

Appendix B. Using Unit Quaternions to Represent Rotations: How a Unit Quaterion Applied to a Reference Vector Can Create Our Fault Parameters, Strike, Dip, and Rake

Two alternative representations of a 3D rotation are quaternions and Euler angle rotations. Typically, Euler angle rotations are applied to a reference vector to describe an earthquake slip vector in terms of the fault parameters, strike, dip, and rake $(\Theta, \delta, \lambda)$. This appendix utilizes the relationships between unit quaternions and Euler angles to derive the fault parameters $(\Theta, \delta, \lambda)$ given a unit quaternion applied to a reference slip vector.

Figure B.1 starts with an arbitrary slip vector on a fault plane. The local, rotated coordinates for this slip vector are defined as \hat{E}''' , \hat{N}''' , and \hat{U}_p''' where \hat{E}''' and \hat{N}''' are on the fault plane and \hat{U}_p''' is perpendicular to the fault plane. \hat{N}''' is aligned with the slip vector. The slip vector represents the motion of the footwall; therefore, this is primarily a normal fault with a small amount of right-lateral strike-slip motion. To represent the slip vector in terms of the coordinates, \hat{E} , \hat{N} , and \hat{U}_p , we rotate the coordinates with Euler angle rotation matrices. The first rotation matrix is

$$R_\lambda = \begin{pmatrix} \cos \lambda & -\sin \lambda & 0 \\ \sin \lambda & \cos \lambda & 0 \\ 0 & 0 & 1 \end{pmatrix}, \quad (\text{B.1})$$

which is a clockwise rotation of the coordinate system by the rake angle, λ . The second one is

$$R_\delta = \begin{pmatrix} \cos \delta & 0 & \sin \delta \\ 0 & 1 & 0 \\ -\sin \delta & 0 & \cos \delta \end{pmatrix}, \quad (\text{B.2})$$

which is a clockwise rotation of the coordinate system by the dip angle, δ . The last and final rotation matrix is

$$R_{\Theta} = \begin{pmatrix} \cos \Theta & \sin \Theta & 0 \\ -\sin \Theta & \cos \Theta & 0 \\ 0 & 0 & 1 \end{pmatrix}, \quad (\text{B.3})$$

which is a counter-clockwise rotation of the coordinates by the strike angle, Θ . The three consecutive rotations are shown in Figure B.1, where the triple primed coordinates, \hat{E}''' , \hat{N}''' , and $\hat{U}p'''$ are transformed into the unprimed coordinates, \hat{E} , \hat{N} , and $\hat{U}p$.

Indeed, if we begin with the slip vector $\vec{l}''' = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}$ in the triple primed coordinates, aligned

with the \hat{N}''' direction, and apply these three rotation matrices to transform the coordinates, we derive

$$\vec{l} = \begin{pmatrix} \sin \Theta \cos \lambda - \cos \Theta \cos \delta \sin \lambda \\ \cos \Theta \cos \lambda + \sin \Theta \cos \delta \sin \lambda \\ \sin \delta \sin \lambda \end{pmatrix},$$

which is the same as Equation A.9 from Appendix A.

Slip occurs on the footwall; therefore, this is a normal fault.

