

THE ECONOMICAL SPACING
OF
ROOF TRUSSES

Thesis by
David Yue-Kwong Wong

In
Partial Fulfillment
of the
Requirements for the Degree of
Master of Science

CALIFORNIA INSTITUTE OF TECHNOLOGY
Pasadena, California
1933

Table of Contents.

| | |
|--------------------------|-------|
| 1. Introduction | 1-2 |
| Truss Diagram | 3 |
| 2. Discussion | 4-9 |
| 3. Results of Design | 10-16 |
| 4. Discussion of Results | 11-29 |

INTRODUCTION

The economical spacing of roof trusses is usually affected by a great deal of factors that it has been quite impossible to develop a theoretical formula giving the exact spacing for different spans. However, as a common practice and from the experiences of different engineers, the spacing of roof trusses usually varies from about $\frac{1}{3}$ of the span for shorter trusses to about $\frac{1}{5}$ of the span for the longer trusses.

The object of this problem has been, therefore, to try to confirm the statement above by actually designing trusses of different spans at different spacings, and to see what are the factors which enter into this question of economical spacing of roof trusses. In so doing, the author tried as much as possible to keep everything constant except the span and spacing.

The type of truss used by the author was the Fink steel truss with a pitch of $\frac{1}{4}$ as shown in Fig. I. The roof covering consisted of corrugated steel supported on purlins. The specifications of the A.I.S.C. were used to govern the design of the members. Three different spans were tried at 40 feet, 60 feet, and 100 feet.

The spacings used were as follows:

- (1) For 40' span, spacing at

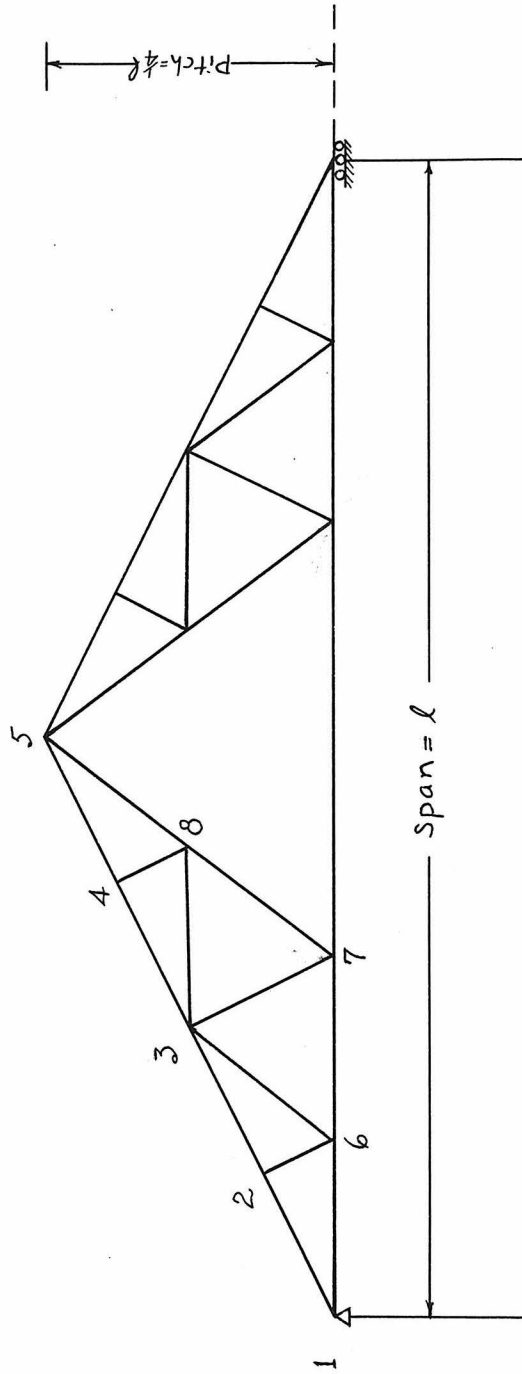
8' = 1/5 span
10' = 1/4 span
12' = 3/10 span
15' = 3/8 span

(2) For 60' span, spacing at

10' = 1/6 span
12' = 1/5 span
15' = 1/4 span
18' = 3/10 span
20' = 1/3 span
22.5' = 3/8 span

(3) For 100' span spacing at

15' = 1/6.6 span
20' = 1/5 span
25' = 1/4 span
30' = 1/3.3 span



TRUSS DIAGRAM

Fig. 1

DISCUSSION.

In the discussion given in Hood and Johnson's "Hand-book of Building Construction", Vol. 1, the theoretical spacing of trusses for least total cost of trusses, purlins, and roof covering depends upon the relative cost of the component parts. Let X = total cost of construction per square foot of roof.

(1) for truss: t = cost of truss per square foot of roof.
 k = constant
 s = spacing
 $t = \frac{k}{s}$

(2) for purlin: p = cost of purlin per square foot of roof.
 n = constant
 $p = ns^2$

(3) for roof covering: c = cost of roofing per square foot of roof
 m = constant
 $c = ms$

then

$$X = t + p + c = \frac{k}{s} + ns^2 + ms$$

To obtain the minimum unit cost, with respect to different spacings,

$$\frac{dx}{ds} = 0 = -\frac{k}{s^2} + 2ns + m = 0$$

multiplying by s

$$-\frac{k}{s} + 2ns^2 + ms = 0$$

$$\therefore t = 2p + c$$

According to the equation above then, for the least cost, the spacing of trusses must be such that the above equation be satisfied. Hood and Johnson mentioned, however, that the relation given above can not be used directly for the determination of the truss spacing because the spacing does not appear in the equation.

After designing the 14 trusses, the author has made a study of the different factors which are involved in the determination of the value for t, p, and c. These factors as found seemed to vary a great deal with respect to local conditions and requirements, and to the time when and place where the structure is to be built.

The cost of steel structures may be divided into:

- (1) cost of material
- (2) cost of fabrication
- (3) cost of erection, and
- (4) cost of transportation.

Under these items there are the cost of drafting, mill details, shop labor, placing, bolting, hauling, falsework, etc.

In order to make a simple investigation, the author has neglected the minor costs and chosen the following ones to find t , p , and c .

