

Quantum Measurements with Superconducting Nanowire Single Photon Detectors

Thesis by
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The logo for the California Institute of Technology (Caltech), featuring the word "Caltech" in a bold, orange, sans-serif font.

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ABSTRACT

The Superconducting Nanowire Single-Photon Detector (SNSPD) is a type of high-performance time-correlated photon counting detector. These detectors usually operated just a few degrees above absolute zero. They are made from a current-biased and often meandered nanowire that partially transitions between a superconducting and resistive state when a photon is absorbed. This produces a voltage pulse, which is amplified and time-tagged, providing an accurate measurement of the photon arrival time.

SNSPDs, first demonstrated in the 1990s [1], are now mature devices used widely in fields from deep space optical communication, to biological imaging, to quantum communication and computation [2], [3]. They are available commercially and are under continued development at national labs and universities. Much of the ongoing research into SNSPDs is centered around leveraging the device physics of the superconducting material to achieve higher performance across a number of metrics including efficiency, jitter, and count rate. However, getting the best performance out of both novel and more conventional SNSPD designs is not trivial. This thesis explores techniques for improving count rate, dark count rate, timing resolution, and photon number resolution of both emerging and more established types of SNSPDs.

We first show a novel optical filtering technique can minimize the dark count rate of an SNSPD. Although geared towards applications that employ free space coupling, this work also demonstrates a dark count rate lower than the state of the art for fiber-coupled SNSPDs.

We then study the dynamics that usually limit the maximum count rate of SNSPDs in application, namely the advent of bias-current reset and pileup-induced distortions that degrade timing resolution. Through a calibration and in-situ software correction procedure, we show that high count rate jitter can be reduced by a factor of 2 or more without the need for additional hardware or offline processing. This technique has wide applicability to many SNSPD systems that would benefit from the ability to run at higher count rates without sacrificing timing resolution.

SNSPDs are used in the ground receiver for NASA's Deep Space Optical Communication (DSOC) project, which demonstrates high-rate optical communication with the Psyche spacecraft through a Pulse Position Modulation (PPM) scheme [4]. We demonstrate SNSPD detection of a comparable PPM protocol operating 10 times faster than DSOC, and develop a novel method for resolving and correcting the presence of photon-number dependent effects in SNSPDs.

In our final demonstration, we leverage the strengths of novel low-jitter SNSPDs [5] in a high-rate entanglement distribution system based on a fast mode-locked laser. We show these detectors enable the use of highly stable and compact interferometers as well as readily available telecom multiplexing equipment. We demonstrate entanglement visibilities up to 99.4%, distillable entanglement rate of up to 3.55 MHz across 8 frequency channels, and predict a straightforward path towards achieving an order of magnitude improvement in rates without compromising visibility.

This thesis works to uncover and demonstrate the best performance that can be obtained from both novel and more conventional SNSPDs. As we mainly study how to optimize the use and application of these devices — as opposed to the device physics or development of new SNSPDs — the content of this thesis has broad applicability to all users of this single photon detecting technology.

PUBLISHED CONTENT AND CONTRIBUTIONS

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- [2] **A. Mueller**, S. Davis, B. Korzh, et al., High-rate multiplexed entanglement source based on time-bin qubits for advanced quantum networks, 2023. arXiv: 2310.01804 [quant-ph].
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Chapter 1

INTRODUCTION

1.1 Introduction to SNSPDs

Superconducting Nanowire Single Photon Detectors (SNSPDs) are high performance single-photon detectors that operate at cryogenic temperatures. They stand out as the most capable single photon detection technology for near-infrared and increasingly mid-infrared wavelengths. They may be customized to exhibit extraordinary performance along a number of metrics including count rate [6], detection efficiency [7], [8], dark count rate [9], [10], and timing resolution [11]. Some designs achieve excellent performance across all such metrics simultaneously, which makes them uniquely qualified for certain quantum communication and optics applications [5]. This section elaborates on the fundamental principles underlying SNSPD operation, and reviews some recent SNSPD advancements and their relevance to certain applications.

Operating principles

An SNSPD consists of a thin superconducting nanowire patterned on a substrate biased by a DC current. The nanowire is typically made of a superconducting material such as niobium nitride (NbN), niobium titanium nitride (NbTiN), or tungsten silicide (WSi). The nanowire is connected to a readout circuit which is used to detect the electrical signals generated by the SNSPD upon absorption of a single photon.

When a photon hits the wire, it breaks a superconducting electron pair, or Cooper pair. This disruption creates quasiparticles and initiates a down-conversion cascade. This localized disruption of superconductivity in turn leads to the formation of region of reduced superconductivity called a hot-spot. The hot-spot has a higher resistance than the superconducting state, which due the initial flow of current, induces a voltage pulse from this region. This pulse is shunted out of the nanowire and into a readout circuit, which amplifies the pulse, and may include electronics for digitizing the pulse arrival time. Following the formation of the hotspot, the nanowire cools down through electron-phonon interaction with the substrate and returns back to the superconducting state, making it ready for the next photon detection.

The readout scheme typically adopted for the detection of these electrical signals involves separating the RF and DC components of the RF line from the SNSPD using a bias-T circuit. The RF component is afterwards amplified using one or more cryogenic or room temperature amplifiers. This is then followed by a free-running or TCSPC based time tagger which digitizes pulse arrival time.

Recent advancements

Recent SNSPDs advancements revolve around improving the detection efficiency, count rate, timing jitter, sensitive wavelength range, and scalability to large arrays. Ultra-fast measurements of short superconducting wires have demonstrated timing jitters as low as 3 ps and illuminated the relationship between timing jitter and intrinsic detection latency effects [11]. System detection efficiencies from 98% to 99.5% have been demonstrated as well, and highlight the necessity to enhance the quality of the optical cavity surrounding the detector by using ultra-high reflectivity mirrors or distributed Bragg reflectors [8], [12]. More recently, single photon sensitivity has been demonstrated out to 29 μm in thin silicon-rich WSi nanowires, paving the way for unique new SNSPD applications in astronomy and dark matter detection [13]. Finally, with the development of a novel thermally coupled readout architecture, a 400,000 pixel SNSPD array has been demonstrated — more than doubling the number of pixels from any previous superconducting detector array [14].

Going forward, there is a plethora of opportunities to improve the practicality of fabricating and using SNSPDs. There is a growing interest in wide superconducting strips with performance that rivals much narrower nanowire designs [15] thereby accommodating scalable photolithography processes. Finally, ongoing efforts are being made to increase the critical current and critical temperatures in advanced SNSPD superconducting materials.

Applications

Superconducting nanowire single-photon detectors (SNSPDs) have been employed in various applications, highlighting their versatility and potential in the field of photonics. These applications span different areas, ranging from astrophysics to biomedical imaging. This section provides a brief overview of some recent applications of SNSPDs.

Dark Matter Searches: SNSPDs have been utilized in experiments aimed at detecting dark matter particles. For example, one study has investigated using SNSPDs for direct detection of sub-GeV dark matter [16], while others have proposed using SNSPDs as photosensors in cryogenic scintillator-based experiments [17]. Another notable approach involves the search for dark photon dark matter using multilayer dielectric haloscopes [18,]. SNSPDs are employed to achieve efficient photon detection. By improving the limits on the kinetic mixing parameter for dark photon dark matter, these experiments provide valuable insights into the nature of dark matter in the eV mass range.

Cerebral Blood Flow Measurement: SNSPDs were used for diffuse correlation spectroscopy (DCS) measurements for the observation of cerebral blood flow [Ozana2021]. The high sensitivity of SNSPDs improved the signal-to-noise ratio and enabled the detection of low-intensity signals associated with pulsatile flow. This advancement in DCS technology has the potential to improve the understanding and diagnosis of cerebral blood flow-related conditions.

Deep Space Optical Communication: SNSPDs played a crucial role in the development of ground laser receiver (GLR) systems for deep space optical communication [4]. The GLR, equipped with an array of SNSPDs, received optical downlink signals from spaceborne transceivers. These detectors facilitated the processing of discrete downlink data rates over large distances, making significant contributions to the success of the Deep Space Optical Communication (DSOC) project.

Photon Counting LIDAR: SNSPDs also found application in LIDAR systems operating at 2.3 μm wavelength [19]. These detectors demonstrated enhanced photon counting performance in the mid-infrared region, making them suitable for free-space photon counting applications. This development opens up opportunities for LIDAR systems to operate in environments with low atmospheric absorption and background solar flux. In the more accessible wavelength range near 1.5 μm , LIDAR with SNSPDs has also been demonstrated with km range [20] and mm scale resolution [21].

In addition to these specific applications, SNSPDs have been extensively used in quantum key distribution and quantum communication experiments. Notably, they have been employed in demonstrating high-quality quantum teleportation [22] and will continue to be integral components in the development of advanced quantum networks [23].

This brief overview highlights the broad range of applications that have used SNSPDs, showcasing their potential to advance various fields of science and technology. With ongoing advancements in SNSPD technology and further optimization, these detectors will continue to play a vital role in enabling groundbreaking research and innovation.

1.2 The differential single pixel SNSPD

SNSPDs offer high efficiency, low dark count rates, high count rates, and low timing jitter. However, traditional SNSPD designs face challenges in achieving both high detection efficiency and low jitter, especially for large-area detectors. Marco Colangelo et al. [5] proposed a new device design for SNSPDs that combines differential readout and impedance matching tapers to overcome these challenges. This design enables high detection efficiency and low jitter simultaneously along with pixel-level imaging capabilities and photon-number resolution.

Detectors of the type demonstrated by Colangelo et al. [5] have been fabricated at JPL (Fig. 1.1 a) for the duration of this PhD research, and are used primarily for three projects detailed in this thesis: the low dark count rate project, the Pulse Position Modulation (PPM) and Photon Number Resolution (PNR) project, and the high rate entanglement project. Given the significance of the differential tapered SNSPD to much of this body of work, we review its key design and performance features here.

Jitter cancellation through differential readout

Two main types of jitter arise in high efficiency SNSPD designs: amplifier jitter and geometric jitter. Amplifier jitter is the effect of readout electrical noise on timing jitter. In contrast, geometric jitter originates from propagation delays due to detection events happening at varying locations along the nanowires' twist. Nanowires made of thin-film materials exhibit high kinetic inductance and behave like transmission lines with high characteristic impedance and slow phase velocity. These transmission line properties result in pulse propagation delays that contribute to the timing jitter of the detector. The arrival time of voltage pulses from the detector to time tagging equipment depends on the location of photon absorption in the nanowire, as detections closer to the ground termination and farther from the single readout must travel farther at low phase velocity through the nanowire before

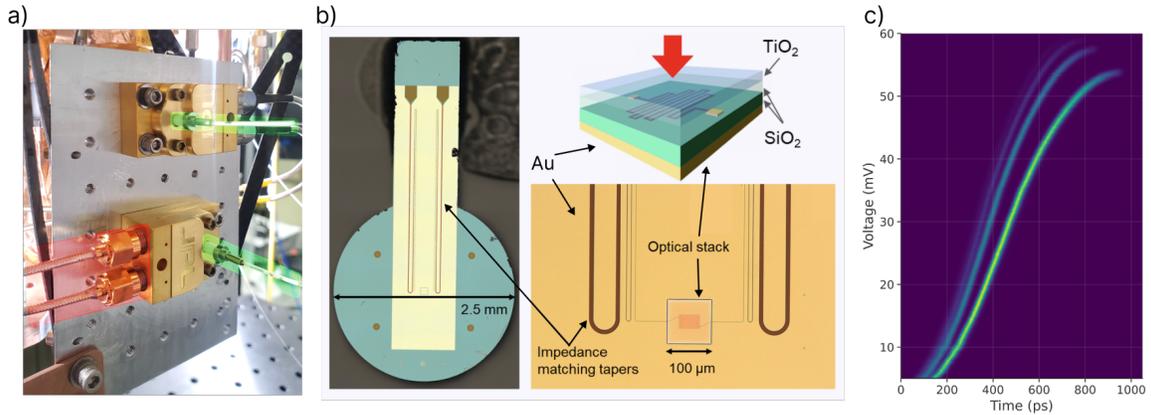


Figure 1.1: **Differential single pixel** a) Two packaged differential single pixel detectors. Coupled fibers highlighted in green, differential SMA readout highlighted in red b) Magnified images of the detector's lollipop-shaped wafer, highlighting where the tapers and efficiency-enhancing optical stack are located c) Integrated 2D histogram showing different heights and shapes of RF pulse rising edge in response to incident multi-photon optical pulses.

existing. For large detectors, geometric jitter can contribute tens of picoseconds to the total system jitter. Increasing detector size for resolving a given optical mode usually improves detection efficiency. Thus, using single-ended readout leads to a tradeoff between system detection efficiency and jitter induced by longitudinal geometric effects.

Adopting a differential readout approach can resolve the aforementioned issues. Instead of just isolating the positive voltage pulse, the negative pulse from the other end of the nanowire is also collected. Simple processing of both pulses reveals information about photon arrival time as well as photon arrival location.

If the measurements of arrival time t_F and absorption location along the nanowire are both significant to the application, then the timing of the t_{neg} negative and positive t_{pos} voltage pulses may be read out with two time taggers or high-speed oscilloscope channels. The difference of arrival time $t_{pos} - t_{neg}$ of these signals constitutes the photon absorption location information, while the average $(t_{pos} + t_{neg})/2$ of the arrival times constitutes the photon arrival time information. For practical single photon counting applications, however, the photon arrival time information is typically sufficient and real-time processing of two time tags per detection event is not practical. Therefore, a 2:1 balun transformer can be used to perform an equivalent hardware difference of the positive and negative pulses (analogous to the averaging of timetags t_{pos}, t_{neg}). After amplification, the two sides of the

detector are connected to the differential inputs of the balun, with the output being sent to a TCSPC or equivalent time tagging module. The threshold voltage of the time tagger can be set to minimize the spread of time tag distribution, corresponding to the condition where the timing measurement $t_{tagger} \approx t_F$ so that the photon arrival location information is negated.

Impedance matching tapers

In a typical SNSPD, the nanowire exhibits impedance on the order of $k\Omega$, while the readout circuit has an impedance of 50Ω . This mismatch can lead to RF pulses that exhibit reflections and distortions. These effects reduce slew rate and lower Signal to Noise Ratio, bringing about higher amplifier jitter [11], [24].

The higher jitter that results from the impedance mismatch can be mitigated by designing the SNSPD to preserve the integrity of the output pulse. An impedance-matching taper interfacing the nanowire to the readout line can be integrated. Thanks to the gradual impedance transformation of a Klopfenstein-style taper, the output pulse has a higher amplitude and a faster slew rate. In a simplified theoretical SNSPD model by Colangelo et al. [5], the incorporation of a taper increases pulse amplitude by a factor of 3.3.

For the research in this thesis, these detectors are usually used with a differencing balun for geometric jitter cancellation. The type fabricated at JPL typically has active areas of $22 \times 15 \mu\text{m}$, formed by a meander of 100 nm-wide and 5-nm-thick niobium nitride (NbN) nanowires on a 500 nm pitch (Fig. 1.1 b). They are embedded in an efficiency-enhancing optical stack made of alternating layers of TiO_2 and SiO_2 and a gold mirror layer and typically have FWHM timing jitter of about 14 ps. The FW1%M jitter, which is a measure of the width of the jitter response function or histogram at 1% height, is an important metric for quantum or classical communication protocols that expect to reliably place photon timing measurements into time bins measured with respect to a clock. This is the case for pulsed Quantum Key Distribution and classical Pulse Position Modulation communication protocols. The differential single pixel SNSPDs exhibit FW1%M jitter of 49 ps.

Impedance matching tapers can also help distinguish between instances when one or multiple photons are absorbed in the nanowire on a short timescale (< 100 ps). The absorption of different numbers of photons results in variations in RF pulse height and slew rate (Fig. 1.1 c). This phenomenon gives the detector photon number resolution (PNR) whereby the specific number of photons in an optical pulse can be measured. This is in contrast to the more common binary detection capability offered by conventional SNSPDs that only indicates if one or more photons are absorbed. Chapter 4 explores how the manifestation of photon number resolution in this detector type presents an issue for accurate time-correlated measurements of multi-photon light pulses. Once properly managed, both arrival time and photon number resolution may be resolved accurately, which is potentially useful for various quantum communication and computing applications.

1.3 Structure of this thesis

This thesis is organized into six main sections: an introduction, four chapters, and a conclusion. Each chapter is based on a major research project and includes an introduction, sections describing design choices and methods, and sections that specify results. Later sections in each chapter provide supplementary information and discussion. References to these supplementary discussions can be found throughout the respective chapters.

The first appendix includes exercises derived from Matthew Shaw's 2022 series of guest lectures in the course titled Quantum Hardware and Techniques (Caltech APh/Ph 138b). Both problems delve into concepts closely related to, or motivating, research in this thesis. The first problem examines some subtle and non-intuitive features of effective free space coupling for a single photon detector through a cryostat window. The second problem shows how high-efficiency coupling to a photon number resolving detector is extremely important for heralded generation of non-classical light.

The second appendix includes summaries and links to the major software repositories created for the research in this thesis.

Chapter 2

LOW DARK COUNT RATE DETECTION

2.1 Free-space coupled superconducting nanowire single-photon detector with low dark counts

A version of this chapter is published as:

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2.2 Abstract

A free-space coupled superconducting nanowire single photon detector with high efficiency at 1550 nm, sub-0.1 Hz dark count rate, and sub-15 ps timing jitter is demonstrated.

Background

Superconducting nanowire single photon detectors are highly sensitive devices. Any stray photons from a laboratory environment can be coupled to these devices and produce a detection called a dark count or false count. Dark counts may be present in any situation where the detector is coupled to some experiment or apparatus outside the cryogenic environment. This coupling may be through windows inside the cryostat housing and radiation shields, or through optical fibers that carry single-mode signals directly to detectors.

Visible, near-infrared, and mid-infrared photons are often the main sources of dark counts, because they are ubiquitous in a laboratory environment and are transmitted through common types of fibers and windows. Assuming visible light can be blocked from entering the detector system, the blackbody emission of the room temperature laboratory environment presents is the primary source of dark counts. The spectrum of blackbody photons, defined by Planck's law, is peaked at about 10 μm , though it can contribute dark counts at significant rates up through near-infrared wavelengths.

Without filtering in fiber or free-space, dark counts from blackbody emission will overload most SNSPDs and overpower the extremely faint signal of interest. In this work we investigate minimizing dark counts through the use of cryogenic free-space filtering.

2.3 Introduction

Quantum communication applications require detection systems with performance optimized across 3 metrics: system detector efficiency, timing jitter and dark count rate. The dimensionless figure of merit H specifies this application-specific performance as $H = \frac{\eta}{(\Delta t D)}$ [25].

Here, we focused on lowering the Dark Count Rate (DCR) of a telecom-band SNSPD system by filtering thermal photons, without sacrificing efficiency or jitter. We demonstrated a free-space coupled SNSPD with sub-0.1 Hz DCR, 14 ps timing jitter, and 72% total system detection efficiency (SDE) by using a differential single-pixel SNSPD [26] to image a single-mode fiber through an optimized free-space filter stack.

The highest system detection efficiencies have been achieved using self-aligned fiber coupling where dark counts can be reduced using cryogenic fiber looping [27] or spliced narrow-band filters [28]. But it is difficult to achieve strong filtering without losses at the target wavelength. Low-loss, high-rejection filters are typically available as free-space components, so some of the highest reported H-values were achieved with cryogenic, fiber to free-space to fiber coupling, but exhibit an SDE of only a few percent [9]. The filtering method presented here takes advantage of commercially-available filters, achieves a high free-space coupling efficiency using a cryogenic lens, and is compatible with both fiber and free-space optical inputs.

