns/steradian calculated from the run shown (averaged over the seven channels) with no correction for resolution effects.

5

is the cross section in microbarns/steradian computed for all data available at the given point.

 $d\overline{\sigma}$ 

is the statistical error associated with  $\overline{\sigma}$  (see Section V-F).

ر م is the value of  $\chi$ -squared obtained for the several runs at the given point.

deg f

is the number of degrees of freedom (number of runs
-1) associated with χ-squared at the given point.

				•													٠		
Point No.	O <sub>k</sub>	ረኍ	₽°°	<b>D</b>	K Eig	K max	X X	'n,	<u>.</u>	- Enget	E APT	Empty Tanget	×	CCORA	15	iЬ	16	<sup>7</sup> %	e P
34-3	34.0		462	49.1	508.	545	675.	677.	3357	159.9	0	28.8	2.521	0.065		9.551		9.48	. M
34-2	34.0			50.3	564.	628.	733.	677.	3349	117.2	37	28.8	2.623			10,353		4.90	~
34-1	34.0	68.26		51.6	629.	<b>.</b> 069	199.	169.	6655	151.9	78	50.9	2.486		11.209	11.061	0.180	0.60	_
40-3				57.5	525.	575.	698	677.	3689	149.8	28		2.518	0	9,313	9,182	0.17	0.80	_
40-2	40.0	61.11	513	58.9	585	644.	761.	677.	3099	121.3	28	28.8	2.545	0.060	9.570	9.716	0.184	0.84	
40-I				4.09	656.	723.	834.	769.		199.5			2.424	0	11.083	11.132	0.18	0.09	-
4-84	48		417	67.1	496	544.	661.	677.		156.5		38.1	•	90	N	36	9	0.42	
48-3	48.0	54.86	462	68.6	554.	611.	737.	677.	2824	132.9		28.8	2.411	0.058	8.281	8.498	0.168	2.36	
48-2	48			70.2	622.	689	809	769.		194.5		50.3	Š	90.	Gr.	96	+22		•
48-1	43		570	72.1	703.	781.	893.	871.		103.4	69	103.4	~	90,	•	7	2	0.64	~
56-4	56.	49.28	4	77.6	525.	580.	716.	677.		185.8		38.4	2.204	0.5	•	7.468	4.0	2.89	-
56-3	56.	54.86	462	79.4	592.	657.	787.	769.		295.0		97.0	2.079	90	•	7.971	0.12	4.79	7
2-95	26.0	61.11	513.	81.4	670.	748.	871.	871.	3775	204.7	87 1	103.3	1.956	0.065	8.888	8.754	0.164	0.89	
56-1	56.	68.26	571	83.6	765.	859.	•696	974.		423.1		111.4	1.852	Ş	•	4.260	0.08	0.31	
64-5	49			86.1	496	550.	695.	677.		168.3			2.004	0	6.238	50	07.	6.13	~
4-49	64.0	49.28	417.	87.9	562.	626.	166.	769.	3569	263.3	72 1	6.101	1.886	190'0	6.730	6.528	0.088	2.54	m
64-3	49			89.9	639.	716.	850.	769.		388.6			1.929	0	7.629	75	=	1.57	~
64-2	49			92.2	732.	826.	951.	871.		171.0			1.795	0	5.415	56	• 03	1.42	~
64-1	40		570	94.9	847.	964.	1177.	1076.		458.0			1.594	0	2,361	32	.05	1.62	m
74-6	74		338	96.5	477.	531.		677.		270.1			1.759	0.05	5.674	5,555	0.13	0.09	~
74-5	74		375	98.2	541.	.909		677.		568.9		_	1.851	0.05	5.270	5,283	01.0	0.02	
4-42	74		417.	100.3	620.	700.		769.		452.5		~	1.731	0,05	6,203	6,234	0.10	0.39	
74-3	~		462	102.7	716.	815.	_	871.		192.9		_	1.606	0.06	5.935	5.677	0.08	3.94	
74-2	14.0	61.11	513.	105.4	836.	962.	1086.	1076.	1899	459.5	25 1	114.8	1.416	0,071	2,687	2,706	0.068	0.11	
74-1	74		570.	108.5	991.	1155.		1179.		461.8		_	1.233	90.0	1,639	1.732	90.0	4.85	

TABLE 6a

80	. <b> ~</b> .	<b></b>	~	₩	-	~	ņ	~	m	~		~	~	4	7	~	-	~	~	4	m	m	8	4	~	~	'n
**	9.03	0.11	6.07	10.17	1.21	1.28	0.43	0.97	7.27	•	0.31	•	•	•	. 6	9.89	0	۲.	•	φ.	0.14	9	G	6.17	0.07	4.48	1.17
140	0.092	0.109	0.071	~ <del>*</del> 0 • 0	ç	60°	0.088	0.	ဝိ	.07	0.083	90	<u>.</u> 0	÷0.	0	0.073	.07	.07	90	Ö	ő	ó	0.045	0.064	0.065	2.061	0.050
Ь	4.336	3.958	2.884	0.736	87	5.9	4.008	25	č	52	3.598	78	5	24	~	3.084	~	•	•	2,306	3.147	2.365	1651	2.934	2,760	2,306	1.424
16-	4.587	3.932	2.833	0.801	3,955	<b>4</b> ° 500	3.961	3, 132	1.097	3.491	3,745	3.749	2.816	1.303	26	3.038	28	69	30	2.909	3,118	2,390	1.548	88	2,757	36	42
CCORR	0.056	0.066	0.075	0.086	0.058	0.061	0.065	9.00	0.085	0.056	0.059	0.062	120.0	0.085	0.5	0.051	0.5	90	08	1,0.0	C.051	0.059	0.072	150.0	0.045	0.053	0.064
×	1.592				1.328	1.265	1.195	1.044	0.912	-	1.094	0	O.	~	1.021	1.043	0.959	0.190	0.638	0.940	0.861	0.741	109.0	Ċ	0.767	ċ	ċ
ots tanget	94.0	110.3	119.5	222.0	95.7	Ģ	109.8	<b>.</b>	ŝ	95.8	103.0	11.	119.3	90	95.2	95.7	104.1	119.5	135.0	96.4	104.5	376.0	159.3		103.1		
K 3	46.40	24.2	24	12	31	[]	28	16	53	56	25	21	13	Ś	21	9	22	1	13	11	16	43	=	26	20	10	23
araet Object	9 360.6 5 400.5	431.	476.	453	ø	0	29	2	<b>~</b>	389.	409.8	423.	473	452.	399.	389.0	413.	474.	414.	392		456	999	582	410.4	645	<b>601</b>
Ē,	2996	2411	1730	4 4	2212	2421	2176	1653	634	1709	1811	1768	1301	504	1442	1326	1416	1083	468	1163	1190	884	704	1599	970	1063	536
m,	769.			1384.	169.					769.	871.	974.	1179.	1384.	769.	769.	871.	1179.	1384.	769.	871.	1076.	1384.	769.	871.	1076.	1384.
X F	710.	1039.	1178.	1394.	876.	894.	1006.	1178.	1407.	•	871.		•		758.	865.	1005.	1195.	1481.				1433.	767.	943.	1129.	1405.
X	545. 628.	874.	1051.	1320.	603.	708.	848	1038.	1300.	582.	<b>.</b> 069	831	1035.	1334.	561.	669	818	1027.	1361.	584.	769.	974.	1290.	592.	724.	920.	1234.
Kan	487. 556.				532.			,	_		597.			_		577.			_				1010		609		
•	108.7	113.4	116.3	119.7	117.4	13	7	7	28	27	129.3	131	134	137	38	139.9	1	144	146	1	151	152	154	163	164.6	165	166
•∆	321.	33	~ .	4	321.	56	C	33	87	33	321.	36	ው	39	•	289.	$\sim$	56	95	•	289.	2	56	234.	260.	89	321.
Ψ	37.82	200	6.	•	37.82			'n.	~	34.02	۲,	÷	ġ	ż	0.5	34.02	₽.	1.9	6.1	0.5	34.02	7.8	1.9	7.5	30.59	4.0	7.8
θ <sub>da</sub>	84.0	* *	<b>,</b>	•	94.0	•	•	÷	•	8	106.0	8	90	90	20.	120.0	20.	•	20.	134.0	134.0	34	3.	155	155.4	155	155
Pont No.	64-6 64-5	+ +	<u>ا</u> .	<b>.</b>	94-5	÷	ţ.	ţ.	†	-90	106-4	-90	-90	-90	20-	120-4	20	20-	20-	34-	134-3	134-	34-	156-4	156-3	156-2	1-951

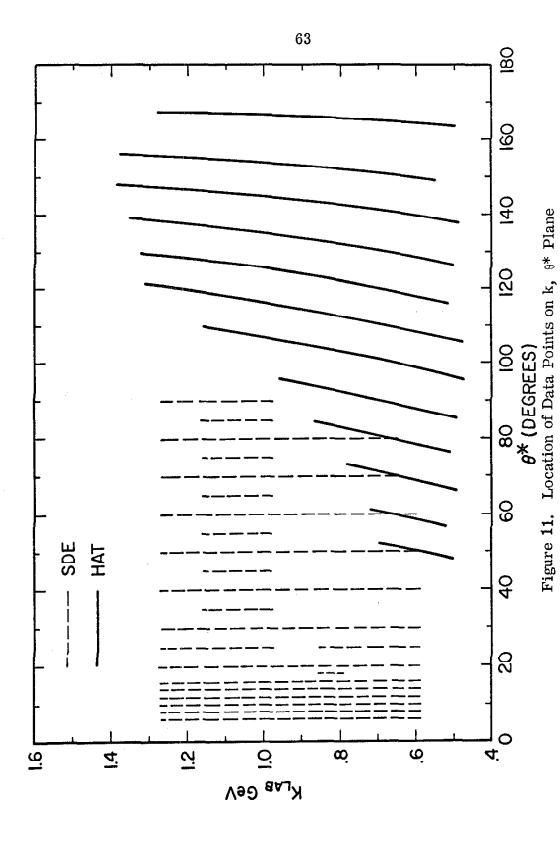
TABLE 6b

photon energies available. The region of the  $(k, \theta^*)$  plane which was investigated in this experiment is shown in Figure 11. In addition, the region scanned by S. Ecklund<sup>(9)</sup> is also shown.

The basic experimental parameters for each data point are given in Table 6. The momentum was calculated from the magnetometer calibration and includes a 2.7 MeV/c correction for momentum lost in the hydrogen target structure. Several useful kinematic quantities derived from the basic parameters are also given.

The observed  $\pi^+$  rates and a few intermediate results of the cross section calculation are also presented in Table 6. These quantities may be used to check the cross section computation or to estimate count rates for similar experiments using the 600 MeV/c Magnet. The  $\pi^+$  rates shown are for a typical pair of full and empty target runs only. At least twice this much data was used for the final results which are presented in Section V-D.

The internal consistency of the data was investigated by comparing the yields for the sum of the seven momentum channels at each point. This method should show up normalization inconsistencies more clearly than investigating the channels separately because of the better statistics of the sum. The observed value of  $\chi$ -squared and the number of degrees of freedom at each point are presented in Table 6. The integral  $\chi$ -squared probability distribution is presented in Figure 12. This figure indicates that the quoted errors are approximately correct, but that there is an excess of runs in the low probability tail. This effect is probably a result of the fact that the normalization errors do not have a Gaussian distribution. Three runs deserve special comment. The cross section for point 48-2 was computed from



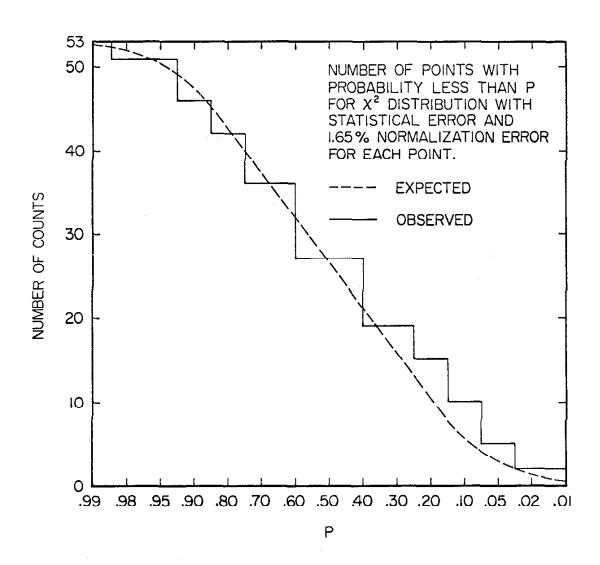


Figure 12

one run because the second run at this point had inconsistencies in beam monitoring which could not be resolved. Point 84-6, which is one of the two points with  $\chi$ -squared probability less than 1%, is a point at which the high energy magnet was in the beam line for one of the two runs, and the two runs disagreed by 10%. Since this effect was not observed for other points, it was assumed that each of the two runs was equally likely to be wrong and thus neither run was thrown away. Point 120-5, which was the other point with probability less than 1%, consisted of three runs. After the first two runs were taken, it was observed that there was a 15% discrepancy for 3% statistics. A third run was taken and the results of this run fell almost exactly at the mean of the two preceeding runs. Thus, there was no way of distinguishing the observed discrepancy at this point from a large statistical fluctuation.

#### D. Tabulation of Data

The data are presented in Tables 7A - 7L, in which the spectrometer lab angle is a constant for each table. The (unfolded) data are also plotted in Figures 13a - 13l, and the spectrometer lab angle is also a constant for each figure. A smooth curve has been drawn through the data on five of these figures. The same smooth curves are also shown on Figures 13m - 13q, along with a representative set of data from other experiments. (9, 12, 13, 15, 16, 37) Since all of the data from this experiment have been plotted in Stan Ecklund's thesis (9), only a small part of the data available from his experiment is shown here.

### TABLES 7A - 7L

## Average and Unfolded Cross Sections

POINT NO. corresponds to the designation of the kine-

matical parameters given in Tables 6-a and 6-b.

THETA LAB is the mean laboratory angle of the spectrometer

in degrees.

K is the mean photon lab energy in MeV.

W is the total c.m. energy in MeV.

THETA C. M. is the pion laboratory angle in degrees.

SIGMA AVERAGE is the measured c.m. cross section in micro-

barns/steradian without resolution corrections.

DSIGMA AVERAGE is the statistical error associated with Sigma

Average (see Section V-F).

SIGMA UNFOLDED is the measured c.m. cross section in micro-

barns/steradian including a correction for the 'tails' of the resolution functions (see Section

V-B).

DSIGMA UNFOLDED is the statistical error associated with Sigma

Unfolded (see Section V-F).

 $\Delta K_{max}$  is the r.m.s. resolution in photon energy in MeV

after correction for the tails of the resolution

functions.

TABLE 7a

AVE	RAGE AND	UNFOLDE	D CROSS	SECTIONS					
POINT NO.	THETA LAB	К	₩	THETA C.M.	SIGMA AVER	DSIGMA AGE	SIGMA UNF	DSIGMA GLUED	<b>∆</b> K RMS
34-3	34.0	 508.	1354.	48.6	9.791	0.254	9.787	 0•289	6.8
34-3	34.0	515.	1359.	48.8	9.349	0.253	9.290	0.281	6.8
34-3	34.0	522.	1364.	48.9	9.607	0.253	9.581	0.280	6.9
34-3	34.0	530.	1369.	49.1	9.321	0.246	9.254	0.273	7.0
34-3	34.0	538.	1374.	49.2	9.661	0.248	9.631	0.275	7.2
34-3	34-0	546	1380	49.4	10-028-	0+245	10-033	0.271	7.4
34-3	34.0	555.	1386.	49.6	9.805	0.234	9.773	0.258	7.8
34-2	34.0	504.	1392.	49.7	10.463	0.266	10.500	0.293	7.6
34-2	34.0	572.	1397.	49.9	9.810	0.262	9.764	0.288	7.6
34-2	34.0	580.	1433.	50.1	10.517	0.266	10-542	0.291	7.7
34-7	<del>34</del> ▼0	589	1409	5û+2	10-680-	-0-263	10+712-	_0+287	_7-9-
34-2	34.0	598.	1415.	50.4	9.776	0.250	9.712	0.271	8.1
34-2	34.0	60A.	1421.	50.6	10.913	0.266	10.955	0.287	8.4
34-2	34.0	617.	1428.	50.8	10.422	0.248	10.411	0.266	8.8
34-1	34.0	629.	1435.	51.0	10.995	0.353	11.017	0.382	8.6
34-1	34+0	638	1441	51+2	_10+536-	0+351	10509	0+379	_8.6-
34-1	34.0	648.	1447.	51.3	10.470	0.341	10.435	0.367	8.8
34-1	34.0	658 •	1454.	51.5	10.684	0.341	10.063	0.365	8.9
34-1	34.0	668.	1461.	51.7	11.094	0.343	11.095	0.365	9.2
34-1	34.0	679.	1468.	51.9	11.931	0.349	11.981	0.370	9.5
34-1	34.0	690 •	1475.	52.1	11.634	0.337	11.650	0.362	10.0

AVE	RAGE AND	UNFOLDED	CROSS	SECTIONS					
POINT NO.	THETA LAB	ĸ	H	THETA	SIGMA AVEF	DSIGMA RAGE		OSIGMA OLDED	۵ K RM
40-3	40.0	525.	1366.	57.0	9.729	0.392	9.761	0.445	7.4
40-3	40.0	533.	1371.	57.1	9.650	0.387	9.672	0.428	7.4
40-3	40.0	540.	1376.	57.3	9.085	0.361	9.046	0.398	7.5
40-3	40.Q	549.	1382.	57.5	8.984	0.370	8.942	0.408	7.7
40-3	40.0	557.	1388.	57.7	8.662	0.346	8.583	0.382	7.9
40-3-	40-0	566	1394.	57.9	8.990	0.356	8-950	0.392	8.1.
40-3	40.0	576.	1400.	58.1	9.384	0.340	9.380	0.374	8.5
40-2	40.0	585.	1407.	58.3	9.146	0.399	9.106	0.436	8.4
40-2	40.0	594.	1412.	58.5	9.693	0.402	9.707	0.438	8.4
40-2	40.U	603.	1418.	58.7	10.406	0.407	10.476	0.442	8.5
_40-2	40-0	613	1425.	58.9	9.615	_0.384	9-600_	_0.415	8.7_
40-2	40.0	623.	1431.	59.1	9.347	0.382	9.301	0.411	9.0
40+2	40.0	633.	1438.	59.3	10.215	0 - 400	10.241	0.427	9-2
40-2	40.0	644.	1445.	59.5	9.684	0.384	9.658	0.407	9-6
40-1	40.0	656.	1453.	59.8	10.667	0.346	10.681	0.374	9.6
-40-1	40-0	666	1459-	60-0	11.126	0.363		_0.391	9.6
40-1	40.0	677.	1466.	60.2	11.392	0.356	11.435	0.382	9.8
40-1	40.0	688.	1473.	60.4	11+269 .	0.351	11.289	0.374	10.0
40-1	40.0	699.	1480.	60.6	11.324	0.346	11.341	0.367	10.3
40-1 -	40.G	711.	1488.	60-9	11.807	357	.11.855	0.377	10.7
46-1	40.0	723.	1496.	61.1	10.389	0.326	10.336	0.348	11.1

TABLE 7c

, , <b>, _</b> ,	NAOL AND	ONFOCIE	D CKU33	SECTIONS					
POINT NO.	THETA LAB	K	W	THETA C.M.	SIGMA AVEF	DSIGMA RAGE		DSTGMA	∆K RMS
48-4	48.0	496.	1345.	66.5	8.940	0.366	8.999	0.421	7.5
48-4	48.0	503.	1350.	66.7	8.036	0.353 .	7.969	0.395	7.5
48-4	48.0	51C.	1356.	66.9	8.716	0.354	8.747	0.395	7.6
48-4	48.0	518.	1361.	67.1	8.207	0.342	8-175	0.382	7.7
48-4	48.0	527.	1367.	67.3	8.239	0.347	8.211	0.389	7.9
48-4	48.0	535	1373	67.5		0.336		0.376	8.2
48-4	48.0	544.	1379.	67.7	8.031	0.320	7.978	0.357	8.5
48-3	48.0	554.	1386.	67.9	7.969	0.365	7.904	0.406	8.5
48-3	48.V	563.	1391.	<b>55∙</b> 1	6.369	0.370	8.350	0.411	8.5
48-3	48.0	571.	1397.	68.3	8.503	0.358	8.494	0.396	8.7
48-3	48.0	581	1404	68.6	8.431	0-366	8.404	0.404	8.8
48-3	48.0	591.	1410.	68.8	8.256	0.354	8.202	0.388	9.1
48-3	48.0	601-	1417_	69-0	9-201	0.377	9.235	0.412	9.4
48-3	48.0	611.	1424.	69.3	8.427	0.351	8.367	0.381	9.8
48-2	48.0	622.	1431.	69.5	9.228	0.437	9.213	0.482	9.8
48-2	48 • G	632 •	1437	69.7	_10-641_	-0.470	-10.770	0.517	9.8
48-2	48.0	642 €	1444.	70.0	9.831	0.452	9.847	0.496	10.0
48-2	48.0	653.	1451.	70.2	9.549	0.441	9.529	0.482	10.2
48-2	48.0	665.	1459.	70.5	9.596	0.427	9.572	0.464	10.5
48-2	48.0	676.	1466.	70.7	10.587	0.452	10.651	0.489	10.9
48-2	48.0	689.	1474.	71.0	10.361	0.430	10.387	0-469	11.4
48-1	48.0	763.	1483.	71.3	10.853	0.285	10.972	0.308	11.4
48-1	48.0	715.	1490.	71.6	10.095	0.278	10.151	0.300	11.5
48-1	48.0	727.	1498.	71.8	10.164	0.271	10.242	0.291	11.7
48-1	48.0	739.	1506.	72.1	9.418	0.253	9.457	0.271	12.0
48-1	48.0	753.	1514.	72.4	7.686	0.229	7.625	0.244	12.4
48-1	48.0	_767	1523	72.7	7.329	0.222	_7_286_	_0-235	12.8
48-1	48.0	781.	1532.	73.0	6.196	0.197	6.096	0.211	13.5

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TABLE 7d

OINT	THETA	к	₩	THETA	SIGMA	DSIGMA	SIGMA	DSIGMA OLDED	ALK RMS
NO.	LAB			C.M.	AVER	AGE	UNF	acoeo	KIIJ
56-4	56.0	525.	1366.	77.0	7.815	0.312	7.843		8.0
56-4	56.0	533.	1371.	77.2	7.455	0.310	7.435	0.345	8.6
56-4	56.0	542.	1377.	77.4	7.693	0.305	7.706	0.339	8.8
56-4	56.0	551.	1383.	77.6	7.143	0.295	7.091	0.328	8.9
56-4	56.0	560.	1390.	77.9	7.293	0.291	7.262	0.323	9.2
56-4-	56+U	570+		78.1	7.237			0.324	
56-4	56.0	580.	1403.	78.4	7.480	0.287	7.467	0.317	9.9
56-3	56.0	592•	1411.	78.6	7.396	0.246	7.341	0.275	9.9
56-3	56.0	601.	1417.	78.9	7.517	0.248	7.469	0.277	10.0
56-3	56.0	611.	1424.	79.1	7.844	0.246	7.827	0-274	10.2
56-3-	56.0	622	1431	79 <del>_4</del> _	8.308	0.255		0.283	10.4
56-3	56.0	633.	1438.	79.6	7.742	0.238	7.687	0.263	10.7
56-3	56.0	645.	1446.	79.9	8.155	0.250	8.137	0.275	11.1
56 <del>-</del> 3	56.0	657.	1454.	80.2	8.855	0.251	8.902	0.275	11.7
56-2	56.0	670.	1462.	80.5	8.434	0.348	8.477	0.385	11.7
56-2-	56.0	682	1469	80.8	9.040_	_0.358	9.154_		
56-2	56.0	694.	1477.	81.0	8.876	0.352	8.965	0.387	12.0
56-2	56.0	706.	1485.	81.3		0.363			12.3
56−2	56.0	720.	1494.	81.6	8.525	0.335	8.591	0.366	12.7
56-2	56.0	734.	1502.	81.9	9.397			0.380	13.2
56-2	56.0	748.	1511.	82.3	7.385	0.299	7.396	0.323	13.9
56-1	56.0	765.	1522•	.82.6	6.976	0.238	7.040	0.258	14.0
56-1	56.0	779.	1530.	82.9	5 • 576 -	0.216		0.233	14-1
50-1	56.0	793.	1539.	83.3	4.918	0.194	4.893	0.209	14.4
56-1	56.0	808.	1548.	83.6	4.006	0 - 172		0.184	14.8
56-1	56.0	825.	1558.	83.9	3.343	0.157	3.286	0.167	15.4
56-1	56.0	841	1568.	84.3	3,103	0.149	3-065		16.0
56-1	56.0	859.	1578.	84.6	2.432	0.133	2.366	0.143	16.8