A. t , the cost of truss per square foot of roof is made up of:

1. cost of material of truss at 1.5 ¢/lb^o
2. cost of shop labor--see table I 0.55 - 1.1 ¢/lb
3. cost of erection at 0.35 ¢/lb

Total = 2.4 ¢/lb to 2.95 ¢/lb

B. p , the cost of purlin per square foot of roof is made up of:

1. cost of material--I beams and channels
3" to 15" at 1.45 ¢/lb
2. cost of laying--punching holes and
erection at 0.35 ¢/lb

Total = 1.80 ¢/lb

C. c , the cost of roofing per square foot of roof is made up of

1. cost of material at 2.0 ¢/lb
2. cost of laying at 0.9 - 1.49 ¢/lb

Total = 2.9 ¢/lb to 3.49 ¢/lb

^oThese values were obtained from M. S. Ketchum's "Structural Engineer's Handbook".

The cost of shop labor was calculated for the structure as a whole. The following costs are based on an average charge of 40¢ per hour, and include detailing and shopwork.

In lots of at least six, the shop cost of ordinary riveted roof trusses in which the ends of the members are cut off at right angles is about as follows:

| Total weight of truss | Cost in cents per pound |
|-----------------------|-------------------------|
| 1,000 # | 1.15 - 1.25 ¢ |
| 1,500 | 0.90 - 1.00 ¢ |
| 2,500 | 0.75 - 0.85 ¢ |
| 3,500 - 7,500 | 0.60 - 0.75 ¢ |

The values in Table I were obtained from the above figures

The cost of erection includes the cost of placing and bolting and was obtained from the following figures (40 ¢/hour basis).

| Kind of structure | Cost of erection in dollars/ton |
|--------------------------------------|---------------------------------|
| Mill building for ordinary condition | \$6.00 - \$8.00 |
| Steel office building | \$5.00 - \$9.00 |
| Steel bins | \$10.00 - \$15.00 |
| Head frames | \$12.00 - \$18.00 |

For this particular problem the author chose the value of \$7.00/ton for the cost of erection. This amounts to 0.35¢/lb. See Table I, on the following page.

Table I.

Values of t

(t = the unit cost of truss per pound)

| Spacing | Total wt. of truss | Cost of Labor in ¢/# | Cost of Material in ¢/# | Cost of Erection in ¢/# | Span | t ¢/# |
|---------|--------------------------|----------------------------|-------------------------------|-------------------------------|------|------------|
| 8' | 1290 | 1.1 | 1.5 | 0.35 | 40' | 2.95 |
| 10' | 1290 | 1.1 | " | " | | 2.95 |
| 12' | 1366 | " | " | " | | 2.95 |
| 15' | 1393 | " | " | " | | 2.95 |
| 10' | 2250 | 0.85 | " | " | 60' | 2.70 |
| 12' | 2273 | 0.85 | " | " | | 2.70 |
| 15' | 2513 | 0.80 | " | " | | 2.65 |
| 18' | 2625 | 0.80 | " | " | | 2.65 |
| 20' | 3202 | 0.75 | " | " | | 2.60 |
| 22.5' | 3416 | 0.75 | " | " | | 2.60 |
| 15' | 6219 | 0.70 | " | " | 100' | 2.55 |
| 20' | 7318 | 0.60 | " | " | | 2.45 |
| 25' | 9246 | 0.55 | " | " | | 2.40 |
| 30' | 10295 | 0.55 | " | " | | 2.40 |

Results of Design.

RESULT

The result of the design as shown in the tables below showed the economical spacings as follows:

| Span | Economical spacing | Acceptable Economic spacing. |
|------|--------------------|------------------------------|
| 40' | 10' = $1/4$ span | 12' = $3/10$ span |
| 60' | 12' = $1/5$ span | 10' = $1/6$ span |
| 100' | 15' = $1/6.6$ span | 20' = $1/5$ span |

Table II.
Weight of Trusses
40'-span

| | | 8' spac. | 10' | 12' | 15' |
|----------------------------------|---------------------------|-----------------|-----------------|-----------------|-----------------|
| | Total number of pieces | wt. in # | wt. in # | wt. in # | wt. in # |
| Chord members: | | | | | |
| 1-5 | 4L @ 22.5' | 369.00 | 369.00 | 442.00 | 442.00 |
| 1-7 | 4L @ 13.0' | 166.00 | 166.00 | 166.00 | 166.00 |
| 7-7' | 2L @ 15.0' | 95.50 | 95.50 | 95.50 | 95.50 |
| 2-6, 4-8 | 4L @ 2.7' | 34.50 | 34.50 | 34.50 | 34.50 |
| 3-7 | 2L @ 5.3' | 52.00 | 52.00 | 52.00 | 52.00 |
| 3-8, 3-6 | 4L @ 5.9' | 75.20 | 75.20 | 75.20 | 75.20 |
| 5-7 | 4L @ 12.0' | 153.00 | 153.00 | 153.00 | 153.00 |
| Sag tie | 1L @ 9.0' | 28.70 | 28.70 | 28.70 | 28.70 |
| Weight of members: | | 974.00# | 974.00# | 1047.00# | 1047.00# |
| Connection Factor: | | | | | |
| Joint 1 | 2 gusset pls. | 67.40 | 67.40 | 67.40 | 90.00 |
| " 2,4 | 4 " " | 12.00 | 12.00 | 12.80 | 12.80 |
| " 3 | 2 " " | 40.80 | 40.80. | 40.80 | 40.80 |
| " 5 | 1 " " | 57.50 | 57.50 | 60.00 | 64.50 |
| " 6,8 | 4 " " | 17.90 | 17.90 | 17.90 | 17.90 |
| " 7 | 2 " " | 20.40 | 20.40 | 20.40 | 20.40 |
| shoe L, shoe plates, rivets etc. | | 100.00 | 100.00 | 100.00 | 100.00 |
| Total connection: | | 316.00# | 316.00# | 319.30# | 346.40# |
| Total Truss weight | | 1290.00# | 1290.00# | 1366.30# | 1393.00# |