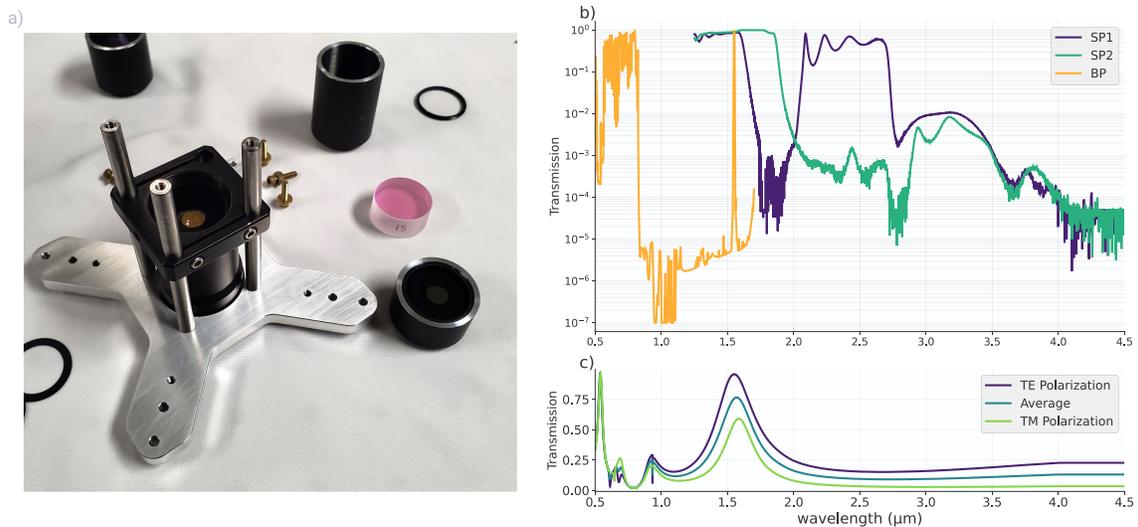


Figure 2.1: **Filters and transmission spectra** a) various optics and hardware used for free-space coupling inside the cryostat, including one of the Semrock bandpass filters (purple)

The system was designed around the use of two types of ultra-high rejection custom short-pass filters, two each with pass-bands below $1.6\mu\text{m}$ and $1.9\mu\text{m}$ (Andover Corp.). As shown in Fig. 2.1 b, any mid-IR passbands of one filter complement a high rejection spectral region of the other. They reject wavelengths shorter than $3\mu\text{m}$ through reflective optical coatings, and attenuate longer wavelengths through material absorption in the N-BK7 glass substrate. Since the filtering depends on the attenuation of the glass itself, the filters are unusually thick, measuring 12.7 mm .

As initial modelling showed that 4 filters in series were required to sufficiently block mid-IR light, the cryostat design had to accommodate a set of filters several inches thick. This thickness, and the desire to couple to a single-mode fiber-compatible detector with low jitter, also necessitated the use of a cryogenic lens. A 1-inch diameter lens, if mounted outside the cryostat with a focal length surpassing the filter-stack thickness, could not have focused to a sufficiently small spot.

2.4 Design

A modified translatable 0.8 K stage was designed at JPL. It positioned the 0.8 K stage very close to the 4 K stage above, and was attached to the 0.8 K pot of the sorption cryocooler via a copper braid. Bendable carbon fiber rods connected the 0.8 K stage to a 4 K mount through which an optical stack of filter and lens could be positioned.

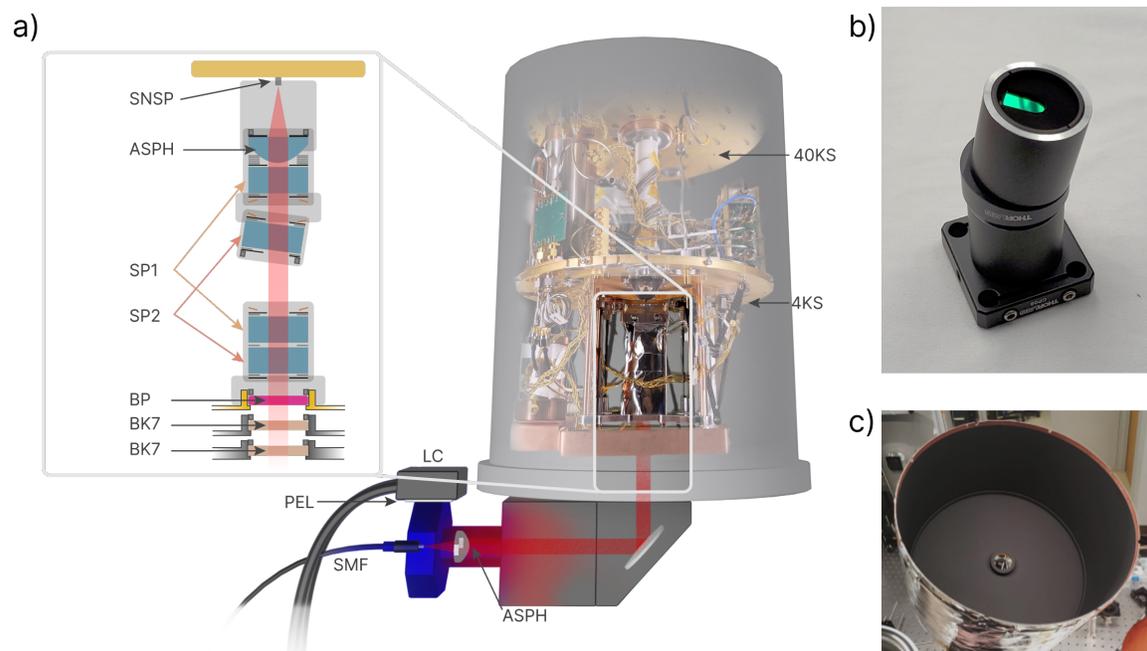


Figure 2.2: **Full system layout** a) System hardware. ASPH: aspheric lens, (Edmund Optics #47-729) SP1 & SP2: custom short-pass filters (semrock), BP: band-pass filter, (Semrock NIR01-1550/3-25), BK7: glass windows, SMF: Single-mode fiber, PEL: Peltier element, LC: Liquid cooling block b) Lens tube structure used in the fridge that holds the cryogenic lens and 2 short pass filters. c) Radiation shield painted with Mid-IR absorbing paint

A single mode fiber was used to image onto the detector using two $f = 18.75$ mm lenses. One lens collimated light from an optical fiber face outside the cryostat (Photon Spot), and the other focused light onto the detector inside [29]. In the collimated region between, the beam passed through the short pass filter stack (Fig. 2.2 a). One of the short-pass filters was angled to avoid ghosting or etalon effects. The 40 K radiation shield and outer cryostat housing were fitted with anti-reflection coated BK7 windows. The filters were spring loaded to prevent cracking at low temperatures. To minimize effects of stray light, the interior of the 4 K shield was painted with mid-IR absorbing paint (Aeroglaze Z306) as shown in Fig. 2.2 c [30], while gaps between filters and the windows were covered with metal tape.

The system was based on 1-inch optics, although the $f = 18.75$ mm lenses lead to a $1/e^2$ intensity diameter of about 5 mm in the collimated region. To reduce the larger-than-required numerical aperture of the system, painted 8 mm apertures (Acktar Spectral Black) were added in the collimated region. These are large enough to allow minor alignment

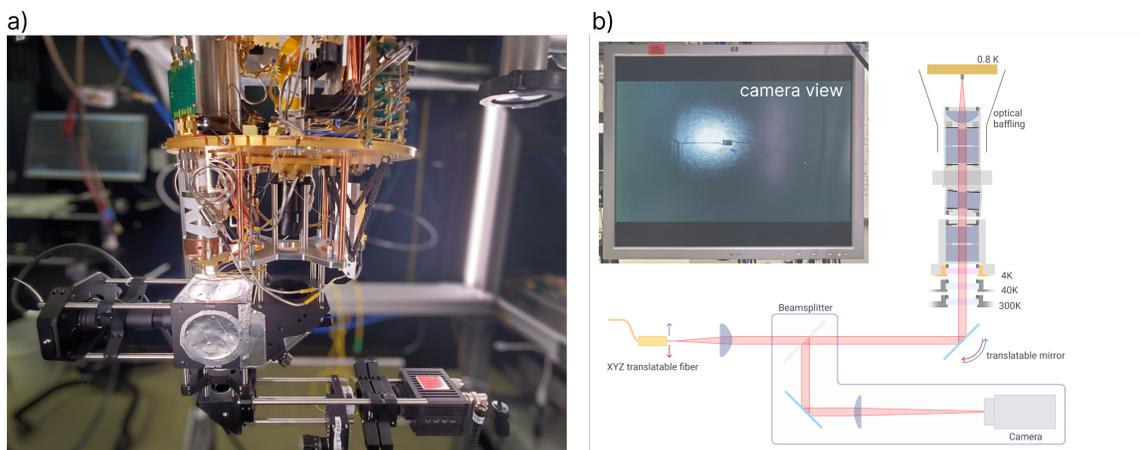


Figure 2.3: **Method of optical alignment** a) Configuration used for checking alignment of the cryo-lens with the fridge open. b) Diagram of the optics in the same configuration. The 4 K radiation shield (not shown in full) supports 2 of the short pass filters and bandpass filter (pink).

adjustments — by translating the exterior collimating lens — without vignetting. Upon discovering that the short-pass filters alone did not provide leading dark count rate performance, we incorporated a bandpass filter mounted in the 4 K radiation shield optical port.

2.5 Alignment

The cryo-lens and 0.8 K optical stage had to align using a configuration that worked whether the fridge was open or closed. The x-bracket design, supporting the 0.8 K stage, accommodated optical posts at the same positions as the standoffs on the cryostat's exterior can. Fig. 2.3 a shows the free-space optics attached to the internals of the cryostat. This included fiber collimation optics and a beamsplitter/camera module that could be removed to achieve maximum coupling efficiency. The camera images the plane of the detector, and is able to observe features of the nanowire wafer (like the detector and impedance matching taper barely visible in the camera view in Fig. 2.3 b). Adding a bandpass filter to the system blocked any broadband light source used for detector imaging. Consequently, we achieved detector alignment by iteratively: de-focusing the source laser to flood illuminate the detector, identifying the detector's location in the camera view and marking it, and finally refocusing the source laser onto the detector and reducing it to a single photon level to measure efficiency.

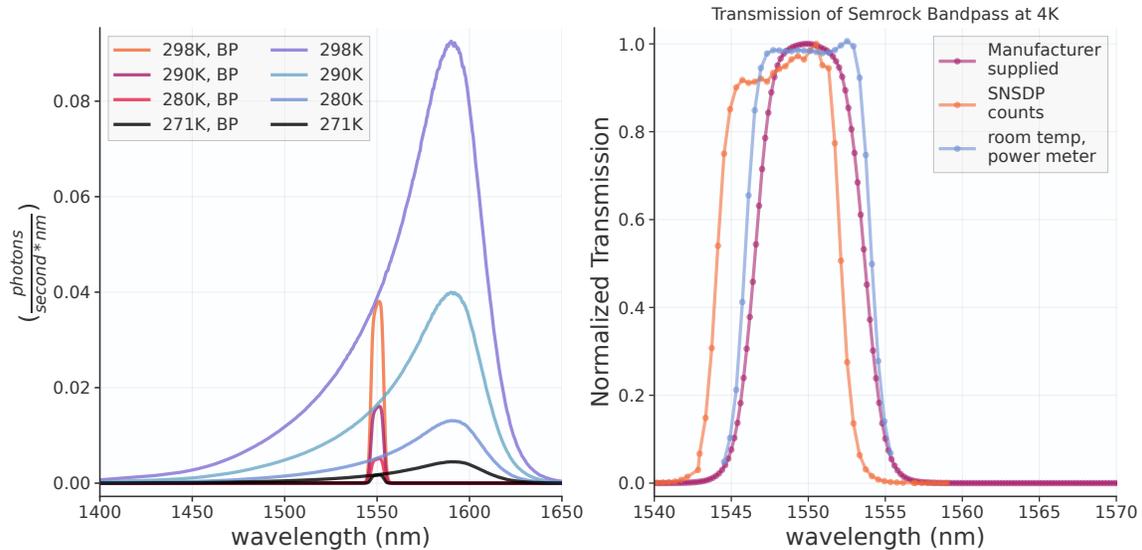


Figure 2.4: **Dark count rate simulation & bandpass transmission** a) Simulated photon flux at various laboratory temperatures with and without the 1550 nm bandpass filter (BP). b) Normalized transmission spectrum of the bandpass filter. Plotted at low temperature by measuring SNSDP count rate versus frequency of the illuminating laser.

2.6 Modelling & external cooling

The filtering of the optical stack was modeled by assuming a black-body emitter at 298 K and a field of view defined by the 18.75 mm focal length of the cryogenic lens and the 8 mm diameter of the apertures. The resulting spectrum was multiplied by the transmission of the filters and detector optical stack (see Fig. 2.1). The model showed that two each of the 1.6 μm and 1.9 μm short pass filters were necessary to suppress mid-infrared light to where it was no longer the dominant source of dark counts. With the inclusion of the four shortpass filters, the dominant source of dark counts is the spectral region near 1550 nm as shown in Fig. 2.4 a, which also illustrates the effect of the bandpass filter.

While the bandpass filter (FWHM = 7 nm) was found to blue-shift by about 2 nm at cryogenic temperatures, the passband was wide enough such that significant attenuation was not observed at the original target wavelength of 1550 nm. This filter is also sufficiently wide to avoid Fourier-limited broadening of ultra-short laser pulses.

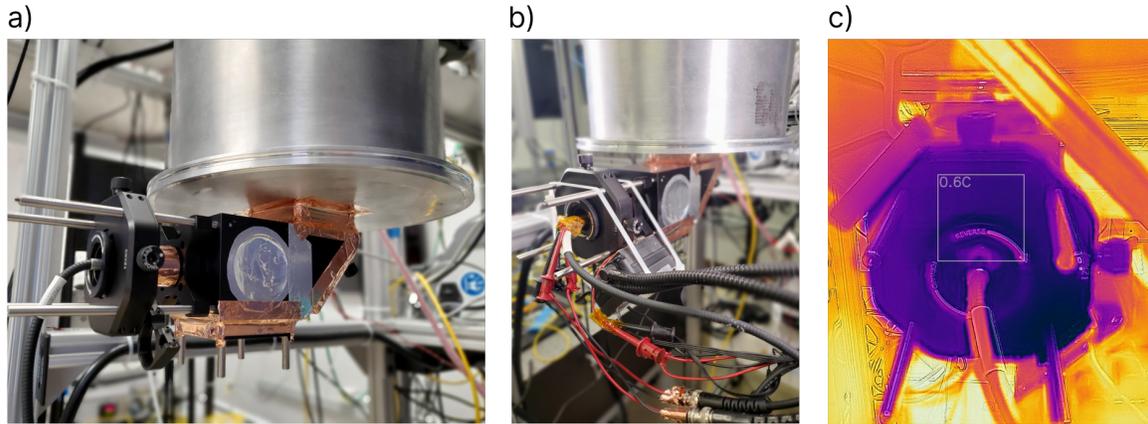


Figure 2.5: **External optics and cooling** a) The mirror and XYZ translation fiber mount used on the exterior of the cryostat during normal low-dark-count operation. b) The liquid cooling block attached over a thermoelectric element onto the XYZ translation mount. Cooling a surface as close as possible to the fiber output reduced dark counts the best. Other visible wires power thermal probes. c) Infrared image showing the cooling effect on the XYZ mount.

Also evident in Fig. 2.4 a is the strong dependence of DCR on the temperature of the final surface outside the cryostat emitting thermal radiation. This motivated the exterior cooling apparatus sketched in Fig. 2.2 a and shown in Fig. 2.5 b and c. The bulkhead holding the fiber connector is cooled to around -2°C using a Peltier element and liquid cooling block. This addition reduced the system DCR from 0.4 Hz to below 0.1 Hz. While dark counts from multiple spatial modes are present in this system — modes that would not be present in a purely fiber based approach — the external cooling technique works to minimize their effect. Compared with the use of piezo-electric actuators or servos inside the cryostat for optical alignment, the external cooling approach is simple and cost-effective.

This work used a low-jitter SNSPD of the tapered differential design [5], with an active area of $22 \times 15 \mu\text{m}$, formed by a meander of 100 nm-wide and 5-nm-thick niobium nitride (NbN) nanowires on a 500 nm pitch. A more conventional single-ended readout SNSPD of similar area would also achieve low DCR in this coupling system, but would likely achieve a lower performance metric H from correspondingly higher jitter. The nanowire is embedded in an efficiency-enhancing optical stack made of alternating layers of TiO_2 and SiO_2 and a gold mirror layer. As shown in Fig. 2.6 a and b, when fiber coupled (without any fiber-based filtering methods applied), this detector achieved a saturated SDE of $84\% \pm 4.4\%$ and a DCR of 20 Hz at a bias current of $16 \mu\text{A}$.

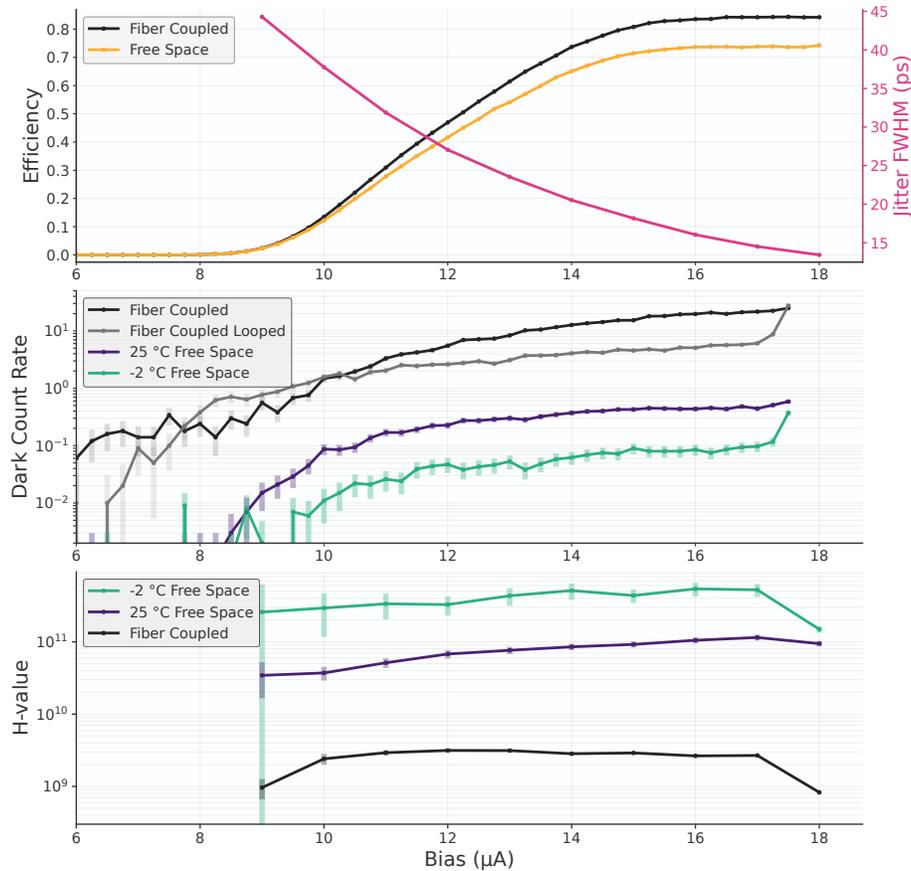


Figure 2.6: **Main results** a) Photon count rate vs. bias current showing saturated system detection efficiency of 72%. Detector jitter is also plotted, which decreases with increasing bias current. b) dark count rate vs. bias current for fiber coupled and free space coupled setups. c) values for the H metric derived from the data above for the free and fiber coupled configurations.