TABLE 7e

POINT	THETA	K	w	THETA	SIGMA	DSIGMA	SIGMA	DSIGMA	ΔK
NO.	LAB			C.M.	AVER	AGE	UNF	DLDED	RMS
64-5	64.0	496.	1346.	85.4	6.517	0.247	6.513	0.287	8.6
64-5	64.0	504.	1351.	85.7	6.938	0.251	6.996	0.284	8.7
64-5	64.0	513.	1357.	85.9	6.537	0.239	6.534	0.269	8.8
64-5	64.0	521.	1363.	86.1	6.299	0.233	6.265	0.263	9.0
64-5	64.0	531.	1370.	86.3	6.388	0.227	6.370	0.256	9.2
64-5	64.Q	540	_1376-	86-6		0.231	6.594		
64-5	64.0	550.	1383.	86.8	6.344	0.219	6.319	0.246	9.9
64-4	64.0	562.	1391.	87.1	6.572	0.181	6.561	0.205	10.0
64-4	64.0	571.	1397		6.246	0.173	6.184	0.196	10.1
64-4	64.0	581.	1404.	87.6	5.971	0.169	5.865	0.191	10.3
64-4	64-0_	591	_1411	97.9	6.912	<u> </u>	6.933	_0.198	_10.5
64-4	64.0	602.	1418.	88.2	6.334	0.170	6.262	0.191	10.9
64-4	64.0	614.	1425.	88.4		0.168	6.554	0.188	11.2
64-4	64.0	626.	1433.	86.7	6.993	0.169	6.986	0.188	11.8
64-3	64.0	639.	1442.	89.0	7.459	0.219	7.496	0.243	11.9
64-3-	64.0	650	1449-	89.3	7.001	0.215	6.969	0.237	12.0
64-3	64.0	662.	1457.	89.6	7.254	0.216	7.240	0.238	12.2
64-3	64.0		1465.	89.9	7.831	.0.222	_7.864	0.243	12.5
64-3	64.0	688.	1474.	90.2	8.035	0.221	8.074	0.240	13.0
64-3	64.0	702.	1482.	90.5	8.292	. 0 - 233	8.344	0.252	13.4
64-3	64.0	716.	1491.	90.9	8.273	0.222	8.315	0.239	14.0
64-2	64.0	732•	1501.	91.2	7.963	0.245	8.083	0.268	14.3
64-2	64+0	746 •	1510-	91.5		0-230		0.251	14.5
64-2	64.0	760.	1519.	91.8	6.383	0.219	6.399	0.237	14.8
64-2	64.0	776	1528	92•2		_0.199	5.441		15.2
64-2	64.0	792•	1538.	92.5	4.605	0.179	4.549	0.192	15.8
64-2	64.0	800.	1548.	97.9	4.131	0-173	4-080	0.185	<u> 1</u> 6.3
64-2	64.0	826.	1559.	93.3	3.631	0.159	3.580	0.169	16.6
64-1	64.0	847.	1572.		2.765	0.111	2.716	0.120	17.6 17.9
64-1.	64.0	864 <b>-</b>	1582	94-1	2.641_	_0_106	2.612	0.114	18.4
64-1	64.0	882.	1592.	94.4 94.8	2.328	0.099	2.296 2.112	0.100	19-0
64-1-	64-0	901-	1615.	95.2	2.034	0.090	2.011	0.096	19.8
64 <del>-1</del>	64.0	942	1627.	95.6	2.327	0.094	2.333	0.100	20.6
64-1	64.0	964.	1640.	96.0	2.075	0.088	2.064	0.094	21.7
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TABLE 7f

POINT	THETA	к	w	THETA	SIGMA	DS I GMA	SIGMA	DSIGMA	Δĸ
NO.	LAB			C.M.		RAGE		OLDED	RM
74-6	74.0	477.	1333.	95.8	6.076	0.315	6.145	0.371	8.9
74-6	74.0	485.	133A.	96+0	5.672	0.317	5.671	0.363	9.0
74-6	74.0	493.	1344.	96.2	5.595	0.296	5.588	0.337	9.1
74-6	74.0	502.	1350.	96.4	5.758	0.303	5.781	0.346	9.3
74-6	74.0	511.	1356.	96 <b>.7</b>	5.812	0.290	5.849	0.331	9.6
_74-6	74+0		1363	96.9		0.296		0.337	
74~6	74.0	531.	1370.	97.2	5.445	0.272	5.440	0.309	10.3
74~5	74.0	541.	1377.	97.4	5.146	0.238	5.097	0.270	10.4
74~5 74~5	74.0 74.0	550. 560.	1383. 1390.	97.7	5.309	0.232	5.289	0.263	10.5
_74~5 74~5				97.9 98.2	5.368	0.232 0.225	5.361	0.261 0.253	10.7
74~5	74.0	582.	1404.	98.5	5.294	0.221	5.280	0.246	11.3
74~5	74.0	594	1412.	98.7	5.219	0.225	5.190	0.250	11.7
74~5	74.0	606.	1420.	99.0	5.322	0.221	5.302	0.244	12.3
74~4	74.0	620•	1429.	99.4	5.587	0.198	5.556	0.222	12.5
_74-4	74.0	631	1437	99.7	5.690	0.203	_5.662	. 0.227	12.7
74-4	74.0	644.	1445.	100.0	5.848	0.203	5.827	0.226	12.9
74-4	74.0	657.	1453.	100.3	5.999		5.981	0.218	13.3
74~4	74.0	670.	1462.	100.6	6.756	0.206	6.807	0.227	13.7
74-4	, ,	685.	1471.	100.9		0.211	6.934	0.231	14.3
74-4	74.0	700.	1481.	101.2	6.745	0.207	6•759 	0.225	15.0
74~3	74.0	716.	1491.	101.6	7.536	0.201	7.710	0.222	15.3
74-3 74-3	74.0	730	1500.	101.9		0.192		0.211	15.5
74-3	74.0 74.0	746. 762.	1510. 1520.	102.3	6.256	0.181 .0.171	6.297 5.692	0.198 0.186	15.9
74-3	74.0	779.	1530.	103.0	5.690. 5.101	0.157	5.083	0.170	16.4 17.0
74-3_	74.0	797				0.152		_0.164	
74-3	74.0	816.	1553.	103.8	3.825	0.137	3.758	0.146	18.3
74-2	74.0	836.	1565.	104.2	3.298	0.151	3.264	0.166	19.2
74-2	74.0	854.		104.5		. 0.150		0.165	
74-2	74.0	873.	1587.	104.9	2.487	0.133	2.429	0.145	20.1
74-2	74-0_	894-			2.639			0-146	20.8
74-2	74.0	915.	1612.	105.7	2.622	0.129	2.612	0.140	21.7
	74.0					_0.131			
74-2	74.0	962•	1639.	106.6	2.515	0.127	2.511	0.136	24.1
74-1	74-0	991.	1655.	107.1	2.829	0.157	2.875	0.169	24.9
74=1	74.0	_1014	-1668.	_107.6		_0.148	_2-404_		25.5
74-1	74.0	1039.	1682.	108.0	2.126	0.133	2.131	0.142	26.3
74-1		1065				.0.123			27-2
74-1	74.0 74.0	1093. 1123.	1712.	108.9	1.331	0.112	1.309	0.118	28.1
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73 TABLE 7g

AVERAGE AND UNFOLDED CROSS SECTIONS

POINT NO.	THETA LAB	K	Ж	THETA C.M.	SIGMA AVER	DSIGMA LAGE	SIGMA UNF	DSIGMA FOLDED	ΔK RM
					•				
84-6	84.0	487.	1339.	106.2	4.749	0.218	4.792	0.258	9.9
84-6	84.0	496.	1345.	106.4	4.279	0.204	4.243	0.234	10.0
84-6	84.0	505.	1352.	106.6	4.662	0.208	4.693	0.237	10.2
84-6	84.0	514.	1358.	106.8	4.268	0.196	4.240	0.223	10.4
84-6	84.0	524.	1365.	107.1	4.254	0.187	4.227	0.213	10.7
_84-6	84.0_	535 • _		167.3	4.323	0.186	_4.309	0.212	11.0
84-6	84.0	545.	1380.	107.6	4.039	0.177	3.980	0.202	11.5
84-5	84.0	556.	1387.	107.9	4.719	0.174	4.744	0.200	11.8
84-5	84.0	567.	1394.	108.1	4.464	0.173	4.441	0.199	11.9
84-5	84.0	578.	1402.	108.4	3.902	0.162	3.786	0.185	12.1
84-5	84.0_	589	1409	108.7	4.362	_0.162	_4.313	_0.185	12.4
84-5	84.0	602.•	1418.	109.0	4.436	0.161	4.389	0.183	12.9
84-5	84.0	615.	1426.	109.3	.4.735	0.171	4.718	0.194	13.3
84-5	84.0	628.	1435.	109.6	4.537	0.163	4.479	0.183	14.0
84-4	84.0	645.	1446.	109.9	5.279	0.222	5.324	0.252	14-4
84-4	84.0	658	1454	110+2	5.418_	0.230	_5.468.	0.261	14.6
84-4	84.0	672.	1463.	110.5	5.214	0.218	5.223	0.246	15.0
84-4	84.0	687.	1473.	110.9	-5.928	0.228	6.025	0.256	15.4
84-4	84.0	702.	1483.	111.2	5.776	0.223	5.842	0.250	16.0
84-4	84.0	719.	1493.	111.6	6.329	0.233	6.458	0.259	16.7
84-4	84.0	736.	1504.	111.9	5.728	0.219	5.783	0.242	17.6
84-3	84.0	756.	1516.	112.3	5,595	0.216	5.697	0.241	18.1
84-3	84.0	773.	1526.	112.7	5.032	0.204	5.084	0.227	18.4
84-3	84.0	791.	1537.	113.0	4.276	0.181	4.261	0.200	19.0
84-3	84.0	810.	1549.	113.4	3.739	0.173	3.696	0.191	19.6
84-3	84.0	830.	1561.	113.8	3.499	0.160	3.463	0.175	20.5
84-3	R4+C	R51.	1574.	114.2	2.980	0.157	2.919	_0.171	.21.4
84-3	84.0	874.	1587.	114.6	2.909	0.143	2.868	0.155	22.7
84-2	84.0	896.	1601.	115.0	2.823	0.150	2.803	0.166	23.4
84-2	84.0	918	1613.	115.4	2.942	0.156	_2.952.	0.172	24.0
84-2	84.0	941.	1627.	115.8	2.903	0.147	2.914	0.161	24.8
84-2	84+0	966.	1641		3-048_	0.150	3.083	0.164	25.8.
84-2	84.0	993.	1656.	116.7	3.028	0.146	3.066	0.158	27.1
84-2	- 84.0	1021.	1672.	117.2	2.973_	_0.150	3.018	0.162	28.5
84-2	84.0	1051.	1689.	117.7	2.418	0.133	2.425	0.143	30.3
84-1	84.0	1085.	1707.	118.2	1.636	0.087	1.624	0.094	31.6
84-1-	84_C	_1114	1724	118.7	1.054	0.076	1.016_		32.6
84-1	84.0	1146.	1741-	119-2	0.800	0.068	0.765	0.073	34.0
84-1	84.C		1759.			-0.061			35.5
84-1	84.0	1216.	1778.	120.2	0.432	0.058	0.407	0.062	37.5
84-1	84.0		1799.		0.391		0.375	0.059	39.3
84-1	84.0	1297.	1820.	121.3	0.377	0.058	0.366	0.062	39.4

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TABLE 7h

AVE	KAGE AND	UNFOLDED	CK022	2ECLION2					
POINT NO.	THETA LAB	. <b>K</b>	W	THETA C.M	SIGMA	DSIGMA RAGE	SIGMA	DSIGMA	A K RMS
94-5	94.0	532.	1371.	116.7	4.151	0.215	4.162	0.254	11.9
94~5	94.0	542.	1378.	116.9	3.952	0.216	3.931	0.248	12.1
94-5	94.0	553.	1385.	117.2	3.720	0.204	3.666	0.233	12.3
94-5	94.0	565.	1393.	117.4	3.535	. 0.200	3.452	0.228	12.6
94~5	94.0	577.	1401.	117.7	3.435	0.189	3.333	0.216	13.1
_ 94~5	94.0	590.	1410.	118+0	4-202	0.207	_4.214_	_0-236	13-5_
94~5	94.0	603.	1419.	118.5	4.109	0.195	4.093	0.222	14.2
94-4	94.0	617.	1427.	118.6	4.166	0.202	4.156	0.232	14.6
94~4			1436.			0.200	_4.021	0.229	14.8
94-4	94.0	643.	1445.	119.1	4.226	0.203	4.211	0.232	15.2
94-4	94-0	658	1454.	119.4	4.629	_0-206	_4.664		15-6-
94-4	94.0	674.	1464.	119.7	4.617	0.203	4.640	0.230	16.2
94~4	94+0		_1475		5.416		5.539		16.9
94~4	94.0	708.	1486.	120.4	4.885	0-203	4.927	0.228	17.9
94-3	94.0	729.	1499.	120.8	5.610	0.233	5.793	0.263	16.5
_94-3_	94.0	746	1510.	121-2	4.504	_0.215	4.533	0.242	18-9
94~3	94.0	764.	1521.	121.5	4.232	0.204	4.243	0.229	19.5
94~3	94•0			121.9	4.087_	_0.197	_4.099_	_0.220	20.2
94~3	94.0	804.	1545.	122.2	3.648	0.183	3.627	0.203	21.1
94~3	<u> </u>	825	1558		3.244_	_0.176	_3.199_		22.1
94-3	94.0	848.	1572.	123.0	2.929	0.162	2.873	0.178	23.5
94-2	94.0	875.	1588.	123.5	2.938	0.156	2.914	0.174	24.4
_94~2	94.0	898	1601.	123.9	3.022_	_0.160	_3.023	0 • 1.78	25-1
94~2	94.0	922•	1616.	124.3	3.009	0.156	3.015	0.173	26.0
_94-2	94.0	948		124_7	2.842	_0.153		.0.169	27.1
94-2	94.0	976.	1647.	125.1	3.456	0.159	3.523	0.174	28.5
94-2	94+0	_1006	1664	125.6	3.279	_0.155	3.334_	_0-169	30-2_
94~2	94.0	1038.	1682.	126.1	2.809	0.143	2.827	0.155	32.2
94-1	94.0	1070.	1699.	126.6	2.207	0.110	2.220	0.120	33.5
_94~1	94.0		1717.	127.0	_1.678_	0.098		_0.107	34-7
94~1	94.0	1135.	1735.	127.5	1.006	0.085	0.951	0.092	36.3
94-1	94.0	_1172	1755.	128-0	0.758	0.073	0.708	0.079	38-1
94-1	94.0	1212.	1776.	128.5	0.630	0.070	0.592	0.075	40.4
_94-1_	94.0	1254	1798.	129+0	_0.592_	_0.070	0.567	_0-074	42-3
94-1	94.0	1300.	1822.	129.6	0.533	0.072	0.513	0.077	41.8

TABLE 7i

_				TAI	BLE 71				
AVE	RAGE AND	UNFOLDE	D CROSS	SECTIONS					
POINT NO.	THETA LAB	к	н	THETA	SIGMA AVE	DSIGMA RAGE	SIGMA UNF	DSIGMA OLDED	A K
106-5	106.0	512.	 1357•	126.7	3.773	0.190	3.791	0.228	12.3
106-5	106.0	522.	1364.	126.9	3.948	0.192	3.999	0.223	12.5
106-5	106.0	533.	1371.	127.1	3.639	0.178	3.637	0.206	12.7
106-5	106.0	544.	1379.	127.4	3.399	0.178	3.361	0.206	13.0
106-5	106.0	556.	1387.	127.6	3.006	0.164	2.904	0.190	13.4
106-5	106.0	569.	1396	127+9_	3.491	0.167	3.479		13.9.
106-5	106.0	582.	1405.	128.1	3.450	0.167	3.426	0.194	14.5
106-4	106.0	597.	1415.	128.4	3.441	0.180	3.410	0.209	15.1
106-4	106.0	611.	1423.	128.7	3.636	0.189	3.635	0.219	15.3
106-4	106.0	624.	1432.	129.0	3.284	0.171	3.218	0.198	15.7
106-4	106-0_	639+	1442	129+2_	3.606_		_3.591_	_0.197	16.2
106-4	106.0	655.	1453.	129.5	3.873	0.178	3.895	0.204	16.9
106-4	106-0	672.	1463.	129+8					17.6
106-4	106.0	690.	1475.	130.1	4.118	0.183	4.157	0.208	18.6
106-3	106.0	708.	1486.	130.5	4.931	0.234	5.115	0.268	19.2
106=3_	106-0	725		130-8	4.479			_0.262	19.6.
106-3	106.0	743.	1508.	131.1 —131.4—	4.486 3.489	0.219	4.596	0.249	20.3
	106.0	785 •	1534.		3.839	0.199	3.463 3.884	0.220	
106-3 106 <b>-</b> 3	106.0 106.0			131.7		_0.199	_2.987	0.223	22.0
106-3	106.0	831.	1562.	132.5	2.567	0.159	2.487	0.176	24.6
106-2	106.0	861.	1580.	132.9	2.759	0.168	2.737	0.189	25.8
106-2			1594			0.169		0.190	26.5
106-2	106.0	910.	1609.	133.7	2.648	0.159	2.627	0.177	27.6
106-2	106.0		1625.	134.1			2.956	0.178	28.9
106-2	106.0	968.	1642.	134.5	2.846	0.158	2.862	0.174	30.5
106-2	106.0	_1000-		134.9		0.163	2.852		32.4.
06-2	106.0	1035.	1680.	135.4	3.031	0.166	3.079	0.180	34.8
06-1	106.0	1075.	1702.	135.9	2.341	0.121	2.368	0.133	36.6
			1721			0.103		.0.113	
106-1	106.0	1147.	1742.	136.8	1.104	0.090	1.042	0.098	40.0
106-1-	106.0	1189	1764	<del>_137-2</del> _	1.048		_1.004_		42.2
106-1	106.0	1234.	1787.	137.7	1.053	0.084	1.028	0.090	44.7
	106.0		1813	138.3	0.797_	_0.082	_0.764_		.44.9
106-1	106.0	1334.	1840.	138.8	0.764	0.097	0.734	0.106	44.9
		·			<del></del>		<del></del>		
			······································			<del></del>	·		

TABLE 7j

POINT NO.	THETA LAB	K	W	THETA C.M.	SIGMA AVEF	DSIGMA RAGE	SIGMA	OSIGMA OLDED	<b>∆</b> K RM
120-5	120.0	492•	1343.	137.7	3.467	0.180	3.510	0.216	12.6
120-5	120-0	501-	1349.	137.9	3.163	0.165	3-148	0.192	12.7
120-5	120.0	512.	1357.	138 • 1	3.505	0.173	3.554	0.200	13.0
120-5	120.0	523.	1365.	138.3	3.292	0.166	3.307	0.191	13.3
120-5	120.0	535.	1373.	138.5	3.257	0.160	3.270	0.184	13.7
120-5	120.0_	548	1381	138_7	2.838	155	_2.788 _	0.178	14-2
120-5	120.0	561·	1390.	138.9	3.168	0.153	3.182	0.174	14.9
120-4	120.0	577.	1401.	139.1	2.805	0.161	2.741	0.187	15.5
120-4	120.0	<b>590.</b>	1410.	139.4	2.679	0.166	2.597	0.192	15.8
120-4	120.0	604.	1419.	139.6	3.304	0.174	3.327	0.201	16.2
120-4-	120.0	619+_	1429	139-8		_0.163		.0.187	.16.7
120-4	120.0	635.	1439.	140.1	3.195	0.165	3.189	0.188	17.4
	120.0	651.	1450.	140.3		0.166	2.973	0.188	18.1
120-4	120.0	669.	1462.	140.6	3.482	0.170	3.504	0.191	19•1
120-3	120.0	690•	1475.	140.9	3.577	0.185	3.620	0.210	20.0
120-3-	_120.0_	707•		141-2	3.887_			.0.217	20.5.
120-3	120.0	726.	1498.	141.4	3.718	0.182	3.774	0.205	21-1
	120.0	747.		141.7			.3.575	0.193	21.9
120-3	120.0	769.	1524.	142.0	3.384	0.164	3.405	0.182	23.0
	120.0	792.	1539.	142.3	2.550		2.483	0.173	23.9
120-3	120.0	818.	1554.	142.6	2.625	0.147	2.583	0.161	23.8
120-2	120.0	843.	1569.	143.0	2.424	0.174	2.377	0.198	27.0
120-2		868.	1584.		2.656		2-654	0.196	27.9
120-2	120+0	895.	1600.	143.6	2.557	0.165	2.543	0.186	29.0
120-2	120.0	924			2.576		2.574	0.178	30.5
120-2	120.0	956+	1635.	144.3	2.598	0.168	2.601	0.187	32.3
120-2-	120.0	990+		_144-7_	2.686		_2-708_	0.190	.34.4
120-2	120.0	1027.	1675.	145-1	2.795	0.167	2.834	0.183	37.1
20-1	120-0	1073.	1701.	145.6	2-212	0-140	2-229	0.155	39.4
	_120.0		_ 1722•		1.771			0.146	41.2
120-1	120.0	1152.	1744.	146.3	1.547	0.121	1.524	0.133	43.4
20-1-	120.0	1197-	1768	146-8-		-0-105		0-114	46-1-
20-1	120.0	1247.	1795.	147.2	0.794	0.094	0.735	0.102	48.3
20-1		1301			0.874	_0-109	-0.838	-	
20-1	120.0	1361.	1853.	148.2	0.747	0.129	0.698	0.143	54.5
							V		