Table III.
Weight of Trusses
60'-span

| | | 10' | 12' | 15' | 18' | 20' | 22.5' |
|--------------------------------|------|----------|----------|----------|----------|----------|----------|
| | | wt. in # | wt. in # | wt. in # | wt. in # | wt. in # | wt. in # |
| Members: | | | | | | | |
| 1-5 | 4 Ls | 1974.0 | 1974.0 | 1110.0 | 1325.0 | 1528.0 | 1580.0 |
| 1-7 | 4 Ls | 244.0 | 246.0 | 282.0 | 354.0 | 388.0 | 488.0 |
| 7-7' | 2 Ls | 120.0 | 120.0 | 126.0 | 136.0 | 184.5 | 184.5 |
| 2-6, 4-8 | 4 Ls | 58.0 | 58.0 | 58.0 | 58.0 | 58.0 | 58.0 |
| 3-7 | 4 Ls | 144.0 | 144.0 | 144.0 | 144.0 | 144.0 | 144.0 |
| 3-8, 3-6 | 4 Ls | 115.0 | 115.0 | 115.0 | 115.0 | 115.0 | 115.0 |
| 5-7 | 4 Ls | 227.0 | 227.0 | 227.0 | 227.0 | 227.0 | 227.0 |
| Sag tie | 1 C | 45.3 | 45.3 | 45.3 | 45.3 | 45.3 | 45.3 |
| Weight of mem | | 1927.3 | 1929.3 | 2117.3 | 2404.3 | 2689.3 | 2841.8 |
| Connection Factor: | | | | | | | |
| Jt. 1 | | 63.8 | 76.4 | 112.0 | 112.0 | 153.0 | 168.0 |
| " 2,4 | | 13.7 | 13.7 | 16.7 | 16.3 | 16.3 | 18.4 |
| " 3 | | 36.7 | 36.7 | 36.7 | 40.0 | 40.0 | 58.0 |
| " 5 | | 57.2 | 64.5 | 72.6 | 83.0 | 99.0 | 108.8 |
| " 6,8 | | 20.4 | 20.4 | 20.4 | 20.4 | 20.4 | 27.2 |
| " 7 | | 27.6 | 27.6 | 33.0 | 33.0 | 36.7 | 46.0 |
| Shoe L, Shoe pl., rivets etc. | | 104.6 | 104.6 | 104.6 | 125.8 | 146.6 | 148.3 |
| wt. of Conn. Factor | | 322.0 | 344.0 | 395.0 | 420.5 | 512.0 | 574.4 |
| Total weight of Trusses | | | | | | | |
| | | 2249.0 # | 2273.0 # | 2513.0 # | 2625.0 # | 3202.0 # | 3416.0 # |

Table IV.
Weight of Trusses
100'-span

| | | 15' | 20' | 25' | 30' |
|---------------------------|--|----------------------------|----------------------------|----------------------------|------------------------------|
| | | wt. in # | wt. in # | wt. in # | wt. in # |
| Members: | | | | | |
| 1-5 | | 2925.00 | 3830.00 | 5400.00 | 6040.00 |
| 1-7 | | 906.00 | 978.00 | 1252.00 | 1551.00 |
| 7-7' | | 539.00 | 539.00 | 539.00 | 576.00 |
| 2-6,4-8 | | 200.00 | 200.00 | 200.00 | 200.00 |
| 3-7 | | 416.00 | 416.00 | 416.00 | 416.00 |
| 3-8,3-6 | | 426.00 | 426.00 | 426.00 | 426.00 |
| 5-7 | | 100.00 | 100.00 | 100.00 | 100.00 |
| Sag tie | | 176.00 | 176.00 | 176.00 | 176.00 |
| wt. of members | | 5688.00 [#] | 6665.0 [#] | 8509.00 [#] | 9485.00 [#] |
| Connection Factor: | | | | | |
| Joint 1 | | 137.00 | 151.00 | 181.00 | 186.00 |
| " 2,4 | | 40.80 | 40.80 | 40.80 | 40.80 |
| " 3 | | 84.00 | 84.00 | 84.00 | 84.00 |
| " 5 | | 97.50 | 121.50 | 153.00 | 191.00 |
| " 6,8 | | 32.60 | 32.60 | 32.60 | 32.60 |
| " 7 | | 33.60 | 33.60 | 33.60 | 43.00 |
| | | 177.60 | 190.00 | 212.00 | 232.40 |
| wt. of Conn. Factor | | 603.10 [#] | 653.40 [#] | 737.00 [#] | 809.80 [#] |
| | | | | | |
| Total wt. of Truss | | 6291.00[#] | 7318.40[#] | 9246.00[#] | 10,294.00[#] |

Table VIII.
Comparison of Cost
40'-span

| | wt. per sq. ft. # | unit cost ¢/# | cost per sq. ft. | 2p | 2p + e | t | Spac- ing |
|--|-------------------------|---------------------|------------------------|---------------------------|--------|------|--------------|
| Roofing | 2.46 | 3.49 [¢] | 8.60 [¢] | | | | |
| Purlin | 1.64 | 1.80 | 2.95 | 5.90 | 14.5 | 11.9 | 8' |
| "w" | | | | | | | |
| Cost per sq. ft. of roof = | 4.03 | 2.95 | 11.90 | | | | |
| | | | 23.45 | | | | |
| Roofing | 2.46 | 3.49 | 8.60 | | | | |
| Purlin | 2.16 | 1.80 | 3.89 | 7.78 | 16.38 | 9.5 | 10' |
| "w" | 3.22 | 2.95 | 9.50 | | | | |
| Cost of Truss per sq. ft. of roof = | | | 21.99 | <i>Economical Spacing</i> | | | |
| Roofing | 2.46 | 3.49 | 8.60 | | | | |
| Purlin | 3.00 | 1.80 | 5.40 | 10.80 | 19.4 | 8.38 | 12' |
| "w" | 2.84 | 2.95 | 8.38 | | | | |
| Cost of Truss per sq. ft. of roof = | | | 22.38 | | | | |
| Roofing | 2.46 | 3.49 | 8.60 | | | | |
| Purlin | 4.00 | 1.80 | 7.20 | 14.40 | 23.00 | 6.85 | 15' |
| "w" | 2.32 | 2.95 | 6.85 | | | | |
| Cost of Truss per sq. ft. of roof = | | | 22.65 | | | | |

Table IX.
Comparison of Cost
60'-span

| Spacing | | wt. per sq. ft. # | unit cost ¢/# | cost per sq. ft. | 2p | 2p e | t |
|---------|-------------------------------------|-------------------|---------------|---------------------------|-------|-------|-------|
| 10' | Roofing | 2.46 | 3.49 | 8.60¢ | 8.20 | 16.80 | 10.12 |
| | Purlin | 2.28 | 1.80 | 4.10 | | | |
| | "w" | 3.75 | 2.70 | 10.12 | | | |
| | Cost of Truss per sq. ft. of roof = | 22.82 | | | | | |
| 12' | Roofing | 2.46 | 3.49 | 8.60 | 11.10 | 19.70 | 8.54 |
| | Purlin | 3.08 | 1.80 | 5.55 | | | |
| | "w" | 3.16 | 2.70 | 8.54 | | | |
| | Cost of Truss per sq. ft. of roof = | 22.69 | | <i>Economical Spacing</i> | | | |
| 15' | Roofing | 2.46 | 3.49 | 8.60 | 14.40 | 23.00 | 7.42 |
| | Purlin | 4.00 | 1.80 | 7.20 | | | |
| | "w" | 2.80 | 2.65 | 7.42 | | | |
| | Cost of Truss per sq. ft. of roof = | 23.22 | | | | | |
| 18' | Roofing | 2.46 | 3.49 | 8.60 | 18.00 | 26.60 | 6.45 |
| | Purlin | 5.00 | 1.80 | 9.00 | | | |
| | "w" | 2.43 | 2.65 | 6.45 | | | |
| | Cost of Truss per sq. ft. of roof = | 24.05 | | | | | |
| 20' | Roofing | 2.46 | 3.49 | 8.60 | 22.00 | 30.60 | 6.94 |
| | Purlin | 6.12 | 1.80 | 11.00 | | | |
| | "w" | 2.57 | 2.60 | 6.94 | | | |
| | cost of truss per sq. ft. = | 26.54 | | | | | |
| 22.5' | Roofing | 2.46 | 3.49 | 8.60 | 26.50 | 35.10 | 6.58 |
| | Purlin | 7.36 | 1.80 | 13.25 | | | |
| | "w" | 2.53 | 2.60 | 6.58 | | | |
| | Cost of truss per sq. ft. = | 28.43 | | | | | |