2.7 Results

As also shown in Fig. 2.6 a, the free-space coupling system achieves up to $72\% \pm 3.7\%$ SDE as measured from the fiber outside the cryostat. The reduction in efficiency is likely due to surface reflections in the free-space optics, and potential misalignment in the optical baffles. The minimum DCR (Fig. 2.6 b) at 72% SDE is about 0.1 Hz, with a bias current of 16 μA . These metrics, with the jitter measurements shown in Fig. 2.6 a, give a maximum H value of 5×10^{11} (Fig. 2.6 c). Values as high as 1.8×10^{12} have been reported before, but at 1.5% system detection efficiency [9]. Our system shows a low DCR can be achieved without severe reduction of SDE or usable target wavelength bandwidth. This is paramount for the future of terrestrial and space-to-ground quantum communication, since it increases

success rate with finite statistics [28]. The same techniques can be applied to emerging SNSPD applications at longer wavelengths, such as laser ranging [19], where fiber filtering is impractical. Beyond single-mode applications, our work paves the way to scalable, low-DCR, multi-mode coupling to SNSPD arrays [31].

Chapter 3

TIME WALK AND JITTER CORRECTION

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3.1 Abstract

Superconducting nanowire single-photon detectors (SNSPDs) are a leading detector type for time correlated single photon counting, especially in the near-infrared. When operated at high count rates, SNSPDs exhibit increased timing jitter caused by internal device properties and features of the RF amplification chain. Variations in RF pulse height and shape lead to variations in the latency of timing measurements. To compensate for this, we demonstrate a calibration method that correlates delays in detection events with the time elapsed between pulses. The increase in jitter at high rates can be largely canceled in software by applying corrections derived from the calibration process. We demonstrate our method with a single-pixel tungsten silicide SNSPD and show it decreases high count rate jitter. The technique is especially effective at removing a long tail that appears in the instrument

response function at high count rates. At a count rate of 11.4 MCounts/s, we reduce the full width at 1% maximum level (FW1%M) by 45%. The method, therefore, enables certain quantum communication protocols that are rate-limited by the FW1%M metric to operate almost twice as fast.

3.2 Introduction

Over the last decade, SNSPDs have advanced rapidly to become essential components in many optical systems and technologies, owing to their high efficiency ($> 90\%$) [8], [12], fast reset times (< 1 ns) [32] and scalability to kilopixel arrays [31]. The timing jitter of SNSPDs is also best-in-class – values as low as 3 ps have been demonstrated in short nanowires [11], and new high-efficiency designs exhibit sub-10 ps jitter [26], [33].

SNSPD jitter increases with count rate due to properties of the nanowire reset process and features of the readout circuit. The effect bears resemblance to time walk observed in silicon avalanche diodes and other detectors where the pulses have varying heights and slew rates [34] thereby causing a timing measurement using a fixed threshold to ‘walk’ along the rising edge of the pulse (the labeled delay in Fig. 3.1 a). At low count rates SNSPDs exhibit very uniform pulse heights. However, at high counts rates where the inter-arrival time is on the order of the reset time of the detector, current-reset and amplifier effects lead to smaller and distorted pulses. If photon inter-arrival times are not known a priori in the intended application, the uncorrected time walk manifests as a perceived increase in jitter (Fig. 3.1 b).

The time-walk effect in SNSPDs is typically not reported, as jitter is usually measured at low count rates where the detector has ample time to reset following each detection. But as communication and quantum information applications push into higher count rates, the high count rate induced jitter becomes more relevant. LIDAR, quantum and classical optical communication, and imaging applications may all benefit from the development of new detection systems and methods that keep jitter as low as possible in this regime.

We first consider the features of SNSPD operation and readout that cause an increase in jitter with count rate. Then we present multiple ways of mitigating or avoiding these effects, before reviewing our preferred method that relies on a calibration and correction process.

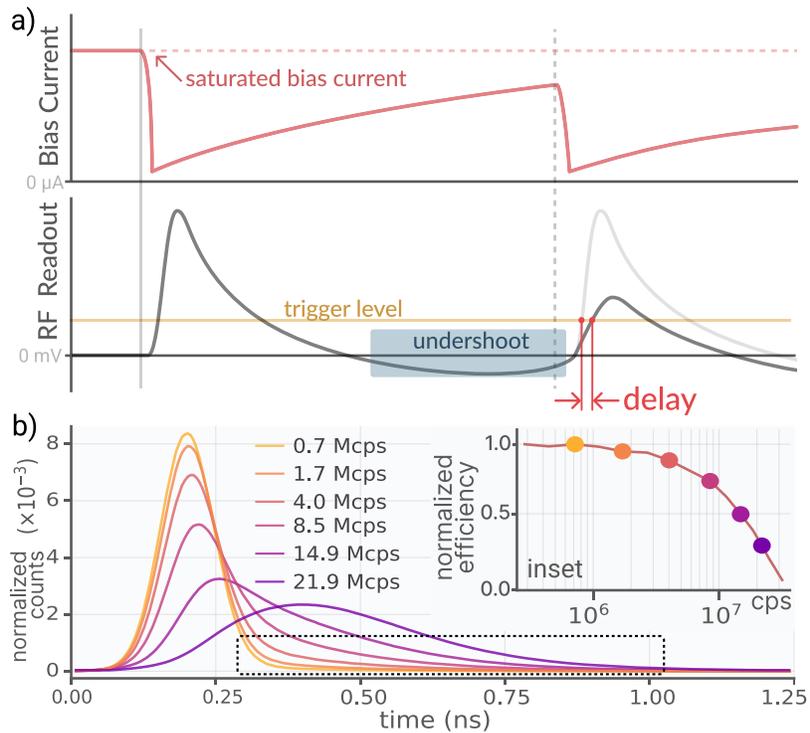


Figure 3.1: **Introduction to the time walk effect** a) Diagram illustrating two major sources of correlated high count rate jitter. First, detections may occur during the reset time of a previous detection. At this time the bias current in the nanowire is below its saturated value so that a photodetection triggers an RF pulse with correspondingly lower amplitude. Second, an RF pulse may arrive in the undershoot region of a previous pulse, where the undershoot is a period of negative voltage induced by the low-frequency cutoff properties of the readout amplifier chain. (b) Measured histograms of detections from short 3 ps mode-locked laser pulses. With lower attenuation and higher count rate, the observed timing uncertainty is greater. Inset shows where respective count rates fall on a maximum count rate (MCR) curve [35]. The MCR of an SNSPD is often quoted at the 3 dB point, where the normalized efficiency drops to -3 dB of its maximum value. The jitter increase due to time walk manifests as a tail in the instrument response functions (inside dashed black box) even at count rates significantly below the 3-dB point where detector efficiency has not started to drop significantly (e.g., the 1.7 Mcps data).

The jitter increase observed at high rate originates from two groups of system characteristics: (i) the intrinsic reset properties of the nanowire, and (ii) properties of the amplification chain. These influence the system's jitter differently, thus it is helpful to consider them separately. Added jitter from either or both sources can emerge when an SNSPD system is operated at high count rates.

The nanowire reset process determines how the detector becomes single-photon sensitive again after a detection. When an SNSPD fires, the current flow in the nanowire momentarily drops to near zero, then recovers in an inverted exponential fashion (Fig. 3.1 a). An incident photon may trigger another detection before the bias current fully returns to its saturated value, producing a pulse with a lower amplitude and slew rate. A fixed threshold comparator will trigger on this lower pulse later in time than a full amplitude pulse. If uncorrected for, this time walk manifests as an increase in jitter at high count rates.

The choice of readout amplifiers may also contribute to added high count rate jitter. Pulses may be shifted in voltage and distorted if they arrive when the RF signal has not yet reached a steady zero state following the previous detection. For example, pulses may arrive within an amplifier-induced undershoot region following previous pulses. This phenomenon is illustrated in Fig. 3.1 a as the area below 0 mV. The duration of ringing or undershoot effects varies widely depending on the design of the readout circuit. If they last longer than the reset time of the nanowire bias current, the calibration technique may correct for the potentially complex interactions between pulse waveforms that overlap in time.

Jitter mitigation methods at high count rates

There are various methods for correcting for increased jitter at high count rates. These include (i) the use of extra hardware that cancels out some distortions, or (ii) simple software-based data filtering that ignores distorted time-tags. We review these techniques before covering the calibration and correction approach.

Variations in pulse height are a primary component of the distortions that appear at high rates. Such variations in other systems are commonly corrected with a constant fraction discriminator (CFD) that allows for triggering at a fixed percentage of pulse height rather than at a fixed voltage. Adding a CFD to an existing setup is straightforward for a single channel, however it does require additional hardware such as multiple high-speed discrimi-

nators and a D-type flip-flop [36], which significantly increases the circuit complexity and power budget of a multi-channel system. In addition, CFDs are not expected to optimally correct for distortions of the pulse rising edge which may arise from the overlap of one pulse with a signal reflection or undershoot features on the falling edge of a previous pulse. Multi-channel time-to-digital converters (TDCs) used to read out large SNSPD arrays typically only include fixed-threshold comparators [31].

In a simple software-based jitter mitigation method, each time-tagged event may be accepted or rejected based on how soon it arrives after the previous pulse. Those that arrive within some pre-determined dead time are assumed to be corrupted by pulse distortions. These are rejected, and the rest are accepted. This method can lower system jitter and maintain high data rates, especially in the cases where only a few percent of pulses are filtered out. However, it can severely limit count rate near the 3 dB point where the majority of counts are rejected (see section 3.4 for details).

Our correction method preserves original count rate and works with timing measurements from a fixed-threshold free-running TDC – the type that is often used for SNSPD readout. Pulse pileup correction techniques have been demonstrated with systems that fully digitize detector pulse waveforms [37]–[39]. But capturing the fast rising edges of SNSPD pulses in this way would require very high sample rates and subsequently, impractically large data streams. In contrast, our method assumes one timing measurement is acquired from triggering on the rising edge of each SNSPD pulse.

We calculate the time between a given *current* SNSPD detection event and a preceding event. This inter-arrival time is used to determine a timing correction for the current event using a lookup table. A calibration routine described next is needed to build this lookup table. Applying these corrections during real-time processing removes deterministic delays correlated with the time between time-tags, leaving only stochastic jitter.

3.3 Method and results

The measurements used for calibration and correction were acquired with a high rate mode locked laser (Pritel). The minimum repetition rate of this laser was too high to produce a calibration dataset for the Tungsten Silicide detector at highest count rate, given the constraints addressed in the main text. Therefore, the laser was set at a repetition rate of 10.75

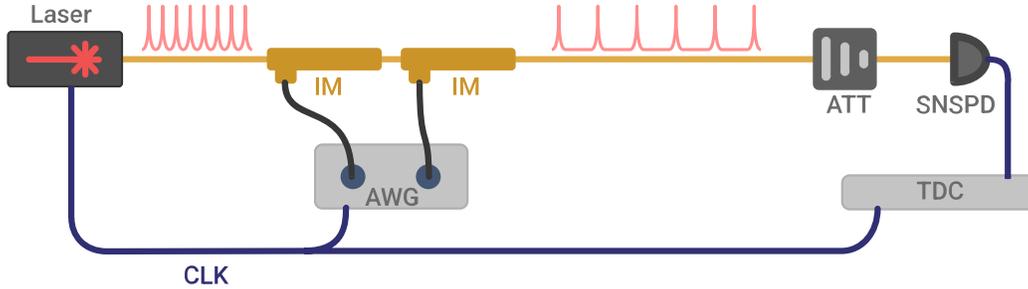


Figure 3.2: **Experimental Setup** CLK: clock synchronization signal; AWG: Arbitrary Waveform Generator (*Keysight*); IM: Intensity Modulator (*IXBlue*); TDC: Time to Digital Converter (*Swabian Instruments*). The extinction ratio of both modulators exceeds 30 dB.

GHz and modulated down to 537.5 MHz using two lithium niobate intensity modulators in series. Residual peaks from suppressed mode-locked laser pulses are not observed above the noise floor in the collected data, so their effect was not further considered. Clock jitter is minimized in post-processing with the help of a software-based Phase Locked Loop.

Detector and trigger level

We study the pulse distortions observed in a fiber coupled single-pixel tungsten silicide (WSi) SNSPD with $380 \mu\text{m}^2$ active area and 160 nm nanowire width. The detector is biased at $9.3 \mu\text{A}$, roughly 90% of the switching current. The readout is handled by a cryogenic DC-coupled amplifier, mounted on the 40 K-stage of the cryostat, which has 43 dB of gain and a 3 dB bandwidth of 700 MHz, followed by a 1 GHz amplifier with 20 dB of gain (*MiniCircuits ZFL-1000LN+*). The system reaches a 3 dB maximum count rate (MCR) of 15.6 MHz. The time constant of supercurrent recovery $\tau_{bias} \approx 40$ ns is significantly longer than the decay time constant of the RF pulse $\tau_{RF} \approx 5$ ns, owing to our use of a low-frequency cut-on of ≈ 80 MHz (-3 dB point from the peak gain) in the DC-coupled amplifiers. For this detector, the calibration process primarily corrects for the lower bias current effects, rather than for any overlapping between RF pulse waveforms (see section 3.4). Other detector types and readout systems may operate in a different regime.

The jitter increase with count rate is highly dependent on trigger level. High rate distortions affect the timing measurements less if the threshold voltage is set just above the noise floor.

But triggering on the pulse higher, where it achieves maximum slope, minimizes jitter at low-to-medium count rates. This level varies from 20% to 50% of pulse height depending on the detector. We found the minimum low-rate jitter at a trigger level of 50 mV, about 40% of the pulse height. All further calibration and analysis is performed by triggering at this level in order to optimize jitter across all count rates.

Mode locked laser calibration

To perform our calibration, we illuminated the SNSPD with an attenuated 537.5 MHz mode locked laser with a mean photon number per pulse between $5e-4$ and 0.016. The 1.86 ns period of the pulse sequence is large enough that almost all SNSPD detections can be unambiguously matched with a preceding laser pulse — the period of the pulse train used must be greater than the worst detector jitter for this to succeed. The uncorrected jitter for the WSi detector varies from 50 ps FWHM at low count rates, to about 350 ps at high rates.

We collect sorted time-tags and first consider adjacent pairs of SNSPD events as illustrated in Fig. 3.3 a. The time between the two photons that produced these event pairs is defined as t' , which is an integer number of laser periods ($t' = nt_l$). Second, we derive the delay between the second event and its corresponding laser pulse, defined as d . For each laser period spacing t' , we make a histogram of the second event delays and find the median (\tilde{d}) and the FWHM (Δd) of this distribution. For shorter separations t' , the distribution is expected to have larger delays and FWHM (Fig. 3.3 b) due to the smaller pulse height of the second event. Finally, we use the median delay as a function of laser spacing (Fig. 3.3 c) to form a curve \tilde{d} -vs- t' for the added time-walk versus inter-arrival time.

Fig. 3.4 a shows the \tilde{d} -vs- t' and Δd -vs- t' curves collected from our measurements of the WSi detector. The \tilde{d} -vs- t' curve is the main result of the calibration process and is used as a lookup table in the correction method. Δd is a measure of the more intrinsic jitter that the correction method cannot cancel out. While it is larger for small t' due to triggers on lower amplitude pulses, it notably stays at a nearly minimized value down to around $t' = 50$ ns. \tilde{d} grows more dramatically with decreasing t' , especially in the range from 50 to 100 ns. For count rates that do not exhibit many inter-pulse arrival times smaller than 50 ns, a method for removing the time-walk effect's contribution to jitter should bring entire system jitter back down to near the intrinsic limit implied by the Δd curve.

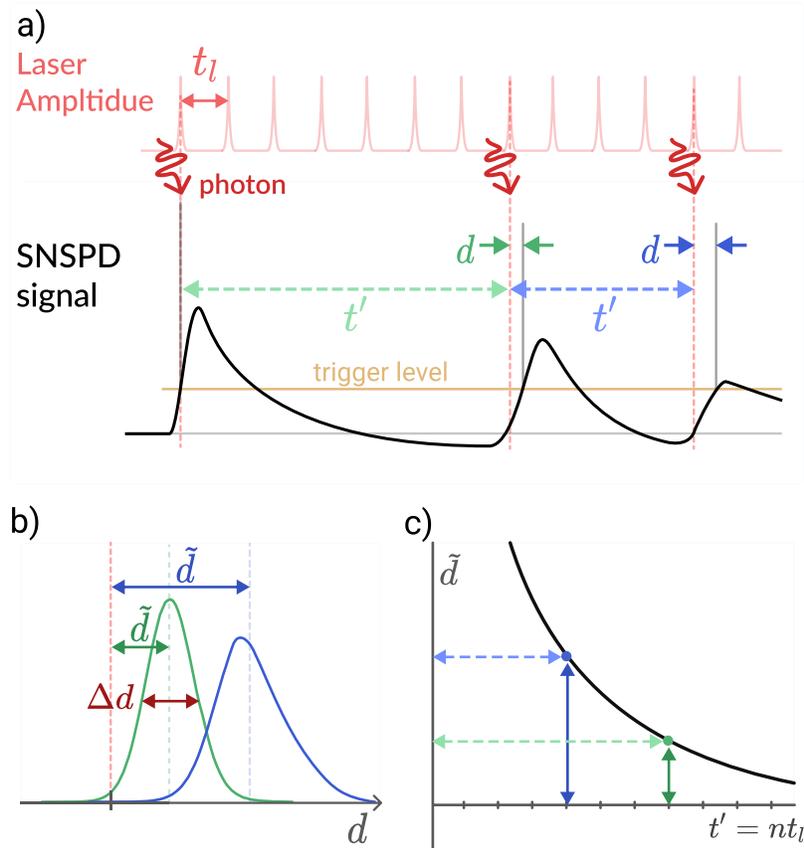


Figure 3.3: **Calibration Method** a) A qualitative diagram illustrating how inter-pulse timing measurements t' and d are extracted. A small fraction of laser pulses contain a photon due to the low mean photon number per pulse of the attenuated laser. Pairs of subsequent photon arrivals are separated by a time denoted by $t' = nt_l$. b) Possible distributions of delay d measurements for two different t' . The median of these defines the extracted delay parameters \tilde{d} which form the y-axis in the calibration curve illustrated in (c). The \tilde{d} vs t' curve in (c) approaches zero for t' approaching infinity. Blue and green arrows with matching color and style denote the same measure in (a), (b), and (c).