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TABLE 7k

NO. LAB  C.M. AVERAGE  UNFOLDED  134-4 134.0 541. 1377. 149.0 3.046 0.139 3.059 0.167 15. 134-4 134.0 554. 1385. 149.1 2.701 0.138 2.651 0.160 15. 134-4 134.0 567. 1394. 149.3 2.837 0.135 2.815 0.156 15. 134-4 134.0 581. 1403. 149.5 2.876 0.137 2.860 0.158 16. 134-4 134.0 596. 1413. 149.7 2.995 0.134 2.997 0.154 16. 134-4 134.0 696. 1413. 149.7 2.995 0.134 2.997 0.154 16. 134-4 134.0 628. 1435. 150.1 2.688 0.124 2.636 0.142 18. 134-3 134.0 668. 1448. 150.3 2.990 0.151 3.003 0.175 19. 134-3 134.0 665. 1459. 150.5 3.200 0.153 3.246 0.178 19. 134-3 134.0 683. 1470. 150.7 3.238 0.158 3.285 0.182 20. 134-3 134.0 722. 1482. 150.9 3.570 0.154 3.673 0.177 21. 134-3 134.0 723. 1496. 151.2 3.280 0.147 3.333 0.168 22. 134-3 134.0 723. 1496. 151.2 3.280 0.147 3.333 0.168 22. 134-3 134.0 769. 1524. 151.7 2.785 0.132 2.783 0.148 25.  134-2 134.0 826. 1555. 152.2 2.131 0.127 2.064 0.145 27. 134-2 134.0 826. 1555. 152.2 2.131 0.127 2.064 0.145 27. 134-2 134.0 874. 1588. 152.7 2.503 0.130 2.509 0.146 28. 134-2 134.0 905. 1606. 153.0 2.503 0.127 2.511 0.142 31. 134-2 134.0 974. 1588. 152.7 2.503 0.127 2.511 0.142 31. 134-2 134.0 974. 1588. 152.7 2.503 0.127 2.511 0.142 31. 134-2 134.0 974. 1687. 154.5 153.9 2.491 0.128 2.500 0.142 33. 134-1 134.0 1010. 1666. 153.9 2.503 0.127 2.511 0.142 31. 134-1 134.0 1010. 1666. 153.9 2.503 0.127 2.511 0.142 31. 134-1 134.0 1017. 1687. 154.5 1.703 0.880 1.692 0.086 39. 134-1 134.0 1017. 1687. 154.5 1.703 0.880 1.692 0.096 39. 134-1 134.0 1017. 1687. 154.5 1.703 0.880 1.692 0.096 39. 134-1 134.0 1017. 1687. 154.5 1.703 0.080 1.692 0.096 39. 134-1 134.0 1017. 1687. 154.5 1.703 0.080 1.692 0.096 39. 134-1 134.0 1017. 1687. 154.5 1.703 0.080 1.692 0.096 39. 134-1 134.0 1017. 1687. 155.5 1.703 0.080 1.692 0.096 39. 134-1 134.0 1017. 1687. 155.5 1.703 0.080 1.692 0.0973 48. 134-1 134.0 1179. 1759. 155.5 1.703 0.087 1.008 0.073 48. 134-1 134.0 1179. 1759. 155.5 1.700.67 1.008 0.073 48.										
NO. LAB  C.M. AVERAGE  UNFOLDED  134-4 134.0 541. 1377. 149.0 3.046 0.139 3.059 0.167 15. 134-4 134.0 554. 1385. 149.1 2.701 0.138 2.651 0.156 15. 134-4 134.0 567. 1394. 149.3 2.837 0.135 2.815 0.156 15. 134-4 134.0 581. 1403. 149.5 2.876 0.137 2.860 0.158 16. 134-4 134.0 596. 1413. 149.7 2.995 0.134 2.997 0.154 16. 134-4 134.0 628. 1435. 150.1 2.688 0.124 2.636 0.142 18. 134-3 134.0 628. 1435. 150.1 2.688 0.124 2.636 0.142 18. 134-3 134.0 648. 1448. 150.3 2.990 0.151 3.003 0.175 19. 134-3 134.0 665. 1459. 150.5 3.200 0.153 3.246 0.178 19. 134-3 134.0 6683. 1470. 150.7 3.238 0.158 3.285 0.182 20. 134-3 134.0 7.22. 1482. 150.9 3.570 0.154 3.673 0.177 21. 134-3 134.0 723. 1496. 151.2 3.280 0.147 3.333 0.168 22. 134-3 134.0 769. 1524. 151.7 2.785 0.132 2.783 0.148 25. 134-2 134.0 796. 1541. 151.9 2.413 0.136 2.377 0.156 26. 134-2 134.0 846. 1571. 152.4 2.838 0.141 2.831 0.160 23. 134-3 134.0 796. 1541. 151.9 2.413 0.136 2.377 0.156 26. 134-2 134.0 846. 1571. 152.4 2.204 0.129 2.160 0.146 28. 134-2 134.0 905. 1606. 153.0 2.503 0.127 2.511 0.142 31. 134-2 134.0 905. 1606. 153.0 2.503 0.127 2.511 0.142 31. 134-2 134.0 905. 1606. 153.0 2.503 0.127 2.511 0.142 31. 134-2 134.0 905. 1606. 153.0 2.503 0.127 2.511 0.142 31. 134-2 134.0 905. 1606. 153.0 2.503 0.127 2.511 0.142 31. 134-1 134.0 1010. 1666. 153.9 2.358 0.093 2.509 0.142 33. 134-1 134.0 1010. 1666. 153.9 2.358 0.093 2.500 0.142 33. 134-1 134.0 1010. 1666. 153.9 2.358 0.093 2.500 0.142 33. 134-1 134.0 1010. 1666. 153.9 2.503 0.127 2.511 0.142 31. 134-1 134.0 1010. 1666. 153.9 2.503 0.127 2.511 0.142 31. 134-1 134.0 1010. 1666. 153.9 2.503 0.127 2.511 0.142 31. 134-1 134.0 1010. 1666. 153.9 2.500 0.144 2.174 0.136 35.	AVER	RAGE AND	UNFOLDED	CROSS	SECTIONS					
134-4       134.0       554.       1385.       149.1       2.701       0.138       2.651       0.160       15.134-4       134.0       567.       1394.       149.3       2.837       0.135       2.815       0.156       15.134-4       134.0       581.       1403.       149.5       2.876       0.137       2.880       0.158       16.15.15.15.15.1       16.134-4       134.0       596.       1413.       149.7       2.995       0.134       2.997       0.154       16.15.15.15.1       16.15.15.15.15.15.15.15.15.15.15.15.15.15.			<b>к</b>	· #						<b>∆</b> K RF
134-4       134.0       554.       1385.       149.1       2.701       0.138       2.651       0.160       15.134-4       134.0       567.       1394.       149.3       2.837       0.135       2.815       0.156       15.134-4       134.0       581.       1403.       149.5       2.876       0.137       2.880       0.158       16.15.15.15.15.1       2.995       0.134       2.997       0.154       16.15.15.15.1       16.15.15.15.15.15.15.15.15.15.15.15.15.15.	134-4	134.0	541.		149-0	3-046	0-139	 3.050	0.167	15.2
134-4       134.0       567.       1394.       149.3       2.837       0.135       2.815       0.156       15.134-4       134.0       581.       1403.       149.5       2.876       0.137       2.860       0.158       16.134-4       134.0       596.       1413.       149.7       2.995       0.134       2.997       0.154       16.134-4       134.0       601.       1424-149.9       3.020       0.132       3.023       0.151       17.134-4       134.0       628.       1435.       150.1       2.688       0.124       2.636       0.142       18.134-3       134.0       648.       1448.       150.3       2.990       0.151       3.003       0.175       19.134-3       134.0       665.       1459.       150.5       3.200       0.153       3.246       0.178       19.134-3       134.0       663.       1470.       150.7       3.238       0.158       3.285       0.182       20.134-3       134.0       762.       1482.       150.9       3.570.       0.154       3.673.       0.177       21.343.       0.147       3.333.       0.168       22.134.       134.0       745.       1509.       151.4       2.838.       0.147       3.333.       0.168       22.134.       0.148										15.5
134-4       134.0       596.       1413.       149.7       2.995       0.134       2.997       0.154       16. 134-4       134.0       611.       1424.       149.9       3.020       0.132       3.023       0.151       17. 17. 134-4       134.0       628.       1435.       150.1       2.688       0.124       2.636       0.142       18.         134-3       134.0       648.       1448.       150.3       2.990       0.151       3.003       0.175       19. 134-3       134.0       665.       1459.       150.5       3.200       0.153       3.246       0.178       19. 134-3       134.0       663.       1470.       150.7       3.238       0.158       3.285       0.182       20. 134-3       134.0       70.2       1482.       150.9       3.570       0.154       3.673       0.177       21. 134-3       134.0       723.       1496.       151.2       3.280       0.147       3.333       0.168       22. 134-3       134.0       745.       1509.       151.4       2.838       0.141       2.831       0.160       23. 134-3       134.0       796.       1541.       151.9       2.413       0.136       2.377       0.156       26. 134-2       134.0       866.			567.	1394.						15.8
134-4 134-0 611 1424 149-9 3.020 0.132 3.023 0.151 17. 134-4 134.0 628. 1435. 150.1 2.688 0.124 2.636 0.142 18.  134-3 134.0 648. 1448. 150.3 2.990 0.151 3.003 0.175 19. 134-3 134.0 665. 1459. 150.5 3.200 0.153 3.246 0.178 19. 134-3 134.0 683. 1470. 150.7 3.238 0.158 3.285 0.182 20. 134-3 134.0 762. 1482. 150.9 3.570 0.154 3.673 0.177 21. 134-3 134.0 723. 1496. 151.2 3.280 0.147 3.333 0.168 22. 134-3 134.0 745. 1509. 151.4 2.838 0.141 2.831 0.160 23. 134-3 134.0 769. 1524. 151.7 2.785 0.132 2.783 0.148 25.  134-2 134.0 820. 1555. 152.2 2.131 0.127 2.064 0.145 27. 134-2 134.0 846. 1571. 152.4 2.204 0.129 2.160 0.146 28. 134-2 134.0 874. 1588. 152.7 2.503 0.130 2.509 0.146 29. 134-2 134.0 905. 1606. 153.0 2.503 0.127 2.511 0.142 31. 134-2 134.0 938. 1625. 153.3 2.491 0.128 2.500 0.142 33. 134-2 134.0 974. 1646. 153.6 2.195 0.124 2.174 0.136 35.  134-1 134.0 1010. 1666. 153.9 2.358 0.093 2.407 0.105 38. 134-1 134.0 1047. 1687. 154.5 1.703 0.080 1.692 0.096 39. 134-1 134.0 1087. 1709. 154.5 1.703 0.080 1.692 0.096 39. 134-1 134.0 1087. 1709. 154.5 1.703 0.080 1.692 0.096 39. 134-1 134.0 1179. 1759. 155.5 1.116 0.067 1.088 0.073 51.	134-4	134.0	581.	1403.	149.5	2.876	0.137	2.860	0.158	16.3
134-4       134.0       628.       1435.       150.1       2.688       0.124       2.636       0.142       18.         134-3       134.0       648.       1448.       150.3       2.990       0.151       3.003       0.175       19.         134-3       134.0       665.       1459.       150.5       3.200       0.153       3.246       0.178       19.         134-3       134.0       683.       1470.       150.7       3.238       0.158       3.285       0.182       20.         134-3       134.0       702.       1482.       150.9       3.570       0.154       3.673       0.177       21.         134-3       134.0       723.       1496.       151.2       3.280       0.147       3.333       0.168       22.         134-3       134.0       745.       1509.       151.4       2.838       0.141       2.831       0.160       23.         134-2       134.0       796.       1541.       151.9       2.413       0.136       2.377       0.156       26.         134-2       134.0       86.       1571.       152.4       2.204       0.127       2.160       0.145       27.	134-4	134.0	596.	1413.	149.7	2.995				16.9
134-3       134.0       648.       1448.       150.3       2.990       0.151       3.003       0.175       19.         134-3       134.0       665.       1459.       150.5       3.200       0.153       3.246       0.178       19.         134-3       134.0       683.       1470.       150.7       3.238       0.158       3.285       0.182       20.         134-3       134.0       762.       1482.       150.9       3.570       0.154       3.673       0.177       21.         134-3       134.0       723.       1496.       151.2       3.280       0.147       3.333       0.168       22.         134-3       134.0       745.       1509.       151.4       2.838       0.141       2.831       0.160       23.         134-3       134.0       769.       1524.       151.7       2.785       0.132       2.783       0.148       25.         134-2       134.0       796.       1541.       151.9       2.413       0.136       2.377       0.156       26.         134-2       134.0       826.       1555.       152.2       2.131       0.127       2.064       0.145       27.										17.6
134-3       134.0       665.       1459.       150.5       3.200       0.153       3.246       0.178       19.134-3       134.0       683.       1470.       150.7       3.238       0.158       3.285       0.182       20.134-3       134.0       762.       1482.       150.9       3.570       0.154       3.673       0.177       21.134-3       21.134.0       723.       1496.       151.2       3.280       0.147       3.333       0.168       22.134-3       134.0       745.       1509.       151.4       2.838       0.141       2.831       0.160       23.134-3       134.0       769.       1524.       151.7       2.785       0.132       2.783       0.148       25.         134-2       134.0       796.       1541.       151.9       2.413       0.136       2.377       0.156       26.134-2       2.340.0       820.       1555.       152.2       2.131       0.127       2.064       0.145       27.134-2       134.0       846.       1571.       152.4       2.204       0.129       2.160       0.146       28.134-2       134.0       874.       1588.       152.7       2.503       0.130       2.509       0.146       29.134-2       134.0       938.       162	134-4	134.0	628.	1435.	150.1	2.688	0.124	2.636	0.142	18.6
134-3       134.0       683.       1470.       150.7       3.238       0.158       3.285       0.182       20.         134-3       134.0       762.       1482.       150.9       3.570       0.154       3.673       0.177       21.         134-3       134.0       723.       1496.       151.2       3.280       0.147       3.333       0.168       22.         134-3       134.0       745.       1509.       151.4       2.838       0.141       2.831       0.160       23.         134-3       134.0       769.       1524.       151.7       2.785       0.132       2.783       0.148       25.         134-2       134.0       796.       1541.       151.9       2.413       0.136       2.377       0.156       26.         134-2       134.0       826.       1555.       152.2       2.131       0.127       2.064       0.145       27.         134-2       134.0       874.       1588.       152.7       2.503       0.129       2.160       0.146       28.         134-2       134.0       905.       1606.       153.0       2.503       0.127       2.511       0.142       31.										19.5
134-3       134.0       7C2.       1482.       150.9       3.570       0.154       3.673       0.177       21.         134-3       134.0       723.       1496.       151.2       3.280       0.147       3.333       0.168       22.         134-3       134.0       745.       1509.       151.4       2.838       0.141       2.831       0.160       23.         134-3       134.0       769.       1524.       151.7       2.785       0.132       2.783       0.148       25.         134-2       134.0       796.       1541.       151.9       2.413       0.136       2.377       0.156       26.         134-2       134.0       820.       1555.       152.2       2.131       0.127       2.064       0.145       27.         134-2       134.0       846.       1571.       152.4       2.204       0.129       2.160       0.146       28.         134-2       134.0       874.       1588.       152.7       2.503       0.130       2.509       0.146       29.         134-2       134.0       938.       1625.       153.3       2.491       0.128       2.511       0.142       31.										19.9
134-3       134.0       723.       1496.       151.2       3.280       0.147       3.333       0.168       22.         134-3       134.0       745.       1509.       151.4       2.838       0.141       2.831       0.160       23.         134-3       134.0       769.       1524.       151.7       2.785       0.132       2.783       0.148       25.         134-2       134.0       796.       1541.       151.9       2.413       0.136       2.377       0.156       26.         134-2       134.0       820.       1555.       152.2       2.131       0.127       2.064       0.145       27.         134-2       134.0       846.       1571.       152.4       2.204       0.129       2.160       0.146       28.         134-2       134.0       874.       1588.       152.7       2.503       0.130       2.509       0.146       29.         134-2       134.0       905.       1606.       153.0       2.503       0.127       2.511       0.142       31.         134-2       134.0       974.       1646.       153.3       2.491       0.128       2.500       0.142       33.										20.6
134-3       134.0       745.       1509.       151.4       2.838       0.141       2.831       0.160       23.134-3       134.0       769.       1524.       151.7       2.785       0.132       2.783       0.148       25.         134-2       134.0       796.       1541.       151.9       2.413       0.136       2.377       0.156       26.         134-2       134.0       820.       1555.       152.2       2.131       0.127       2.064       0.145       27.         134-2       134.0       846.       1571.       152.4       2.204       0.129       2.160       0.146       28.         134-2       134.0       874.       1588.       152.7       2.503       0.130       2.509       0.146       29.         134-2       134.0       905.       1606.       153.0       2.503       0.127       2.511       0.142       31.         134-2       134.0       938.       1625.       153.3       2.491       0.128       2.500       0.142       33.         134-2       134.0       974.       1646.       153.6       2.195       0.124       2.174       0.136       35.         134-1										21.4
134-3       134.0       769.       1524.       151.7       2.785       0.132       2.783       0.148       25.         134-2       134.0       796.       1541.       151.9       2.413       0.136       2.377       0.156       26.         134-2       134.0       826.       1555.       152.2       2.131       0.127       2.064       0.145       27.         134-2       134.0       846.       1571.       152.4       2.204       0.129       2.160       0.146       28.         134-2       134.0       874.       1588.       152.7       2.503       0.130       2.509       0.146       29.         134-2       134.0       905.       1606.       153.0       2.503       0.127       2.511       0.142       31.         134-2       134.0       938.       1625.       153.3       2.491       0.128       2.500       0.142       33.         134-2       134.0       974.       1646.       153.6       2.195       0.124       2.174       0.136       35.         134-1       134.0       1010.       1666.       153.9       2.358       0.093       2.407       0.105       38.		-								
134-2       134.0       796.       1541.       151.9       2.413       0.136       2.377       0.156       26.         134-2       134.0       820.       1555.       152.2       2.131       0.127       2.064       0.145       27.         134-2       134.0       846.       1571.       152.4       2.204       0.129       2.160       0.146       28.         134-2       134.0       874.       1588.       152.7       2.503       0.130       2.509       0.146       29.         134-2       134.0       905.       1606.       153.0       2.503       0.127       2.511       0.142       31.         134-2       134.0       938.       1625.       153.3       2.491       0.128       2.500       0.142       33.         134-2       134.0       974.       1646.       153.6       2.195       0.124       2.174       0.136       35.         134-1       134.0       1010.       1666.       153.9       2.358       0.093       2.407       0.105       38.         134-1       134.0       1047.       1687.       154.2       1.992       0.086       2.002       0.096       39. <td></td>										
134-2       134.0       820.       1555.       152.2       2.131       0.127       2.064       0.145       27.134.0       27.134.0       846.       1571.       152.4       2.204       0.129       2.160       0.146       28.134.0       2.509       0.146       29.134.0       2.509       0.146       29.134.0       2.509       0.146       29.134.0       2.509       0.146       29.134.0       2.500       0.146       29.134.0       2.500       0.142       31.134.2       31.134.0       938.       1625.       153.3       2.491       0.128       2.500       0.142       33.134.2       134.0       974.       1646.       153.6       2.195       0.124       2.174       0.136       35.134.2       134.0       1010.       1666.       153.9       2.358       0.093       2.407       0.105       38.134.1       134.0       1047.       1687.       154.2       1.992       0.086       2.002       0.096       39.134.1       134.0       1087.       1709.       154.5       1.703       0.080       1.692       0.089       42.134.1       134.0       1131.       1733.       154.8       1.255.       0.070       1.208       0.077       44.134.1       134.0       1179.       1759.	134-3	134.0	1044	17240	151+1	2.109	U+132	2.103	0.140	23+1
134-2     134-0     846.     1571.     152-4     2-204     0-129     2-160     0-146     28.       134-2     134.0     874.     1588.     152.7     2-503     0-130     2-509     0-146     29.       134-2     134.0     905.     1606.     153.0     2-503     0-127     2-511     0-142     31.       134-2     134.0     938.     1625.     153.3     2-491     0-128     2-500     0-142     33.       134-2     134.0     974.     1646.     153.6     2-195     0-124     2-174     0-136     35.       134-1     134.0     1010.     1666.     153.9     2.358     0.093     2-407     0-105     38.       134-1     134.0     1047.     1687.     154.2     1.992     0.086     2.002     0.096     39.       134-1     134.0     1087.     1709.     154.5     1.703     0.080     1.692     0.089     42.       134-1     134.0     1179.     1759.     155.5     1.057     0.067     1.088     0.077     44.       134-1     134.0     1179.     1759.     155.5     1.116     0.067     1.088     0.073     51.										26.3
134-2     134.0     874.     1588.     152.7     2.503     0.130     2.509     0.146     29.       134-2     134.0     905.     1606.     153.0     2.503     0.127     2.511     0.142     31.       134-2     134.0     938.     1625.     153.3     2.491     0.128     2.500     0.142     33.       134-2     134.0     974.     1646.     153.6     2.195     0.124     2.174     0.136     35.       134-1     134.0     1010.     1666.     153.9     2.358     0.093     2.407     0.105     38.       134-1     134.0     1047.     1687.     154.2     1.992     0.086     2.002     0.096     39.       134-1     134.0     1087.     1709.     154.5     1.703     0.080     1.692     0.089     42.       134-1     134.0     1179.     1759.     155.5     1.070     0.067     1.008     0.077     44.       134-1     134.0     1179.     1759.     155.5     1.070     0.067     1.008     0.073     51.       134-1     134.0     1232.     1787.     155.5     1.116     0.067     1.088     0.073     51.										27.2
134-2     134.0     905.     1606.     153.0     2.503     0.127     2.511     0.142     31.       134-2     134.0     938.     1625.     153.3     2.491     0.128     2.500     0.142     33.       134-2     134.0     974.     1646.     153.6     2.195     0.124     2.174     0.136     35.       134-1     134.0     1010.     1666.     153.9     2.358     0.093     2.407     0.105     38.       134-1     134.0     1047.     1687.     154.2     1.992     0.086     2.002     0.096     39.       134-1     134.0     1087.     1709.     154.5     1.703     0.080     1.692     0.089     42.       134-1     134.0     1131.     1733.     154.8     1.255     0.070     1.208     0.077     44.       134-1     134.0     1179.     1759.     155.2     1.057     0.067     1.088     0.073     51.       134-1     134.0     1232.     1787.     155.5     1.116     0.067     1.088     0.073     51.										
134-2       134.0       938.       1625.       153.3       2.491       0.128       2.500       0.142       33.         134-2       134.0       974.       1646.       153.6       2.195       0.124       2.174       0.136       35.         134-1       134.0       1010.       1666.       153.9       2.358       0.093       2.407       0.105       38.         134-1       134.0       1047.       1687.       154.2       1.992       0.086       2.002       0.096       39.         134-1       134.0       1087.       1709.       154.5       1.703       0.080       1.692       0.089       42.         134-1       134.0       1131.       1733.       154.8       1.255       0.070       1.208       0.077       44.         134-1       134.0       1179.       1759.       155.2       1.057       0.067       1.088       0.073       51.         134-1       134.0       1232.       1787.       155.5       1.116       0.067       1.088       0.073       51.			-							
134-2     134.0     974.     1646.     153.6     2.195     0.124     2.174     0.136     35.       134-1     134.0     1010.     1666.     153.9     2.358     0.093     2.407     0.105     38.       134-1     134.0     1047.     1687.     154.2     1.992.     0.086     2.002.     0.096     39.       134-1     134.0     1087.     1709.     154.5     1.703.     0.080.     1.692.     0.089.     42.       134-1     134.0     1179.     1759.     155.2     1.057.     0.067.     1.008.     0.073.     48.       134-1     134.0     1232.     1787.     155.5     1.116.     0.067.     1.088.     0.073.     51.										
134-1     134.0     1047.     1687.     154.2     1.992.     0.086.     2.002.     0.096.     39.       134-1     134.0     1087.     1709.     154.5     1.703.     0.080.     1.692.     0.089.     42.       134-1     134.0     1131.     1733.     154.8     1.255.     0.070.     1.208.     0.077.     44.       134-1     134.0     1179.     1759.     155.2     1.057.     0.067.     1.088.     0.073.     51.       134-1     134.0     1232.     1787.     155.5     1.116.     0.067.     1.088.     0.073.     51.										35.3
134-1     134.0     1047.     1687.     154.2     1.992.     0.086.     2.002.     0.096.     39.       134-1     134.0     1087.     1709.     154.5     1.703.     0.080.     1.692.     0.089.     42.       134-1     134.0     1131.     1733.     154.8     1.255.     0.070.     1.208.     0.077.     44.       134-1     134.0     1179.     1759.     155.2     1.057.     0.067.     1.088.     0.073.     51.       134-1     134.0     1232.     1787.     155.5     1.116.     0.067.     1.088.     0.073.     51.	134-1	124 0	1010.	1666	153.0	2.358	0.003	2-407	0.105	38.2
134-1     134.0     1087.     1709.     154.5     1.703     0.080     1.692     0.089     42.       134-1     134.0     1131.     1733.     154.8     1-255     0.070     1-208     0-077     44.       134-1     134.0     1179.     1759.     155.2     1.057     0.067     1.008     0.073     48.       134-1     134.0     1232.     1787.     155.5     1.116     0.067     1.088     0.073     51.				- :						39.9
134-1 134-0 1131 1733 154-8 1-255 0.070 1-208 0-077 44. 134-1 134-0 1179 1759 155-2 1.057 0.067 1.008 0.073 48. 134-1 134-0 1232 1787 155-5 1.116 0.067 1.088 0.073 51.										42.1
134-1 134.0 1179. 1759. 155.2 1.057 0.067 1.008 0.073 48. 134-1 134.0 1232. 1787. 155.5 1.116 0.067 1.088 0.073 51.										
										48.2
134-1 134.0 1290, 1817, 155.9 0.877 0.066 0.829 0.073 50.	134-1	134.0	1232.	1787.	155.5	1-116	0.067	1-088	0.073	51.1
	134-1	134.0	1290.	1817.	155.9	0.877	0.066	0.829	0.073	50.5
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TABLE 71

POINT NO.	THETA LAB		W	THETA C.M.	SIGMA AVER	DSIGMA LAGE	S I GMA UNF	DSIGMA OLDED	<b>∆</b> κ RM
156-4	155.4	510.	1355.	163.6	3.057	0.160	3.088	0.196	15.1
156-4	155.4	522.	1363.	163.7	3.225	0.161	3.288	0.190	15.3
156-4	155.4	534.	1372.	163.8	2.742	0.152	2.709	0.178	15.6
156-4	155.4	547.	1381.	163.9	2.662	0.144	2.621	0.169	16.1
156-4	155.4	561.	1390.	164.0	2.855	0.147	2.855	0.172	16.6
156-4-	155_4_	576	_1400		3.104_			0.172	
156-4	155.4	592.	1411.	164.2	2.841	0.139	2.835	0.161	18.2
156-3	155.4	609.	1422.	164.3	2.782	0.158	2.782	0.185	19.1
l56-3	155.4	625.	1433.	164.4	3.077	0.156	3.137	0.183	19.6
156-3	155.4	642.	1444.	164.5	2.700	0.146	2.692	0.170	20.2
l5o-3	155.4		1456	164.6	2.816_	0.151	_2.835_	_0.176	.20.9
156-3	155.4	680.	1468.	164.7	2.541	0.141	2.517	0.163	21.9
56-3	155.4	761.	1482.	164.9		.0.154	2.978		23.0
156-3	155.4	724.	1496.	165-0	2.455	0-138	2.431	0.156	24.4
156-2	155.4	750 •	1513.	165.1	2.410	0.149	2.398	0.173	25.8
156-2	155.4	773 •	_1527	165.3	2.173_	0.137	2.129.	0 . 159	
56-2	155.4	798.	1542.	165.4	2.544	0.145	2.570	0.167	27.8
56-2	155.4	825	1558.	165.6			2.373	0.157	29.1
56-2	155.4	854.	1576.	165.7	2.164	0.131	2.140	0.149	30.9
56-2	155.4	886	1594.	165.9	2.069	0.136	2.040	0.153	32.9
56-2	155.4	920.	1615.	166.0	2.348	0.131	2.362	0.146	35.5
56-1	155.4	965.	1637.	166.2	2.298	0.129	2.353	0.147	37.7
56-1	155.4	995.	1658.	166.4	2.185	0.130	2.233	0.147	39.4
56-1	155,4	1034.	1679.	166.5	1.834	0.119	1.845	0.134	41.7
56-1	155.4	1077.	1703.	166.7	1.329	0.103	1.293	0.115	44.4
56-1	155.4	1125.	1729.	166.9	1.075	0.091	1.030	0.100	48.0
56-1	155.4	_1177.	757		_0.848.	0.082	0.796	_0.090	51.9
56-1	155.4	1234.	1788.	167.3	0.452	0.072	0.364	0.080	55.2
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						W			

LAB ANGLE 79
34. DEGREES

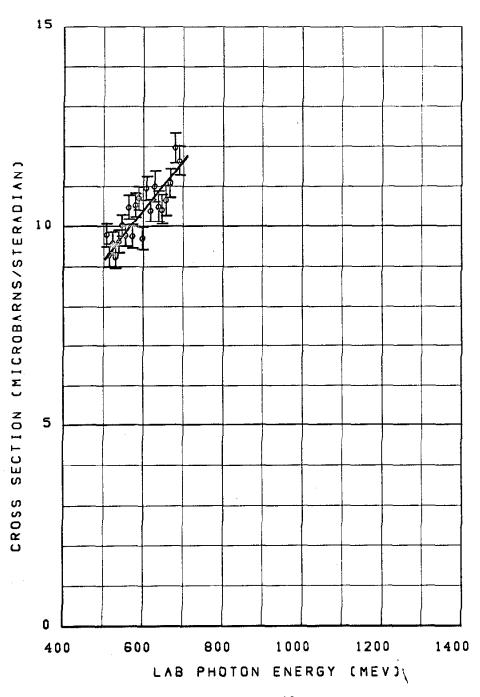


Figure 13a

LAB ANGLE 80 40. DEGREES

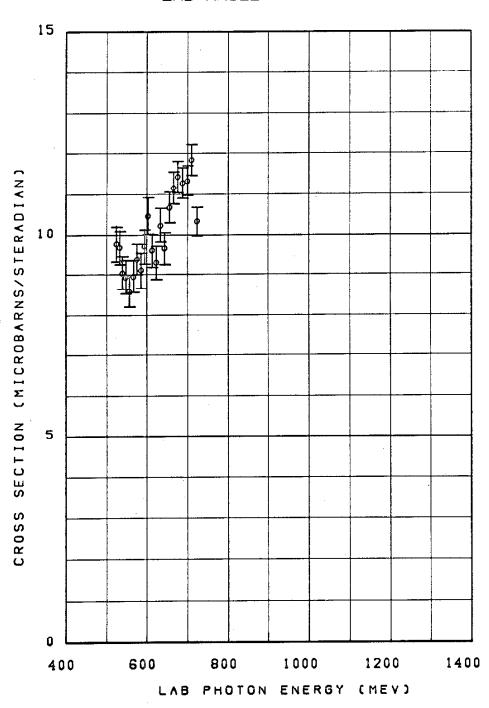


Figure 13b.