Table X.
Comparison of Cost
100'-span

| Spac- ing | | wt. per sq.ft. # | unit cost ¢/# | cost per sq.ft. | 2p | 2p e | t |
|------------------|-----------------------|------------------------|---------------------|-----------------------|-----------------------------|-------|-------|
| Cost of Truss | | 3.36# | 2.90¢ | 9.75¢ | | | |
| | per sq. ft. of roof = | 3.67 | 1.80 | 6.60 | 13.2 | 22.95 | 10.70 |
| | | 4.20 | 2.55 | 10.70 | | | |
| | | | | 27.05 | <i>✓ Economical Spacing</i> | | |
| Cost of Truss | | 3.36 | 2.90 | 9.75 | | | |
| | per sq. ft. of roof = | 4.90 | 1.80 | 8.82 | 17.64 | 27.39 | 8.95 |
| | | 3.65 | 2.45 | 8.95 | | | |
| | | | | 27.52 | | | |
| Cost of Truss | | 3.36 | 2.90 | 9.75 | | | |
| | per sq. ft. of roof = | 6.00 | 1.80 | 10.80 | 21.60 | 31.35 | 8.85 |
| | | 3.69 | 2.40 | 8.85 | | | |
| | | | | 29.40 | | | |
| Cost of Truss | | 3.36 | 2.90 | 9.75 | | | |
| | per sq. ft. of roof = | 8.64 | 1.80 | 15.54 | 31.08 | 40.83 | 8.25 |
| | | 3.44 | 2.40 | 8.25 | | | |
| | | | | 33.54 | | | |

Discussion of Results.

DISCUSSION OF RESULTS

Mr. M. S. Ketchum in his "Structural Engineer's Handbook" stated that he tried this problem of economical spacing for a 60' span and found that the least weight was at a spacing of 10'. The author's result showed that this value was the second value for the economical spacing of a 60' span truss.

As it can be noted from Tables VIII, IX, and X, the results did not check with the theoretical condition in the formula $t = 2p + c$ by Hood and Johnson.

The estimated value of c was much too great to give the value of $2p + c$ a much larger value than that of t . But in every case except the 60' span, the economical spacing occurred when $t > 2p$, having a surplus for the value of c . However, c was kept a constant value and thus did not affect the equation:

$$X = t + p + c$$

to give a different economical spacing. We can say then in this particular case that the economical spacing of trusses occurs when the value of $2p$ is just less than the value of t .

Besides the different factors affecting the cost of the structure, there are minor factors in the design of the component parts themselves. Roof covering costs vary with the nature

of the covering. In the design of purlins and members of the truss, if it were possible to obtain rolled sections which would provide exactly the required areas for all members, the result of the problem would have come out more accurate. But as could be seen from the designs above, the sizes of many members were determined by the specifications and by the requirements of standard practice. For the web members such as 2-6, 4-8, 3-6, and 3-8, the designed members provided much larger areas than were required. The author therefore made a study of this factor, which he called "specification factor". He picked the members which were affected by it; the percentage weight of these members to the total weight of the whole truss is tabulated in the following tables: Tables XI, XII, and XIII.

These tables also give the percentage of the "Connection Factor", which includes the weight of connection plates, shoe plates, etc. The sum of the "Specification Factor" and the "Connection Factor" therefore gives the percentage in the roof construction that is fixed by specifications and standard practice. Subtracting the above sum from 100% gives the percentage that the designer has a right to vary the sizes and forms of the members. The relationship between these percentages is shown in Table XIV. As can be seen, the values of the "Specification Factor" varies with the spacing, decreasing as the spacing is

increased. The "Connection Factor" seemed to be quite a constant percentage ranging from:

23.4% - 25.7% for 40' span truss

14.3% - 16.8% for 60' span truss

7.88% - 9.6% for 100' span truss.

Tables below give values of the "Specification Factor" and the "Connection Factor" in percentage of the Total Weight of Truss.