The correction method we implement involves subtracting off the distortion-induced delays a time-tag is expected to have based on the inter-pulse-time that precedes it. For each time tag t_n in a set, the inter-pulse time is $t_n - t_{n-1} = \Delta t$, where t_{n-1} is the previous tag on the same channel. Using Δt as an index, a corresponding delay correction \hat{d} is found by interpolating the \tilde{d} -vs- t' curve from the calibration. Given the density of points in the \tilde{d} -vs- t' acquired here, a linear interpolation is sufficient. The correction may benefit

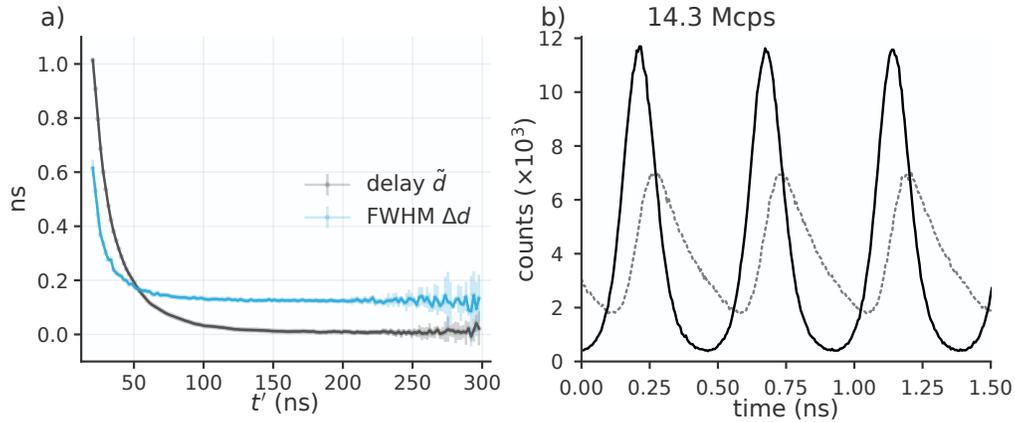


Figure 3.4: **t-prime curve and correction effect** (a) Delay and intrinsic jitter curves extracted from the 537.5 MHz pulsed light dataset. (b) Histogram of corrected (black) and uncorrected (dashed grey) time tags from a 2.15 GHz pulse train, corrected using a calibration curve developed with the 537.5 MHz dataset. The improvement affirms that the light modulation used for an application need not match the repetition rate of the calibration laser.

from higher order interpolation if the \tilde{d} -vs- t' curve is more sparse. This would be the case for calibrations built from a slower repetition rate pulsed light source. An assumption underlying the correction is that the interpolated value \hat{d} is a good estimator of the true delay added to the current time-tag due to high count rate pulse distortions.

With the interpolation operation expressed as a function D , the correction is written as $\bar{t}_n = t_n - D(\Delta t)$, where \bar{t}_n is the corrected version of tag t_n . Whether t_{n-1} is itself corrected or uncorrected has negligible influence on the t_n correction, as we assume $d \ll \Delta t$. The data correction shown here was applied in post-processing. But since D depends only on the current time tag and information available from earlier, the correction can be applied in real-time in an FPGA or computer used for time tagging.

The correction we perform using the \tilde{d} -vs- t' curve in Fig. 3.4 a is applicable to a wide range of count rates and arbitrary modulation patterns; there is no requirement that applications match the repetition rate of the calibration laser. Fig. 3.4 b shows that the correction method, derived from the 537.5 MHz calibration data, significantly reduces jitter when applied to detections from a 2.15 GHz pulse train. A similar jitter reduction can be demonstrated for repetition rates below 537.5 MHz.

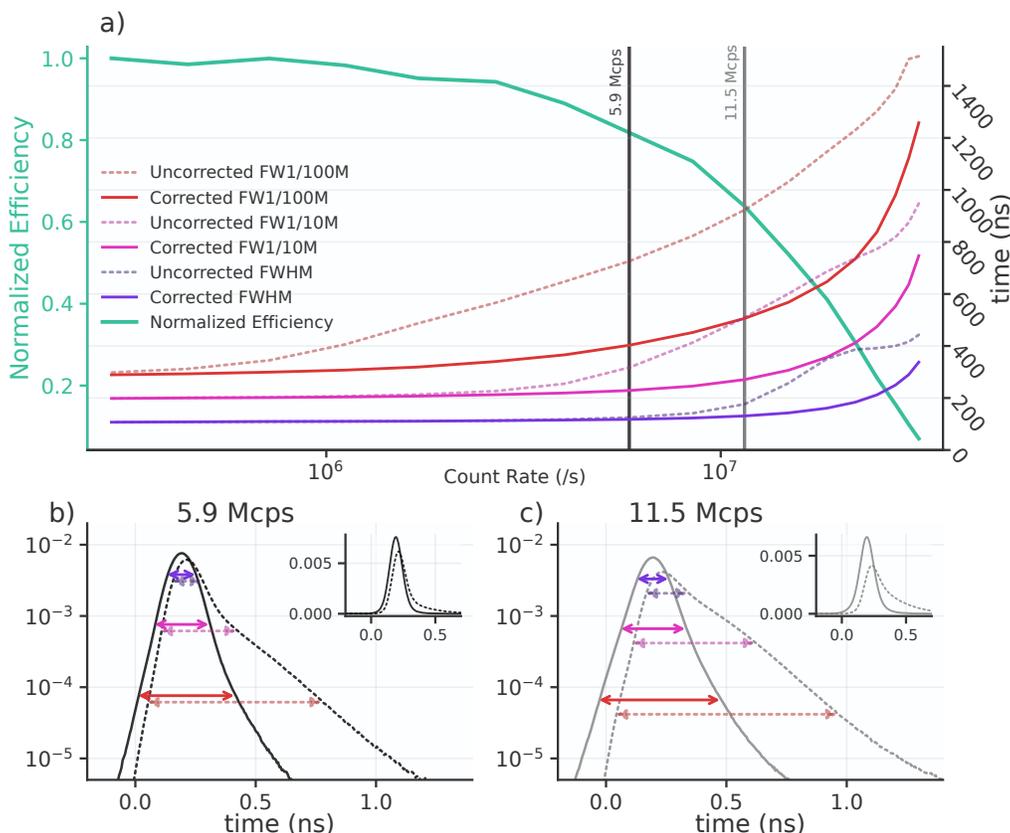


Figure 3.5: **Jitters metrics across incident powers** (a) Effect of the correction on measurements of system jitter over a range of rates approaching the maximum count rate. (b) Corrected (solid) and uncorrected (dashed) instrument response functions with color-matched arrows showing the location of the width-statistics plotted above in (a). The black vertical line in (a) is drawn at the count rate of this plot. Inset shows linear scaling. (c) Corrected (solid) and uncorrected (dashed) histogram analogous to (b), but at a higher count rate indicated by the grey line in (a).

To study the effectiveness of our correction method at different count rates, we apply it to data collected at different mean photon numbers per pulse, with the same 537.5 MHz pulse train. As shown in Fig. 3.5 c, the correction improves the FWHM at rates approaching the 3 dB point, and improves FW10%M and FW1%M (full width at ten percent/one percent maximum) dramatically, even at count rates significantly below the 3 dB point, where detector efficiency is nearly maximized. This reduction is evident in Fig. 3.5 c, where the correction works to remove a time-walk induced tail in the instrument response function. The ratio of corrected FW1%M over uncorrected FW1%M reaches a minimum of 0.55 at a count rate of 11.5 MCounts/s. Therefore if an application sets its repetition rate or bin size based on the FW1%M metric, the repetition rate can be increased and the bin

size decreased by up to 45% without any increase in event misattribution errors. These improvements are notable for applications including biomedical imaging [40], [41], quantum communication [25] and laser ranging [42] that have stringent timing requirements over a large dynamic range.

3.4 Higher order correction & the PEACOQ detector

The Performance Enhanced Array for Counting Optical Quanta (PEACOQ) is a new fiber-coupled SNSPD design that achieves high count rate by spreading the photon flux across a parallel array of short niobium nitride nanowires. Each wire may achieve count rates as high as 50 MCounts/s, so the 32-wire array as a whole can handle photon rates in excess of 1 GCounts/s. The PEACOQ is described in detail in Reference [6].

From early tests of the PEACOQ, it became evident that jitter increased dramatically at high single wire count rates. One of the overarching goals the the PEACOQ project was to demonstrate near-100 ps jitter at 1 GCount/s. Therefore, we investigated the possibility of applying time walk correction techniques to this detector. This began with collecting a calibration dataset like that discussed in section 3.3.

A 1-GHz repetition rate 1550 nm mode locked laser was used (Pritel UOC) for calibration. The 1 GHz repetition rate was chosen so that uncorrected jitter even at the highest count rates (approaching 400 ps at the FW1%M), was smaller than the laser period. Then, each time tag may be matched to the timing of the original optical pulse. A dataset with a count rate of 20 MCounts/s was used for calibration. At this rate, there is a good balance of statistics available for t' ranging between 5 and 150 ns.

The calibration process for the PEACOQ showed that high-rate pulse distortions are primarily due to amplifier effects and the overlap of RF pulses with the overshoot or ringing effects of previous RF pulses. This occurs because the PEACOQ was designed and fabricated to minimize the intrinsic reset time of the nanowire. The time it takes for bias current to re-saturate in the device is generally faster than the time for all amplifier effects to disappear following a previous RF pulse. Fig. 3.6 b is the delay vs. t' curve derived from the calibration process. Unlike the in Fig. 3.4, the delay vs. t' curve for the PEACOQ shows features that are closely related to the falling edge of the RF pulse (Fig. 3.6 a). In particular, the calibration

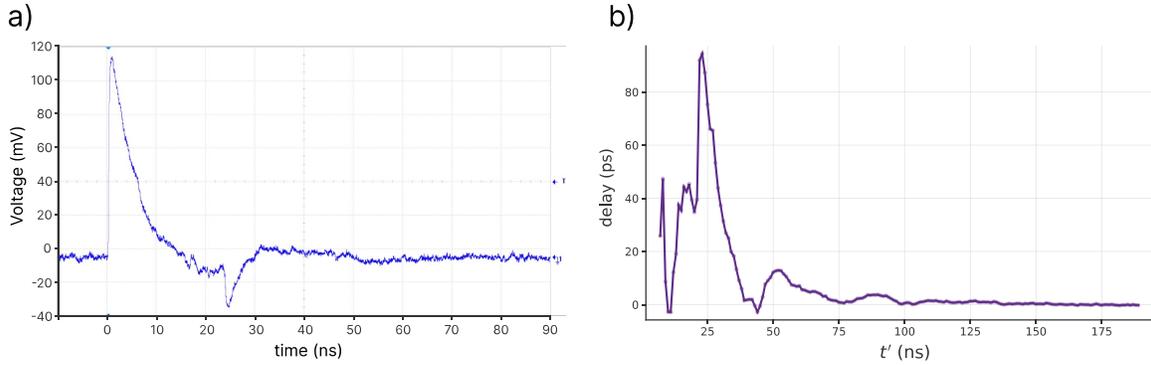


Figure 3.6: **PEACOQ RF pulse and calibration curve** a) The RF pulse of one of the PEACOQ nanowires. The effect of an impedance mismatch reflection is visible at 25 ns. b) The delay vs t' curve for wire 1 of the PEACOQ. The peak at 25 ns lines up in time with the RF reflection visible in (a), and works to correct for the time-walk delays it causes.

curve shows a peak near 25 ns that aligns with an undershoot in the RF waveform caused by a reflection off a cryogenic amplifier. Future implementations of the PEACOQ will optimize the amplification chain to minimize RF reflections. Though even with such optimizations, it is likely that time-walk correction will improve high rate jitter.

As before with the meandered SNSPD, there is no requirement that the calibration only be used in an application that is based on the same repetition rate of 1 Ghz. As interpolation between points on the delay vs. t' vs lookup curve is possible, delay corrections for arbitrary t' measurements may be found.

Second order calibration

The 2nd order time-walk correction is a new technique that builds on the methods previously introduced in this chapter. The intrinsic reset time of the PEACOQ nanowires is considerably shorter than the time it takes an RF pulse to return to a steady zero voltage. So multiple pulses can arrive in the time it takes one RF pulse to fully decay as seen by the timing electronics. Therefore, a given RF pulse can be level shifted not only by the presence of one pulse before, but even two or three before. The calibration and correction process was extended to correct a given pulse timing measurement based on two inter-pulse time measurements t' and t'' as shown in Fig. 3.7 a. The calibration process uses the same mode-locked laser derived pulse train as the 1st order calibration. For each t' there is a full

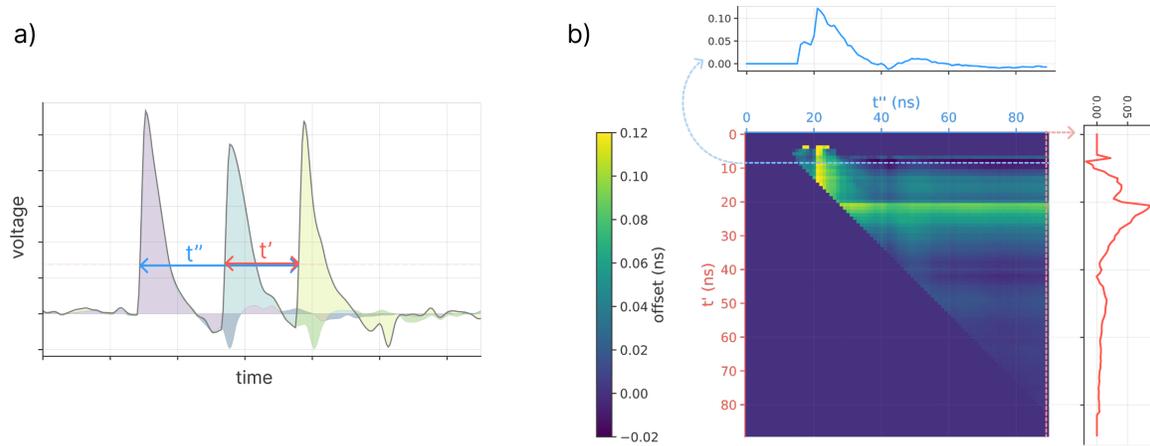


Figure 3.7: **PEACQ 2D calibration parameterization & results** a) A diagram showing how RF pulse waveforms can interfere additively, and how t' and t'' are parameterized. For illustrative purposes only. b) The result of 2nd order calibration, a grid of delay measurements indexed by t' and t'' . The blue/red slices and corresponding graphs show how the effect of varying t'' for a given t' is similar to varying t' for a given t'' .

range of possible t'' times and vice versa, so the result of calibration becomes a 2D grid of delay corrections indexed by t' and t'' . t' is always less than t'' for the parameterization chosen, where both are measured from the latest or 'current' time tag (Fig. 3.7 a). Therefore, the space of valid measurements is triangular as shown in Fig. 3.7 b.

Predominant features of the 2d calibration grid seem to be orthogonal and aligned to the axes. This is a result of the parametrization chosen for t' and t'' . Features of the calibration that arise due to additive mixing of overlapped RF pulse waveforms manifest as orthogonal structures in the 2d-calibration grid.

In the limit of large t'' , a slice of the calibration grid bears close resemblance to the t' vs delay curve used for 1D calibration and correction (Fig. 3.6 b). Like in the 1D correction method, a delay correction can be found during real-time acquisition and processing by interpolating on a lookup table. Only now, the lookup table has an extra dependent variable t'' , and the interpolation is two dimensional.

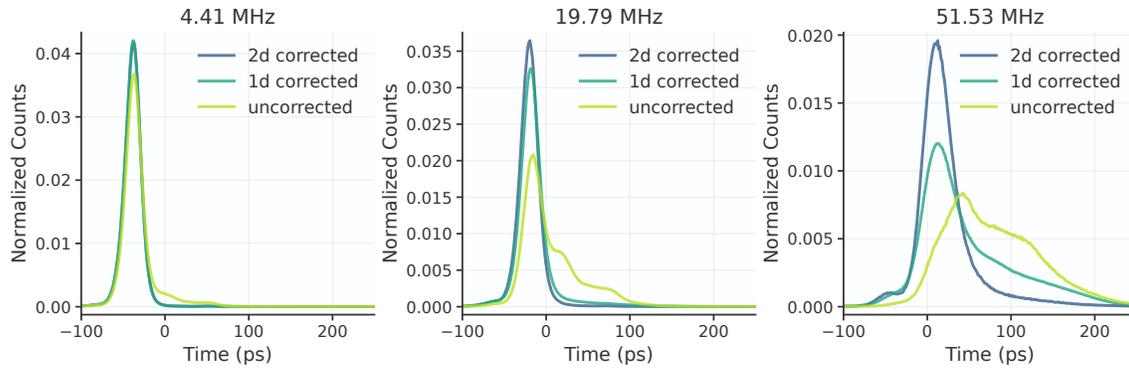


Figure 3.8: **PEACOQ single wire time-walk correction** jitter response functions for 3 count rates from one wire of the PEACOQ detector.

Proper handling of inter-pulse arrival measurements that fall outside the 2D grid is necessary for good correction performance. When both t' and t'' fall outside the 2D grid, no correction is applied. When t'' falls outside the grid but t' does not, a 1st order correction is applied to determine what delay must be subtracted to the current tag to correct its distortion. When both t'' and t' fall within the 2d grid, a full 2d spline interpolation on the grid in Fig. 3.7 b is applied to find the necessary delay correction.

Like the 1st-order correction, the 2nd-order method makes the assumption that the delays to be corrected are small relative to the inter-pulse times t' and t'' .

Fig. 3.8 shows how the 1st and 2nd order corrections improve jitter of the one wire of the PEACOQ detector tested. Each of these response functions have full width at half maximum (FWHM), full width at one tenth maximum (FW1/10M) and full width at one hundredth maximum (FW1/100M) metrics. The FW1/100M width is relevant for quantum communication applications that design the fundamental experiment repetition rate or bin size based on this metric. We plot how these metrics scale with count rate for the single nanowire as shown in Fig. 3.9.

With data available over a wide range of single-wire count rates, and the correction method, we simulate the performance of the whole PEACOQ detector with time walk correction. This is based on matching count rate measurements (Fig. 3.10) from the full array to count rates available in the single-wire dataset used for calibration and correction. The full-array rate measurements are from another cryostat and time tagger setup that supports full-readout of the PEACOQ

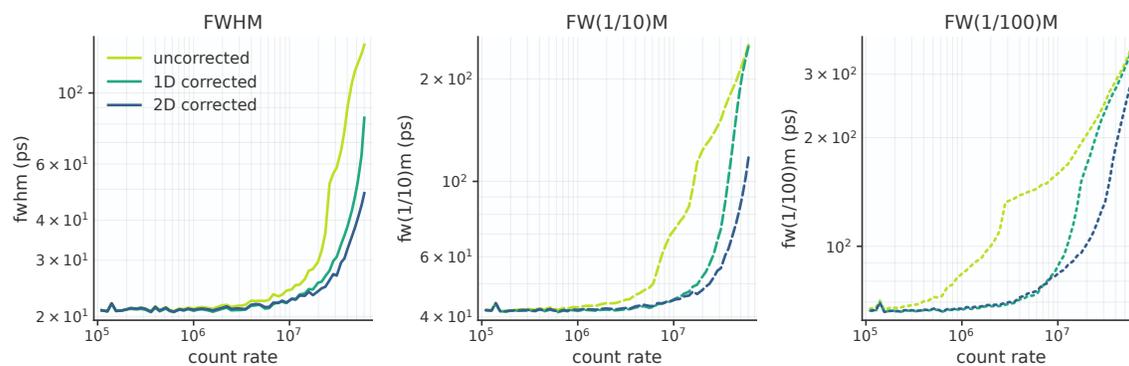


Figure 3.9: **PEACQ single wire width metrics** Width metrics versus count rate. The FW1/100M metric benefits greatly from both the 1st and 2nd order time-walk correction. Only when count rate is sufficiently high and pulses are very close together does it become more likely that any one pulse can be corrupted by its previous-previous pulse.