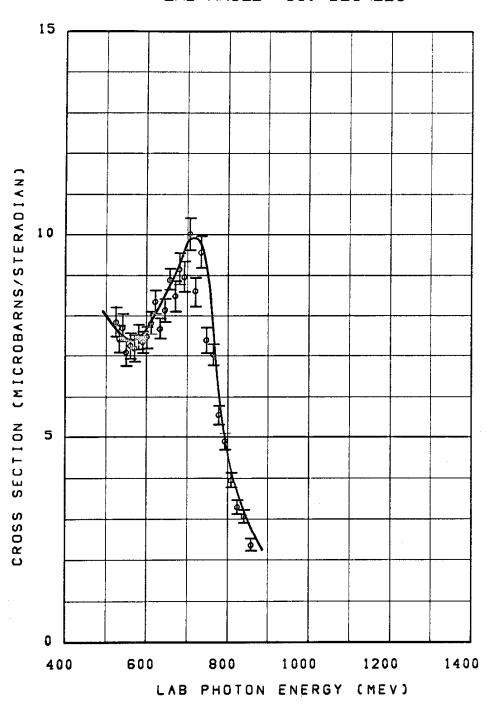


Figure 13c

LAB ANGLE 8264. DEGREES

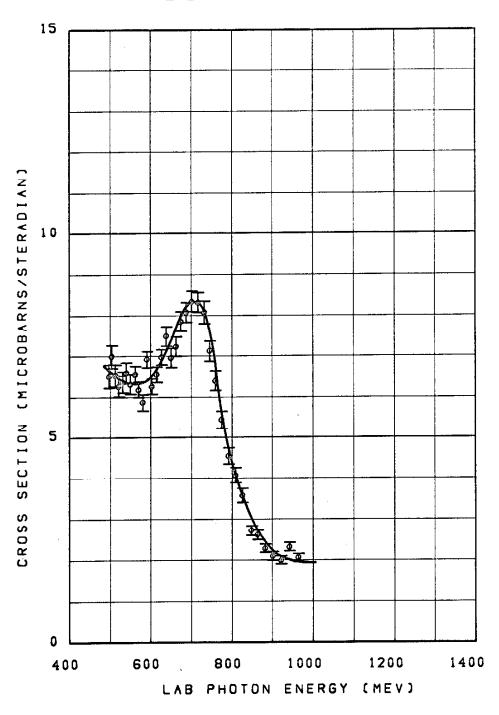


Figure 13d

LAB ANGLE 8348. DEGREES

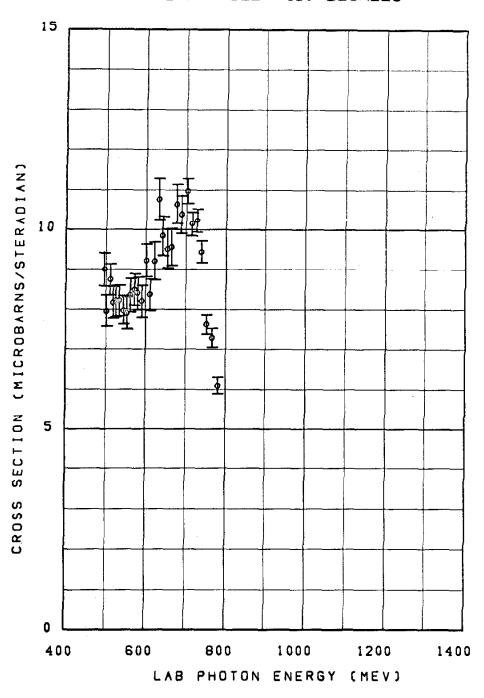


Figure 13e

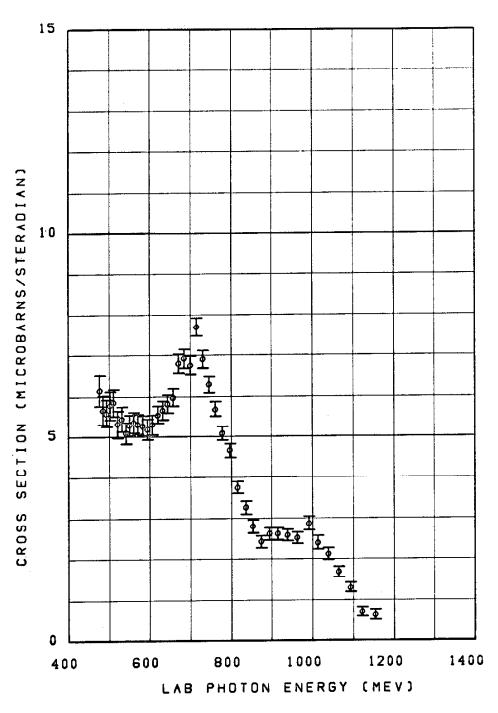


Figure 13f

LAB ANGLE 8584. DEGREES

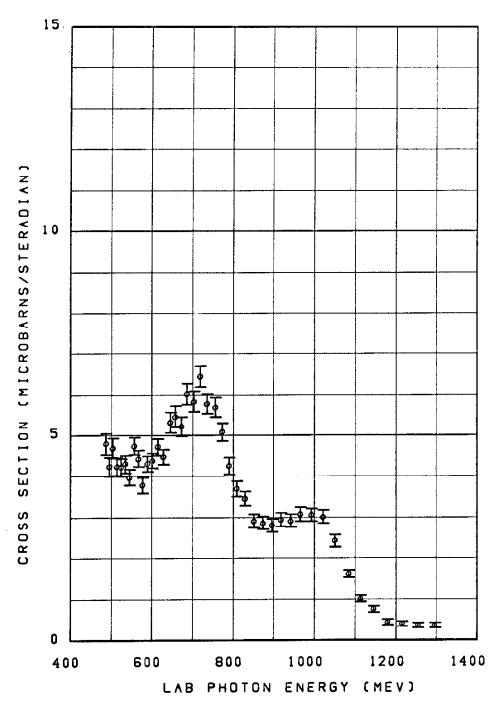


Figure 13g

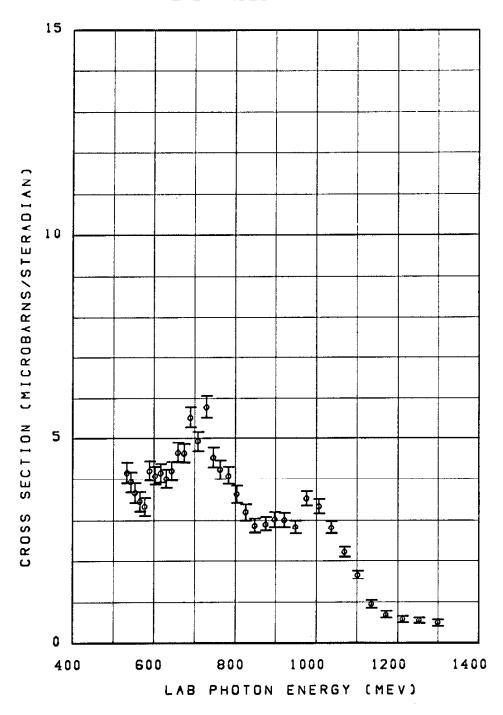


Figure 13h

LAB ANGLE 106. DEGREES

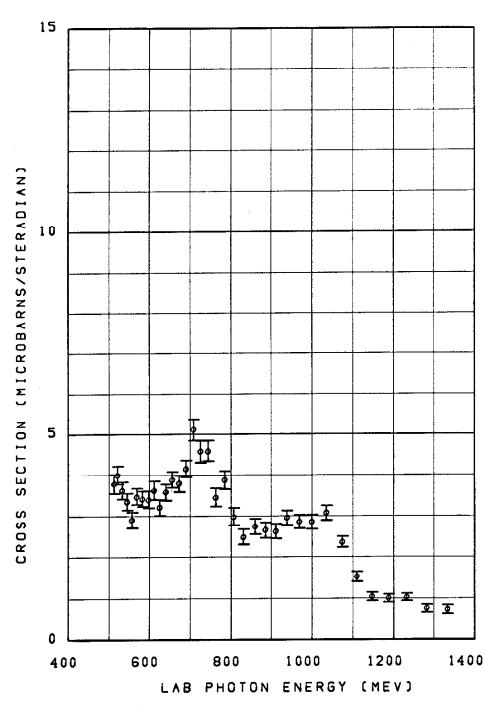


Figure 13i

LAB ANGLE 120. DEGREES

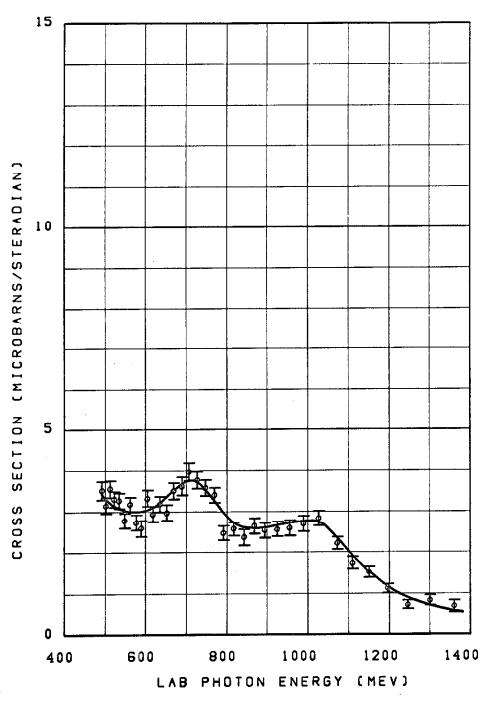


Figure 13j

LAB ANGLE 134. DEGREES

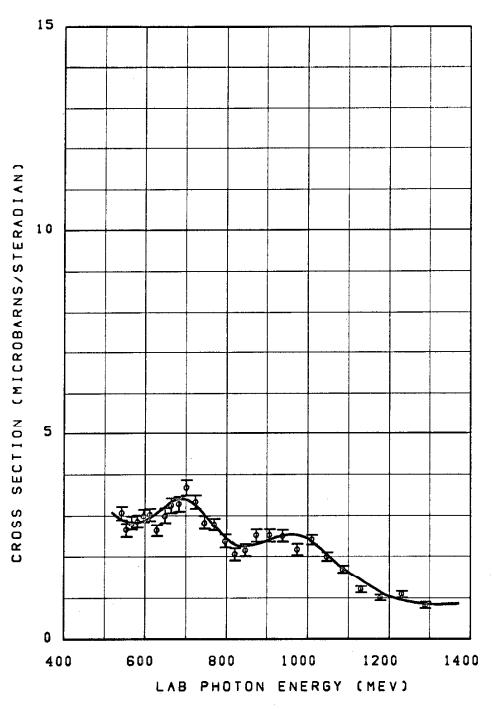


Figure 13k

LAB ANGLE 155. DEGREES

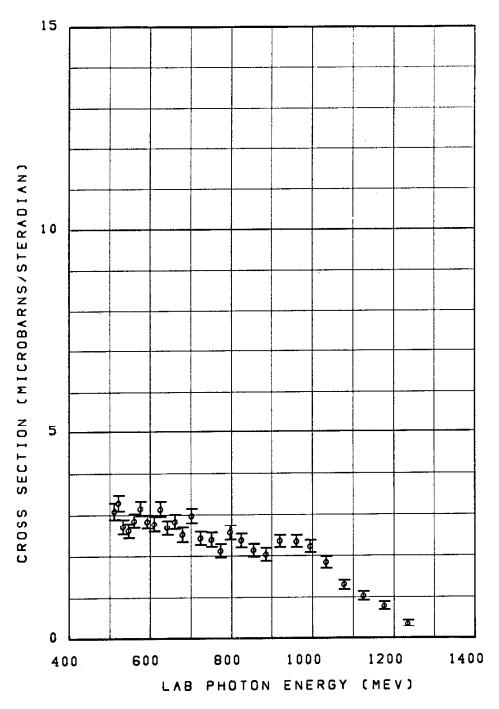
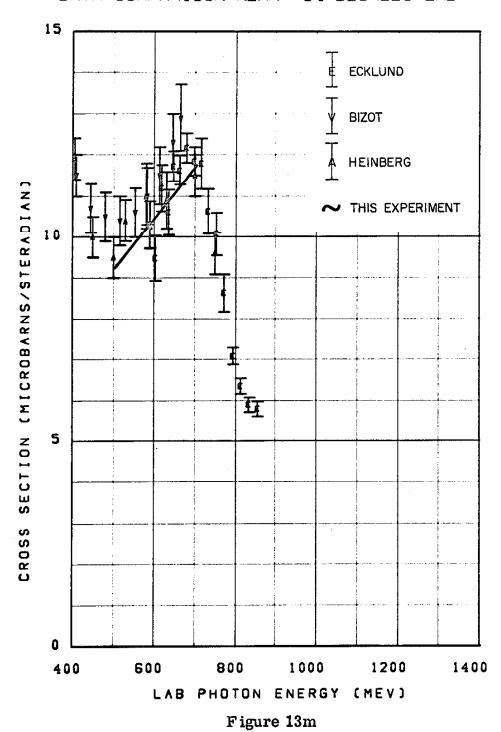
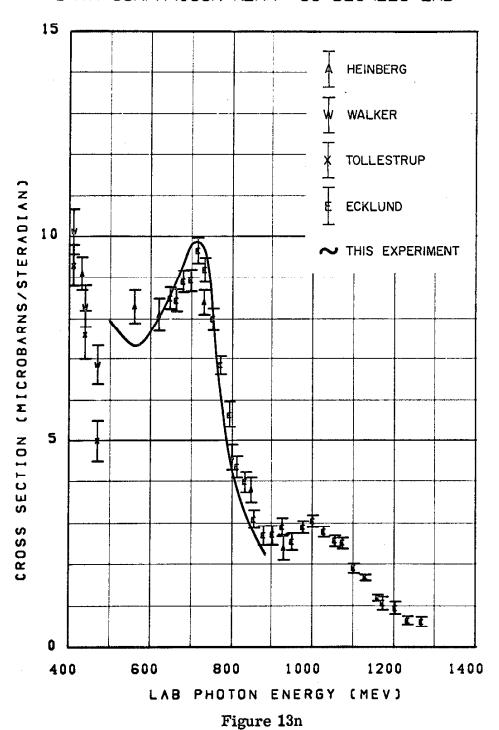


Figure 13 1

DATA COMPARISON NEAR 34 DEGREES LAB



DATA COMPARISON NEAR 56 DEGREES LAB



# DATA COMPARISON NEAR 64 DEGREES LAB

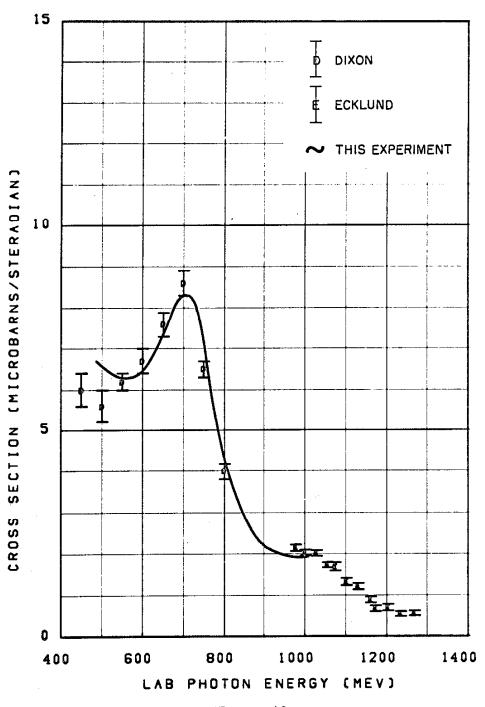
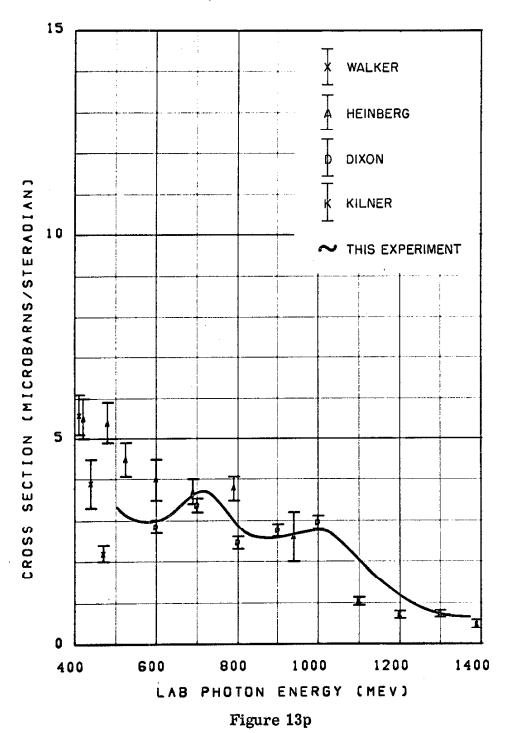
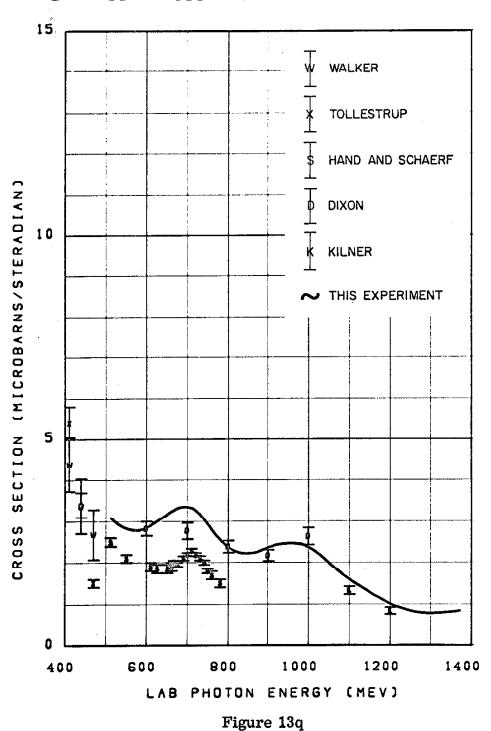


Figure 13 o

DATA COMPARISON NEAR 120 DEGREES LAB



DATA COMPARISON NEAR 134 DEGREES LAB



In general, this experiment agrees with other experiments as well as can be expected. There is excellent agreement with the data of Ecklund and Walker. (9) A detailed comparison of the results in the region of overlap of the two experiments gives a difference of 2.5 ± 2.0%, where the cross sections of this experiment are smaller than those of Ecklund and Walker. This experiment also agrees very well with Dixon and Walker (12) after a small correction is made to interpolate their results to constant lab angle. This experiment is in good agreement with the results of Kilner (13) at 1300 and 1390 MeV, but his data seem to be systematically smaller than the data of this experiment at 1100 MeV and 1200 MeV, especially at 120 degrees in the lab. Since this experiment agrees with Dixon and Walker at 1000 MeV at the same angle and varies smoothly through the region of 1000 to 1350 MeV, it is hard to explain the 30-50% disagreement with Kilner.

An important experimental problem is the matching of this experiment with lower energy experiments near the first resonance. Only two experiments provide any data which overlap both the first and second resonance, namely, the experiments of Heinberg et al. (15) and Bizot et al. (37) The Heinberg data is in agreement with this experiment at 3° and 58° in the lab, but the 118° data are significantly larger near 500 MeV. The data of Bizot et al. at 35° are approximately 10% larger than the data of this experiment. On the other hand, the two previous experiments at 470 MeV, namely Walker et al. (35) and Tollestrup et al., (36) gave cross sections systematically 20% to 50% smaller than those of this experiment at ~ 500 MeV. Both of those experiments agree to the order of 10% with other data at 400 MeV and lower. It is possible that their results at 470 MeV were in error because the synchrotron end point

energy was very near the photon energy (the synchrotron end point energy was  $500 \pm 5$  MeV for all data taken in both experiments). If the data of Walker and Tollestrup at 470 MeV are ignored, it is possible to draw a smooth curve which passes through the low energy data and the data of this experiment.

There is a serious disagreement between this experiment and the experiment of Hand and Schaerf. (16) This experiment reproduced the energy dependence of the cross section measured by Hand and Schaerf at 135° lab, but their data are systematically 30% smaller. Since these authors assumed that no muons were counted in their apparatus, a correct treatment of the decay correction is likely to make the discrepancy as large as 40% - 50%. Hand and Schaerf estimate their systematic errors to be less than 25%. A portion of the experiment was repeated by Schaerf. (17) The new results agreed with the old to the order of 5%, and again Schaerf estimated his systematic errors to be on the order of 20%. Because the results of this experiment are larger than those of Hand and Schaerf, the possibility exists that an undetected background is included in our data. However, the excitation curve measured at 134° indicates that the background is 1.0  $\pm$  1.0% (see Section IV-D). Thus, we conclude that Hand and Schaerf made a beam monitoring or magnet calibration error, and that their data should be multiplied by the factor 1.5 to get an absolute cross section which agrees with this experiment.

## E. Angular Distributions by Interpolation

For some purposes, angular distributions of the cross section are more useful than data in the form of energy distributions at constant angle. A set of angular distributions was obtained by linear interpolation in the data of Table 7a - 7e. The energies chosen were the nominal energies of Stan Ecklund's angular distributions (9), with a few additional energies below 589 MeV. For the lowest and highest energies, the interpolated data may represent an extrapolation of the measured data. However, no data were used which came from an extrapolation of more than 20 MeV. The error bars on the interpolated data were arbitrarily taken to be equal to the error bars on the nearest measured point. The interpolated angular distributions are presented in Tables 8a - 8d.