Table XI. 40'-span

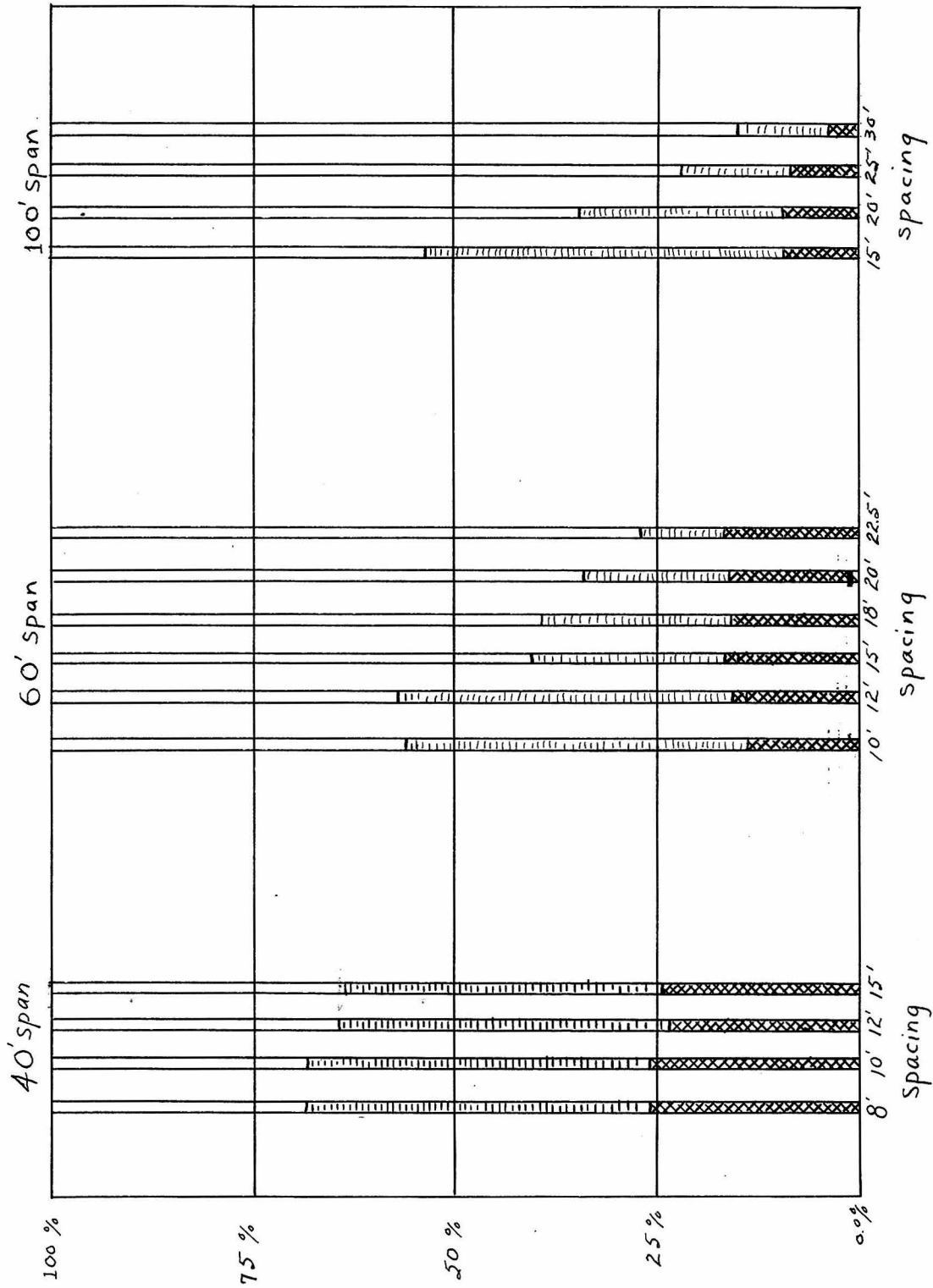
| | 8' | | 10' | | 12' | | 15' | |
|-----------------|-------------------|------|-------------------|------|-------------------|------|-------------------|------|
| | wt. | % | wt. | % | wt. | % | wt. | % |
| Weight of Truss | 1290 [#] | 100% | 1290 [#] | 100% | 1366 [#] | 100% | 1393 [#] | 100% |
| Spec. Factor | 553 | 42.8 | 553 | 42.8 | 553 | 40.5 | 553 | 39.7 |
| Conn. Factor | 316 | 25.7 | 316 | 25.7 | 319 | 23.4 | 346 | 24.8 |

Table XII. 60'-span

| | 10' | | 12' | | 15' | | 18' | | 20' | | 22.5' | |
|--------------|-------------------|------|-------------------|------|-------------------|------|-------------------|------|-------------------|------|-------------------|------|
| | wt. | % | wt. | % | wt. | % | wt. | % | wt. | % | wt. | % |
| Truss wt. | 2249 [#] | 100% | 2273 [#] | 100% | 2513 [#] | 100% | 2625 [#] | 100% | 3201 [#] | 100% | 3416 [#] | 100% |
| Spec. Factor | 953 | 42.4 | 953 | 42.0 | 589 | 23.5 | 589 | 22.5 | 589 | 18.4 | 362 | 10.6 |
| Conn. Fac. | 322 | 14.3 | 344 | 15.1 | 396 | 15.8 | 420 | 16.0 | 572 | 16.0 | 574 | 16.8 |