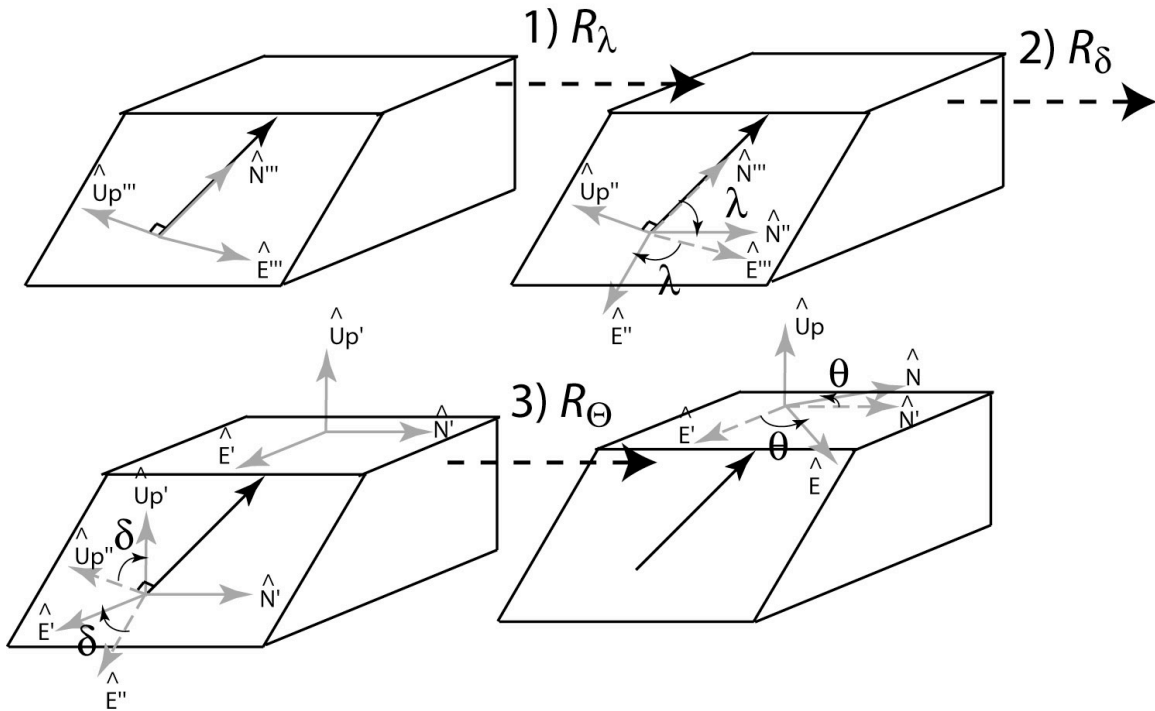


Figure B.1. Our triple primed coordinates are oriented so that our slip vector is aligned with \hat{N}''' . We rotate the coordinate system with three rotations: 1) A clockwise rotation of angle λ about the \hat{U}_p''' axis. 2) A clockwise rotation of angle δ about the \hat{N}'' axis. 3) A counter-clockwise rotation of angle Θ about the \hat{U}_p' axis.

This demonstration of fault parameters strike, dip, and rake $(\Theta, \delta, \lambda)$ using Euler angle rotations on a reference slip vector, will help us explain how to apply a unit quaternion to a reference slip vector to produce $(\Theta, \delta, \lambda)$.

To work with unit quaternions, we start with the reference slip vector, $\vec{l}''' = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}$

in the local, triple primed coordinate system, and measure other slip vectors in terms of

their rotations relative to \vec{l}''' . The unit quaternion, $\vec{q}''' = [q_0''', q_1''', q_2''', q_3'''] = [1, 0, 0, 0]$, produces a rotation of zero degrees; therefore, when applied to \vec{l}''' , simply reproduces \vec{l}''' . We then translate our Euler angle rotations $(\Theta, \delta, \lambda)$ into unit quaternions, and rotate \vec{l}''' into the global, unprimed coordinate system. From Chapter 3, we can rewrite Equation 3.12 in terms of a Cartesian coordinate system for our Euler angle rotations:

$$\begin{aligned}
 q_0 &= \cos(\omega/2) \\
 q_1 &= \sin(\omega/2)u_1 \\
 q_2 &= \sin(\omega/2)u_2 \\
 q_3 &= \sin(\omega/2)u_3
 \end{aligned} \tag{B.4}$$

where $\vec{u} = [u_1, u_2, u_3]$ is the rotation axis for the Euler rotations, and $|\vec{u}| = \sqrt{u_1^2 + u_2^2 + u_3^2} = 1.0$.

If $u_1 = \hat{E}'''$, $u_2 = \hat{N}'''$, and $u_3 = \hat{U}p'''$, for the first Euler rotation of angle λ , then the corresponding unit quaternion would be

$$\begin{aligned}
 q_0^\lambda &= \cos \frac{\lambda}{2} \\
 q_1^\lambda &= 0 \\
 q_2^\lambda &= 0 \\
 q_3^\lambda &= \sin \frac{\lambda}{2} .
 \end{aligned} \tag{B.5}$$

If $u_1 = \hat{E}''$, $u_2 = \hat{N}''$, and $u_3 = \hat{U}p''$, for the second Euler rotation of angle δ , then the corresponding unit quaternion would be

$$\begin{aligned}
q_0^\delta &= \cos \frac{\delta}{2} \\
q_1^\delta &= 0 \\
q_2^\delta &= \sin \frac{\delta}{2} \\
q_3^\delta &= 0.
\end{aligned}
\tag{B.6}$$