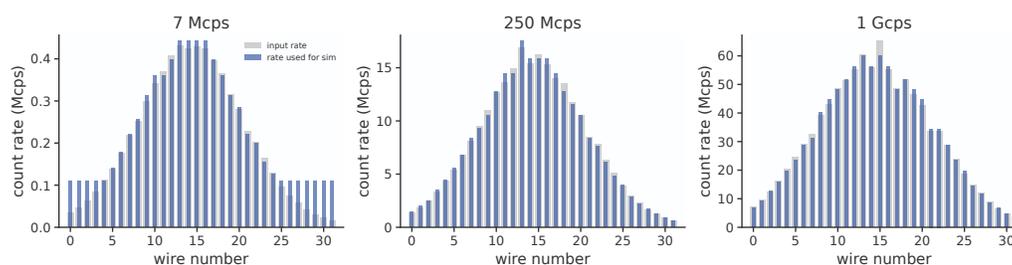


Figure 3.10: **Matching PEACQ wire count rates to calibration dataset** Blue bars represent count rates of data files for which the time-walk correction can be performed. Grey bars represent unique wire count rates from an integrated full-array measurement of the PEACQ in another experiment setup. The count rates have a Gaussian shape with respect to wire number as the coupled optical fiber has a lateral intensity profile that is roughly Gaussian.

Fig. 3.11 a shows simulated full-array jitter response functions for 3 choice count rates, normalized from their peaks. The FWHM, FW1/10M, and FW1/100M width metrics are indicated with continuous, dashed, and dotted lines, respectively.

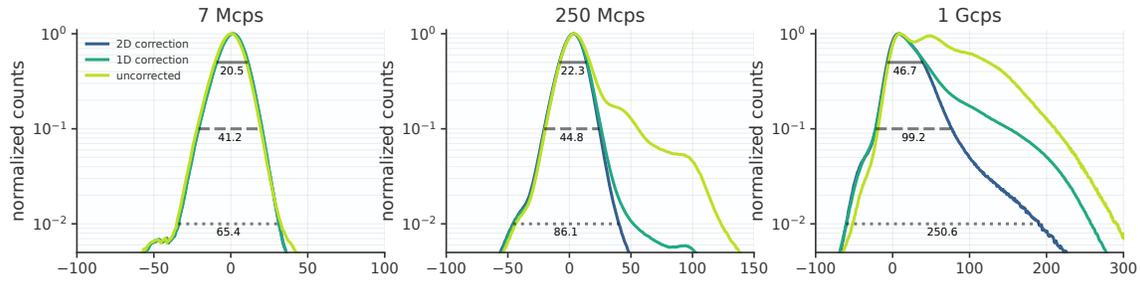


Figure 3.11: **Simulated full PEACIQ array jitter performance with time-walk correction** Each simulated jitter histogram (2D corrected, 1D corrected, or uncorrected) is a weighted sum of 32 response functions for the 32 wires, each with count rate representative of a certain wire in the array (Fig. 3.10).

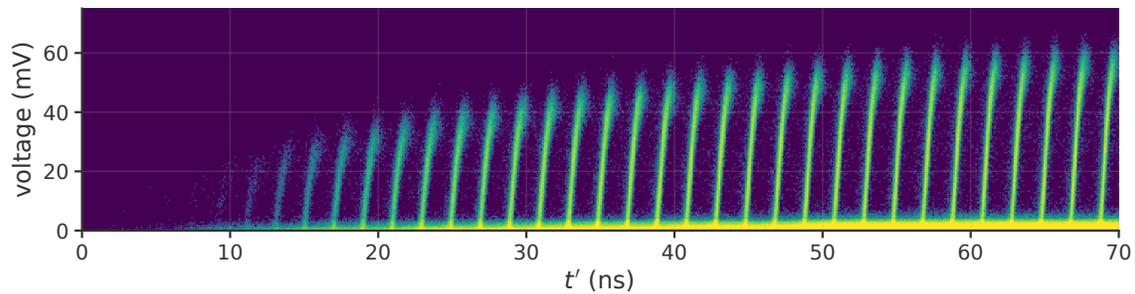


Figure 3.12: **WSi detector pulse recovery** Sweep of trigger levels for pulse rising edges after a previous pulse (not shown). This is similar to a scope trace in overlay false color mode. The detector is illuminated by a 537.5 MHz pulse train.

Performance regime of the tungsten silicide detector

When our calibration and correction method is applied to the Tungsten Silicide SNSPD, the walk-cancellation method primarily corrects for pulse height variations. These variations are caused by varying levels of bias current in the device at the time of photo-detection. An oscilloscope trace shows an exponentially decaying increase in SNSPD pulse height following a previous detection. This exponential recovery shape reinforces evidence that this detector operates in this ‘bias current recovery’ regime, rather than the regime where amplifier reset dynamics dominate.

Software dead time for high count rate jitter suppression

In certain cases a software-based dead time is an effective way of reducing jitter at high count rates. SNSPD pulses that arrive soon after a previous pulse are ignored because their timing is assumed to be corrupted due to pulse distortions (Fig. 3.13a). With a long software-based dead time, data is filtered to keep only events for which the SNSPD was in a fully reset state prior to detection. This results in low jitter measurements even at high rate as shown in Fig. 3.13d where the dashed and solid (red, orange) lines are response functions of unfiltered and filtered data, respectively. However, the use of software-based dead times can severely limit usable count rate. This paradoxically contrasts with the main intended goal, which is to operate an SNSPD at the highest possible count rates. As shown in the Fig. 3b, adding a 100 ns software dead time to our WSi single pixel SNSPD limits its usable maximum count rate to about 4 MHz, while the raw count rate exceeds 10 MHz. Furthermore, the usable count rate drops to zero for higher incident photon rates, as the dead time starts to reject most events. This behavior can be unexpected and problematic for any applications that occasionally over-saturate the detector.

3.5 Conclusion & outlook

The original research paper on time walk analysis [43] included comments on the potential for time walk correction in situations where the reset time of the nanowire is considerably shorter than the reset dynamics of the amplifier chain:

To optimally correct for this, higher-order correction techniques are needed based on higher-dimensional lookup tables. There is an avenue for exploring such methods for unique use-cases. [43]

This potential for higher order correction methods turned out to be fruitful, which is why the prior section about **higher order correction** adapted from the PEACOQ paper [6] is included. The original paper went on to claim that there are avenues for exploring time walk correction for pulses measured at multiple voltage levels, or even fully digitized pulses captured with high speed ADCs and FPGAs. These more rigorous readout techniques may be needed to deconvolve photon timing and Photon Number Resolution (PNR) effects

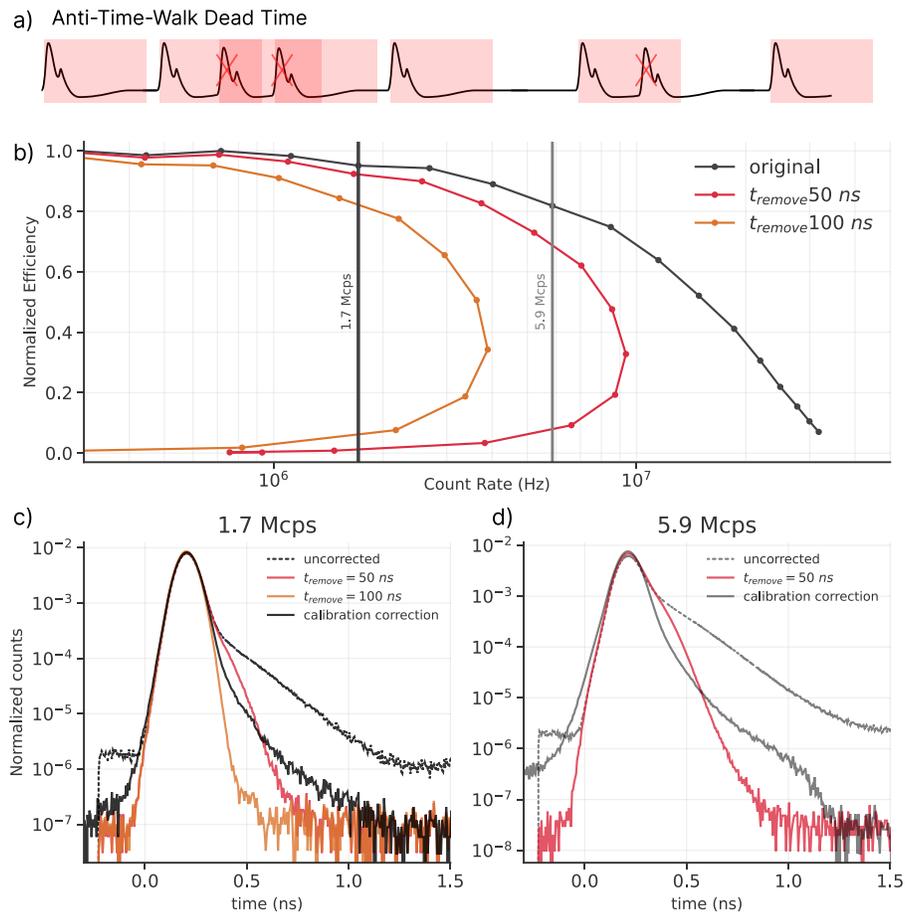


Figure 3.13: **Removing time walk with dead time** a) Illustration of the RF signal out of an SNSPD with red highlighted regions signifying a software-based dead time that rejects some events. b) Count rate vs normalized efficiency, similar to the curve in green in Fig. 3.5. (c) & (d) Response functions for timetaggs at two count rates denoted by the vertical lines in (b), similar to Fig. 3.5 (b) and (c). The dark grey solid lines show response functions from the calibration and correction method which does not limit count rate. The 100 ns dead time filtered data does not reach the 5.9 Mcps of figure (d) and is therefore not shown in (d).

from the same nanowire at high count rates [44]. While drafting this thesis, methods for simultaneous time walk correction and PNR correction have not been demonstrated in the literature. However, I believe there is imminent potential to extend the Gaussian mixture model methods introduced in the next section for these purposes.

There are other types of extensions and modifications to the presented time walk correction method that may prove to be useful. However, the single- Δt measurement approach primarily detailed in this chapter is broadly applicable and straightforward to implement. For insight into developing a streamlined calibration process and in-situ time walk correction as part of larger quantum communication experiments, see the section 5.12.

As applications like LIDAR and quantum communication demand ever higher data rates, multiple techniques for increasing photon and data throughput of SNSPD systems are being explored. Arrays or multi-channel SNSPD systems will play a role in satisfying that demand. However, compared to multiple lower count rate SNSPDs operating in parallel, a single detector operating at high rate has certain advantages. First, it makes more efficient use of the extensive bandwidth of the RF readout channel. Second, the single detector with single readout line puts less thermal load on the cooling system than multiple detectors with multiple readout lines. Therefore, paths toward operating individual SNSPDs at the limits of their count rate performance should be explored before extending to multi-pixel systems. This work is a step towards unlocking all available performance and timing precision of SNSPDs operated at high count rates.

*Chapter 4*DATA RECOVERY AND PULSE POSITION MODULATION WITH A PHOTON
NUMBER RESOLVING SNSPD

This chapter is temporarily redacted until the corresponding publication is submitted to a journal.

Chapter 5

HIGH RATE ENTANGLEMENT GENERATION

A version of this chapter is currently under review. A preprint is released as:

A. Mueller, S. Davis, B. Korzh, et al., High-rate multiplexed entanglement source based on time-bin qubits for advanced quantum networks, 2023. arXiv: 2310.01804 [quant-ph].

5.1 Abstract

Entanglement distribution based on time-bin qubits is an attractive option for emerging quantum networks. We demonstrate a 4.09 GHz repetition rate source of photon pairs entangled across early and late time bins separated by 80 ps. Simultaneous high rates and high visibilities are achieved through frequency multiplexing the spontaneous parametric down conversion output into 8 time-bin entangled channel pairs. We demonstrate entanglement visibilities as high as 99.4%, total entanglement rates up to 3.55×10^6 coincidences/s, and predict a straightforward path towards achieving up to an order of magnitude improvement in rates without compromising visibility. Finally, we resolve the density matrices of the entangled states for each multiplexed channel and express distillable entanglement rates in ebit/s, thereby quantifying the tradeoff between visibility and coincidence rates that contributes to useful entanglement distribution. This source is a fundamental building block for high-rate entanglement-based quantum key distribution systems or advanced quantum networks.

5.2 Introduction

Entangled photons play a vital role in the development of quantum information processing and communication systems [45]–[50]. The ability to generate entangled photon pairs at a high rate is essential for establishing reliable and scalable quantum networks with quantum repeaters, as well as for implementing entanglement-based quantum key distribution (QKD) systems [51]–[54]. Unlike QKD implementations that rely on attenuated lasers [55], [56] entanglement distribution systems may fulfill the objectives of QKD while also serving as the foundation for advanced quantum networks that rely on entanglement as a fundamental resource.

Entanglement distribution and entanglement-based QKD have been demonstrated with impressive performance across a number of metrics. These include 40 kbps data rates in a QKD system deployed over 50 km of fiber [57] as well as multiple polarization entangled sources that leverage spectral multiplexing. These polarization sources include a demonstration of 181 kebits/s across 150 ITU channel pairs and a high-throughput source potentially capable of gigabit rates with many added channels and detectors [58], [59]. Multiple works have highlighted the need to leverage high total brightness, spectral brightness, collection efficiency, and visibility from pair-generating non-linear crystals to realize practical high-rate entanglement distribution [59]–[65].

A time-bin entangled photon source has certain advantages over a polarization-based system [66]. Time-bin entanglement can be measured with no moving hardware and does not require precise polarization tracking to maximize visibility [67], [68]. Also, with suitable equipment, robust time-bin modulation is possible over free space links with turbulence [69]. Therefore, the possibility of simplified fiber-to-free-space interconnects and larger quantum networks based on a shared time-bin protocol motivates development of improved time-bin sources. Furthermore, time-bin encoding is suited for single-polarization light-matter interfaces [70], [71].

We direct 4.09 GHz mode locked laser light into a nonlinear crystal via 80-ps delay-line interferometers (12.5 GHz free-spectral range) to realize a high-rate entanglement source. The ability to resolve time-bin qubits into 80 ps wide bins is enabled by newly developed low-jitter differential superconducting nanowire single-photon detectors (SNSPDs) [5]. Wavelength multiplexing is used to realize multiple high visibility channel pairings which together sum to a high coincidence rate. Each of the pairings can be considered an independent carrier of photonic entanglement [72], [73] and therefore the system as a whole is applicable to flex-grid architectures through the use of wavelength selective switching [74], [75]. However, we focus on maximizing the rate between two receiving stations, Alice and Bob (Fig. 5.1a). Each station is equipped with a DWDM that separates the frequency multiplexed channel into multiple fibers for detection. The SNSPDs are used with a real-time pulse pileup and time-walk correction technique [43] to keep jitter low even at high count rates.

We quantify per-channel brightness and visibility as a function of pump power, as well as collection efficiencies, coincidence rates across 8 channel pairs, and expected performance of a partially realized 16-channel pair configuration. We show that the 8 channel system achieves visibilities that average to 99.3% at low mean photon number $\mu_L = 5.6 \times 10^{-5} \pm 9 \times 10^{-6}$. At a higher power ($\mu_H = 5.0 \times 10^{-3} \pm 3 \times 10^{-4}$), we demonstrate a total coincidence rate of 3.55 MHz with visibilities that average to 96.6%. Through quantum state tomography we bound the distillable entanglement rate of the system to between 69% and 91% of the μ_H coincidence rate (2.46 - 3.25 Mebits/s).

Quantifying a source's spectral mode purity is important for gauging its utility in advanced quantum networks that rely on interferometric measurements like two-photon interference which enables Bell-state measurements (BSM) [22]. With Schmidt decomposition we quantify the modal purity of single DWDM channel pairs and derive the inverse Schmidt number which serves as an estimate for two-photon interference visibility between two such sources. Ultimately, we demonstrate that an entanglement generation source of this design makes for a robust and powerful building block for future high-rate quantum networks.

5.3 System

Fig. 5.1 shows the experimental setup. Pulses from the 4.09 GHz mode-locked laser, with a center wavelength at 1539.47 nm, are sent through an 80 ps delay-line interferometer (Optoplex). This generates the pulses used to encode early/late basis states ($|e\rangle, |l\rangle$), which are subsequently up-converted by a second harmonic generation (SHG) module (Pritel) and down-converted into entangled photon pairs by a type-0 spontaneous parametric down conversion (SPDC) crystal (Covesion) [76]. The up-converted pulses at 769 nm have a FWHM bandwidth of 243 GHz (0.48 nm), which along with the phase matching condition of the SPDC waveguide, defines a wide joint spectral intensity (JSI) function [77].

The photon pairs, which are separated by a coarse wavelength division multiplexer (CWDM), are of the form $|\psi\rangle = \frac{1}{\sqrt{2}} (|e\rangle_s |e\rangle_i + e^{i\phi} |l\rangle_s |l\rangle_i)$. Entangled idler and signal photons are sent to the receiving stations labeled Alice and Bob, respectively. One readout interferometer at each station projects all spectral bands into a composite time-phase basis. From here, dense wavelength division multiplexers (DWDM) divide up the energy-time entangled photon pairs into spectral channels.

DWDM outputs are sent to differential niobium nitride (NbN) single pixel SNSPDs [5] with $22 \times 15 \mu\text{m}$ active areas formed by meanders of 100-nm-wide and 5-nm-thick niobium nitride (NbN) nanowires on a 500 nm pitch. These measure the arrival time of photons with respect to a clock signal derived from the mode locked laser. Use of the high system repetition rate and compact 80 ps delay interferometers is only possible due to the high timing resolution of these detectors. Low jitter performance is achieved by incorporating impedance matching tapers for efficient RF coupling, resulting in higher slew rate pulses, and by enabling RF pulse readout from both ends of the nanowire. The dual-ended readout allows for the cancellation of jitter caused by the variable location of photon arrival along the meander when the differential signals are recombined with a balun. We use two SNSPDs for this demonstration with efficiencies at 1550 nm of 66% and 74%. A full 8-channel implementation of this system would require 16 detectors operating in parallel at both Alice and Bob. To read out both outputs of both interferometers, 4 detectors per channel are required, resulting in 32 detectors total.

A novel time-walk or pulse-pileup correction technique is used to extract accurate measurements of SNSPD pulses that arrive between 23 and 200 ns after a previous detection on the same RF channel. Without special handling of these events, timing jitter will suffer due to RF pulse amplitude variations and pileup effects. As detailed in section 5.12, the correction method works by subtracting off predictable timing distortions based on the inter-arrival time that precedes them [6], [43]. An in-situ calibration process is used to build a lookup table that relates corrections and inter-arrival time. At the highest achievable pump power, this correction method leads to 320% higher coincidence rates compared to a data filtering method that rejects all distorted events arriving within $\simeq 200$ ns of a previous pulse.

5.4 Results

By pairing up particular 100 GHz DWDM channels and recording coincidence rates, a discretized form of the JSI of our pair source is measured (Fig. 5.2 a). Due to the wide pump bandwidth, the spectrum of signal photons spans several ITU channels for a given idler photon wavelength. Pairs along the main diagonal are optimized for maximum coincidence

rates by tuning the pump laser frequency, and are therefore used for all remaining measurements. In Fig. 5.1 b, these pairs are highlighted with matching colors. Coupling efficiencies η shown in Fig. 5.2 a are derived from a JSI fitting analysis in 5.8 and include all losses between the generation of entangled pairs in the SPDC and final photo-detection.

A joint spectral analysis of the 100 GHz filters applied to the wide-bandwidth pumped JSI shows only a fraction of idler (signal) photons that pass through one filter will be detected with their corresponding signal (idler) photon. This is true even for ideal filters that are 100% transmissive within their passbands, which demonstrates a geometrical limit on the ratio of coincidence rates to singles rates in this regime of large bandwidth JSI and narrowband filters. For calculations of μ in terms of the coincidence rate C_{AB} , repetition rate R , and singles rates S_A, S_B , we account for this by adding a geometric compensation factor δ to the commonly used equation:

$$\mu = \frac{\delta S_A S_B}{R C_{AB}}. \quad (5.1)$$

This gives a definition of μ for the JSI region where signal and idler filters overlap according to energy conservation, and the probability of transmitting entangled pairs to both Alice and Bob is not negligible. It is valid in the low μ regime where generation of higher order photon number states from the SPDC are rare. For filter pairings along the main diagonal in Fig. 5.2 a, values for δ are fairly consistent and average to $\delta = 0.393 \pm 0.012$. The derivation of δ is detailed in section 5.9.