## TABLE 8a - 8d

# Interpolated Angular Distributions

THETA is the c.m. pion angle in degrees

SIGMA is the c.m. differential cross section in microbarns

per steradian

DSIGMA is the statistical error associated with SIGMA in

microbarns per steradian

K is the laboratory photon energy in MeV

W is the total center of mass energy in MeV

### INTERPULATED ANGULAR DISTRIBUTIONS

THETA* SIGMA DSIGMA	THETA* SIGMA DSIGMA	THETA* SIGMA DSIGMA
K= 490. W= 1342. 48.3 11.029 0.289 66.4 9.775 0.421 85.3 6.128 0.287 96.1 5.620 0.363 106.2 4.605 0.258 137.7 3.565 0.216 163.5 2.740 0.196	K= 570.  W= 1396.  49.9 9.920 0.293  58.0 7.126 0.392  68.3 8.471 0.411  78.1 7.200 0.324  87.4 6.224 0.205  98.2 5.316 0.261  108.2 4.244 0.199  117.5 3.401 0.228  127.9 3.475 0.194  139.0 2.930 0.187  149.4 2.826 0.158  164.0 3.038 0.172	K= 635. W= 1439. 51.1 10.671 0.382 59.3 10.125 0.427 69.8 10.508 0.517 79.7 7.753 0.275 89.0 7.347 0.243 99.8 5.712 0.227 109.7 4.819 0.252 118.9 4.095 0.232 129.2 3.482 0.198 140.1 3.184 0.188 150.2 2.761 0.175 164.5 2.874 0.183
K= 510. W* 1355. 48.7 9.609 0.289 56.7 9.935 0.445 66.9 8.706 0.395 76.6 8.584 0.357 85.8 6.673 0.284 96.6 5.841 0.346 106.7 4.431 0.237 126.7 3.756 0.228 138.0 3.477 0.200 163.6 3.088 0.196	K= 589. W= 1409. 50.2 10.690 0.287 58.4 9.358 0.438 68.7 8.233 0.404 78.6 7.369 0.317 87.8 6.689 0.198 98.6 5.225 0.250 108.7 4.295 0.185 118.0 4.159 0.236 128.3 3.419 0.209 139.4 2.605 0.192 149.6 2.938 0.158 164.2 2.888 0.172	K= 647. W= 1447. 51.3 10.439 0.379 59.6 9.944 0.407 70.1 9.710 0.496 80.0 8.270 0.275 89.2 7.117 0.243 100.0 5.868 0.226 110.0 5.348 0.261 119.2 4.322 0.234 129.4 3.736 0.204 140.3 3.030 0.188 150.3 2.986 0.175 164.5 2.732 0.176
K= 530.  H= 1369.  49.1 9.273 0.275  57.1 9.701 0.445  67.3 8.212 0.389  77.1 7.589 0.357  86.3 6.364 0.263  97.2 5.432 0.337  107.2 4.274 0.213  116.6 4.209 0.254  127.1 3.722 0.223  138.4 3.286 0.191  148.9 3.437 0.167  163.7 2.881 0.190	K= 603. W= 1418. 50.5 10.366 0.287 58.7 10.468 0.442 69.1 9.028 0.412 78.9 7.533 0.277 88.2 6.277 0.191 99.0 5.278 0.250 109.0 4.419 0.194 118.3 4.096 0.236 128.5 3.506 0.219 139.6 3.295 0.201 149.8 3.009 0.154 164.2 2.801 0.185	K= 663.  W= 1458.  51.6 10.885 0.365 59.9 11.018 0.391 70.4 9.566 0.482 80.3 8.707 0.385 89.6 7.285 0.243 100.4 6.370 0.227 110.4 5.380 0.261 119.5 4.657 0.234 129.7 3.849 0.204 140.5 3.315 0.191 150.5 3.223 0.178 164.6 2.790 0.176
K= 550.  m= 1383.  49.5 9.909 0.271  57.5 8.884 0.408  67.8 7.935 0.406  77.6 7.139 0.339  86.8 6.319 0.260  97.7 5.285 0.270  107.7 4.305 0.202  117.1 3.745 0.248  127.5 3.136 0.206  138.7 2.853 0.178  149.1 2.768 0.167  163.9 2.674 0.172	K= 618.  H= 1428.  50.8 10.448 0.382  59.0 9.439 0.415  69.4 8.896 0.482  79.3 8.144 0.283  88.5 6.705 0.188  99.3 5.525 0.244  109.3 4.662 0.194  118.6 4.142 0.232  128.8 3.410 0.219  139.8 2.962 0.201  150.0 2.872 0.151  164.3 2.980 0.185	K= 680.  W= 1468.  52.0 11.948 0.370 60.3 11.389 0.382 70.8 10.572 0.489 80.7 9.065 0.395 90.0 7.947 0.243 100.8 6.894 0.231 110.7 5.662 0.256 119.9 4.982 0.245 130.0 3.958 0.208 140.8 3.565 0.210 150.7 3.279 0.182

TABLE 8b

## INTERPOLATED ANGULAR DISTRIBUTIONS

K= 698.	THETA* SIGMA DSIGMA	THETA* SIGMA DSIGMA	THETA* SIGMA DSIGMA
1	W- 400	K 777	K= 857.
11.417 0.370			
Second Color			
71.2 10.772 0.469 92.1 5.659 0.237 104.6 2.740 0.167 90.4 8.268 0.252 112.7 5.110 0.241 123.2 2.686 0.171 90.4 8.268 0.252 112.7 5.110 0.241 123.2 2.686 0.178 101.2 6.778 0.231 121.7 4.180 0.229 132.9 2.706 0.189 120.2 5.261 0.245 131.5 3.636 0.223 143.1 2.534 0.198 120.2 5.261 0.245 142.0 3.287 0.182 152.5 2.294 0.146 130.3 4.601 0.268 151.7 2.741 0.156 165.7 2.131 0.155 141.0 3.788 0.217 165.3 2.141 0.173 150.9 3.593 0.182 164.9 2.912 0.177			
81.2 9.334 0.398			104.6 2.740 0.165
101.2		102.8 5.325 0.186	114.3 2.906 0.171
111.1 5.893 0.256	90.4 8.268 0.252		
120.2   5.261   0.245   142.0   3.287   0.182   152.5   2.294   0.146   130.3   4.601   0.268   151.7   2.741   0.156   165.7   2.131   0.153   141.0   3.788   0.217   165.3   2.141   0.173   150.9   3.593   0.182   164.9   2.912   0.177	101.2 6.778 0.231		
130.3 4.601 0.268			
141.0 3.788 0.217 165.3 2.141 0.173 150.9 3.593 0.182 164.9 2.912 0.177  K= 715.			
150.9   3.593   0.182			103.1 2.131 0.133
		103.3 2.141 0.173	
K= 715.			
## 1491. 61.0 11.353 0.377 73.3 5.096 0.235 94.4 2.330 0.114 71.6 10.155 0.300 83.3 4.898 0.233 105.1 2.493 0.146 81.5 9.095 0.398 92.6 4.513 0.192 114.7 2.850 0.166 90.8 8.318 0.252 103.3 4.755 0.170 123.6 2.938 0.178 101.6 7.652 0.225 113.1 4.187 0.200 133.2 2.673 0.190 111.5 6.315 0.259 122.0 3.869 0.220 143.4 2.604 0.196 120.6 5.235 0.263 131.9 3.549 0.223 152.8 2.509 0.146 130.6 4.885 0.268 142.3 2.485 0.173 165.8 2.058 0.153 141.3 3.894 0.217 151.9 2.425 0.156 151.1 3.463 0.177 165.4 2.486 0.167 165.0 2.641 0.177   K= 733.  M= 1502.  K= 813.  M= 1502.  K= 151.1 3.467 0.268 113.5 3.657 0.191 124.0 3.022 0.178 102.0 6.805 0.211 122.4 3.422 0.203 133.6 2.637 0.190 111.9 5.907 0.259 132.2 2.865 0.208 143.7 2.551 0.186 120.9 5.467 0.263 142.6 2.565 0.173 153.0 2.511 0.146 130.9 4.589 0.262 152.1 2.158 0.156 165.9 2.191 0.153 141.5 3.709 0.205 165.5 2.458 0.167 151.3 3.107 0.168 165.1 2.419 0.173   K= 752.  K= 834.  K= 834.  K= 926.  K= 1514.  72.4 7.721 0.271 84.1 3.160 0.167 95.3 2.088 0.100 82.4 7.312 0.323 93.4 3.262 0.169 105.9 2.591 0.146 130.9 4.589 0.262 152.1 2.158 0.156 165.9 2.191 0.153 141.5 3.709 0.205 165.5 2.458 0.167 151.3 3.107 0.168 165.1 2.419 0.173	10449 24912 01177		
61.0 11.353 0.377 73.5 5.096 0.235 94.4 2.330 0.114 71.6 10.155 0.300 83.3 4.898 0.233 105.1 2.493 0.146 81.5 9.095 0.398 92.6 4.513 0.192 114.7 2.850 0.166 90.8 8.318 0.252 103.3 4.755 0.170 123.6 2.938 0.178 101.6 7.652 0.225 113.1 4.187 0.200 133.2 2.673 0.190 111.5 6.315 0.259 122.0 3.869 0.220 143.4 2.604 0.196 120.6 5.235 0.263 131.9 3.549 0.223 152.8 2.509 0.146 130.6 4.885 0.268 142.3 2.485 0.173 165.8 2.058 0.153 141.3 3.894 0.217 151.9 2.425 0.156 151.1 3.463 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.0 2.641 0.177 165.0 2.641 0.177 165.0 2.641 0.177 165.0 2.641 0.177 165.0 2.641 0.177 165.0 2.641 0.177 165.0 2.641 0.177 165.0 2.641 0.177 165.0 2.641 0.177 165.0 2.641 0.177 165.0 2.641 0.177 165.0 2.641 0.177 165.0 2.641 0.166 115.5 2.616 0.166 115.5 2.616 0.166 115.0 2.641 0.166 115.0 2.641 0.166 115.0 2.641 0.166 115.0 2.641 0.166 115.0 2.641 0.166 115.0 2.641 0.167 165.0 2.641 0.167 165.0 2.641 0.167 165.0 2.641 0.167 165.0 2.641 0.167 165.0 2.641 0.167 165.0 2.641 0.167 165.0 2.641 0.167 165.0 2.641 0.167 166 115.0 2.641 0.167 165.0 2.641 0.	K= 715.	K= 793.	
71.6 10.155 0.300 83.3 4.898 0.233 105.1 2.493 0.146 81.5 9.095 0.398 92.6 4.513 0.192 114.7 2.850 0.166 90.8 8.318 0.252 103.3 4.755 0.170 123.6 2.938 0.178 101.6 7.652 0.225 113.1 4.187 0.200 133.2 2.673 0.190 111.5 6.315 0.259 122.0 3.869 0.220 143.4 2.604 0.196 120.6 5.235 0.263 131.9 3.549 0.223 152.8 2.509 0.146 130.6 4.885 0.268 142.3 2.485 0.173 165.8 2.058 0.153 141.3 3.894 0.217 151.9 2.425 0.156 151.1 3.463 0.177 165.4 2.486 0.167 165.0 2.641 0.177  K= 733. K= 813. K= 813. K= 902.  M= 1502. H= 1551. H= 1604.  102.0 6.805 0.211 122.4 3.492 0.203 133.6 2.637 0.190 111.9 5.907 0.259 132.2 2.865 0.208 143.7 2.551 0.186 120.9 5.467 0.263 142.6 2.565 0.173 153.0 2.511 0.146 130.9 4.589 0.262 152.1 2.158 0.156 141.5 3.709 0.205 165.5 2.458 0.167 151.3 3.107 0.168 165.1 2.419 0.173  K= 752. K= 834. K= 926.  M= 1514. H= 1564. H= 1564. H= 1618.  72.4 7.721 0.271 84.1 3.160 0.167 165.9 2.191 0.153 141.5 3.709 0.205 165.5 2.458 0.167 151.3 3.107 0.168 165.1 2.419 0.173  K= 752. K= 834. K= 926.  M= 1514. H= 1564. H= 1564. H= 1618.  72.4 7.721 0.271 84.1 3.160 0.167 105.9 2.598 0.141 191.7 6.813 0.251 104.1 3.308 0.166 115.6 2.939 0.172 102.4 6.057 0.198 113.9 3.356 0.175 124.3 2.988 0.173 112.2 5.714 0.242 122.8 3.076 0.194 133.9 2.898 0.141 121.3 4.430 0.242 132.5 2.511 0.189 144.0 2.576 0.187 131.2 4.101 0.249 142.9 2.449 0.198 153.2 2.504 0.142 141.8 3.536 0.193 152.3 2.115 0.146 166.1 2.361 0.147			
81.5 9.095 0.398 92.6 4.513 0.192 114.7 2.850 0.166 90.8 8.318 0.252 103.3 4.755 0.170 123.6 2.938 0.178 101.6 7.652 0.225 113.1 4.187 0.200 133.2 2.673 0.190 111.5 6.315 0.259 122.0 3.869 0.220 143.4 2.604 0.196 120.6 5.235 0.263 131.9 3.549 0.223 152.8 2.509 0.146 130.6 4.885 0.268 142.3 2.485 0.173 165.8 2.058 0.153 141.3 3.894 0.217 151.9 2.425 0.156 151.1 3.463 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.680 0.291 13.5 3.657 0.191 124.0 3.022 0.178 102.0 6.805 0.211 122.4 3.442 0.203 133.6 2.637 0.190 111.9 5.907 0.259 132.2 2.865 0.208 143.7 2.551 0.186 120.9 5.467 0.263 142.6 2.565 0.173 153.0 2.511 0.146 130.9 4.589 0.262 152.1 2.158 0.156 165.9 2.191 0.153 165.1 2.419 0.173 165.5 2.458 0.167 165.5 2.458 0.16			
90.8 8.318 0.252 103.3 4.755 0.170 123.6 2.938 0.178 101.6 7.652 0.225 113.1 4.187 0.200 133.2 2.673 0.190 111.5 6.315 0.259 122.0 3.869 0.220 143.4 2.604 0.196 120.6 5.235 0.263 131.9 3.549 0.223 152.8 2.509 0.146 130.6 4.885 0.268 142.3 2.485 0.173 165.8 2.058 0.153 141.3 3.894 0.217 151.9 2.425 0.156 151.1 3.463 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.4 2.486 0.167 165.0 2.641 0.177 165.0 2.641 0.177 165.0 2.641 0.177 165.0 2.641 0.177 165.0 2.641 0.177 165.0 2.681 13.5 3.657 0.191 124.0 3.022 0.178 125.0 3.62 0.650 0.211 122.4 3.442 0.203 133.6 2.637 0.190 111.9 5.907 0.259 132.2 2.865 0.208 143.7 2.551 0.186 120.9 5.467 0.263 142.6 2.565 0.173 153.0 2.511 0.146 130.9 4.589 0.262 152.1 2.158 0.156 165.9 2.191 0.153 141.5 3.709 0.205 165.5 2.458 0.167 151.3 3.107 0.168 165.1 2.419 0.173 165.4 2.499 0.173 165.4 2.939 0.172 102.4 6.057 0.198 113.9 3.356 0.166 115.6 2.939 0.172 102.4 6.057 0.198 113.9 3.356 0.175 124.3 2.988 0.103 112.2 5.714 0.242 122.8 3.076 0.194 133.9 2.811 0.178 121.3 4.430 0.242 132.5 2.511 0.189 144.0 2.576 0.187 131.2 4.101 0.249 142.9 2.449 0.198 153.2 2.504 0.142 141.8 3.536 0.193 152.3 2.115 0.146 166.1 2.361 0.147 151.5 2.817 0.160 165.6 2.300 0.157			
101.6 7.652 0.225			
111.5 6.315 0.259			
120.6 5.235 0.263	<del></del>		
130.6 4.885 0.268			
141.3 3.894 0.217 151.9 2.425 0.156 151.1 3.463 0.177 165.4 2.486 0.167  K= 733.			
151.1   3.463   0.177   165.4   2.486   0.167   165.0   2.641   0.177   165.0   2.641   0.177   165.0   2.641   0.177   165.0   2.641   0.177   165.4   2.486   0.167   165.0   2.641   0.177   165.0   2.641   0.177   165.1   165.			
K= 733.       K= 813.       K= 902.         M= 1502.       W= 1551.       W= 1604.         61.3 9.148 0.377       83.7 3.764 0.184       94.8 2.106 0.101         72.0 9.843 0.291       93.0 3.956 0.185       105.5 2.616 0.146         81.9 9.544 0.380       103.7 3.879 0.164       115.1 2.843 0.172         91.2 8.007 0.268       113.5 3.657 0.191       124.0 3.022 0.178         102.0 6.805 0.211       122.4 3.442 0.203       133.6 2.637 0.190         111.9 5.907 0.259       132.2 2.865 0.208       143.7 2.551 0.186         120.9 5.467 0.263       142.6 2.565 0.173       153.0 2.511 0.146         130.9 4.589 0.262       152.1 2.158 0.156       165.9 2.191 0.153         141.5 3.709 0.205       165.5 2.458 0.167       165.9 2.191 0.153         151.3 3.107 0.168       165.1 2.419 0.173       84.1 3.160 0.167       95.3 2.088 0.100         82.4 7.312 0.323       93.4 3.262 0.169       105.9 2.598 0.141         91.7 6.813 0.251       104.1 3.308 0.166       115.6 2.939 0.172         102.4 6.057 0.198       113.9 3.356 0.175       124.3 2.988 0.173         112.2 5.714 0.242       122.8 3.076 0.194       133.9 2.811 0.178         121.3 4.430 0.242       132.5 2.511 0.189       144.0 2.576 0.187         131.2 4.010 0.249       142.9 2.449		165.4 2.486 0.167	
N= 1502.	165.0 2.641 0.177		
N= 1502.		· · · · · · · · · · · · · · · · · ·	
61.3 9.148 0.377 83.7 3.764 0.184 94.8 2.106 0.101 72.0 9.843 0.291 93.0 3.956 0.185 105.5 2.616 0.146 81.9 9.544 0.380 103.7 3.879 0.164 115.1 2.843 0.172 91.2 8.007 0.268 113.5 3.657 0.191 124.0 3.022 0.178 102.0 6.805 0.211 122.4 3.442 0.203 133.6 2.637 0.190 111.9 5.907 0.259 132.2 2.865 0.208 143.7 2.551 0.186 120.9 5.467 0.263 142.6 2.565 0.173 153.0 2.511 0.146 130.9 4.589 0.262 152.1 2.158 0.156 165.9 2.191 0.153 141.5 3.709 0.205 165.5 2.458 0.167 151.3 3.107 0.168 165.1 2.419 0.173	K= 733.		
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K=       752.       K=       834.       K=       926.         W=       1514.       W=       1564.       W=       1618.         72.4       7.721       0.271       84.1       3.160       0.167       95.3       2.088       0.100         82.4       7.312       0.323       93.4       3.262       0.169       105.9       2.598       0.141         91.7       6.813       0.251       104.1       3.308       0.166       115.6       2.939       0.172         102.4       6.057       0.198       113.9       3.356       0.175       124.3       2.988       0.173         112.2       5.714       0.242       122.8       3.076       0.194       133.9       2.811       0.178         121.3       4.430       0.242       132.5       2.511       0.189       144.0       2.576       0.187         131.2       4.101       0.249       142.9       2.449       0.198       153.2       2.504       0.142         141.8       3.536       0.193       152.3       2.115       0.146       166.1       2.361       0.147         151.5       2.817       0.160       165.6       2.30			
Wa       1514.       Wa       1564.       Wa       1618.         72.4       7.721       0.271       84.1       3.160       0.167       95.3       2.088       0.100         82.4       7.312       0.323       93.4       3.262       0.169       105.9       2.598       0.141         91.7       6.813       0.251       104.1       3.308       0.166       115.6       2.939       0.172         102.4       6.057       0.198       113.9       3.356       0.175       124.3       2.968       0.173         112.2       5.714       0.242       122.8       3.076       0.194       133.9       2.811       0.178         121.3       4.430       0.242       132.5       2.511       0.189       144.0       2.576       0.187         131.2       4.101       0.249       142.9       2.449       0.198       153.2       2.504       0.142         141.8       3.536       0.193       152.3       2.115       0.146       166.1       2.361       0.147         151.5       2.817       0.160       165.6       2.300       0.157	165.1 2.419 0.173		
Wa       1514.       Wa       1564.       Wa       1618.         72.4       7.721       0.271       84.1       3.160       0.167       95.3       2.088       0.100         82.4       7.312       0.323       93.4       3.262       0.169       105.9       2.598       0.141         91.7       6.813       0.251       104.1       3.308       0.166       115.6       2.939       0.172         102.4       6.057       0.198       113.9       3.356       0.175       124.3       2.968       0.173         112.2       5.714       0.242       122.8       3.076       0.194       133.9       2.811       0.178         121.3       4.430       0.242       132.5       2.511       0.189       144.0       2.576       0.187         131.2       4.101       0.249       142.9       2.449       0.198       153.2       2.504       0.142         141.8       3.536       0.193       152.3       2.115       0.146       166.1       2.361       0.147         151.5       2.817       0.160       165.6       2.300       0.157			
Wm       1514.       Wm       1564.       Wm       1618.         72.4       7.721       0.271       84.1       3.160       0.167       95.3       2.088       0.100         82.4       7.312       0.323       93.4       3.262       0.169       105.9       2.598       0.141         91.7       6.813       0.251       104.1       3.308       0.166       115.6       2.939       0.172         102.4       6.057       0.198       113.9       3.356       0.175       124.3       2.988       0.173         112.2       5.714       0.242       122.8       3.076       0.194       133.9       2.811       0.178         121.3       4.430       0.242       132.5       2.511       0.189       144.0       2.576       0.187         131.2       4.101       0.249       142.9       2.449       0.198       153.2       2.504       0.142         141.8       3.536       0.193       152.3       2.115       0.146       166.1       2.361       0.147         151.5       2.817       0.160       165.6       2.300       0.157	K= 752.	K= 834.	K= 926.
72.4     7.721     0.271     84.1     3.160     0.167     95.3     2.088     0.100       82.4     7.312     0.323     93.4     3.262     0.169     105.9     2.598     0.141       91.7     6.813     0.251     104.1     3.308     0.166     115.6     2.939     0.172       102.4     6.057     0.198     113.9     3.356     0.175     124.3     2.988     0.173       112.2     5.714     0.242     122.8     3.076     0.194     133.9     2.811     0.178       121.3     4.430     0.242     132.5     2.511     0.189     144.0     2.576     0.187       131.2     4.101     0.249     142.9     2.449     0.198     153.2     2.504     0.142       141.8     3.536     0.193     152.3     2.115     0.146     166.1     2.361     0.147       151.5     2.817     0.160     165.6     2.300     0.157			
91.7 6.813 0.251 104.1 3.308 0.166 115.6 2.939 0.172 102.4 6.057 0.198 113.9 3.356 0.175 124.3 2.988 0.173 112.2 5.714 0.242 122.8 3.076 0.194 133.9 2.811 0.178 121.3 4.430 0.242 132.5 2.511 0.189 144.0 2.576 0.187 131.2 4.101 0.249 142.9 2.449 0.198 153.2 2.504 0.142 141.8 3.536 0.193 152.3 2.115 0.146 166.1 2.361 0.147 151.5 2.817 0.160 165.6 2.300 0.157	72.4 7.721 0.271	84.1 3.160 0.167	95.3 2.088 0.100
102.4 6.057 0.198 113.9 3.356 0.175 124.3 2.988 0.173 112.2 5.714 0.242 122.8 3.076 0.194 133.9 2.811 0.178 121.3 4.430 0.242 132.5 2.511 0.189 144.0 2.576 0.187 131.2 4.101 0.249 142.9 2.449 0.198 153.2 2.504 0.142 141.8 3.536 0.193 152.3 2.115 0.146 166.1 2.361 0.147 151.5 2.817 0.160 165.6 2.300 0.157			
112.2     5.714     0.242     122.8     3.076     0.194     133.9     2.811     0.178       121.3     4.430     0.242     132.5     2.511     0.189     144.0     2.576     0.187       131.2     4.101     0.249     142.9     2.449     0.198     153.2     2.504     0.142       141.8     3.536     0.193     152.3     2.115     0.146     166.1     2.361     0.147       151.5     2.817     0.160     165.6     2.300     0.157			
121.3 4.430 0.242 132.5 2.511 0.189 144.0 2.576 0.187 131.2 4.101 0.249 142.9 2.449 0.198 153.2 2.504 0.142 141.8 3.536 0.193 152.3 2.115 0.146 166.1 2.361 0.147 151.5 2.817 0.160 165.6 2.300 0.157	#		
131.2 4.101 0.249 142.9 2.449 0.198 153.2 2.504 0.142 141.8 3.536 0.193 152.3 2.115 0.146 166.1 2.361 0.147 151.5 2.817 0.160 165.6 2.300 0.157			
141.8 3.536 0.193 152.3 2.115 0.146 166.1 2.361 0.147 151.5 2.817 0.160 165.6 2.300 0.157			
151.5 2.817 0.160 165.6 2.300 0.157			
	<del> </del>		
	165.2 2.376 C.173		