Table XIII. 100'-span

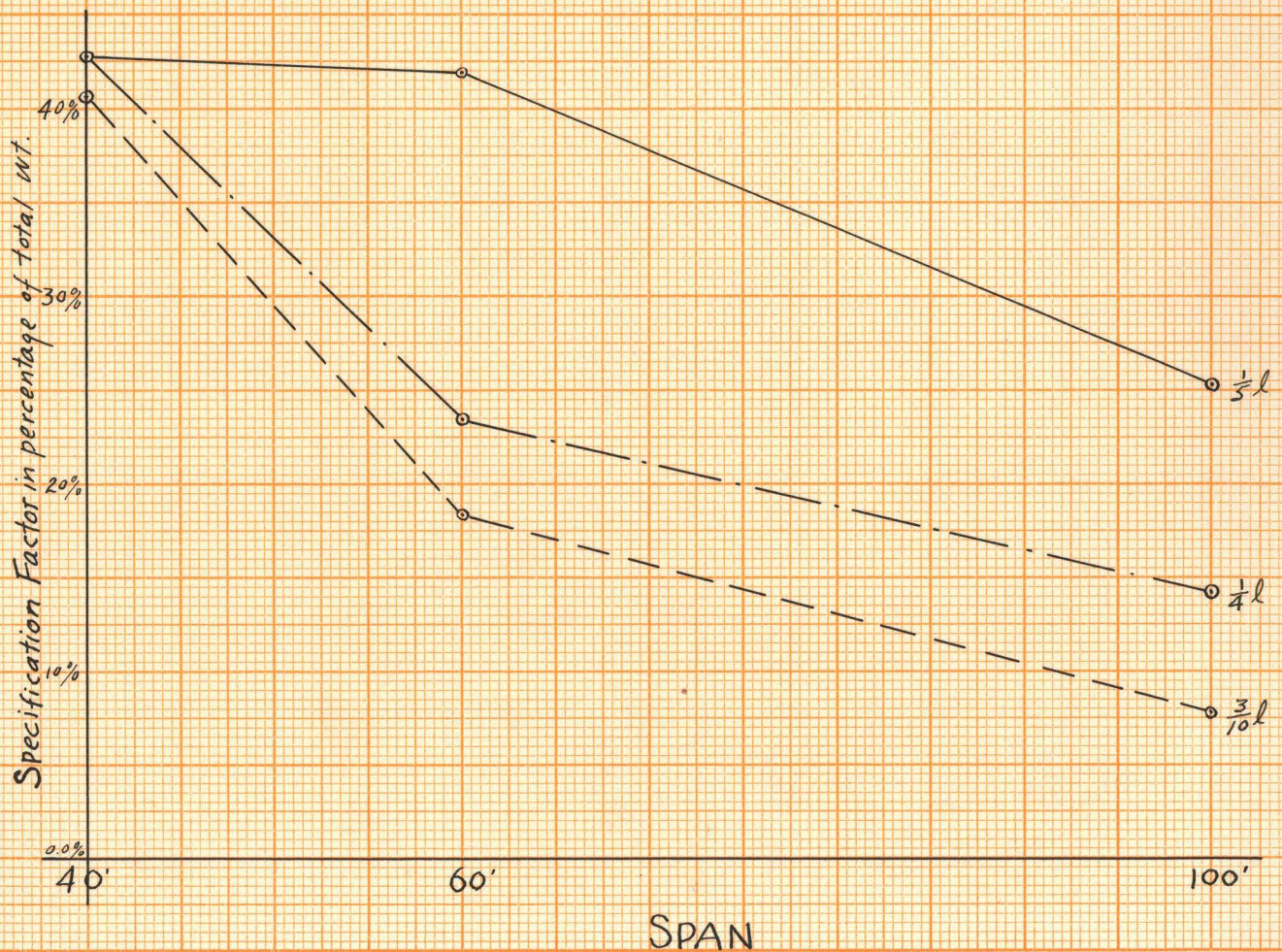
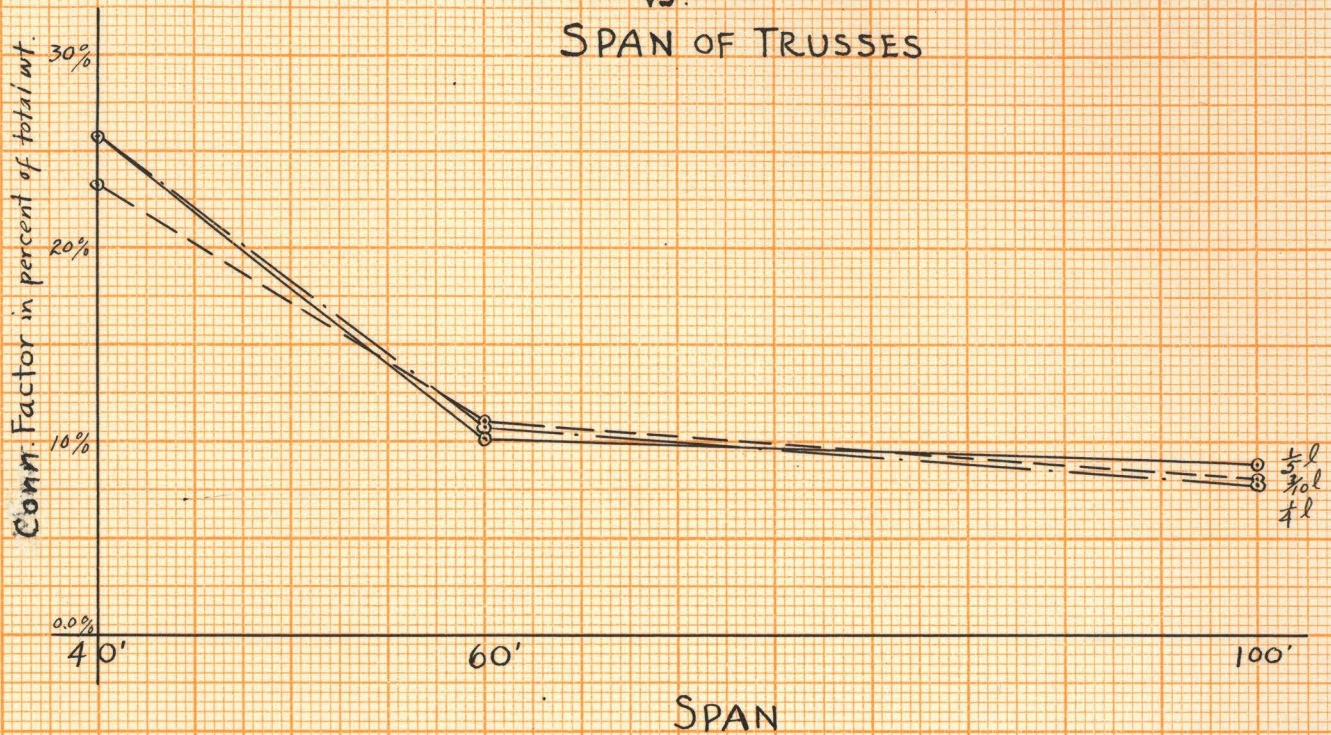
| | 15' | | 20' | | 25' | | 30' | |
|--------------|-------------------|------|-------------------|------|-------------------|-------|--------------------|------|
| | wt. | % | wt. | % | wt. | % | wt. | % |
| Truss wt. | 6291 [#] | 100% | 7318 [#] | 100% | 9246 [#] | 100% | 10295 [#] | 100% |
| Spec. Fac. | 2763 | 44.0 | 1857 | 25.4 | 1318 | 14.25 | 802 | 7.8 |
| Conn. Factor | 603 | 9.6 | 653 | 8.93 | 737 | 7.97 | 810 | 7.88 |



"Specification Factor"
in % of total weight

"Connection Factor"
in % of total weight

SPECIFICATION FACTOR & CONNECTION FACTOR VS. SPAN OF TRUSSES



In the calculation of stresses, w was obtained using Howe's formula:

$$w = \frac{pL}{150 + 5L + ps/3}$$

There are, however, different formulas to determine the value of w . Among them are the following ones taken from the discussion of Mr. R. Fleming on "Weight of steel Roof Trusses by Empirical Formulas"—Eng. News Recd., March 20, 1919.

T = wt. of truss

$$w = \frac{\text{wt.}}{\text{sq. ft. horiz. area}}$$

s = spacing

L = span

P = loading of truss in $\frac{\text{lb.}}{\text{sq. ft. horiz. area}}$

Cambria Steel Co., for spans of 75' or less:

$$T = 5 \cdot Ls$$

Carnegie Steel Co., 1917, for loads of 40# or more per sq. ft.

$$w = \frac{P}{40} \cdot \frac{1}{5} (\sqrt{L} + \frac{L}{8})$$

Fowler, 1909, for Fink trusses up to 200' span

$$w = 0.06 \cdot L + 0.6 \text{ for heavy loads}$$

$$w = 0.04 \cdot L + 0.04 \text{ for light loads}$$

Johnson, Bryan, and Turneure

$$w = \frac{L}{25} + 4.0$$

Jones and Laughlin, 1916

$$w = \frac{P}{40} \left(\frac{L}{20} + \frac{12}{s} \right)$$

Ketchum, 1916

$$w = \frac{P}{45} \left(1 + \frac{L}{5\sqrt{s}} \right)$$

Maurer, 1903

$$w = \frac{L}{25} + 1$$

Merriman, 1911

$$T = \frac{3}{4}Ls \left(1 + \frac{L}{10} \right)$$

Ricker, 1907

$$w = \frac{L}{25} + \frac{L^2}{6000}$$

Ricker, 1912

$$w = \frac{L}{25} + \frac{L^2}{12,600}$$

The values calculated for these different trusses are shown in Table XV on the following page.