In the following, rigorous tests of entanglement are primarily conducted with the 8 ITU 100 GHz channel pairings: Ch. 35-42 at Alice and Ch. 52-49 at Bob. However, in Fig. 5.2 b we investigate rates across 16 pairs by using all 16 channels available on the DWDM at Alice (24 — 34) and a tunable narrowband filter in place of the DWDM at Bob. As the narrowband filter has higher loss and 45 GHz FWHM passband (see section 5.13 for measurements), the coincidence rates are lower (grey bars in Fig. 5.2 b). However the uniformity of coincidence rates across 16 channels implies that the use of 16-channel DWDMs at both Alice and Bob would roughly double the total coincidence rate.

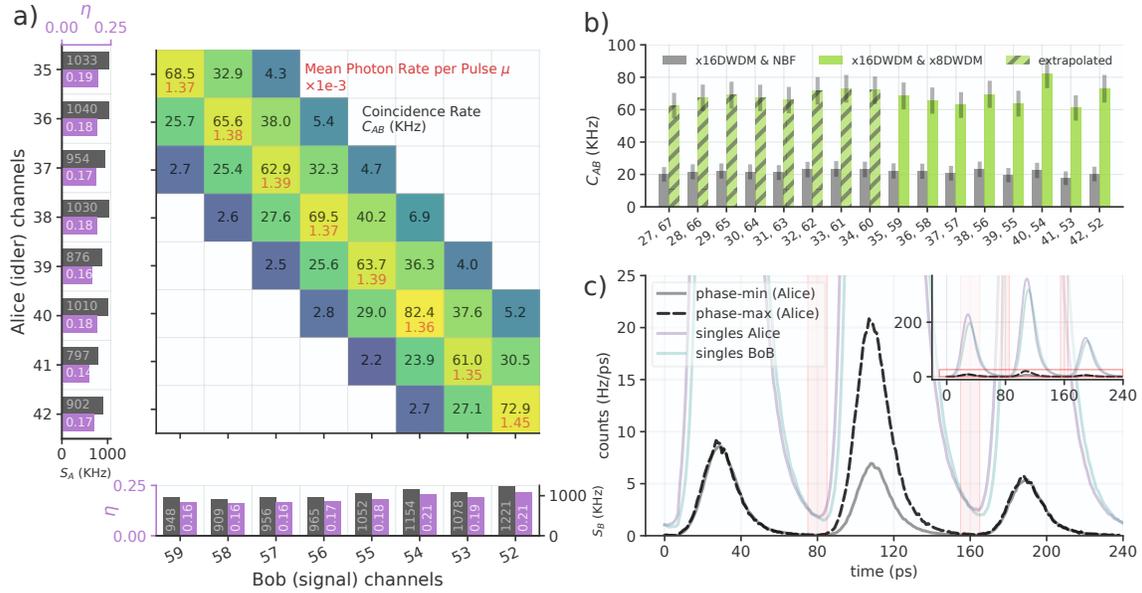


Figure 5.2: Joint spectral intensity measurements and histogram a) The singles rates at Alice S_A and Bob S_B (grey bars), path coupling efficiencies (purple bars), and coincidence rates C_{AB} (black text in colored boxes) for different DWDM channel pairings. All measurements are recorded at a SHG pump power of 14.6 mW, for which μ of the channel pairs along the main diagonal are shown in red text. The joint spectral intensity envelop spans several 100 GHz channels. As detailed in section 5.7, the coincidence rates (kHz, black) are scaled to represent two branches of the total wavefunction, so that they are consistent with the coupling efficiencies η (purple bars) and the singles rates (grey bars). There are four branches for each pairing of the four interferometer output ports. In practice, one output each of Alice and Bob’s interferometers is measured, thereby capturing one branch. See section 5.8 for details on the fitting method used to solve for the coupling efficiencies η . b) Coincidence rates for energy-matched channel pairings. The light green bars depict the main diagonal in (a). Grey bars are measured with x16 DWDM at Alice and a tunable narrowband filter at Bob. Dashed bars predict the rates for a system with x16 DWDMs at both Alice and Bob c) Histogram of photon arrival events with respect to the 4.09 GHz clock. Dashed black and grey lines show the response functions for coincidence events. Red bars represent guard regions where coincidence events are ignored. Events within 10 ps guard regions centered at 80 and 160 ps (shaded red) are discarded for analysis of coincidences between individual bins. This is done to maximize visibility in the presence of some minor overlap of pulses (see section 5.14 for details).

Signals from the SNSPDs are directed to a free-running time tagger (Swabian) and processed with custom software. The resulting histograms, referenced from a shared clock (Fig. 5.2 c), depict three peaks, which are caused by the sequential delays of the source and readout interferometers. Some intensity imbalance between long and short paths is present in these interferometers, which explains the asymmetry between early and late peaks in Fig. 5.2 c. Such imbalances are present in both the source and readout interferometers to varying degrees. The interferometer used for the source exhibits an early/late intensity balance ratio of 1.13. Alice and Bob's interferometers exhibit early/late imbalances of 1.24 and 1.15, respectively. An analysis of how this type of imbalance affects entanglement visibility is included in the interferometer imbalance section, available in the supplemental of the [published manuscript](#).

The coincidence rate across Alice and Bob's middle bins varies sinusoidally with respect to the combined phase relationship of the source and readout interferometers (see section 5.10.) [76], [78]. In Fig. 5.2 c, the coincidences shown are for any combination of early, middle, or late bins. For tomography and visibility measurements, coincidence detections across specific bin pairings are considered.

Due to the small size and temperature insensitivity of the interferometers, minimal temporal phase drift is observed over multiple hours. Nevertheless, software is used to lock the phase at a minimum or maximum with a simple hill-climbing algorithm. This varies the phase by small amounts over several minutes to search for, or maintain, an extremum.

Channels 35 and 59 are chosen for an analysis of entanglement visibility and rates versus pump power. Visibility, with respect to pump power or mean entangled pair rate, is shown in Fig. 5.3 a. We define the entanglement visibility as $V = 100\% * (C_{max} - C_{min}) / (C_{max} + C_{min})$ where C_{min} and C_{max} are the minimum and maximum coincidence rates in the middle bin for varied phase. As this coincidence rate depends on the total phase across the source and readout interferometers, only Bob's interferometer is actively controlled to scan the full state space.

The raw visibility versus μ is shown in blue in Fig. 5.3 a. Relative to similar measurements [79], this drops quickly with increasing μ , and one reason is the presence of accidental coincidences across mutually incompatible spectral modes. The presence of these unwanted coincidences is a consequence of the narrowband filtering regime, and depends on factors

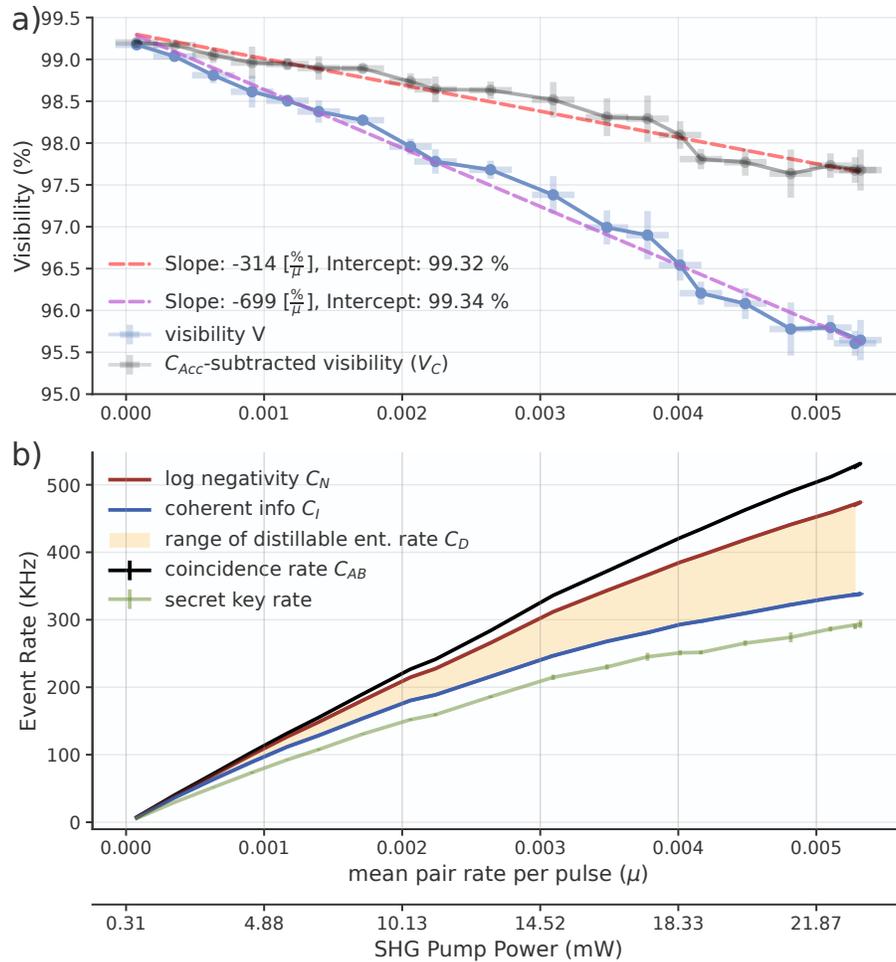


Figure 5.3: **Entanglement visibility and rates vs pump power** a) Visibility versus pump power. Error bars are calculated by taking multiple measurements of the center bin coincidence rate over some integration time. These measurements span small ranges of interferometer phase, as the extremum-finding algorithm jitters the interferometer voltage. b) Bounded distillable entanglement rate versus pump power. Multiple such measurements are made for all the tomographic measurements. These are used to calculate standard deviations for visibility, log negativity, and coherent information. Error bars for the log negativity and coherent information are smaller than the line width shown. Rates shown assume readout of all 4 available interferometer ports, based on data measured using one port each at Alice and Bob.

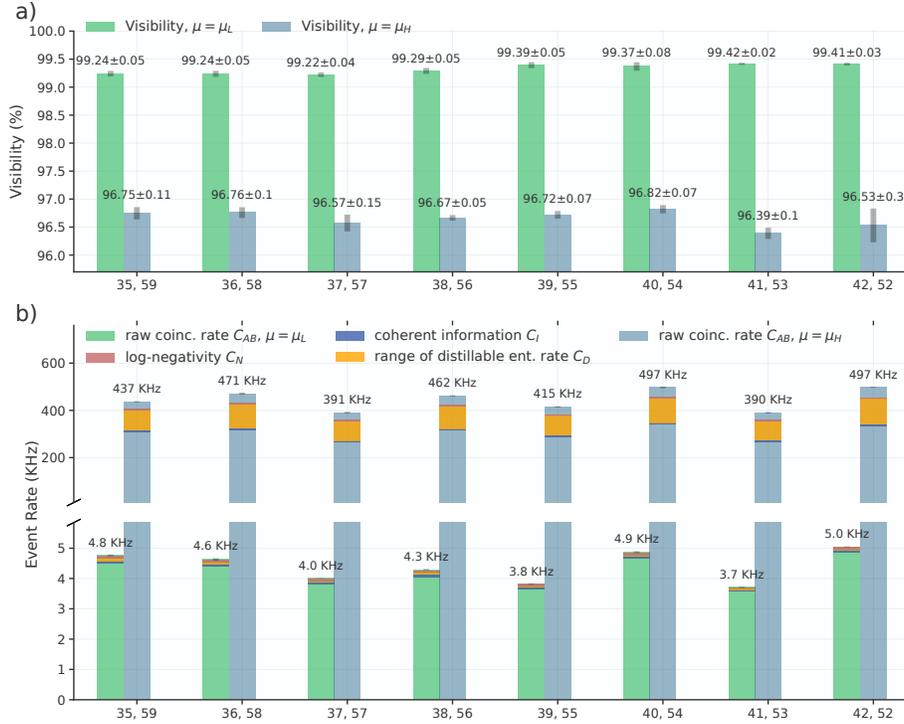


Figure 5.4: **Visibilities and rates for 8 channel pairs** a) Visibility for the main 8 channel pairs, measured at a high (22.9 mW) and a low (0.21 mW) SHG pump power setting. Each power setting results in similar μ for all channels: $\mu_L = 5.6 \times 10^{-5} \pm 9 \times 10^{-6}$ and $\mu_H = 5.0 \times 10^{-3} \pm 3 \times 10^{-4}$. b) Rate metrics for the 8 channel pairs at the same high and low power settings. The range of possible values for distillable entanglement rate is spanned by the yellow regions, bounded above by log-negativity and below by coherent information. Rates shown assume readout of all 4 available interferometer ports, based on data measured using one port each at Alice and Bob

included the singles rates S_A and S_B , and the geometric compensation factor δ (see section 5.15 for derivation). We model this type of accidental coincidence rate C_{Acc} versus μ , and subtract it off from coincidence measurements to produce the grey data in Fig. 5.3 a. This simulated visibility's more gradual drop with an increasing μ highlights the detrimental effect of our high single-to-coincidence rates S_A/C_{AB} , S_B/C_{AB} . As detailed in the discussion section the follows, this motivates special source engineering techniques for future systems.

We quantify the rate of useful entanglement by supplying bounds for the distillable entanglement rate C_D . Measured in ebits/s, C_D is the maximal asymptotic rate of Bell-pair production per coincidence using only local operations and classical communications [58], [80]. It is bounded above by log-negativity $C_N = C_{AB}E_N$ and below by coherent information $C_I = C_{AB}E_I$ [58]. For each pump power setting in Fig. 5.3, a series of tomographic measurements is performed and density matrices are calculated. The values of E_I and E_N are calculated from the density matrices as detailed in section 5.10.

Fig. 5.4 shows visibilities, raw coincidence rates, and bounded distillable entanglement rates for two pump powers and all 8 channel pairings. The highest pump power is currently limited by our EDFA-amplified SHG module. The pump power in principle could be increased until the SNSPD efficiency drops due to saturation, and the net coincidence rate plateaus. Without the time-walk correction, high-rate jitter becomes an issue well before the gradual drop of SNSPD efficiency. At the μ_H (22.9 mW) power, the singles rates S_A, S_B average to 3.84 MHz, for which SNSPD efficiencies are about 78% of nominal.

Using the data in Fig. 5.2 a, we model the JSI for our pair source as a product of pump envelope and phase matching condition functions

$$|f(\omega_s, \omega_i)|^2 = |\psi_{\text{ph}}(\omega_s, \omega_i)|^2 * |\psi_p(\omega_s, \omega_i)|^2,$$

which depends on the wavelength (769.78 nm) and bandwidth (243 GHz FWHM) of up-converted light out of the SHG, measured with a spectrum analyzer. The path efficiencies from SPDC to detectors are also fitted based on integrations over the JSI that model the DWDM transmission passbands (see section 5.8 for details).

We calculate the Schmidt decomposition of the pair source JSI, taking into account the DWDM filters at Alice and Bob, and derive an average inverse Schmidt number $1/K$ of 0.87. This value quantifies the spectral purity of the entangled photon source, and is theoretically equivalent to the visibility of a two-source HOM (Hong-Ou-Mandel) interferogram [81]. If 50 GHz ITU channels are used instead, the resulting filtered JSI better approximates a single mode, and the model predicts $1/K = 0.96$.

Extrapolated rates (MHz)				
rate metric (μ at max)	1 Channel	8 Channels	16 Channels	60 Channels
coincidence rate, C_{AB} (0.014)	0.755	5.41	11.6	34.9
log negativity, C_N (0.010)	0.600	4.30	9.19	27.7
coherent info., C_I (0.006)	0.345	2.47	5.28	15.9
secret key rate, SKR (0.007)	0.309	2.21	4.73	14.3

Table 5.1: Per-channel predicted maximum values for the 4 rate metrics are shown in the column labeled ‘1 Channel.’ Depending on the metric, the maxima are achieved for different pump powers μ (see section 5.16). The μ value that maximizes each metric is shown in parenthesis on the left.

5.5 Discussion

We have demonstrated that a time-bin entanglement source based on a mode-locked laser, spectral multiplexing and low-jitter detectors produces high entangled photon rates suitable for QKD or advanced quantum networks. Still, there is potential to increase rates beyond those measured here with some straightforward changes to the setup. First, a higher power EDFA-amplified SHG module or tapered amplifier may be used. With this, we predict a single channel pair could sustain rates up to those specified in the first column of Table 1. Our measurements of 8 channel and 16 channel configurations imply the approximately multiplicative scalings in columns 2 and 3, as coincidence rates of these channels pairs are all within 27% of each other. From measurements of the SPDC spectrum, it is also possible to extrapolate rates to a 60-channel 100 GHz DWDM configuration that includes channels spanning the L, C, and S ITU bands. This configuration could sustain 34.9 MHz total coincidence rate, and a distillable entanglement rate between 27.7 (C_N) and 15.9 Mebits/s (C_I). These rates are impressive considering they are achievable with existing SNSPDs and other technology. The SPDC spectrum and extrapolation details are found in section 5.16.

The ratio of singles rates S_A, S_B to coincidence rates C_{AB} are high in this system due to the relatively wide-band JSI and narrow filters. Each DWDM channel at Alice picks up a large fraction of photons that cannot be matched with pairs passing through the corresponding channel passband at Bob, a feature quantified by the δ factor. The high singles rates lead to

accidental coincidences from mutually incompatible spectral modes that lower visibility and load the detectors with useless counts. However, there is potential to mitigate these extra counts by embedding the nonlinear crystal undergoing SPDC in a cavity that enhances emission at the center frequencies of multiple DWDM channels [82]–[84]. Also, there are other approaches to achieving such intensity islands that require dispersion engineering [85], [86]. With such periodically enhanced emission, the resulting JSI would exhibit a series of intensity islands lying along the energy-matching anti-diagonal, easily separable with DWDMs at Alice and Bob. The photon flux for each channel would originate primarily from these islands covered by both signal and idler DWDM passbands, resulting in a higher ratio of coincidences to singles. The probability of accidental coincidences C_{Acc} would be lower, and therefore bring the decrease of visibility with μ more in line with the modeled V_C data in Fig. 5.3. Furthermore, this would enable substantially higher maximum rate metrics than those in table 5.1.

This source is a fundamental building block for future space-to-ground and ground-based quantum networks. It leverages the strengths of the latest SNSPD developments — namely simultaneous high count rates, low jitter and high efficiency — and in doing so adopts interferometers and DWDM systems that are compact, stable and accessible. By elevating the system clock rate to 4.09 GHz and shrinking the time bin size to 80 ps, we have demonstrated a new state of the art in quantum communication that enables adoption of mature and extensively developed technologies from classical optical networks. Also, the spectral multiplexing methods used here are potentially compatible with those demonstrated in broadband quantum memories [87] and optical quantum computing [88].

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Data availability

Data underlying the results presented in this paper are available in [89], [90].