102
INTERPOLATED ANGULAR DISTRIBUTIONS

THETA* SIGMA DSIGMA	THETA* SIGMA DSIGMA	THETA* SIGMA DSIGMA
K= 951.	K= 1056.	K≖ 1162.
W= 1632.	W= 1692.	H= 1749.
95.8 2.222 0.100	108.3 1.840 0.142	110.1 0.641 0.122
106.4 2.544 0.141	117.8 2.306 0.143	119.4 0.610 0.073
116.0 2.980 0.164	126.4 2.485 0.155	127.8 0.775 0.092
124.7 2.904 0.174	135.6 2.705 0.180	136.9 1.029 0.098
134.2 2.916 0.178	145.4 2.449 0.183	146.4 1.434 0.133
144.3 2.597 0.187	154.3 1.931 0.096	155.1 1.079 0.077
153.4 2.383 0.142	166.6 1.565 0.134	167.1 0.863 0.100
166.2 2.355 0.147		
K≠ 977.	K= 1074.	K= 1174.
W= 1647.	W= 1702.	W= 1756.
96.3 1.904 0.100	108.6 1.569 0.131	110.3 0.617 0.122
106.9 2.703 0.169	118.1 1.877 0.143	119.6 0.496 0.073
116.5 3.076 0.164	126.6 2.149 0.120	128.0 0.702 0.079
125.2 3.519 0.174	135.9 2.386 0.180	137.1 1.017 0.098
134.6 2.859 0.179	145.6 2.213 0.155	146.6 1.327 0.133
144.6 2.668 0.190	154.4 _ 1.791 0.096	155.1 1.029 0.077
153.6 2.193 0.136	166.7 1.334 0.134	167.1 0.809 0.100
166.3 2.295 0.147		A COMPANY OF THE COMP
K= 1002.	K= 1102.	K= 1204•
W* 1661.	W= 1717.	W= 1772.
107.3 2.643 0.169	109.1 1.138 0.118	120.0 0.419 0.065
116.9 3.050 0.162	118.5 1.265 0.094	128.4 0.615 0.079
125.5 3.359 0.174	127.0 1.650 0.107	137.4 1.012 0.093
134.9 2.863 0.180	136.2 1.713 0.133	146.8 1.069 0.114
144.8 2.750 0.190	145.9 1.862 0.155	155.3 1.046 0.073
153.8 2.353 0.136	154.6 1.524 0.089	167.2 0.592 0.090
166.4 2.165 0.147	166.8 1.156 0.115	
	angananananan (ilai kataman kataman kataman ilai kataman kataman kataman kataman kataman kataman kataman katam	
K= 1028.	K= 1131.	K= 1235.
W= 1676.	W= 1733.	W= 1788.
107.8 2.248 0.159	109.6 0.704 0.122	120.5 0.392 0.062
117.3 2.880 0.162	119.0 0.881 0.082	128.8 0.578 0.075
125.9 2.984 0.169	127.4 1.041 0.107	137.8 1.020 0.090
135.3 3.034 0.180	136.6 1.252 0.113	147.1 0.829 0.114
145.1 2.817 0.183	146.1 1.640 0.146	155.6 1.074 0.073 167.3 0.359 0.090
154.0 2.212 0.105	154.8 1.207 0.077	167.3 0.359 0.090
100.7 1.470 0.147	10047 14002 VAIOO	

## TABLE 8d

## 103

## INTERPOLATED ANGULAR DISTRIBUTIONS

THETA\* SIGMA DSIGMA

THETA\* SIGMA DSIGMA THETA\* SIGMA DSIGMA

Kn 1269. W= 1806. 12C.9 0.372 0.062 129.2 0.550 0.077 138.1 0.834 0.090 147.4 0.777 0.117 155.8 0.923 0.073

## F. Summary of Experimental Errors

The random and rapidly fluctuating errors which have been included in the error bars of all cross sections are as follows:

Counting Statistics	3-5%
Irreproducibility of Runs	1.65%
(see Appendix VI)	
Negative Field Background	0-5%
Unfolding Process	1%

The systematic errors are estimated in the table below (errors of less than  $\pm$  0.5% have been ignored). These errors are to be interpreted in the sense of standard deviations.

Quantameter Calibration (21)	3%
Nuclear Absorption	1.5-3%
Bremsstrahlung Spectrum (30)	<b>2</b> %
Pi-Mu Decay Correction	1%
Liquid Hydrogen Target	1%
Electronic Efficiency	1%
Total Energy Per BIP	0.6%
Total	4-5%

## G. Data Fitting

The most important problem to be solved in data fitting is the multipole and isotopic spin decomposition of the photoproduction amplitudes. Stan Ecklund and Carl Clinesmith are presently working on this problem and are using independent methods. Stan Ecklund is using only  $\pi^+$  cross section data and has fit the angular distributions with a Moravcsik type formula. Then he is attempting to explain the coefficients of the Moravcsik fits with simple functions of energy. (9) Carl Clinesmith is attempting to fit all the data available for all the isotopic spin channels by assuming that the multipole coefficients are either Breit-Wigner forms or slowly varying functions of energy. (10) Since both of these projects are near completion, it is difficult to make a direct contribution to the fitting without also duplicating a large part of the effort.

Rather than work directly on the overall fitting project, an effort was made to explain a striking feature of the  $\pi^+$  cross section at  $180^{\circ}$  which was observed by Hand and Schaerf  $^{(16)}$  and later repeated by Schaerf. The important characteristic of this cross section is that there is a very narrow bump at a photon energy of approximately 710 MeV (W = 1490 MeV). On the basis of evidence from the forward  $\pi^{\circ}$  photoproduction cross section, D. Beder  $^{(38)}$  concluded that the ratio  $E_{2-}/M_{2-}\approx 3$  in the vicinity of the second resonance (N\*\*(1512),  $k_{\gamma}=750$  MeV) which causes the contribution of the second resonance to the photoproduction amplitudes to be small at  $0^{\circ}$  and  $180^{\circ}$ . An extrapolation of the  $\pi^+$  data of Ecklund and Walker to  $0^{\circ}$  gives the same conclusion. Theoretically Bietti has used saturated sum rules to derive the same result. Thus we expect that the second resonance does not contribute to the bump at  $180^{\circ}$  in the  $\pi^+$  cross section.

Sakurai<sup>(39)</sup> suggested that the bump might be a cusp effect at the threshold for production of the eta meson (W = 1487 MeV,  $k_{\gamma} = 708$  MeV). Since the differential cross section for single  $\pi^+$  photoproduction is smallest at  $180^{\circ}$  for energies near 700 MeV, it is possible that a small cusp in the  $S_{11}$  or  $P_{11}$  (first index = 2T, second index = 2J) part of the photoproduction amplitude would show up most at  $180^{\circ}$ .

The most extensive measurements of the eta production reaction come from the experiments of Bulos et al.  $^{(40)}$  and Richards et al.  $^{(41)}$  These experiments show that the eta production angular distribution is isotropic near threshold, which indicates that either the  $\mathbf{S}_{11}$  or the  $\mathbf{P}_{11}$  states dominate. When the total cross section is plotted as a function of energy, the first three points fall on a straight line which also passes through the threshold. From this fact, Richards et al. conclude that the  $\mathbf{S}_{11}$  state is dominant.

An examination of the results of several recent partial wave analyses  $^{(4,6,7,8)}$  of  $\pi\text{-N}$  elastic scattering shows that the  $S_{11}$  absorption parameter,  $\eta_{11}$ , is consistent with 1.0 (no absorption) below the eta threshold, but that it drops rapidly to approximately 0.5 shortly above threshold. The reaction cross section computed from the  $S_{11}$  absorption parameter is consistent with the total cross section for eta production. (41) In addition, at least two authors show a cusp behavior in the  $S_{11}$  phase shift. (4,8) On the basis of this evidence, we may conclude that a cusp at the eta threshold has been observed in S-wave  $\pi\text{-N}$  scattering and that the photoproduction data should be analyzed in terms of the same phenomenon.

The R matrix formalism of Wigner  $^{(42)}$  has been applied to the production of strange particles in  $\pi$ -N and  $\gamma$ -N interactions by Adair.  $^{(43)}$  With only negligible changes, this formalism may be

used for the production of eta mesons in the same interactions. If we assume that the absorption in the  $S_{11}$   $\pi$ -N state is due to eta production (and a small contribution from inverse photoproduction), we may use a three channel S matrix for total angular momentum 1/2, I spin 1/2, odd parity scattering where the three channels are  $\pi$ -N,  $\eta$ -N, and  $\gamma$ -N. Since a nucleon appears in each channel, we may simplify the notation by labelling the three channels,  $\pi$ ,  $\eta$ , and  $\gamma$ -N ear the eta threshold the S matrix may be written in the form

$$S_{if} = e^{+i k_i a_i} (\delta_{if} - N_{if}/D) e^{+i k_f a_f}$$

where

$$N_{if} = -2i \sqrt{k_i P_i R_{ii} R_{ff} P_f k_f}$$

$$D = 1 - i k_{\eta} R_{\eta \eta} - i k_{\eta} R_{\eta \eta} - i k_{\gamma} R_{\gamma \gamma}$$

 $a_i$  = the channel radius for channel i

$$P_i = \begin{cases} 1 \text{ above threshold in channel i } \\ 0 \text{ below threshold in channel i } \end{cases}$$

and we may take the elements of the R matrix to be independent of energy. The total cross section may be written in the form

$$\sigma_{\text{mf}} = \frac{\pi}{k_{\text{m}}^2} \sqrt{\delta_{\text{mf}} - S_{\text{mf}}} \sqrt{2}$$

and

$$\sigma_{\gamma f} = \frac{\pi}{3k_{\gamma}^2} \left| \delta_{\gamma f} - S_{\gamma f} \right|^2$$

The parameters of this formalism may be adjusted to fit the  $S_{11}$  phase shift and absorption parameter, and the eta photoproduction reaction cross section. Because of the inconsistencies of the phase shifts and absorption parameters determined by different authors, the high accuracy of a computer fit to the data is not worthwhile at the present time. However, a hand fit was made. For the purposes of this fit, the absorption parameter was assumed to be 0.5 at a pion kinetic energy (lab) of 660 MeV. The parameters were adjusted to satisfy this condition and to give a reasonable fit to the  $S_{11}$  phase shift data of Cence  $^{(8)}$  and the eta photoproduction data from Stanford. The resulting parameters were (h = c = 1)

$$R_{\Pi\Pi} = 2.096$$
  $GeV^{-1}$ 
 $R_{nn} = 3.699$   $GeV^{-1}$ 
 $R_{\gamma\gamma} = 0.019$   $GeV^{-1}$ 
 $a_{\pi} = 0.200$   $GeV^{-1}$ 
 $a_{\nu} = 0.000$   $GeV^{-1}$ 

In order to fit the  $\pi^+$  photoproduction data at  $180^{\circ}$ , it was necessary to make some assumption about the other contributions to the photoproduction amplitude. The simplest assumption was that this back-

ground was pure imaginary (pure real in the usual convention of perturbation theory). A constant background of + 0.66(  $\mu$  barn) <sup>1/2</sup> gives the best fit to the corrected Schaerf data <sup>(17)</sup> in the region of the cusp (see Section V-D for the correction to the Schaerf data). The fit and the data for the several reactions are presented in Figures 14a and 14b. The branching ratio for  $\eta \rightarrow 2\gamma$  was assumed to be 0.35 in drawing these figures.

The fit to the eta production and eta photoproduction data has the difficulty that it rises too rapidly near threshold. This problem appears to be common to several theories which neglect other open channels.  $^{(45,\,46,\,47)}$  Moorhouse and Hendry  $^{(48)}$  have shown that it is possible to correct this problem by including approximately the multiple pion production channels. However, the fit to the 180 degree  $\pi^+$  photoproduction differential cross section has the property that it gives a good fit to the shape of the cusp for photon energies within  $\pm$  50 MeV of the eta threshold.

The conclusion derived from this fit is that it is possible to explain the  $\pi^+$  photoproduction differential cross section at 180 degrees in terms of a cusp at the eta threshold, and that this interpretation is consistent with present data on pion scattering, eta production, and eta photoproduction. This interpretation removes a possible difficulty with the assumption that  $E_{2-}/M_{2-}=3$  in the vicinity of the second resonance.

On the basis of pion scattering and eta production data, several authors have made conclusions about the source of the cusp. (46, 47, 48) These authors conclude that there is an eta-nucleon state at approximately the eta nucleon threshold (1487 MeV). This state should be called a resonance if the mass of the "particle" is greater than the threshold, or a virtual bound state if the mass is



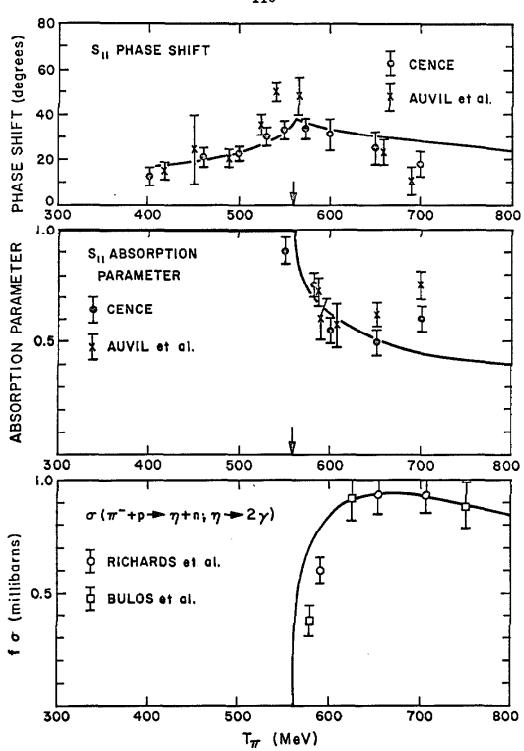


Figure 14a. Cusp Fit to  $\pi$ -N Channel

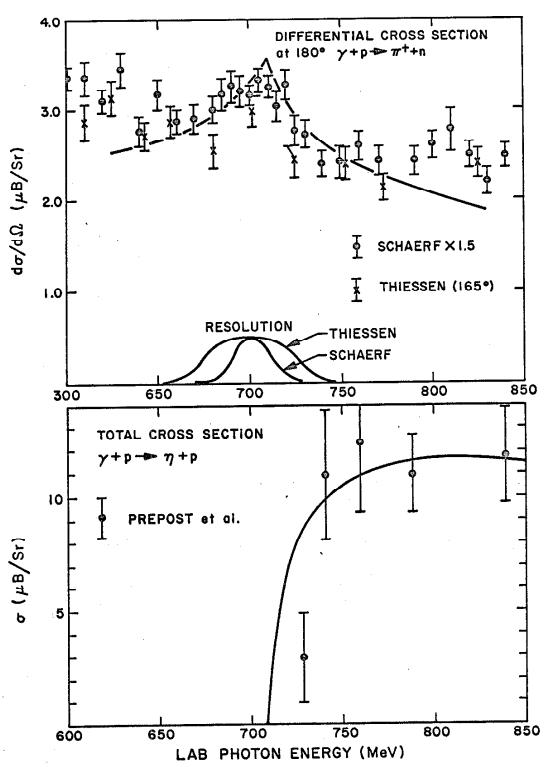


Figure 14b. Cusp Fit to Photoproduction

less than threshold. This particle has been speculatively identified with the  $\widetilde{N}$  particle of the  $\eta$ -baryon octet  $B=(\widetilde{N},\ \widetilde{\Lambda},\ \widetilde{\Sigma},\ \widetilde{\Xi})$  postulated by Gyuk and Tuan. (49) Further data on  $\pi$ -N scattering and eta production are required before the mass of this state can be determined accurately.

### VL CONCLUSIONS AND SUGGESTIONS

A large number of points of the differential cross section for  $\pi^+$  photoproduction at backward angles were measured in this experiment. When combined with the data of Ecklund and Walker  $^{(9)}$ , reasonably complete angular distributions are available for all energies between 589 MeV and 1269 MeV. These data can be used to make a considerable improvement in the precision of the phenomenological analysis of pion photoproduction in the region of the second and third  $\pi\text{-N}$  resonances. Because of operational difficulties with the synchrotron, it was not possible to continue the experiment into the region of the first resonance which has been measured carefully. Thus a similar experiment should be performed covering the energy region from approximately 350 MeV to 650 MeV. It may be necessary to do this experiment at a different accelerator: the Mark III Linac at Stanford University is a logical choice.

In order to obtain a unique multipole and isotopic spin decomposition of the photoproduction amplitudes, it will be necessary to take cross section and polarization data on the other pion photoproduction reactions. The most direct way to start on this program would be to measure the differential cross section for the reaction  $\gamma + n \rightarrow \pi^- + p$  using a deuterium target. A synchrotron subtraction might be used to separate the events coming from free neutrons. With careful planning, it would be possible to take data with both magnets simultaneously. It should be emphasized that absolutely no apparatus changes are required to perform this experiment! Later, a carbon plate spark chamber might be added to measure the recoil proton polarization as an extension of the same experiment.

If a polarized proton target with the order of 20% polarized, free protons can be developed, it would be possible to measure the polarized target asymmetry in the reaction  $\gamma + p \rightarrow \pi^+ + n$ . A synchrotron subtraction would be required to separate the events due to free protons.

Another interesting experiment would be to extend the  $\pi^+$  differential cross section measurements to exactly  $180^\circ$ . However, this experiment would require significant changes in the magnet and beam line geometry. Since some data are already available, this experiment should be assigned a lower priority than the previously suggested experiments.

Two improvements in the apparatus would prove to be useful. First, an electron counter could be installed. Such a counter might reduce the field reversed background which was as much as 10% at high energies. Second, the paper tape punch might be replaced with an on-line link to the campus IBM 360 series computers. Including the price of a remote console (with typewriter input-output), the design and construction cost of the required hardware would be on the order of \$4000. Such a data link would reduce the turn around time for data processing from several days to a few minutes, and experimental errors would be more easily detected. In addition, the reliability of the system would be significantly improved by eliminating the mechanical tape punch and the paper tape to magnetic tape conversion system.

# APPENDIX I. BEAM MONITORING AND HYDROGEN TARGET DETAILS

The several beam monitors used during this experiment include the quantameter, the beam catcher thick ion chamber, two thin ion chambers, a counter telescope mounted at 90° from the beam line under the hydrogen target, and the "40 mc. probe" which monitored the intensity of the circulating beam. The locations of these monitors are shown in Figure 1.

with the standard electronic integrators used in this laboratory for many years. Each time a specified amount of charge has been collected, these integrators put out a pulse called a BIP (beam integrator pulse) and this pulse is usually used to operate a Sodeco mechanical counter. Unfortunately, the generation of the output pulse and the determination of the amount of charge per BIP depend on two relays. If either of these relays chatter or the contacts get dirty, it is possible to get a wrong charge/BIP ratio. For this reason, it is important to use several beam monitors even if the beam monitors themselves are stable. The output of the 40 mc. probe is monitored by a voltage-to-frequency converter and the result is counted on an electronic scaler. The counter telescope output is also counted on an electronic scaler. No difficulties with the readout mechanism for either of these beam monitors was observed.

The normalization of this experiment depends on the quantameter charge output. However, the quantameter cannot be left in the beam line during a data taking run as it absorbs all the energy in the beam. It is not possible to place the quantameter in the beam catcher since the beam spot is too large at that location. Thus this experiment also depends on an intercalibration with secondary monitors.

with the quantameter are the 40 mc. probe and the two thin ion chambers. Unfortunately, the charge collected by thin chamber No. 2 was strongly dependent on the status of the UCLA hydrogen target. In addition, the integrator used with this ion chamber was found to be very unstable. After a short trial period, the use of this ion chamber was discontinued. The two remaining monitors, TC-1 and the 40 mc. probe, were intercalibrated against the quantameter in a short run before and after each data taking run.

The monitors which are available only during a data taking run are the monitor telescope and the beam catcher ion chamber. The beam catcher ion chamber should be as good as the quantameter, except that its calibration depends on the energy of the synchrotron. In addition, the beam catcher ion chamber is not available when the yoke of the High Energy Magnet is in the beam line. Since the beam catcher ion chamber and the quantameter are never available simultaneously, the same integrator was used for both. Thus the ratio Q/BC is independent of slow drifts in the integrator. The monitor telescope has also been demonstrated to be stable. Unfortunately, the monitor telescope was operated from the High Energy Magnet Electronics. Since Mr. F. Wolverton was constantly testing and changing the electronics and turning the power supplies on and off, keeping the monitor telescope calibrated proved to be a tedious chore and its use was eventually discontinued. The monitor telescope probably should be set up as a lab instrument and made to be independent of the transistor power supplies for either magnet.

The procedure used to calculate the number of quantameter BIPs was to calibrate the 40 mc. probe and TC-1 against the quantameter in a short run before and after each data taking run. The average ratios  $\langle$  Q/40 mc. $\rangle$  and  $\langle$  Q/TC-1 $\rangle$  were calculated from these short calibration runs. The number of quantameter BIPs based on each of these intermediate monitors was calculated from these average ratios and the number of TC-1 and 40 mc. BIPs obtained in the data run, i. e.

Q40 = 40 mc. 
$$\times \langle Q/40 \text{ mc.} \rangle$$
  
QTC = TC-1  $\times \langle Q/\text{TC-1} \rangle$ 

The beam catcher ion chamber could be intercalibrated against the quantameter only by comparing BC with Q40 and QTC. This intercalibration was done for each night's running by comparing the total BC for a night with the average of Q40 and QTC. The formula used was

$$\langle Q/BC \rangle = \frac{\Sigma(Q40 + QTC)}{2\Sigma BC}$$

where the sum represents the normal data runs taken during one night. Then the number of quantameter BIPs for each run was computed using BC and the average ratio given above, namely

QBC = BC 
$$\times \langle Q/BC \rangle$$

Finally, the number of quantameter BIPs for a given run was calculated from the average of Q40, QTC, and QBC. This final value, QAVG, was used for all cross section calculations.

This complicated averaging procedure had the advantage that a gross error in one of the monitors was easily detected. When an error of more than  $\sim 2\%$  was detected, the suspected number was ignored and QAVG was recomputed using all the remaining information. Similarly, QBC was ignored when the High Energy Magnet was in the beam line. By using this technique, the r. m. s. deviations of the individual monitors from QAVG were  $\pm$  0.5%, except at  $E_0$  = 1350 MeV where  $\pm$  1.0% was observed. These errors are presumably already included in the random error deduced from a series of plexiglass target runs (see Appendix VI), and this error was included in the error bars on all cross sections measured in this experiment.

The ratio of Q/BC observed at several energies in this experiment may be of use to future experiments. These ratios are given in the following table:

E <sub>o</sub> (meter)	Q/BC
660	11. 32 $\pm$ 0. 07
750	11. $18 \pm 0.07$
850	11.35 $\pm$ 0.07
950	11.67 $\pm$ 0.07
1050	11.64 $\pm$ 0.07
1150	11.79 $\pm$ 0.07
1350	12.07 $\pm$ 0.12

The quantameter calibration constant,  $\mathbf{U}_{\mathbf{Q}}$ , is given by the relation

$$U_Q = (4.80 \pm 0.14) \times \frac{2.730}{P/T} \times 10^{18} \text{ MeV/coulomb}^{(21)}$$

where P and T are the absolute pressure and absolute temperature of the quantameter gas in mm. Hg. and <sup>0</sup>K respectively. The P/T ratio appears to fluctuate by ± 0.5% r.m.s. and, in addition, a gradual drop was observed. The random fluctuation may be due to non-equilibrium thermal effects (see separate report). (50) The typical quantameter gas pressure was 715 mm. Hg. which was well below atmospheric pressure. Thus the gradual drop must be due to an absorption or selective leakage process which has never been understood. In any case, the P/T value for the first period of data taking (run no.  $\leq$  700) was 2.445  $\pm$  0.010, while during the second period of data taking (run no.  $\geq$  701) the ratio of P/T was 2.413  $\pm$ 0.010. Integrator No. 0628 was always used with the quantameter. For some early data (run no. < 407), the integrator was used on scale 3 with a charge/BIP ratio of 2.225  $\pm$  0.005  $\times$  10<sup>-7</sup> coulomb/BIP. For all later data, the integrator was operated on scale 4 with a charge/BIP ratio of 2.235  $\pm$  0.005  $\times$  10<sup>-6</sup> coulomb/BIP. The resulting values for the total energy per QBIP are given in the following table.

Run Number	Total Energy/QBIP
000-407	$(0.1192 \pm 0.0007) \times 10^{13} \text{ MeV/QBIP}$
408-700	$(1.198 \pm 0.007) \times 10^{13} \text{ MeV/QBIP}$
701-1348	$(1.214 \pm 0.007) \times 10^{13} \text{ MeV/QBIP}$

The liquid hydrogen is contained within an 0.005" wall Mylar cylinder approximately 3" in diameter. On September 24, 1965, this cup was accidentally broken during the normal cleaning process (no liquid hydrogen was in the target at the time). The Mylar cup was replaced by a new one which was approximately the same diameter. The cup diameter was measured by Mr. Earl Emery at room temperature with a 15 psi pressure on the inside of the cup. The results for the two cups are:

run number  $\leq 700$  3.003  $\pm 0$ 

 $3.003 \pm 0.005$ " diameter

run number > 700

2.980  $\pm$  0.005" diameter

The diameter of the cup must be reduced by 0.4% to correct for the contraction of the Mylar at liquid hydrogen temperature. (51)

The liquid hydrogen in the cup is operated at the boiling point and a pressure of 0.5 psi is maintained by a safety check valve. Under these conditions, the hydrogen temperature is  $20.30^{\circ} \text{K}^{(52)}$  and its density is  $0.0711 \text{ gm/cm}^3$ . Since the ''empty' target runs were taken with hydrogen gas at the same temperature and pressure, the gas density of  $0.0014 \text{ gm/cm}^3$  (52) must be subtracted from the liquid hydrogen density to give an effective density of  $0.0697 \text{ gm/cm}^3$ .