The author has taken out Howes', Jones and Laughlins', and Ketchum's formulas and compared the values obtained by these formulas with the actual designed values of w , the curves on pages (27) showing the relationship.

In every case the actual w is below the calculated values from the formulas as shown.

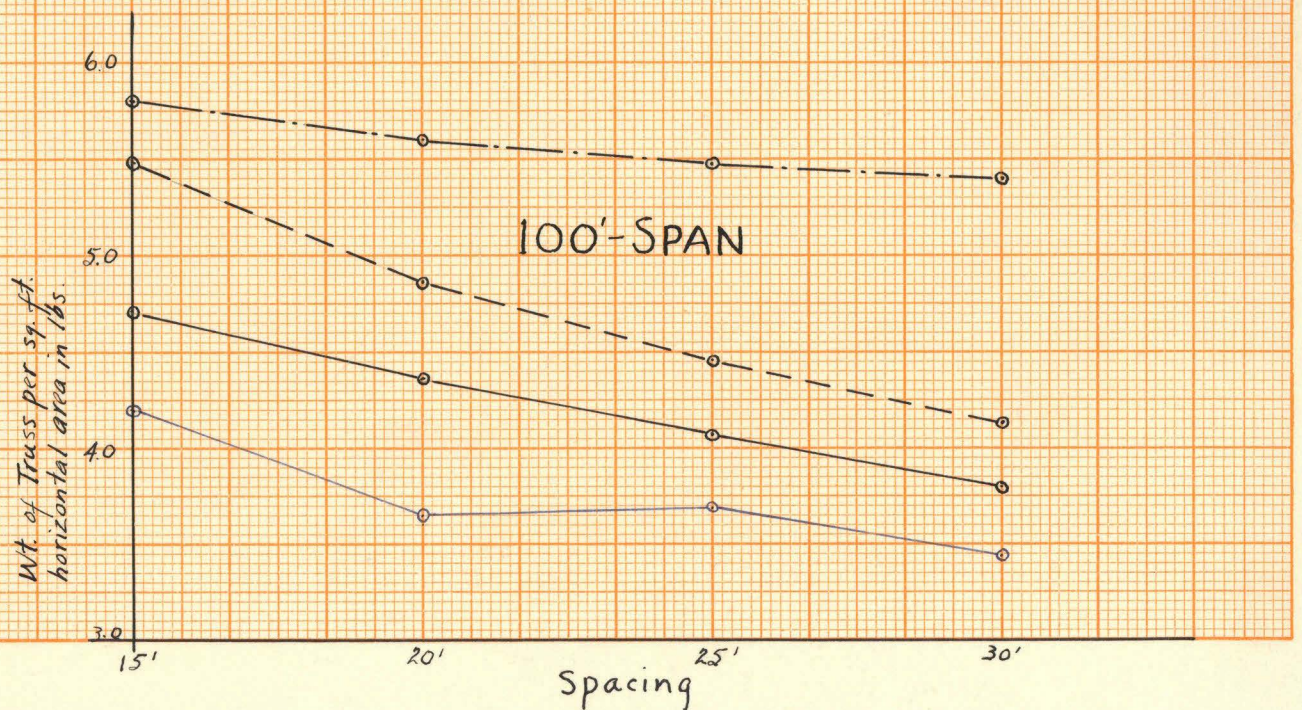
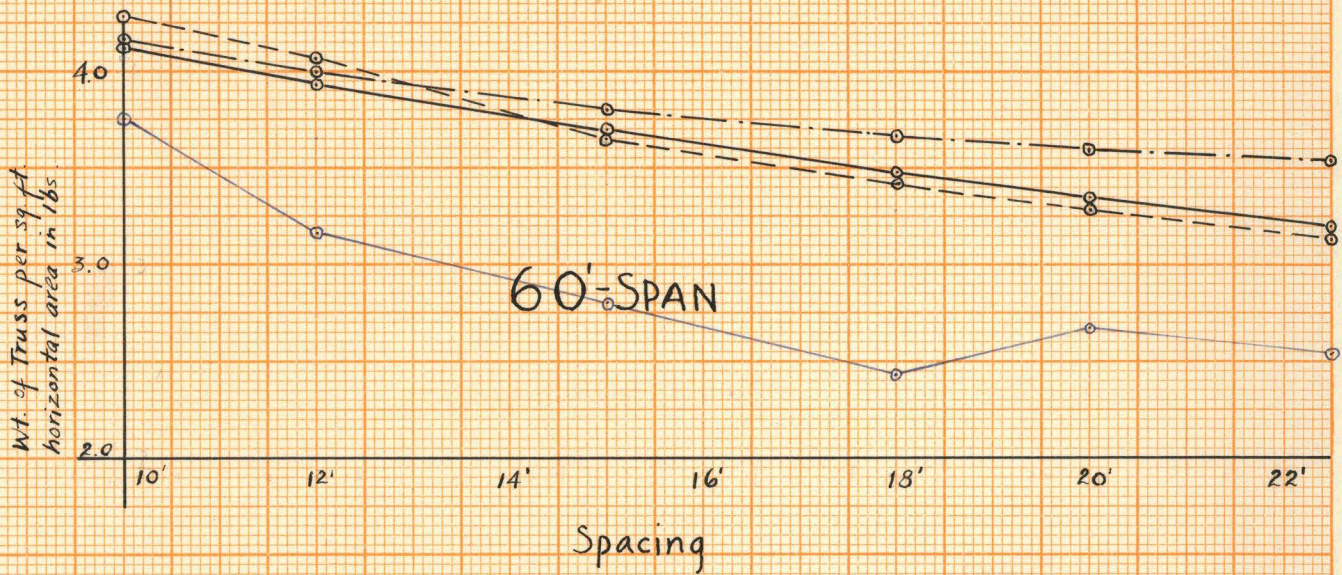
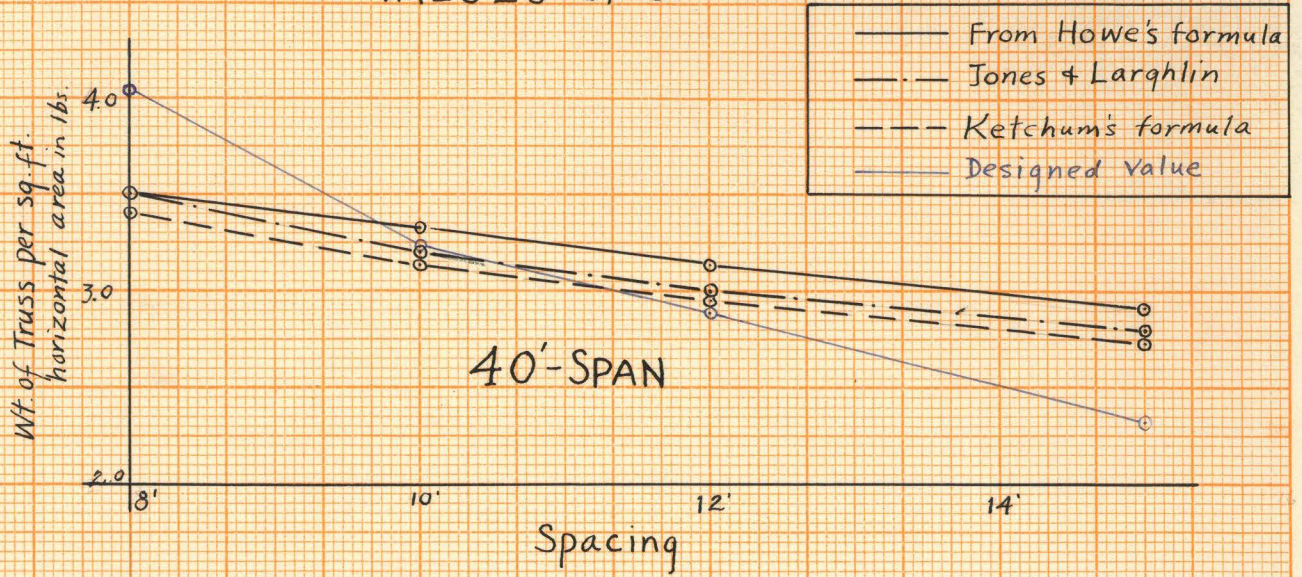
For shorter spans, the three chosen formulas do not seem to deviate from each other very much. For longer spans, Howe's formula seemed to give values closest to the actual designed values of w .