5.6 Phase basis readout

This section uses numbers in kets to signify time delays, such that the notation from section 5.4 transforms as $|e\rangle, |l\rangle \rightarrow |0\rangle, |1\rangle$. Following the creation of the bell pair $\frac{1}{\sqrt{2}}(|00\rangle + e^{i\phi}|11\rangle)$ with the source interferometer, the readout interferometers at Alice and Bob transform each member of the entangled pair according to the operation [76]:

$$|k\rangle \rightarrow \frac{1}{2} \left(|k\rangle_{(A/B)+} + e^{i\phi_s/i} |k+1\rangle_{(A/B)+} + i |k\rangle_{(A/B)-} - ie^{i\phi_s/i} |k+1\rangle_{(A/B)-} \right)$$

where $(A/B)+$ and $(A/B)-$ denote the output ports of Alice (A) or Bob's (B) interferometer. The full state is a 28-term expression made of four so-called 'branches' indexed by the four combinations of interferometer output ports: $A+B+$, $A+B-$, $A-B+$ and $A-B-$. Each branch has a term in the following form, with amplitude dependent on the phase relationship between the interferometers:

$$p \left(e^{i\phi} + qe^{i(\phi_s+\phi_i)} \right) |2\rangle_{Au} |2\rangle_{Bv}$$

where $p, q, u, v \in \{ \{+1, +1, +, +\}, \{i, -1, +, -\}, \{i, -1, -, +\}, \{-1, +1, -, -\} \}$ for the four terms. These terms define the probability amplitude of the quantum state in the so-called phase basis. The modulus squared of these terms gives the phase-dependent probability of coincidences across the center time bins, as measured at interferometer outputs of Alice and Bob.

All the phase terms can be grouped into one variable $\theta = \phi_s + \phi_i - \phi$, and the four $|2\rangle|2\rangle$ terms can be re-expressed in terms of the cosine function [76], [79]:

$$\begin{aligned}
P_{A+B+} &= |\langle 2|2 \rangle|_{A+B+}^2 = 2(1 + v \cos(\theta)) \\
P_{A+B-} &= |\langle 2|2 \rangle|_{A+B-}^2 = 2(1 - v \cos(\theta)) \\
P_{A-B+} &= |\langle 2|2 \rangle|_{A-B+}^2 = 2(1 - v \cos(\theta)) \\
P_{A-B-} &= |\langle 2|2 \rangle|_{A-B-}^2 = 2(1 + v \cos(\theta))
\end{aligned} \tag{5.2}$$

where v was added to denote the visibility of the phase basis. Scanning the phase of the system and measuring coincidence rate across the center bins produces sinusoidal fringes as shown in Fig. 5.9.

5.7 Coincidence rate & interferometer output ports

As each readout interferometer has two output ports, the full output state observed at Alice and Bob cannot be fully measured with two SNSPDs. We label the output ports of Alice (A) and Bob's (B) interferometers with plus (+) and minus (-). The plus ports are used for most measurements. By measuring the relative loss between the plus and minus ports, all singles rates S_i and coincidence rates $C_{ij}, i, j \in \{A+, A-, B+, B-\}$ across different detectors can be estimated.

R_A is the ratio of transmissions t_{A-} over t_{A+} , where t_{A-} is the transmission through the input to output $A-$ and t_{A+} is the transmission through the input to output $A+$. R_B is defined analogously. We measure values for R_A and R_B by sending a pulsed laser into the input and measuring the ratio of power transmitted across the output ports:

$$R_A = 0.99 \pm 0.03, \quad R_B = 1.04 \pm 0.03.$$

The coincidence rates for all wavefunction branches are the same if θ in Eq. 5.2 is set to zero. With this phase state rate $C_{A+B+, \theta=0}$ measured directly (labeled B in Fig. 5.9), it is straightforward to estimate the full wavefunction coincidence rate across all interferometer outputs. As shown in table 5.7, the rate is $C_{A+B+}(1 + R_A + R_B + R_A R_B)$. This estimate is used to express a full coincidence rate for Figures 5.3 and 5.4.

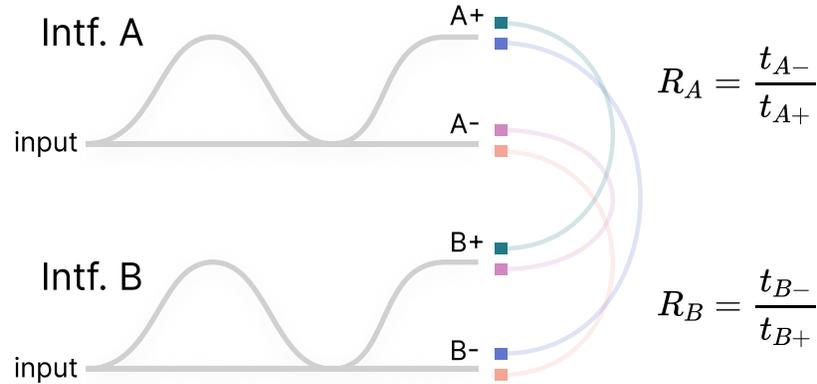


Figure 5.5: **Wavefunction branches** Different pairings of interferometer output ports collect different wavefunction branches.

Predicted Singles and Coincidence Rates for Full Wavefunction				
rate metrics	Branch 1	Branch 2	Branch 3	Branch 4
singles rate 1	S_{A+}	$S_{A-} = R_A S_{A+}$	S_{A+}	$S_{A-} = R_A S_{A+}$
singles rate 2	S_{B+}	S_{B+}	$S_{B-} = R_B S_{B+}$	$S_{B-} = R_B S_{B+}$
coincidence rate	C_{A+B+}	$C_{A-B+} = R_A C_{A+B+}$	$C_{A+B-} = R_B C_{A+B+}$	$C_{A-B-} = R_B R_A C_{A+B+}$

Table 5.2: Singles and coincidence rates for wavefunction branches. The $A+, B+$ branch was measured, and the rates of other branches are predicted using relative transmission factors R_A, R_B .

For Fig. 5.2 in particular, coincidences were measured with the center bin rate tuned to a minimum $\theta = -\frac{\pi}{2}$ (grey solid line in main-text Fig. 5.2c). The rate therefore captures the contribution from the 6 phase-independent terms for the $A+B+$ wavefunction branch. This can be extrapolated to the $\theta = 0$ state by multiplying by $\frac{4}{3}$. For the rate displayed to be consistent with the measures of coupling efficiency η (and so the interferometers are not thought of as a source of $\sim 50\%$ loss), this rate is multiplied again by $(1 + R_A R_B)$ to represent two wavefunction branches. This results in a total scaling of:

$$C_{Fig. 5.2} = \frac{4}{3}(1 + R_A R_B)C_{measured}.$$

5.8 Joint spectral intensity analysis

This entanglement source is potentially useful for future quantum communication systems that make use of two-photon interference, such as teleportation or entanglement swapping. These require the generation of highly pure and indistinguishable photons. The type-0 SPDC crystal used in this source shows strong spectral correlations that make it inappropriate for two-photon interference demonstrations by itself. However, with the application of the DWDM filtering, we create a series of spectral channel pairings that are potentially good individual sources of fairly pure single mode photons. To investigate this, we model the joint spectral intensity function (JSI) produced by the SPDC and fit it to data. Then we and apply a Schmidt decomposition to the spectral modes produced when pairs of DWDM filter channels are applied to the modeled JSI. We derive an inverse Schmidt number which is equal to single photon purity P as well as visibility V of Hong-Ou-Mandel (HOM) interference. An inverse Schmidt number approaching 1 indicates that the source is effective for two-photon interference measurements like HOM and Bell State measurements.

JSI modelling

We follow an analysis for co-linear quasi-phase matching inside a waveguide packaged SPDC crystal [91], [92]. The joint spectral intensity $|f(\omega_s, \omega_i)|^2$ is modelled as a product of phase matching and pump envelope intensities $|\psi_{\text{ph}}(\omega_s, \omega_i)|^2$ and $|\psi_p(\omega_s, \omega_i)|^2$, where ω_s and ω_i are the frequencies of the signal and idler modes, respectively. The phase matching envelope intensity takes the form:

$$|\psi_{\text{ph}}(\omega_s, \omega_i)|^2 = \text{sinc}^2\left(\frac{\Delta k L}{2}\right), \quad \Delta k = 2\pi \left(\frac{n(\lambda_p)}{\lambda_p} - \frac{n(\lambda_s)}{\lambda_s} - \frac{n(\lambda_i)}{\lambda_i} - \Gamma \right)$$

where L is the length of the crystal, Δk is a wave-vector mismatch term, and $n_{p(s)(i)}$ is the refractive index of the crystal at the wavelengths of pump λ_p , signal λ_s and idler λ_i . $\Gamma = 1/\Lambda$ where Λ is the polling period of the crystal. The refractive indices $n(\{\lambda_p, \lambda_s, \lambda_i\})$ are computed from an MgO-doped PPLN Sellmeier equation [93]. In the expression for Δk , λ_p is the function of λ_s and λ_i that imposes energy conservation: $1/\lambda_p = 1/\lambda_s + 1/\lambda_i$.

The pump envelope intensity is modeled as

$$|\psi_p(\omega_s, \omega_i)|^2 = \exp\left(-\frac{(\omega_p - \omega_s - \omega_i)^2}{\sigma_p^2}\right)$$

where ω_p and σ_p are the center frequency and bandwidth of the pump signal out of the EDFA/SHG module. Unlike λ_p in the phase matching expression above, ω_p and σ_p are fixed to known values or chosen as floating fitting parameters.

JSI fitting

The JSI model is fitted to the the 8x8 DWDM data from Fig. 5.2a. The transmission spectrum of one DWDM channel was measured and used to estimate the transmission properties for all pairs of 8 channels. For each measurement of coincidence rate from Fig. 5.2a, we define an integration over the joint spectral intensity and the corresponding filter passbands:

$$C_{u,v} = \int_s \int_i T_u(\lambda_s) T_v(\lambda_i) |f(\omega_s, \omega_i)|^2 d\lambda_s d\lambda_i \quad (5.3)$$

where $T_{u(v)}$ is the transmission spectrum for filter with ITU channel $u(v)$, and the integrations are over the signal and idler wavelengths. Efficiency parameters η_i scale the DWDM filter spectrums, and are used to model all loss between pair generation in the SPDC crystal and detection in the SNSPDs. To fit the η_i values, the singles rates from Fig. 5.2a were also included, and fitted to single-filter integrations:

$$S_u = \int_s \int_i T_u(\lambda_a) |f(\omega_s, \omega_i)|^2 d\lambda_s d\lambda_i$$

where $a \in \{i, s\}$. Parameters of model for $|f(\omega_s, \omega_i)|^2$ were optimized to minimize the error between estimates $C_{u,v}$ and S_u and the measured coincidence and singles rates. The parameters in Fig. 5.6 were either set explicitly based on measurements and known constants (black), or optimized in the fitting process (blue).

Varying MgO doping percentage and varying crystal temperature affect the Sellmeier equations in similar ways [93], [94]. Therefore, crystal temperature T was used as a fitting parameter, to stand in the unknown MgO doping percentage. The true crystal temperature during all measurements was 50.0° C, which was optimized to maximize coincidence rates.

fit R-squared	0.99998543		
pump laser λ	1539.57 nm		
pump laser σ	103 GHz		
SPDC parameters			
T	130 °C		
L	10 mm		
polling period Λ	18.3 μ m		
A	9.01e6		
Sellmeier coefficients 1% doped MgO			
a_1	5.078		
a_2	0.0964		
a_3	0.2065		
a_4	61.16		
a_5	10.55		
a_6	1.59e-2		
b_1	4.67e-7		
b_2	7.822e-8		
b_3	-2.653e-8		
b_4	1.096e-4		
signal channels η_i			
η_{52}	0.2138		
η_{53}	0.1898		
η_{54}	0.2056		
η_{55}	0.1811		
η_{56}	0.1727		
η_{57}	0.1633		
η_{58}	0.1601		
η_{59}	0.1636		
idler channels η_i			
η_{35}	0.1880		
η_{36}	0.1797		
η_{37}	0.1733		
η_{38}	0.1809		
η_{39}	0.1563		
η_{40}	0.1820		
η_{41}	0.1394		
η_{42}	0.1651		

Figure 5.6: **JSI fitting parameters** Pump laser λ and σ were found by measuring the output of the SHG module with a spectrum analyzer.

An ideal photon pair source for scalable optical quantum information processing would not exhibit joint spectral correlations between the signal and idler photons. The Schmidt decomposition, which is equivalent to the singular value decomposition in our computational model, can be used to quantify these correlations [92]. We apply the Schmidt decomposition to the filtered JSIs for filter pairings along the main diagonal in Fig. 5.2a, and derive the inverse Schmidt number for these modes

$$1/K = \sum_i \lambda_i^2$$

where λ_i are the Schmidt coefficients [92]. The inverse Schmidt numbers for all 8 channel pairs are similar, and are not expected to vary due to any phenomena beyond inaccuracies of the model. Therefore, we quote single values for $1/K$ in section 5.4.

5.9 Consequences of narrowband filtering

Calculation of mean photon number per pulse μ

It is common in the literature to calculate signal and idler arm efficiencies with equations of the form:

$$\eta_{s(i)} = \frac{C_{si}}{S_{i(s)}} \quad (5.4)$$

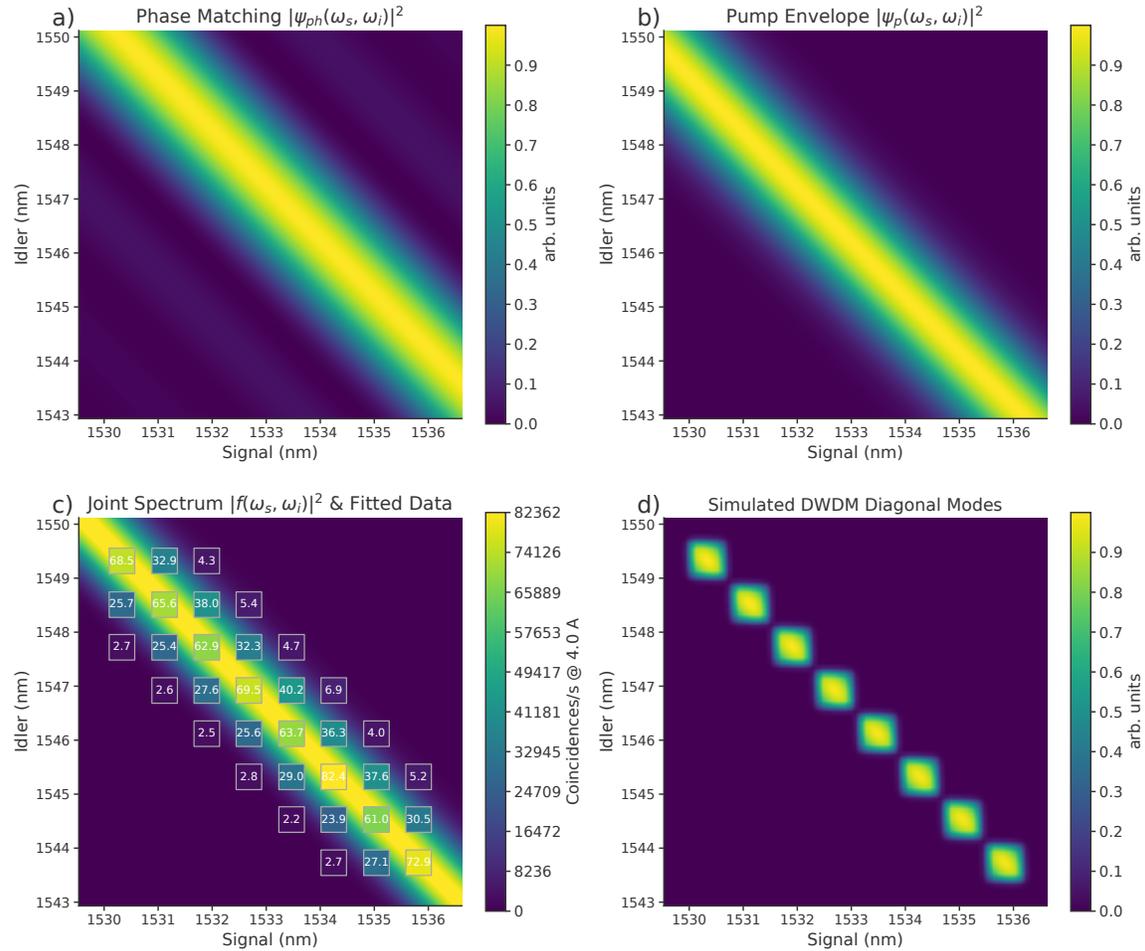


Figure 5.7: **JSI simulation results** a) & b) For type-0 SPDC, the relationship between refractive indices of pump and down-converted wavelengths produces an intensity profile roughly parallel with the pump envelope. This is responsible for the broad output spectrum of these crystals. c) the coincidence rates in Kcounts/s that are fit to filter-defined integrations of the JSI. d) Joint spectral distributions of coincidences expected from the filter pairings that correspond to the main diagonal. Here the joint spectrums of 8 DWDM channels pairs are shown summed together, where each component of the sum is an expression like the integrand of $C_{u,v}$ above.

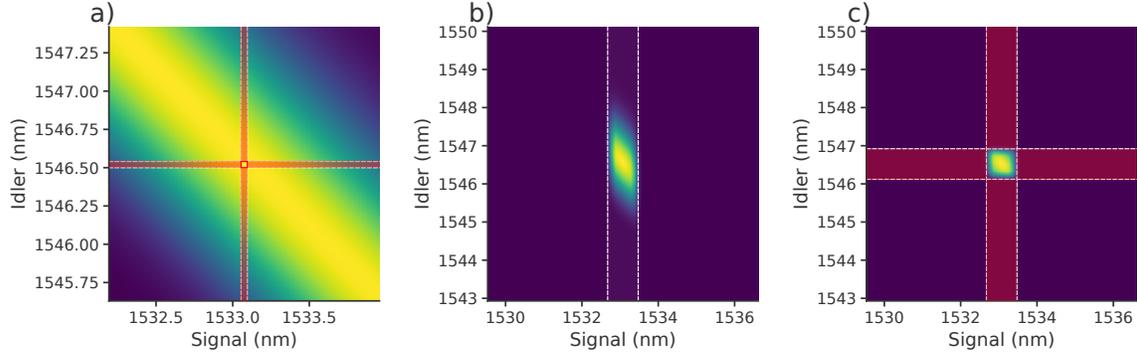


Figure 5.8: **JSI filtering considerations** a) Two filters with bandwidth approximately 0.04 nm are applied to the JSI model. True coincidences are expected only from the region inside the small red square. b) The shape of the JSI with one 100 GHz DWDM filter applied c) the JSI a 100 GHz DWDM filter applied on both signal and idler arms.

where $\eta_{s(i)}$ is coupling efficiency of the signal (idler) arm, C_{si} is the coincidence rate, and $S_{i(s)}$ is the singles rate on the idler (signal) arm. μ , the mean pair rate per period or cycle, may also be defined in terms of the repetition rate R as $R\mu\eta_{s(i)} = S_{s(i)}$. With these, one can define μ in terms of coincidence rate C_{si} and singles rates S_s and S_i :

$$\mu = \frac{S_s S_i}{C_{si} R}. \quad (5.5)$$

However, this definition breaks down in the limit of narrowband filtering, or when the losses on the signal and idler arm cannot be thought of as ‘colorless.’ Consider the situation of two very-narrowband filters, as illustrated in Fig. 5.8 a. This situation can be simulated using the JSI model. We set signal and idler filter bandwidth to 5% of the 100 GHz DWDM bandwidths. Pump power is scaled by 200x. Transmission of the filters at their maximum is set to 100%. This results in $S_s = 58.0$ MHz, $S_i = 57.6$ MHz, and $C_{si} = 567$ KHz. With these values, Eq. 5.5 suggests a μ value of 1.47. This is misleading because it is unreasonable to expect the red outlined region at the intersection of the filters in Fig. 5.8 a — which is responsible for all true detections of entangled pairs — to be the source of more than one entangled pair per pulse. Rather, the high singles rates S_s and S_i are having an adverse effect on the μ calculation. Most of the singles detections are from mutually incompatible spectral modes — the 4 regions that form a cross shape above, below, and to the sides of the red outlined square.