Last, if $u_1 = \hat{E}'$, $u_2 = \hat{N}'$, and $u_3 = \hat{U}p'$, for the third Euler rotation of angle Θ , then the corresponding unit quaternion would be

$$\begin{aligned}
q_0^\Theta &= \cos \frac{\Theta}{2} \\
q_1^\Theta &= 0 \\
q_2^\Theta &= 0 \\
q_3^\Theta &= \sin \frac{-\Theta}{2} = -\sin \frac{\Theta}{2}.
\end{aligned}
\tag{B.7}$$

Since a quaternion is a hyper complex four vector,

$$\vec{q} = q_0 + iq_1 + jq_2 + kq_3, \tag{B.8}$$

with the rules that

$$\begin{aligned}
i^2 &= j^2 = k^2 = -1 \\
ij &= -ji = k \\
jk &= -kj = i \\
ki &= -ik = j,
\end{aligned}
\tag{B.9}$$

we can rewrite our three unit quaternions as

$$\begin{aligned}
\vec{q}^\lambda &= \cos \frac{\lambda}{2} + k \sin \frac{\lambda}{2} \\
\vec{q}^\delta &= \cos \frac{\delta}{2} + j \sin \frac{\delta}{2} \\
\vec{q}^\Theta &= \cos \frac{\Theta}{2} - k \sin \frac{\Theta}{2}
\end{aligned}
\tag{B.10}$$

and simply multiply these three unit quaternions in Equation (B.10), using the rules in Equation (B.9) to produce the unit quaternion that rotates our reference slip vector, \vec{l}''' , into the unprimed, global coordinate system, \hat{E} , \hat{N} , and $\hat{U}p$.

$$\begin{aligned}\bar{q}^{\Theta\delta\lambda} &= \bar{q}^{\Theta}\bar{q}^{\delta}\bar{q}^{\lambda} = \left(\cos\frac{\Theta}{2} - \mathbf{k}\sin\frac{\Theta}{2}\right)\left(\cos\frac{\delta}{2} + \mathbf{j}\sin\frac{\delta}{2}\right)\left(\cos\frac{\lambda}{2} + \mathbf{k}\sin\frac{\lambda}{2}\right) \\ q_0^{\Theta\delta\lambda} &= \cos\frac{\Theta}{2}\cos\frac{\delta}{2}\cos\frac{\lambda}{2} + \sin\frac{\Theta}{2}\cos\frac{\delta}{2}\sin\frac{\lambda}{2} \\ q_1^{\Theta\delta\lambda} &= \cos\frac{\Theta}{2}\sin\frac{\delta}{2}\sin\frac{\lambda}{2} + \sin\frac{\Theta}{2}\sin\frac{\delta}{2}\cos\frac{\lambda}{2} \\ q_2^{\Theta\delta\lambda} &= \cos\frac{\Theta}{2}\sin\frac{\delta}{2}\cos\frac{\lambda}{2} - \sin\frac{\Theta}{2}\sin\frac{\delta}{2}\sin\frac{\lambda}{2} \\ q_3^{\Theta\delta\lambda} &= \cos\frac{\Theta}{2}\cos\frac{\delta}{2}\sin\frac{\lambda}{2} - \sin\frac{\Theta}{2}\cos\frac{\delta}{2}\cos\frac{\lambda}{2}\end{aligned}\tag{B.11}$$

Rewriting equation (B.11), we can also represent our fault parameters, $(\Theta, \delta, \lambda)$ in terms of unit quaternion components, given our reference slip vector.

$$\begin{aligned}\lambda &= \tan^{-1}\left(\frac{q_0^{\Theta\delta\lambda}q_1^{\Theta\delta\lambda} + q_2^{\Theta\delta\lambda}q_3^{\Theta\delta\lambda}}{q_0^{\Theta\delta\lambda}q_2^{\Theta\delta\lambda} - q_1^{\Theta\delta\lambda}q_3^{\Theta\delta\lambda}}\right) \\ \Theta &= \tan^{-1}\left(\frac{q_0^{\Theta\delta\lambda}q_1^{\Theta\delta\lambda} - q_2^{\Theta\delta\lambda}q_3^{\Theta\delta\lambda}}{q_0^{\Theta\delta\lambda}q_2^{\Theta\delta\lambda} + q_1^{\Theta\delta\lambda}q_3^{\Theta\delta\lambda}}\right) \\ \delta &= \tan^{-1}\left(\frac{2(q_0^{\Theta\delta\lambda}q_1^{\Theta\delta\lambda} + q_2^{\Theta\delta\lambda}q_3^{\Theta\delta\lambda})/\sin\lambda}{q_0^{\Theta\delta\lambda}q_0^{\Theta\delta\lambda} - q_1^{\Theta\delta\lambda}q_1^{\Theta\delta\lambda} - q_2^{\Theta\delta\lambda}q_2^{\Theta\delta\lambda} + q_3^{\Theta\delta\lambda}q_3^{\Theta\delta\lambda}}\right)\end{aligned}\tag{B.12}$$