TABLE XV

Values of w from different formulas compared with actual w.

| | 40' span | | | | | 60' span | | | | | 100' span | | | | |
|----------------------|----------|------|------|------|------|----------|-------|------|------|-------|-----------|------|------|------|--|
| | 8' | 10' | 12' | 15' | 10' | 12' | 15' | 18' | 20' | 22.5' | 15' | 20' | 25' | 30' | |
| actual | 4.03 | 3.22 | 2.84 | 2.32 | 3.75 | 3.16 | 2.795 | 2.43 | 2.67 | 2.53 | 4.2 | 3.65 | 3.69 | 3.44 | |
| Howe | 3.5 | 3.31 | 3.14 | 2.91 | 4.12 | 3.94 | 3.70 | 3.48 | 3.35 | 3.2 | 4.7 | 4.36 | 4.07 | 3.8 | |
| Cambria | 5.0 | | | | 5.0 | | | | | | | | | | |
| Carnegie | 2.265 | | | | 3.05 | | | | | | 4.50 | | | | |
| Fowler | 3.0 | | | | 4.2 | | | | | | 6.60 | | | | |
| T. B.T. | 5.6 | | | | 6.4 | | | | | | 8.00 | | | | |
| Jones + Larghlin | 43.5 | 43.2 | 3.0 | 2.8 | 4.2 | 4.0 | 3.8 | 3.66 | 3.6 | 3.54 | 5.8 | 5.6 | 5.48 | 5.4 | |
| Ketchum | 3.4 | 3.14 | 2.95 | 2.73 | 4.27 | 4.07 | 3.65 | 3.41 | 3.28 | 3.14 | 5.49 | 4.87 | 4.45 | 4.13 | |
| Maurer | 2.6 | | | | 3.4 | | | | | | 5.0 | | | | |
| Merriman | 3.75 | | | | 5.25 | | | | | | 8.25 | | | | |
| Ricker, 1907 | 1.87 | | | | 3.0 | | | | | | 5.66 | | | | |
| Ricker, 1912 | 1.73 | | | | 2.69 | | | | | | 4.8 | | | | |
| Trautwine | 2.6 | | | | 3.9 | | | | | | 6.5 | | | | |
| Tyrrell | 3.5 | | | | | | | | | | | | | | |
| Carnegie Handbook | 2.264 | | | | 3.05 | | | | | | 4.5 | | | | |

VALUES OF W



In calculating stresses, the weight of the truss is usually so small compared with the weight of the covering and the snow and the wind, that an error in its assumption is negligible. Table XVI on the following page shows that the actual weight of truss to the total load on the truss for the determination of stresses in different members varied from 7.55% to 10.6%.

For different loadings the variation in weight is usually from 25 to 75% of the variation in loading.^o

It should be noted that the personal equation of the designer and many factors entering into the weight of roof trusses may cause a variation of 5 to 25% in the same truss. Thus the designer must base on his own judgment and experience.

^oEng. News. Recd., March 20, 1919.

TABLE XVI
The Ratio of Trusses Weight to Total Load*

| | Panel loads | Spacing 8' | 10' | 12' | 15' | 18' | 20' | 22.5' | 25' | 30' |
|--------------|--------------------------------|---------------|--------|---------|---------|--------|--------|-------------------|--------|--------|
| 40' span | Truss wt. | 127.5 # | 166. # | 188.5 # | 218.0 # | | | | | |
| | Total vert. load | 1,456. | 1,965. | 2,262. | 2,884. | | | | | |
| | Truss wt. as % of tot. load | 8.75% | 8.45% | 8.34% | 7.55% | | | | | |
| 60' span | Truss wt. | | 309. # | 355. # | 416. # | 470. # | 502. # | 540. # | | |
| | Total load | | 3098. | 3774 | 4792 | 4860 | 6653 | 7690 | | |
| | Truss wt. as % total load | | 10. % | 9.4 % | 8.69% | 9.65 % | 7.55 % | 7.02 % | | |
| 100' span | Truss wt. | | | | 882. | | 1090 | | 1270 | 1425 |
| | Total load | | | | 8327 | | 11,325 | 14,428 | 14,428 | 18,175 |
| | Truss wt. as % total load | | | | 10.6 % | | 9.62 % | | 8.8 % | 7.85 % |

*Total load = Dead + 1/2 snow + Wind (vertical)