The number which is used in the cross section calculation is  $\rm N_H$ , the number of protons per cm² in one diameter of the hydrogen target. Taking Avogadro's number to be 6.025  $\times$  10 $^{23}$  the atomic weight of hydrogen to be 1.008 (which assumes that the deuterium contamination in the liquid hydrogen is small), and the target parameters discussed above, we find that  $\rm N_H$  is

$$N_{H} = \begin{cases} 3.162 \pm 0.030 \times 10^{23} \text{ for run number} \le 700 \\ 3.138 \pm 0.030 \times 10^{23} \text{ for run number} > 700 \end{cases}$$

The error associated with  $\rm N_{\mbox{\scriptsize H}}$  is arbitrarily taken to be  $\pm$  1% which includes the errors in geometry and the hydrogen density.

## APPENDIX II. NUCLEAR ABSORPTION

All of the pions detected in this experiment had to pass through matter including the hydrogen target vacuum jacket, air, and several counters. Some of the pions incident upon the system interacted with this matter and were lost. For the purposes of this experiment, any interaction other than multiple scattering was defined as nuclear absorption.

The nuclear absorption for several locations of absorbers was measured. The technique consisted of placing an additional piece of matter in the path of the pions and noting the difference in counting rate with the additional absorber in or out of the path. In order to get sufficient statistics, a plexiglass target was used, and several runs were taken with absorber in and out. The normal reproducibility of runs over short times precludes any measurement to an accuracy better than  $\pm$  1% of the no absorber rate. The data taken by this direct technique appear in Table 9.

An improved method of measuring the nuclear absorption was used for measuring the effects of nuclear absorption in the counter telescope at the rear of the magnet. For these measurements, a pion was defined by all the counters but the last. A certain fraction of the pions defined in this way did not count in the last counter. This fraction increased when an additional absorber was placed just ahead of the last counter. The difference between the fractional miss rate with and without the additional absorber was defined as the absorption in the additional absorber. In order to measure the effect of an absorber placed a long distance from the last counter, it was necessary to move the last counter further from counter p<sup>1</sup> than the normal configuration. Thus some data were

TABLE 9. Absorption Measurements by Direct Method

Location	Absorber	Momentum	Absorption
At counter S1			·
26 1/2" ahead of S2	1" plexiglass	300	$0.073 \pm 0.010$
		400	$0.044 \pm 0.010$
		570	$0.038 \pm 0.010$
At counter A 87" ahead of S2	1/2" pl exiglass	570	$0.032 \pm 0.010$
At hydrogen target	3/8''aluminum	570	0.039 ± 0.010
	•		

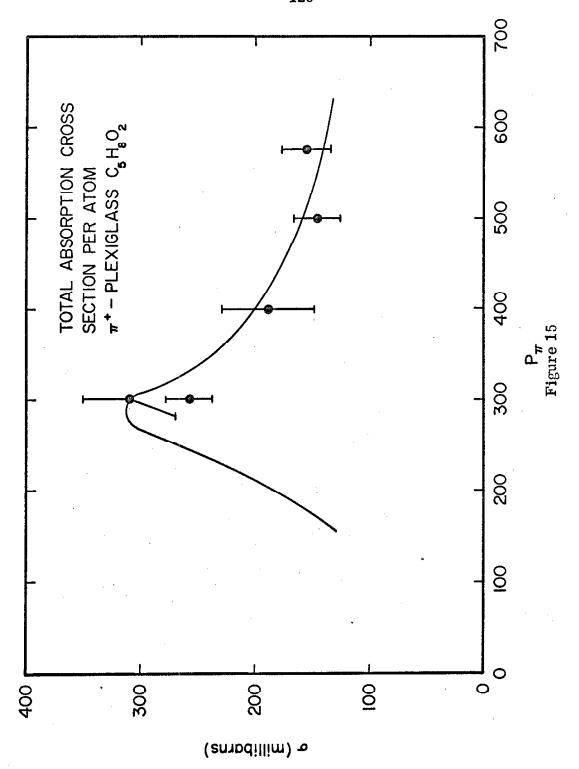
TABLE 10. Absorption Measurements by Improved Method

Distance Absorber to S2	Configuration	Absorber	Momentum	Absorption
18''	long	1" plexiglass	500  MeV/c	$0.0350 \pm 0.0048$
12''	long	1'' plexiglass	$500~{ m MeV/c}$	$0.0227 \pm 0.0044$
8 1/2"	long	1" plexiglass	$500~{ m MeV/c}$	$0.0133 \pm 0.0042$
8 1/2"	normal	1" plexiglass	$500~{ m MeV/c}$	$0.0217 \pm 0.0024$
6"	normal	1'' plexiglass	$500~{ m MeV/c}$	$0.0167 \pm 0.0024$
2 1/2"	normal	2" plexiglass	500  MeV/c	$0.0359 \pm 0.0026$
18''	long	1" plexiglass	$300~{ m MeV/c}$	$0.0590 \pm 0.0050$
14''	long	1" plexiglass	$300~{ m MeV/c}$	$0.0519 \pm 0.0032$
9 1/4"	normal	1" plexiglass	$300~{ m MeV/c}$	$0.0494 \pm 0.0034$
611	normal	1" plexiglass	$300~{ m MeV/c}$	$0.0390 \pm 0.0041$
2 1/2"	normal	1" plexiglass	$300~{ m MeV/c}$	$0.0250 \pm 0.0044$

taken with two different geometries: one with the last counter in its normal position 12" behind S1, and one with the last counter mounted 24" behind counter  $p^i$ . The statistical accuracy of the data taken with this technique is greater than for the data taken by the direct method, however unknown systematic errors may have entered because of the different geometry and the different event definition. The data taken by this method in both configurations is presented in Table 10.

Some data on the interaction of pions with light nuclei exist in the literature. (54,55,56,57,58) The main data for pion momenta comparable to those used in this experiment comes from bubble chamber studies. These studies indicate that the  $\sigma \propto A^{2/3}$  law is verified, but that the constant of proportionality varies with the incident pion momentum. In addition, the majority of the events are inelastic. This is to be contrasted with the  $\pi^+$  p interaction which is almost entirely elastic at low momenta. The number obtained from the bubble chamber experiments is called the total absorption cross section. This cross section includes all events with a scattering angle greater than a specified cutoff, but it does not include diffraction scattering.

The dependence of the nuclear absorption on the distance from the last counter is explained by the fact that the solid angle for detecting a secondary from an absorption event depends on this distance. For an absorber at counter S1, the counter system will accept only those events which scatter less than about 30°. This cutoff is approximately the same as the one used for the total absorption cross section in the bubble chamber measurements. Thus the nuclear absorption measurement for absorber placed 26" from counter S2 can be used to calculate a number for the total



absorption cross section for pions on plexiglass. The cross section must be divided by f, the fraction of events due to pions, for the muons in the beam defined at the rear of the magnet have a much smaller total cross section. The details of calculation are presented in Table 11.

In order to calculate the total absorption cross section per atom for pions on plexiglass ( $C_5H_8O_2$ ), the cross section from each of the three constituent elements was calculated. The total cross section for hydrogen was taken from the well known  $\pi^+$  p total cross section. (59) The carbon and oxygen cross sections were computed from the  $A^{2/3}$  law and the bubble chamber measurement of  $\sigma/\sigma_{geom}$ . (55) The measured and expected values of this total absorption cross section are presented in Figure 15. The data and the calculation agree very well.

The absorption correction which was used for the cross sections of this experiment was calculated in a similar manner. First, each piece of matter through which the pions must pass was reduced to a mass of hydrogen and an equivalent mass of carbon using the  $A^{2/3}$  law. In order to correct for the fact that some of the secondaries from an absorption event may be counted, an empirical factor,  $\eta$ , was defined as the ratio of the measured absorption (from Tables 9 and 10) to the absorption calculated from the total cross section. Then the effective mass of each absorber was defined as the product of  $\eta$  and the equivalent mass of each absorber, and the absorption resulting from the total effective mass of carbon and hydrogen was computed from the total cross sections. Finally, the absorption was multiplied by the fraction of the events which are due to pions, assuming that the muons have negligible total cross section.

TABLE 11. Calculation of Total Absorption Cross Section per Atom for Pions Incident on Plexiglass  $({\rm C_5H_8O_2})$ 

P (MeV/c)	Measured Absorption in 1'' Plexiglass	oT per atom (mb.)	Fraction of Pions in Beam	Corrected  T per atom (mb.)
300	0.070 $\pm$ 0.010	$259\pm37$	0.84	$310\pm45$
300	$\textbf{0.059} \pm \textbf{0.005}$	<b>2</b> 09 ± <b>1</b> 7	0.84	$250 \pm 20$
400	$0.044 \pm 0.010$	$162 \pm 35$	0.87	$187 \pm 40$
500	$0.035 \pm 0.005$	$129 \pm 18$	0.89	$146 \pm 20$
570	0. 038 + 0. 010	140 ± 36	0, 90	156 ± 40

In Table 12 is presented a list of the various absorbers in the system, the mass of each absorber, the factor  $\eta$  for each absorber, and the effective mass of each absorber. The fact that  $\eta$  is statistically consistent with 1.0 for most of the matter of the system is evidence that the calculation is correct. Some intermediate results and the final numerical values for the absorption as a function of momentum are presented in Table 13. The absorption correction used for the cross section calculation was obtained by linear interpolation in this table. Some additional absorption was added because the pions must pass through a thicker part of the hydrogen target structure at certain angles. This additional absorption was 3.0  $\pm$  0.8% at 34° lab and 0.9  $\pm$  0.2% at  $40^{\circ}$  lab. Since only three momenta near 500 MeV/c were used at these angles, the momentum dependence of the additional absorption was ignored.

The error of the absorption correction depends directly on the statistical errors of the absorption measurements. Considering the fact that measurements were made at a very limited number of momenta, it is expected that the error in the absorption correction is  $\pm$  25% of the correction. This results in a 1.5 - 3.0% normalization error in the cross sections.

TABLE 12. Material Through Which Pions Pass

N.	Majerial	Compo-	$ m em/cm^2$	gm/cm C equi- (	$ m gm/cm^2_H$	E	Effectivgm/cm <sup>2</sup> C	Effective Mass $n/cm$ $cm$ $cm$ $cm$ $cm$ $cm$ $dm/cm$ $dmiv$
	I ionid Hudnomen	<u> </u>	0 23	00 0	0, 23	1.0*	0	0, 230
141801	Mylar	CH	0.02	0.02	0		0.03	0
	Heat Shield	ņ Cn	0.04	0.02	0	1, $5 \pm 0$ , 4	0.03	0
	Outer Shield	A1	0.43	0.33	0		0.50	0
Air	Target to Counter A	$N_{8}O_{9}$	0.25	0.23	0	1.0*	0.23	0
Counter A	Ne 102 Scintillator	$C_{10}H_{11}$	0.47	0.44	0.03	1. $2 \pm 0.3$	0.53	0.036
Air	Counter A to Counter S2	N <sub>8</sub> O <sub>2</sub>	0, 25	0.23	00.00	1.0*	0.23	130
Counter S1	Ne 102 Scintillator	$C_{10}H_{11}$	0.69	0.65	0.044	$0.95 \pm 0.05$	0.64	0.042
	Wrapping	Al Al	0.07	0.05	0		0.05	0
Counter Pi	Ne 102 Scintillator	$C_{10}H_{11}$	1.06	1,00	0.067	$0.64 \pm 0.05$	0.64	0.043
	Wrapping	A1	0.07	0.05	0		0.03	0
Counter LC		$C_{\kappa}H_{k}O_{s}$	2, 98	2.66	0.24	$0.40 \pm 0.05$	1.06	0.096
	Wrapping	Ai V	0.07	0,05	0		0.02	0
Counter S2	Ne 102 Scintillator	$C_{10}H_{11}$	0.37	0.35	0.02	$0.30 \pm 0.05$	0.11	0.011
	Wrapping	Ai	0.04	0.02	0	To+0.	0.00	0 458
						Total	4.10	00 P

Δ

\* Assumed

TABLE 13. Calculation of Nuclear Absorption Vs. Pion Momentum

p <sub>π</sub> (MeV/c)	ogeom carbon (mb.)		Absorp- ti on π-C (%)	σ <sub>π-p</sub> (mb.) <sup>4</sup>	Absorption π-p (%)	•	fraction of events due to pions	Total
198	330	0.861	5. 92	70	1. 93	7.85	0.79	6.2
233	330	1.08 <sup>1</sup>	7.43	110	3.02	10.45	0.80	8.3
259	330	1. 17 <sup>1</sup>	8.13	162	4. 45	12. 58	0.82	10.3
282	330	1. 17 <sup>1</sup>	9. 13	205	5.63	13.76	0.83	11.4
305	330	1. 18 <sup>1</sup>	8.20	190	5.25	13.45	0.84	11.3
332	330	1.041	7. 17	158	4.35	11. 52	0.85	9.8
354	330	0.961	6.61	135	3.71	10.32	0.85	8.8
376	330	0.951	6.55	105	2.88	9.43	0.86	8. 1
398	330	0.911	6.21	90	2. 47	8.68	0.87	7.7
522	330	0,822	5.66	<b>2</b> 5	0.69	6.35	0.89	5. 7
6 <b>2</b> 5	330	$0.74^2$	5. 10	20	0.50	5.60	0.90	5.0
727	330	0.663	4.56	17	0.47	5.03	0.91	4. 5

## computed for

<sup>0.458</sup> grams hydrogen 4.16 grams carbon equivalent

<sup>1.</sup> Meshkovskii et al. <sup>(55)</sup>

<sup>2.</sup> Interpolated

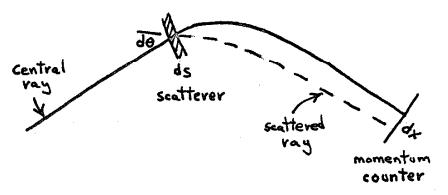
Cronin et al. (58)
 Jacob and Chew (59)

### APPENDIX III. MULTIPLE SCATTERING

Multiple scattering in the matter through which pions pass affects the results of the experiment in two ways. First, some events may be scattered out of the apertures and lost. In addition, multiple scattering causes a degrading of the momentum resolution and angular resolution of the spectrometer.

The loss of events due to scattering out of the apertures was investigated under the assumption that the spectrum of pions incident on the spectrometer is independent of angle and momentum. An analytic calculation verified that these losses are less than 0.5% for pion momenta greater than 200 MeV/c. A similar, but less accurate, result was obtained in a Monte Carlo calculation of multiple scattering losses in the High Energy Magnet by J. Kilner. (13)

In the 600 MeV/c spectrometer, the momentum of a particle is defined by the intercept of the particle trajectory and the momentum counter. Multiple scattering ahead of the plane of the momentum counter causes a smearing of this intercept and results in a wider momentum resolution function. The effects of multiple scattering in an optical system can be calculated analytically if first-order optics and Gaussian multiple scattering are assumed. Under these assumptions, we may calculate the contribution of a scatterer of thickness ds at the point s along the central ray of the spectrometer



to the uncertainty, dx, in the intercept of the ray with the momentum counter. The mean square projected scattering angle resulting from multiple scattering in thickness ds is given by the relation

$$\langle d \theta^2 \rangle = (\frac{E_{ps}}{p \beta}) \frac{ds}{x_0(s)}$$

where  $x_0(s)$  is the radiation length of the scatterer at point s, p and  $\beta$  are the momentum and velocity of the particle, respectively, and  $E_{ps}$  is the multiple scattering constant for the projected distribution.  $E_{ps}$  is related to the constant,  $E_s$ , defined by Rossi<sup>(60)</sup>, by the relation

$$E_{ps} = E_{s} / / 2 = 14.9 \text{ MeV}$$

Since, in the first order approximation, dx and ds are linearly related, we may write

$$\langle d x^2 \rangle = L^2 (s) \langle d \theta^2 \rangle$$

where L(s) is given by the first order magnet theory. Since the scattering at each point along the trajectory is independent of the scattering at any other point, we may write the relation for the total mean square displacement as

momentum
$$\langle d x^{2} \rangle = \frac{E_{ps}}{p \beta}$$

$$\int_{\text{hydrogen target}} \frac{L^{2}(s)}{x_{o}(s)} d s$$

The contributions of the various scatterers to this integral are given in the table below

Scatterer		$\int \frac{L^2(s) d s}{x_0(s)}$
liquid hydrogen		0.05
hydrogen target s	tructure	4.05
air front		6.25
center		10.92
rear		9.60
counter A		54. 40
counter S1		2.22
	Total	87.57 in <sup>2</sup>

To relate the root mean square displacement,  $\langle dx^2 \rangle^{1/2}$ , to a root mean square uncertainty in momentum,  $\langle (\frac{dp}{p})^2 \rangle^{1/2}$ , we must divide by the dispersion of the spectrometer, D = 51.7 inches,

$$\langle \left(\frac{dp}{p}\right)^2 \rangle^{1/2} = \frac{\langle dx^2 \rangle^{1/2}}{D} = 0.181 \frac{E_{ps}}{p \beta}$$

When the multiple scattering is folded into the natural resolution of the spectrometer, the momentum resolution becomes a function of the central momentum of the spectrometer. The r.m.s. width of the momentum resolution at several momenta is given in the table below

P (MeV/c)	$\langle  (rac{\mathrm{d} p}{p})^2   angle^{ 1/2}$ natural	$\langle \left( rac{\mathrm{dp}}{\mathrm{p}}  ight)^2  angle^{1/2}$ multiple scattering	$\langle \left(\frac{dp}{p}\right)^2 \rangle^{1/2}$ total
200	1. 10 × 10 <sup>-2</sup>	1.63 × 10 <sup>-2</sup>	1.94 × 10 <sup>-2</sup>
300	1. 10	0.94	1. 45
400	1. 10	0.71	1. 31
500	1. 10	0.56	1. 23
600	1. 10	0.46	1. 19

A similar method has been used to calculate the r.m.s. angular resolution due to multiple scattering. The result is:

$$\langle d \theta^2 \rangle^{1/2} = 0.194 \frac{E_{ps}}{p \beta}$$

## APPENDIX IV. n-u DECAY CORRECTIONS

The decay of the  $\pi^+$ , namely,  $\pi^+ \to \mu + \nu$  is a problem in any experiment with a long flight path. In this experiment, as many as 30% of the pions decay in the 421 cm. distance from the hydrogen target to counter  $p^i$ . If the counter system of the spectrometer were able to distinguish pions from muons, then the decay would simply reduce the number of events observed. However, since pions and muons were indistinguishable, some of the muons from the decay of pions were counted. In general, the muons counted did not come from pions which had the same momentum that the spectrometer was set for. Thus the momentum resolution functions of the spectrometer had long tails due to pions counted indirectly by the decay process.

The analytic calculation of the number of muons accepted by the spectrometer is a formidable problem involving multiple integrals with variable limits. A calculation of this type was performed by Dixon and Walker. (12) The same calculation can be easily coded for a digital computer if the Monte Carlo method is used. Such programs have been coded by Boyden (18) and Kilner. (13)

The Monte Carlo method was very inefficient and used large amounts of computer time. In order to obtain accurate resolution functions, it was necessary to run the Monte Carlo program for a few points and parameterize the output in such a way that the decay corrections could be used under a wide variety of kinematic conditions. In order to make this parameterization, it was assumed that a resolution function for the central momentum channel could be written as a function of P and  $P_{_{\rm O}}$  only. This resolution function gives the solid angle for accepting the decay muon from a pion with

momentum between P and P + dP and with the magnet set at momentum  $P_o$ . A table of values of the solid angle for several values of  $P_o$  and  $\frac{P-P_o}{P_o}$  was computed by the Monte Carlo program. Then at fixed  $(P-P_o)/P_o$ , the solid angle was fit with a quadratic in  $P_o$ . The coefficients of this fit are presented in Table 14. The raw data were computed for  $P_o = 200$ , 300, 400, 500 and 600 MeV. These data, and the value of  $\Delta\Omega$  computed from the fit, are presented in Figures 16-a - 16-e. The points computed from the fit are connected by straight lines in these figures, since the trapezoid rule has been used for doing integrals with these functions.

The Monte Carlo program which was used to calculate the results of Table 14 was originally written by J. Kilner in FORTRAN II. (13) This program is described in his thesis. The program was converted to FORTRAN IV by the program SIFT, then it was modified to be able to compute results for a nearly vertical rear aperture counter. Finally, a modification was made to correctly compute the off-symmetry plane magnet optics in the first order model. (61)

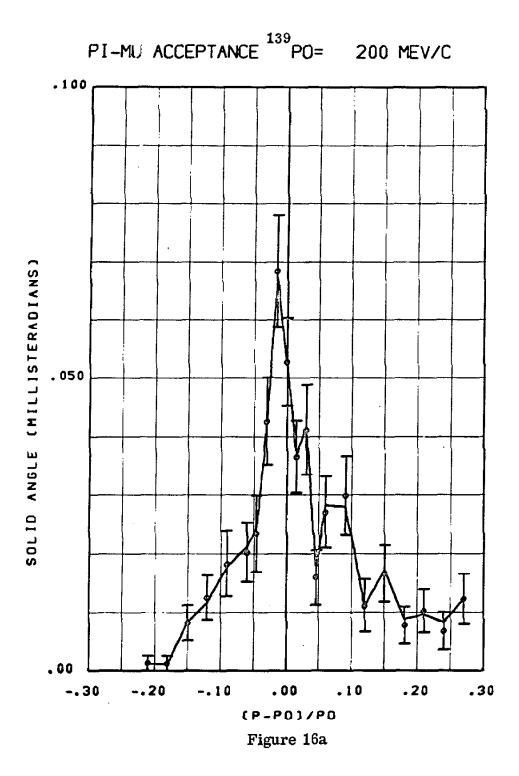
Three approximations are involved in the use of the resolution functions presented in Table 14. The first is that the effect of the lab angle of the spectrometer is negligible. The only place that this angle enters is in the projection of the length of the illuminated region of the hydrogen target on a plane perpendicular to the central ray. All the computations were done for  $\theta_{lab} = 45^{\circ}$ . The second approximation is that the resolution function for the  $i^{th}$  channel can be simply computed from the Monte Carlo results for the central channel. Under the assumption that the fraction of the observed events due to muons in the  $i^{th}$  channel with momentum  $\overline{p}_i$  is the same as the fraction of events due to muons

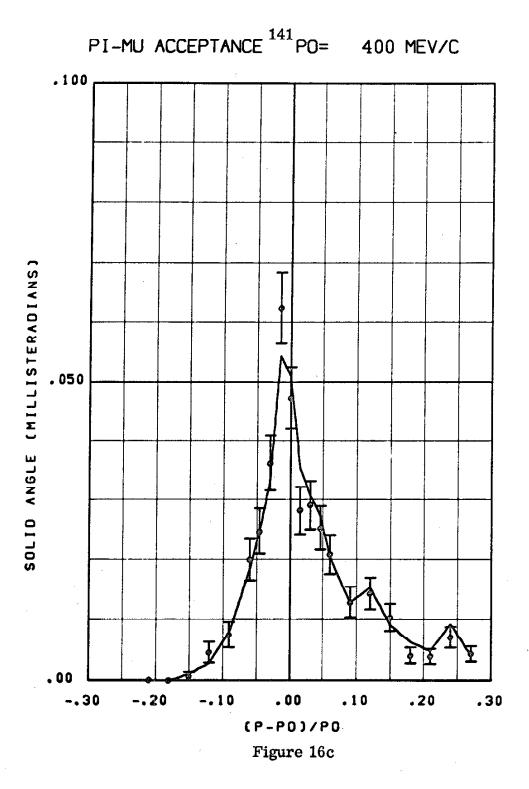
TABLE 14. Resolution Function for Pions Counted by  $\pi$ - $\mu$  Decay Process\*