For a unit quaternion, $\vec{q} = q_0 + \mathbf{i}q_1 + \mathbf{j}q_2 + \mathbf{k}q_3$, the rotation matrix one would apply to

rotate the coordinates of our vector $\vec{l}'' = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}$ into another reference frame, is

$$\vec{l} = \begin{pmatrix} l_1 \\ l_2 \\ l_3 \end{pmatrix} = \begin{pmatrix} q_0^2 + q_1^2 - q_2^2 - q_3^2 & 2q_1q_2 - 2q_0q_3 & 2q_0q_2 + 2q_1q_3 \\ 2q_0q_3 + 2q_1q_2 & q_0^2 - q_1^2 + q_2^2 - q_3^2 & 2q_2q_3 - 2q_0q_1 \\ 2q_1q_3 - 2q_0q_2 & 2q_0q_1 + 2q_2q_3 & q_0^2 - q_1^2 - q_2^2 + q_3^2 \end{pmatrix} \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}. \quad (\text{B.13})$$

In our case, we want to use the unit quaternion described in equation (B.11)

Therefore, we can write the components of \vec{l} as

$$\begin{aligned} l_1 &= 2q_1^{\Theta\delta\lambda} q_2^{\Theta\delta\lambda} - 2q_0^{\Theta\delta\lambda} q_3^{\Theta\delta\lambda} \\ l_2 &= (q_0^{\Theta\delta\lambda})^2 - (q_1^{\Theta\delta\lambda})^2 + (q_2^{\Theta\delta\lambda})^2 - (q_3^{\Theta\delta\lambda})^2 \\ l_3 &= 2q_0^{\Theta\delta\lambda} q_1^{\Theta\delta\lambda} + 2q_2^{\Theta\delta\lambda} q_3^{\Theta\delta\lambda} \end{aligned} \quad (\text{B.14})$$

or as

$$\begin{aligned} l_1 &= 2 \left(\left(\cos \frac{\Theta}{2} \sin \frac{\delta}{2} \sin \frac{\lambda}{2} + \sin \frac{\Theta}{2} \sin \frac{\delta}{2} \cos \frac{\lambda}{2} \right) \left(\cos \frac{\Theta}{2} \sin \frac{\delta}{2} \cos \frac{\lambda}{2} - \sin \frac{\Theta}{2} \sin \frac{\delta}{2} \sin \frac{\lambda}{2} \right) \right) \\ &\quad - 2 \left(\left(\cos \frac{\Theta}{2} \cos \frac{\delta}{2} \cos \frac{\lambda}{2} + \sin \frac{\Theta}{2} \cos \frac{\delta}{2} \sin \frac{\lambda}{2} \right) \left(\cos \frac{\Theta}{2} \cos \frac{\delta}{2} \sin \frac{\lambda}{2} - \sin \frac{\Theta}{2} \cos \frac{\delta}{2} \cos \frac{\lambda}{2} \right) \right) \\ l_1 &= \cos^2 \frac{\Theta}{2} \sin^2 \frac{\delta}{2} \sin \lambda - \sin^2 \frac{\delta}{2} \sin^2 \frac{\lambda}{2} \sin \Theta + \sin^2 \frac{\delta}{2} \cos^2 \frac{\lambda}{2} \sin \Theta - \sin^2 \frac{\Theta}{2} \sin^2 \frac{\delta}{2} \sin \lambda \quad (\text{B.15}) \\ &\quad - \cos^2 \frac{\Theta}{2} \cos^2 \frac{\delta}{2} \sin \lambda + \cos^2 \frac{\delta}{2} \cos^2 \frac{\lambda}{2} \sin \Theta - \cos^2 \frac{\delta}{2} \sin^2 \frac{\lambda}{2} \sin \Theta + \sin^2 \frac{\Theta}{2} \cos^2 \frac{\delta}{2} \sin \lambda \\ l_1 &= \sin^2 \frac{\delta}{2} \cos \lambda \sin \Theta + \sin^2 \frac{\delta}{2} \cos \Theta \sin \lambda + \cos^2 \frac{\delta}{2} \cos \lambda \sin \Theta - \cos^2 \frac{\delta}{2} \cos \Theta \sin \lambda \\ l_1 &= \sin \Theta \cos \lambda - \cos \Theta \cos \delta \sin \lambda \end{aligned}$$