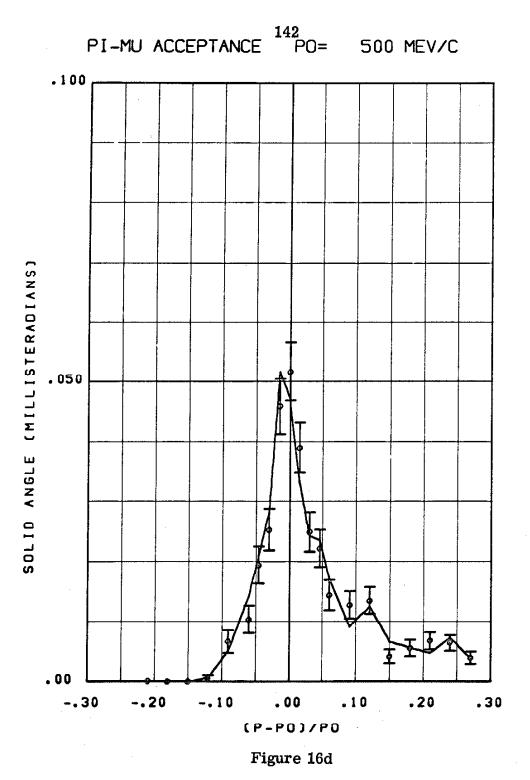
$$\Delta\Omega(\frac{P-P_{0}}{P_{0}}) = A(\frac{P-P_{0}}{P_{0}}) + P_{0}B(\frac{P-P_{0}}{P_{0}}) + P_{0}^{2}C(\frac{P-P_{0}}{P_{0}})$$

P-P <sub>o</sub>	$A(\frac{P-P_0}{P_0})$	$B(\frac{P-P_0}{P_0})$	$C(\frac{P-P_0}{P_0})$
-0, 210	$0.3789 \times 10^{-5}$	$-0.1696 \times 10^{-7}$	$0.1804 \times 10^{-10}$
-0, 180	$0.3684 \times 10^{-5}$	$-0.1649 \times 10^{-7}$	$0.1754 \times 10^{-10}$
-0.150	$0.2177 \times 10^{-4}$	$-0.8289 \times 10^{-7}$	$0.7780 \times 10^{-10}$
-0.120	$0.2709 \times 10^{-4}$	$-0.9321 \times 10^{-7}$	$0.8075 \times 10^{-10}$
-0.090	$0.3332 \times 10^{-4}$	$-0.9218 \times 10^{-7}$	$0.7159 \times 10^{-10}$
-0.060	$0.1761 \times 10^{-4}$	$0.3500 \times 10^{-7}$	$-0.8357 \times 10^{-10}$
-0.045	$0.1279 \times 10^{-4}$	$0.8415 \times 10^{-7}$	$-0.1355 \times 10^{-9}$
-0.030	$0.5264 \times 10^{-4}$	$-0.4960 \times 10^{-7}$	$0.3000 \times 10^{-11}$
-0.015	$0.9100 \times 10^{-4}$	$-0.1454 \times 10^{-6}$	$0.1335 \times 10^{-9}$
0.000	$0.4559 \times 10^{-4}$	$0.5426 \times 10^{-7}$	$-0.1024 \times 10^{-9}$
0.015	$0.3506 \times 10^{-4}$	$0.1964 \times 10^{-7}$	$-0.4764 \times 10^{-10}$
0.030	$0.4990 \times 10^{-4}$	$-0.3524 \times 10^{-7}$	$-0.3221 \times 10^{-10}$
0.045	$-0.1481 \times 10^{-4}$	$0.2197 \times 10^{-6}$	$-0.2860 \times 10^{-9}$
0.060	$0.3823 \times 10^{-4}$	$-0.5499 \times 10^{-7}$	$0.2571 \times 10^{-10}$
0.090	$0.5439 \times 10^{-4}$	$-0.1595 \times 10^{-6}$	$0.1382 \times 10^{-9}$
0.120	$-0.5887 \times 10^{-5}$	$0.1173 \times 10^{-6}$	$-0.1611 \times 10^{-9}$
0, 150	$0.2993 \times 10^{-4}$	$-0.7438 \times 10^{-7}$	$0.5571 \times 10^{-10}$
0,180	$0.1329 \times 10^{-4}$	$-0.2618 \times 10^{-7}$	$0.2187 \times 10^{-10}$
0.210	$0.2091 \times 10^{-4}$	$-0.7228 \times 10^{-7}$	$0.7999 \times 10^{-10}$
0.240	$0.9166 \times 10^{-6}$	$0.5345 \times 10^{-7}$	$-0.8128 \times 10^{-10}$
0.270	$0.3046 \times 10^{-4}$	$-0.1173 \times 10^{-6}$	$0.1285 \times 10^{-9}$

<sup>\*</sup> computed for 3.0" x 9.50" aperture counter







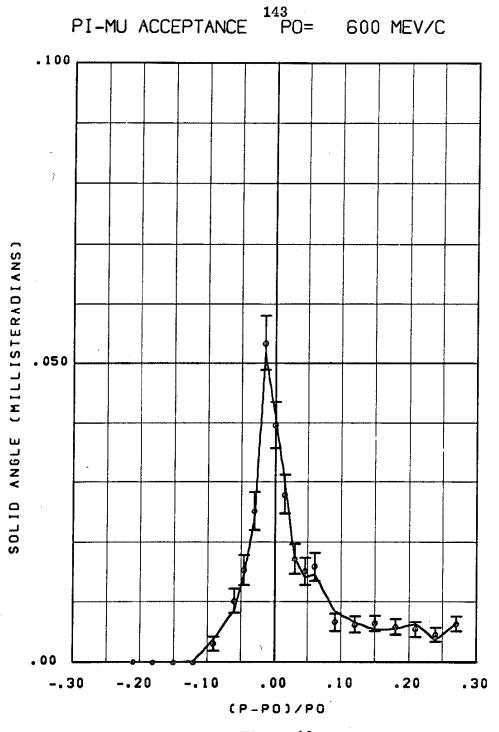


Figure 16e

in the central channel if the central momentum were set to  $\overline{p}_i$ , we find that the decay part of the resolution function for the  $i^{th}$  channel may be written as

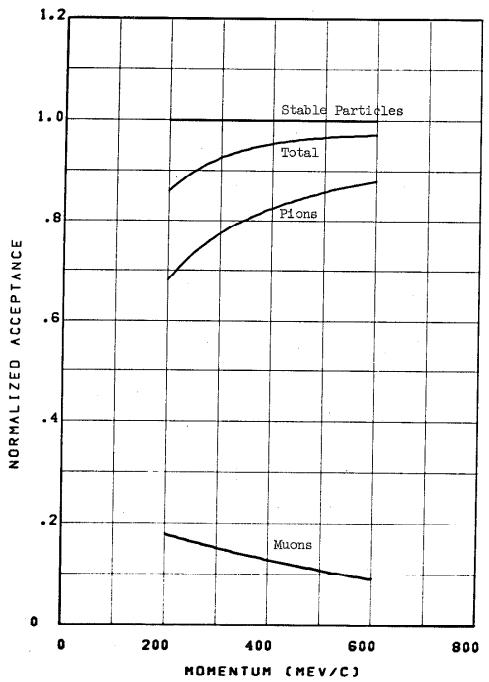
$$\Delta\Omega(\frac{p-\overline{p}_{\mathbf{i}}}{p_{\mathbf{o}}}) = \frac{(\Delta\Omega\Delta p/p_{\mathbf{o}})\mathbf{i}}{(\Delta\Omega\Delta p/p_{\mathbf{o}})_{\mathbf{central}}} \left[A(\frac{p-\overline{p}_{\mathbf{i}}}{p_{\mathbf{o}}}) + \overline{p}_{\mathbf{i}} B(\frac{p-\overline{p}_{\mathbf{i}}}{p_{\mathbf{o}}}) + (\overline{p}_{\mathbf{i}})^{2} C(\frac{p-\overline{p}_{\mathbf{i}}}{p_{\mathbf{o}}})\right]$$

where  $\bar{p}_i$  is the mean momentum of the  $i^{th}$  channel,  $p_o$  is the central momentum of the spectrometer, the coefficients

A( $\frac{p-p_i}{p_o}$ ), B( $\frac{p-p_i}{p_o}$ ), and C( $\frac{p-p_i}{p_o}$ ) are defined in Table 14, and the values of  $(\Delta\Omega\Delta p/p_o)$  for the various channels are given in Table 2. The final approximation is that the resolution functions are proportional to the area of the aperture counter. This approximation is necessary because the resolution functions were computed for a 3.0" × 9.50" aperture counter in the early days of the experiment. The size of this counter was changed to 2.75" × 9.50" before any final data was taken. The correction factor  $\frac{2.75}{3.0}$  = 0.9167 has been used to correct the coefficients of Table 14 for all the cross sections computed in this experiment.

To compute total resolution functions from the resolution functions calculated for particles which do not decay, we first multiply the no decay resolution functions by a factor which gives the fraction of the pions which do not decay in the magnet. Then we add the resolution function calculated from the coefficients of Table 14. Some summarized results of this calculation are presented in Figure 17. The fraction of pions counted by the process  $\pi \rightarrow \mu + \nu$  is computed from the trapezoid rule area of the resolution functions of Table 15. A constant cutoff at  $(P-P_0)/P_0 = +0.27$  has been used

DECAY CORRECTION SUMMARY



Acceptance for events originating as pions in hydrogen target which reach momentum counter in state indicated. Top curve is acceptance for stable particles originating in hydrogen target.

Figure 17

as well as the correction for the smaller aperture counter. The statistical error in the area of the resolution function is  $\pm$  0.3% of the total resolution function. Including the various approximations used, the decay calculation introduces a  $\pm$  1% error into the area of the total resolution functions. The decay resolution function also adds a "long tail" to the total resolution function which causes significant errors when the effects of finite resolution are considered. These effects are discussed separately in Section V-B.

## APPENDIX V. RESOLUTION CALCULATIONS

The angular resolution of the 600 MeV/c spectrometer depends on the size of the hydrogen target cup, the size of the beam spot, the size of the aperture counter, the lab angle of the spectrometer, the central momentum of the spectrometer, and the spectrometer optical properties. The angular resolution functions were computed assuming a uniform beam spot and ignoring effects of pion decay and nuclear scattering. The results of this computation for two typical cases are shown in Figure 18. The effects of multiple scattering discussed in Appendix III have been included.

The momentum resolution functions were calculated for the parameters of each data point. For this calculation the resolution functions of Figure 3 were used as input data and the effects of pion decay and multiple scattering were included. Since, in the cross section computation, the angular resolution in  $\theta^*$  was assumed to be a delta function, whereas the k resolution was treated correctly, a correction was made to the momentum resolution functions to include the effect of finite angular resolution on the photon energy resolution. This correction was made by converting the angular resolution functions discussed above into effective momentum resolution functions by the relation

$$\frac{P_{O}}{P_{O}} = \frac{1}{P_{O}} \frac{\partial k/\partial \theta}{\partial k/\partial P} (\theta - \theta_{O})$$

Then these effective momentum resolution functions were folded into the momentum resolution functions for the spectrometer after



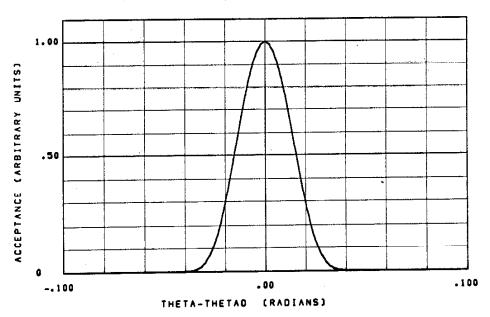
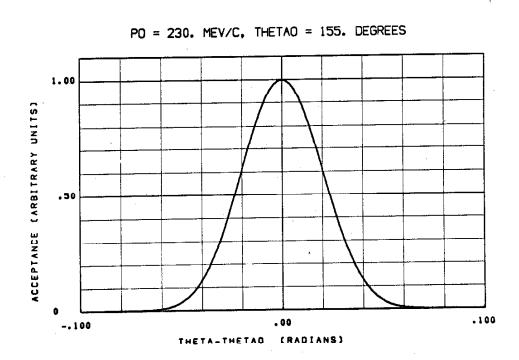


Figure 18. Laboratory Angular Resolution Functions, 600 MeV/c Magnet.



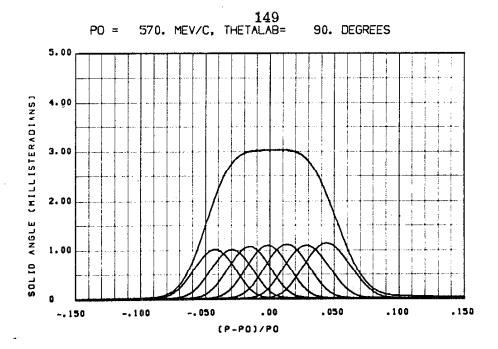
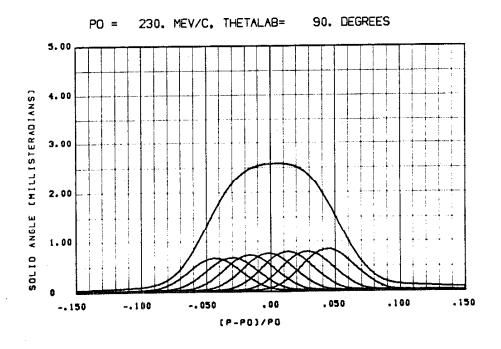


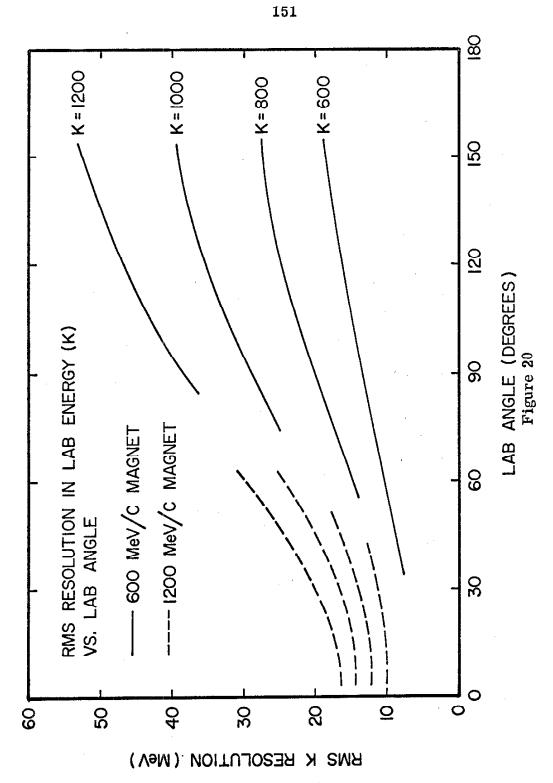
Figure 19. Total Momentum Resolution Functions, 600 MeV/c Magnet



the multiple scattering and decay effects were calculated. Two examples of the total resolution functions are given in Figure 19. Typically, the angular resolution correction increased the width of the total resolution functions by 10 - 20%.

The r.m.s. resolution in photon energy,  $\Delta k_{r.m.s.}$ , was computed from the total momentum resolution functions for each point. Since the effects of the long tails which result from pion decay were corrected by the unfolding process (see Section V-B), the pion decay part of the momentum resolution functions was ignored for the calculation of the photon energy resolution. The values of the r.m.s. resolution obtained are presented in Figure 20. For comparison purposes, the values of the resolution obtained by S. Ecklund  $^{(9)}$  are also shown.

The reasons for calculating the momentum resolution function in great detail while ignoring effects of resolution in  $\theta^*$  were threefold. First, the momentum resolution function is weighted by  $\overline{B}(k,E_0)$  in the cross section calculation and for a few measurements where k was very close to  $E_0$ , a delta function approximation to the momentum resolution function was not accurate enough. Second, the excitation curves of Section IV-D would not be expected to fit the data unless the photon energy resolution was accurately computed. Finally, at the start of the experiment, it was hoped that a successful method for unfolding the photon energy resolution could be found and it was assumed that accurate resolution functions would be required for this purpose. This final reason did not work out in practice (see Section V-B).



## APPENDIX VI. PLEXIGLASS TARGET CALIBRATION RUNS

During the second period of data taking, a series of tests was made to determine the reproducibility of results obtained by this experiment. For these tests, the hydrogen target was replaced by a piece of "Plexiglass G" of the same dimensions as the hydrogen target appendix. The kinematic conditions were set up as follows:

 $E_{o}$  850. MeV (meter)

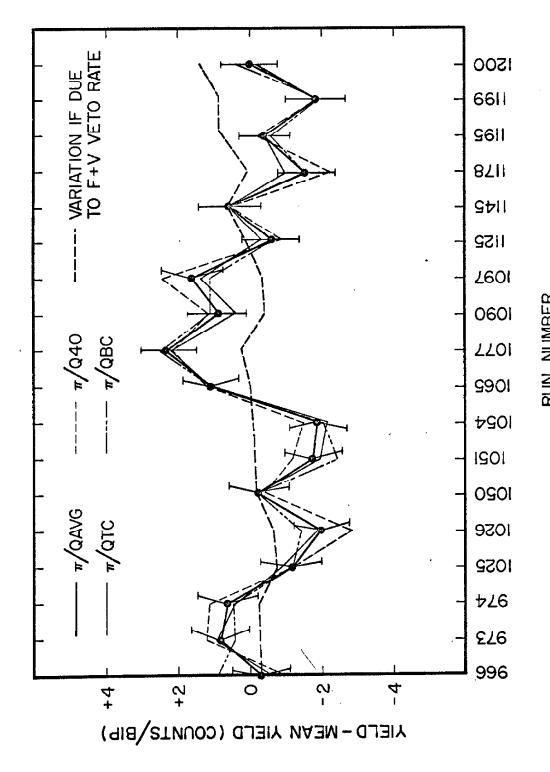
P 573. MeV/c (magnetometer frequency 68.26 mc.)  $\theta_{lab}$  51.00

These settings would yield the results for single pion photo-production at a photon energy of 775 MeV and a center-of-mass pion angle of 76° if the target were free protons. Except for the plexiglass target, the kinematic conditions were thus typical of those used during the experiment.

A plexiglass target calibration run was taken every few days during the second period of data taking. The runs were made with the same synchrotron operating conditions as any normal run. The quantameter calibration procedure used for the normal runs was also followed with one exception, namely, the beam catcher ion chamber was assumed to be stable for the entire period of the experiment and a value of Q/BC of 12.68 was used for all runs. The data obtained in 18 plexiglass target runs are presented in Table 15. These data are also plotted versus run number in Figure 21.

TABLE 15. Plexiglass Target Calibration Run Summary

Date	Run	+=	QTC	<b>Q40</b>	QBC	QAVG	π/QTC	п/Q40	π/QBC	π/QAVG	R=(F+V) veto rate	T(R-R)
26 Jan,	996	6424	103, 3	104, 4	101.0	102.9	62, 21	61, 55	63,62	62, 45	0,090	-0.31
26 Jan,	973	6475	101.8	101.3	102.5	101.9	63, 61	63, 92	63.17	63.54	0.000	-0, 31
27 Jan.	974	6488	102, 7	101.7	102.8	102.4	63.17	63.80	63. 11	63.36	0.000	-0.32
31 Jan,	1025	6416	103.9	104.6	104, 2	104.2	61,75	61,34	61.57	61.57	0,099	-0.88
1 Feb.	1026	6275	103,0	104.8	102, 4	103.4	60.92	59.88	61.28	60, 59	0.096	-0.67
4 Feb.	1050	7073	113.3	112. 2	114.2	113.2	62, 43	63,04	61.94	62, 48	0,089	-0.28
4 Feb.	1021	6257	102.8	101, 7	103, 7	102. 7	60,87	61, 52	30,34	60,93	0,089	-0.27
8 Feb.	1054	6829	105,8	106.9	106.0	106.2	64.83	64.16	64.71	64, 58	0,085	0, 00
9 Feb.	1065	6723	105.4	105.4	105, 4	105.4	63, 79	63, 79	63, 79	63, 79	0.084	0,00
10 Feb.	1077	6892	105,9	106.4	106.0	106, 1	65.08	64, 77	65.02	34,96	0,082	+0.20
12 Feb.	1090	6949	107.1	106, 1	106.2	106.5	63, 20	63,80	63, 74	63, 56	0,092	-0.47
15 Feb.	1097	6721	104,8	103, 3	105.3	104.5	64, 13	65,06	63, 83	64, 32	0.091	-0.40
21 Feb.	1125	6523	104.6	105.4	105,2	105.1	62, 36	61,89	C2.01	62.06	0.086	-0.03
5 Mar.	1145	6746	106,4	106.7	106.6	<b>10</b> 6. 6	63.40	63, 22	63, 28	63, 28	0,076	+0, 60
15 Mar.	1178	6542	106, 1	108, 3	107.0	107.1	61,66	60, 41	31, 14	61.08	0,085	0.00
19 Mar.	1195	6642	106.6	106.5	107,0	106, 7	62, 31	62, 37	62.07	62.25	0.074	+0.73
19 Mar.	1199	6541	107.4	107. €	107,4	107, 5	60,90	60, 79	00,90	ύ <b>0.</b> 85	0,071	+0.91
20 Mar. * " (K-R)	1200 is the e	6741	107.7	20 Mar. 1200 6741 107.7 107.6 107.0 107.4 62.59 62.65 63.00 62.77 $^{\circ}$ (R-R) is the expected variation in $_{\pi}^{+}/OAVG$ under the assumption that the F+V veto rate should be	107, 0 7G under t	107, 4 Mean	62, 59 62, 73 etion that t	62, 65 62, 66 be F+V ve	63.00 62.70 sto rate si		0.061 0.085 constant	+1.34
QAVG		50000										



RUN NUMBER Figure 21. Plexiglass Target Calibration Run Data

It is immediately obvious that these runs are not consistent with the hypothesis that the only errors result from the counting statistics. Deviations of this magnitude should occur approximately one time in  $10^4$ . Thus we must assume that there is some other effect which caused the inconsistencies. In the table below are presented the values of the variance of  $\pi/Q$  obtained using the various beam monitors as well as the "additional r.m.s. error" which is due to errors other than counting statistics.

	variance	counting statistics	additional rms error
$\pi/\mathrm{QTC}$	1. 98%	1. 23%	1.55%
$\pi/\mathrm{Q40}$	2.36%	1. 23%	2.07%
π/QBC	2.07%	1. 23%	1.66%
π/QAVG	<b>2.</b> 06%	<b>1. 23</b> %	1.65%

Figure 20 leads us to look for a slow variation which could take place with a period of several days. Because the singles rates from a lucite target are much higher than those obtained with hydrogen target, it is possible that accidentals or dead time effects could cause the observed discrepancies. However, a study showed that the variation in  $\pi^+/Q$  is not correlated with the average beam intensity. The efficiency of the fan counters might also have fluctuated since these were checked at only infrequent intervals. However, if we assume that the fraction of events which are vetoed by F+V should be a constant, we can compute the variations expected from the fact that the fractional F+V veto rate was not constant. The fractional F+V veto rate is given in Table 15, as well as the expected variation in  $\pi^+/QAVG$  due to this effect.

However, the plot of the expected variation vs. run number shown in Figure 20 clearly shows that this effect is not correlated with the observed fluctuations in  $\pi^+/QAVG$ . The pion and proton separation logic in the spectrometer was also shown to be constant to the order of 0.2%.

The beam monitoring was not completely consistent. However, the fact that the values at  $\pi/QTC$  and  $\pi/QBC$  are consistent to better than 0.5% r, m. s. indicates that the beam monitoring system was not responsible for the major part of the inconsistencies.

There remains the possibility that the plexiglass target was dimensionally unstable or absorbed water from the atmosphere. However, data from the manufacturer's catalog indicate that both these effects could contribute less than 0.3% variations in the  $\pi^+$  rate.

The most likely reason for the discrepancy is that the cross section for  $\pi^+$  photoproduction from free protons is changing rapidly with energy near the kinematic point chosen for the plexiglass runs. The slope of the yield vs. momentum curve can be obtained by looking at the observed yield in the various momentum channels. From this effect, we observe that an 0.25% r.m.s. momentum variation can cause the observed 1.65% r.m.s. variation in yield. The variation of momentum calibration is due to the motion of the beam centroid. An 0.11 inch r.m.s. motion of the beam centroid could cause the observed effect. Since the vertical position of the beam centroid is not under the control of the experimenter, this motion can exist. However, this much motion seems to be inconsistent with polaroid beam pictures taken each day.

Another possibility arising from the rapid variation of the cross section with kinematics is that the momentum of the spectrometer was constant but the synchrotron energy changed. A test run was made with  $E_{_{\rm O}}$  = 890 MeV, or 40 MeV higher than the normal runs. This test yielded the result of 88.0 ± 1.4 pions/QBIP. This amounts to an 8.5 ± 2.0% increase in the yield for a 40 MeV change in  $E_{_{\rm O}}$ . If the end point energy is responsible for all the fluctuations observed, then  $E_{_{\rm O}}$  must be drifting by 0.9% r.m.s.. This much drift is also unreasonable.

The conclusion drawn from the plexiglass target calibration runs is that there is a random error in the yields in addition to the counting statistics. This error can be the result of the compounding of a large number of smaller errors in many separate components including the beam monitoring, the momentum calibration, the synchrotron energy, and the operation of the electronics. On the basis of these runs, a random error of 1.65% was folded into the counting statistics of each run when the error bars on cross sections were computed.

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