$$\begin{aligned}
l_2 &= \\
&= \left(\cos \frac{\Theta}{2} \cos \frac{\delta}{2} \cos \frac{\lambda}{2} + \sin \frac{\Theta}{2} \cos \frac{\delta}{2} \sin \frac{\lambda}{2} \right)^2 - \left(\cos \frac{\Theta}{2} \sin \frac{\delta}{2} \sin \frac{\lambda}{2} + \sin \frac{\Theta}{2} \sin \frac{\delta}{2} \cos \frac{\lambda}{2} \right)^2 \\
&+ \left(\cos \frac{\Theta}{2} \sin \frac{\delta}{2} \cos \frac{\lambda}{2} - \sin \frac{\Theta}{2} \sin \frac{\delta}{2} \sin \frac{\lambda}{2} \right)^2 - \left(\cos \frac{\Theta}{2} \cos \frac{\delta}{2} \sin \frac{\lambda}{2} - \sin \frac{\Theta}{2} \cos \frac{\delta}{2} \cos \frac{\lambda}{2} \right)^2 \\
l_2 &= \cos^2 \frac{\Theta}{2} \cos^2 \frac{\lambda}{2} \left(\cos^2 \frac{\delta}{2} + \sin^2 \frac{\delta}{2} \right) + \sin^2 \frac{\Theta}{2} \sin^2 \frac{\lambda}{2} \left(\cos^2 \frac{\delta}{2} + \sin^2 \frac{\delta}{2} \right) \\
&- \cos^2 \frac{\Theta}{2} \sin^2 \frac{\lambda}{2} \left(\cos^2 \frac{\delta}{2} + \sin^2 \frac{\delta}{2} \right) - \sin^2 \frac{\Theta}{2} \cos^2 \frac{\lambda}{2} \left(\cos^2 \frac{\delta}{2} + \sin^2 \frac{\delta}{2} \right) \\
&+ \sin \Theta \sin \lambda \cos^2 \frac{\delta}{2} - \sin \Theta \sin \lambda \sin^2 \frac{\delta}{2} \\
l_2 &= \left(\cos^2 \frac{\Theta}{2} - \sin^2 \frac{\Theta}{2} \right) \cos \lambda + \sin \Theta \sin \lambda \cos \delta \\
l_2 &= \cos \Theta \cos \lambda + \sin \Theta \cos \delta \sin \lambda
\end{aligned} \tag{B.16}$$

$$\begin{aligned}
l_3 &= \\
&= 2 \left(\left(\cos \frac{\Theta}{2} \cos \frac{\delta}{2} \cos \frac{\lambda}{2} + \sin \frac{\Theta}{2} \cos \frac{\delta}{2} \sin \frac{\lambda}{2} \right) \left(\cos \frac{\Theta}{2} \sin \frac{\delta}{2} \sin \frac{\lambda}{2} + \sin \frac{\Theta}{2} \sin \frac{\delta}{2} \cos \frac{\lambda}{2} \right) \right) \\
&+ 2 \left(\left(\cos \frac{\Theta}{2} \sin \frac{\delta}{2} \cos \frac{\lambda}{2} - \sin \frac{\Theta}{2} \sin \frac{\delta}{2} \sin \frac{\lambda}{2} \right) \left(\cos \frac{\Theta}{2} \cos \frac{\delta}{2} \sin \frac{\lambda}{2} - \sin \frac{\Theta}{2} \cos \frac{\delta}{2} \cos \frac{\lambda}{2} \right) \right) \\
l_3 &= \cos^2 \frac{\Theta}{2} \sin \delta \sin \lambda + \sin^2 \frac{\Theta}{2} \sin \delta \sin \lambda \\
l_3 &= \sin \delta \sin \lambda.
\end{aligned} \tag{B.17}$$

So again, now with unit quaternions, we have calculated that

$$\vec{l} = \begin{pmatrix} \sin \Theta \cos \lambda - \cos \Theta \cos \delta \sin \lambda \\ \cos \Theta \cos \lambda + \sin \Theta \cos \delta \sin \lambda \\ \sin \delta \sin \lambda \end{pmatrix}.$$