We propose a definition of μ similar to the form of Eq. 5.3:

$$\mu_{u,v} = \frac{1}{R} \int_s \int_i W_u(\lambda_s) W_v(\lambda_i) |f(\omega_s, \omega_i)|^2 d\lambda_s d\lambda_i \quad (5.6)$$

where W_u and W_v have the spectrums of filters T_u and T_v but maximum transmissions of 100%. This is an integration of $|f(\omega_s, \omega_i)|^2$ over the bipartite spectral region where filter transmission is non-negligible. As the JSI model is defined, $|f(\omega_s, \omega_i)|^2$ has units of entangled pairs per nm^2 .

Going forward, we use the Eq. 5.6 definition of μ in section 5.4, and do a separate analysis of the effect of the mutually incompatible spectral modes when necessary. Note that in section 5.4, Alice receives idler photons and Bob receives signal photons, so variables transform as $C_{is} \rightarrow C_{AB}$, $S_i \rightarrow S_A$, and $S_s \rightarrow S_B$.

Estimating μ from coincidence and singles rates

As Eq. 5.5 is problematic for the narrowband filtering regime, a conversion is needed that maps this type of expression to the more implicitly defined Eq. 5.6. Luckily, the influence of narrowband filtering as a sort of pseudo-loss can be rolled into a new geometric factor δ . This is the ratio of the JSI captured by two narrowband spectral filters $W_u(\lambda_s) * W_v(\lambda_i)$ to that captured by one $W_v(\lambda_i)$, as illustrated in Fig. 5.8 b and c. Consider an expression for δ in terms of measured and fitted quantities:

$$\delta_{i(s)} = \frac{C_{is}}{\eta_{i(s)} S_{s(i)}}. \quad (5.7)$$

Here, $S_{s(i)}$ is the singles rate through a signal (idler) narrowband filter. $\eta_{i(s)} S_{s(i)}$ would be the coincidence rate if the idler (signal) filter was wide-band (or just colorless loss), but maintained the same efficiency as measured ($\eta_{i(s)}$). Therefore the fraction can be thought of as the ratio of a coincidence rate measurement with two narrowband filters [C_{is}] to a coincidence rate measurement with one narrow-band and one wide-band filter [$\eta_{i(s)} S_{s(i)}$]. As we use the same bandwidth filters on the signal and idler arms, the δ_i and δ_s calculated from the measured data and JSI fitting results are similar. We use an averaged single δ value for all further analysis, unique to our JSI bandwidth and 100 GHz DWDM filters.

$$\delta = 0.393 \pm 0.012$$

This is averaged from 8 δ_i and 8 δ_s values, for the 8 DWDM channel pairs along the main diagonal of the JSI.

We see Eq. 5.7 is a modified form of Eq. 5.4 that includes δ . With $R\mu\eta_{s(i)} = S_{s(i)}$ again, we can define a new expression for μ using singles $S_{s(i)}$ and coincidence C_{is} rates.

$$\mu = \frac{\delta S_s S_i}{RC_{is}} \quad (5.8)$$

This is used to compute μ in section 5.4.

5.10 Quantum state tomography

We perform quantum state tomography of individual channel pairs in order to resolve the full density matrix and calculate bounding terms for the distillable entanglement rate.

Established methods for tomography of time-bin entangled photon pairs involve independent phase control of the two readout interferometers. However, the center bin coincidence rate depends on an overall phase which is the sum of source and readout interferometer phases (see Eq. 5.2). By manipulating the overall phase through control of only one interferometer, we assume that the full phase-dependent behavior of the system is captured. The data for the tomography is captured with Alice's interferometer in 3 phase settings. That which minimizes coincidence rate of the center bin (labelled A in Fig. 5.9), that which maximizes coincidences in the center bin (C), and a state halfway between in phase (B). The (B) state is chosen by setting the interferometer power to a value halfway between the power settings for states A and C. We therefore assume phase scales linearly with power, which is supported by the good agreement in Fig. 5.9 between the phase fringes and a cosine fit.

Multiple measurements involving all three time bins are performed with the phase set in these 3 states. The columns labeled A, B, and C in Fig. 5.10 correspond to these 3 measurement conditions, where the measurements for the 90 degree phase measurements are repeated in columns 2 and 3. We organize the coincidence data in this format to show

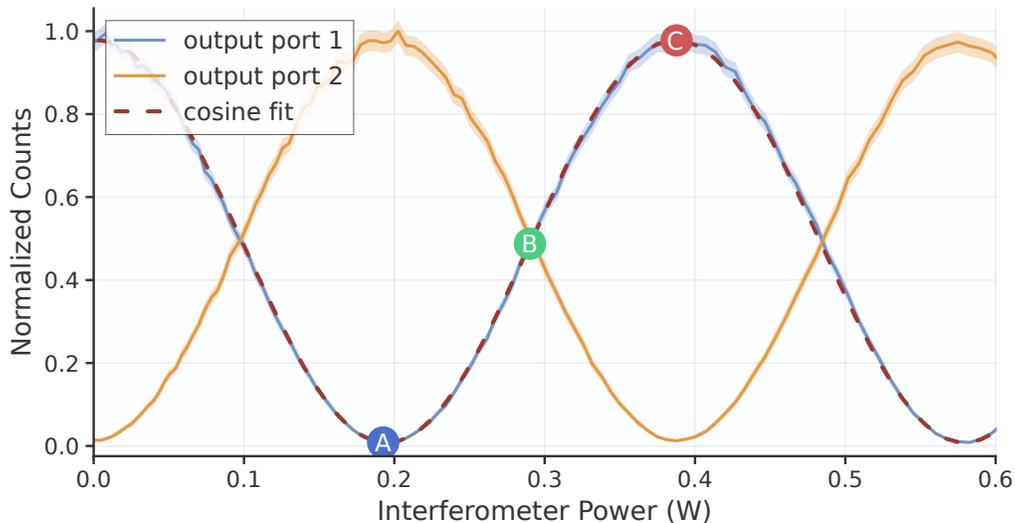


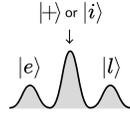
Figure 5.9: **Center bin fringe measurement** Coincidence rate across center time bin with respect to interferometer power. The fringe data was measured for the two output ports of Alice’s interferometer. The output port 1 data was fitted to a cosine curve using linear least squares.

how it relates to more canonical constructions of tomography data where the phases of the two readout stations are controlled independently [95], [96]. Summing the counts in each row yeilds a 16-element vector which is sufficient to calculate a density matrix using a maximum likelihood method [97].

We use a density matrix to calculate bounds on E_D , the distillable entanglement rate. E_D quantifies the rate of maximally entangled Bell pairs which may be created from the received state with local operations and classical communication. E_D is bounded above by log-negativity E_N and below by coherent information ($E_I = \max\{I_{A \rightarrow B}, I_{B \rightarrow A}\}$) [58], [98] both of which may be calculated from the density matrix:

$$E_N = \log_2 \|\rho^A\| \quad I_{A \rightarrow B} = H(\rho^B) - H(\rho^{AB})$$

where $\|\rho^{T_A}\|$ is the trace norm of the partial transpose of ρ , the calculated bipartite density matrix. H is the base-2 von Neumann entropy [99], [100].



		Alice> Bob> Interferometer Phase				n_i
Alice	Bob	$ H\rangle H\rangle$ C	$ H\rangle i\rangle$ B	$ i\rangle H\rangle$ B	$ i\rangle i\rangle$ A	
$ e\rangle$	$ e\rangle$	103.78	102.52	102.52	105.44	414.26
$ e\rangle$	$ l\rangle$	0.49	0.53	0.53	0.34	1.89
$ e\rangle$	$ H\rangle$	88.23	-	89.35	-	177.58
$ e\rangle$	$ i\rangle$	-	89.35	-	89.17	178.52
$ l\rangle$	$ e\rangle$	0.33	0.24	0.24	0.47	1.28
$ l\rangle$	$ l\rangle$	55.99	55.57	55.57	56.14	223.27
$ l\rangle$	$ H\rangle$	64.96	-	63.80	-	128.76
$ l\rangle$	$ i\rangle$	-	63.80	0.0	63.62	127.42
$ H\rangle$	$ e\rangle$	76.62	76.11	-	-	152.73
$ H\rangle$	$ l\rangle$	64.20	64.14	-	-	128.34
$ H\rangle$	$ H\rangle$	271.81	-	-	-	271.81
$ H\rangle$	$ i\rangle$	-	132.85	-	-	132.85
$ i\rangle$	$ e\rangle$	-	-	76.11	80.95	157.06
$ i\rangle$	$ l\rangle$	-	-	64.14	66.33	130.47
$ i\rangle$	$ H\rangle$	-	-	132.85	-	132.85
$ i\rangle$	$ i\rangle$	-	-	-	0.76	0.76

Figure 5.10: **Quantum state tomography measurements** Quantum state tomography data for one low-power (SHG at 1.2 Amps) measurement of channels 35 and 59. The numbers are coincidences per second. Dashes (-) indicate projections that cannot be measured for the particular pairing of time-bin choice (row) and interferometer phase setting (column).

The entanglement rate of the experiment in ebits/s is the coincidence rate C_{AB} times E_D . We therefore plot $C_{AB}E_N = C_N$ and $C_{AB}E_I = C_I$ in Fig. 5.3, as the upper and lower bounds on entangled bit rate $C_{AB}E_D = C_D$. Multiple integrations are performed at each phase and power setting, so that multiple density matrices and multiple measures of coherent information and log-negativity may be derived. The averages and standard deviations of these sets of measurements are used to define the values and error bars for Fig. 5.3 and Fig. 5.4.

Fig. 5.3 also shows a lower bound on secret key rate (SKR) given reasonable assumptions for a slightly different implementation of the entanglement source. This is calculated with a key generation rate formula [52]:

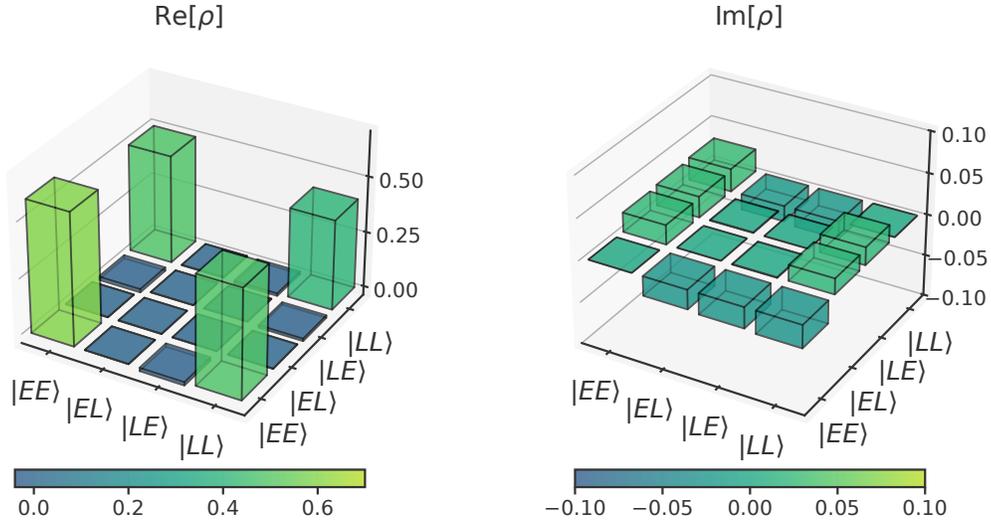


Figure 5.11: **Density matrix at low μ** Density matrix data from channels 35 and 59 at 1.2 A SHG pump power. The $|ee\rangle$ state is higher than all other states due to the interferometer imbalances. For the matrix shown here, $E_N = 0.971$ and $I_{A \rightarrow B} = 0.904$.

$$C_{SKR} = C_{AB}E_S \quad (5.9)$$

$$C_{SKR} = qC_{AB}[1 - f(\mathcal{E})H_2(\mathcal{E}) - H_2(\mathcal{E})] \quad (5.10)$$

Where E_S is the secret key fraction, C_{AB} is the raw coincidence rate, q is a basis reconciliation factor, \mathcal{E} is the quantum bit error rate, and $f(x)$ is the bidirectional error correction efficiency. Quantum bit error rate \mathcal{E} is $(1 - V)/2$ where V is visibility [79]. We choose a constant realistic value for $f(\mathcal{E})$ of 1.1 [101]. $H_2(x)$ is the binary entropy formula defined as

$$H_2(x) = -x \log_2(x) - (1 - x) \log_2(1 - x).$$

We use a basis reconciliation factor of 0.81, thereby assuming a readout configuration at both Alice and Bob where 90% of each channel's flux is directed to a z-basis measurement and may be used to build the shared key. The other 10% is used for phase-basis measurements with the interferometers.

5.11 Interferometer imbalance analysis

It is not trivially clear how much the interferometer early/late imbalances should negatively impact entanglement visibility. The 2nd author of this paper, Samantha Davis, does a theoretical analysis to help answer this question in the supplemental of the manuscript [43].

5.12 Time-walk correction

SNSPD jitter increases with count rate due to properties of the nanowire reset process and features of the readout circuit. A threshold timing measurement set at a specific trigger level will ‘walk’ along the rising edge of SNSPD pulses by varying amounts if those pulses vary in amplitude and slew rate. At low count rates, SNSPDs exhibit very uniform pulse heights and shapes. However, at high counts rates where the inter-arrival time is on the order of the reset time of the detector, current-reset and amplifier effects lead to smaller and distorted pulses in a form of pulse ‘pile-up’ [43].

The effects of time walk can be filtered out by imposing a dead time following each detection. The length of the dead time is tuned so that SNSPD events arriving within it are expected to have distorted timing, and are thrown out. However, as shown in Fig. 5.12, this method can severely limit count and coincidence rates for detector types that exhibit long periods of undershoot or ringing on the falling edge of the RF pulse. For the differential SNSPDs used here, a 200 ns dead time would be necessary to filter out all time-walk effects.

As detailed in [6], [43], a calibration and correction process may be used to cancel out the effects of time walk without losing count rate. It relies on adding timing corrections \tilde{d} to time-distorted SNSPD time tags based on the inter-arrival t' time that precedes each tag. Building a lookup table for \tilde{d} as a function of t' is the objective of the calibration process. With this, real-time running software may largely cancel the increase in jitter from time-walk.

Here we introduce a simplification of the calibration process from [43] that makes use of the pulse sequence already impinging on the detectors from the entanglement source. With the calibration routine written directly into our coincidence analysis software, recomputing the ideal $t' - vs - \tilde{d}$ curve takes no more than a few seconds whenever the detector bias currents or trigger levels are changed.

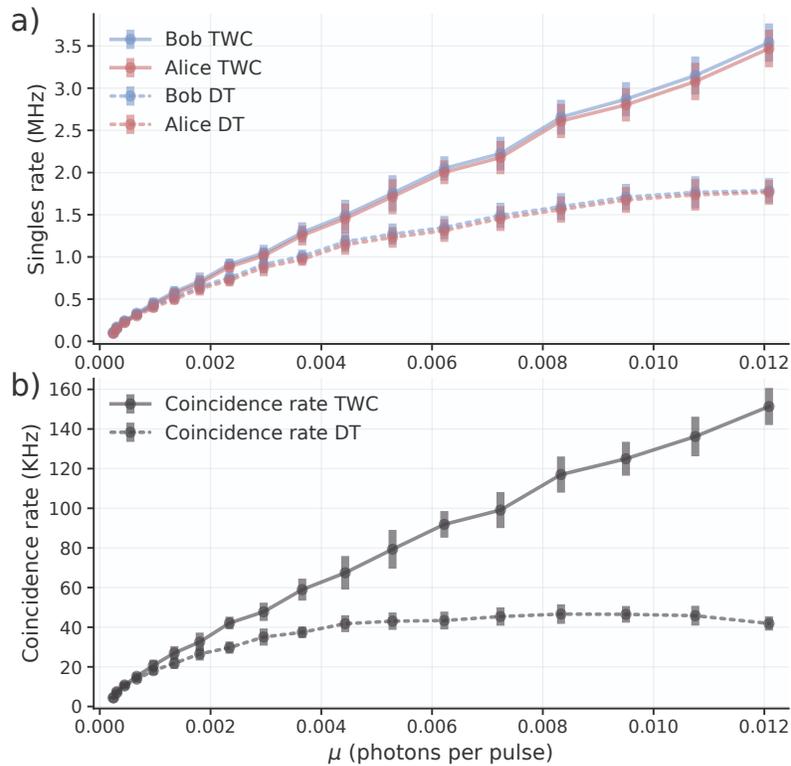


Figure 5.12: **Time walk effect vs dead time rejection** a) Adding 200 ns dead time (DT) to avoid high-rate jitter significantly reduces count rates at higher μ . With time walk correction (TWC), the full available count rate is preserved while keeping the timing jitter low. b) The reduction in count rate for coincidences is more dramatic, because the lost efficiency at both detectors contributes.

We have previously shown how the $t' - vs - \tilde{d}$ curve can be found by illuminating the detector with photons from a pulsed laser source [43]. We imposed the requirement that the period p of the pulses sequence be larger than the largest expected jitter observed due to time walk. This way, any time-tag can be unambiguously associated with the timing of the laser pulse that created it, thereby inferring the relation between t' and \tilde{d} for that event.

Here we rely on a 2D histogram (Fig. 5.13 a) that plots t' on the y-axis and the usual clock-referenced arrival time on the x-axis. Here, any single t' and absolute arrival time measurement does not imply a correction \tilde{d} when considered in isolation. This is because the time-distribution is an irregular pattern of histogram peaks of varying height, as opposed to

a more uniform sequence. Also, delays \tilde{d} can surpass the experiment's fundamental period (244.5 ps from the laser's 4.09 GHz rep rate), initially complicating the matching of trigger events to originating photon timing. But despite these nuances, the 2D histogram structure implies a method for extracting the $t' - vs - \tilde{d}$ calibration curve through a special analysis.

Slices at the bottom of the 2D histogram (Fig. 5.13 a) for large t' are essentially identical to the low-count-rate 3-peak singles histograms like from Fig. 5.2c. As t' decreases from here, the slice as a whole develops some linear offset or rollover (periodic every 244.5 ps). This offset is the \tilde{d} offset of interest. Therefore, $t' - vs - \tilde{d}$ may be extracted by running a template matching algorithm on each horizontal slice, using the large- t' slice as the template. We opt for an absolute differences algorithm (Fig. 5.13 b). As the algorithm progresses to smaller and smaller t' , the offset may approach the fundamental period length and 'roll over' causing a jump-discontinuity. But this can be detected and corrected for, meaning the method may produce a $t' - vs - \tilde{d}$ curve (Fig. 5.13 c) with some \tilde{d} larger than the fundamental period.

Overall, time-walk analysis based on the 2D histogram construction is straightforward to implement and user friendly because it may be applied *in situ* as part of software that already creates histograms and records coincidences.

5.13 Filter bandwidths

Fig. 5.14 shows the transmission spectra of one 100 GHz DWDM filter, and the tunable narroband filter used for the 16-channel source brightness study.

5.14 Guard regions

The width x of the guard regions centered at 80 and 160 ps were set to 10 ps. As shown in Fig. 5.15, this width increase fidelities slightly without significantly impacting coincidence rates. 10 ps was not chosen based on rigorous analysis, though it would be possible to optimize the width to maximize some metric, like secret key rate.

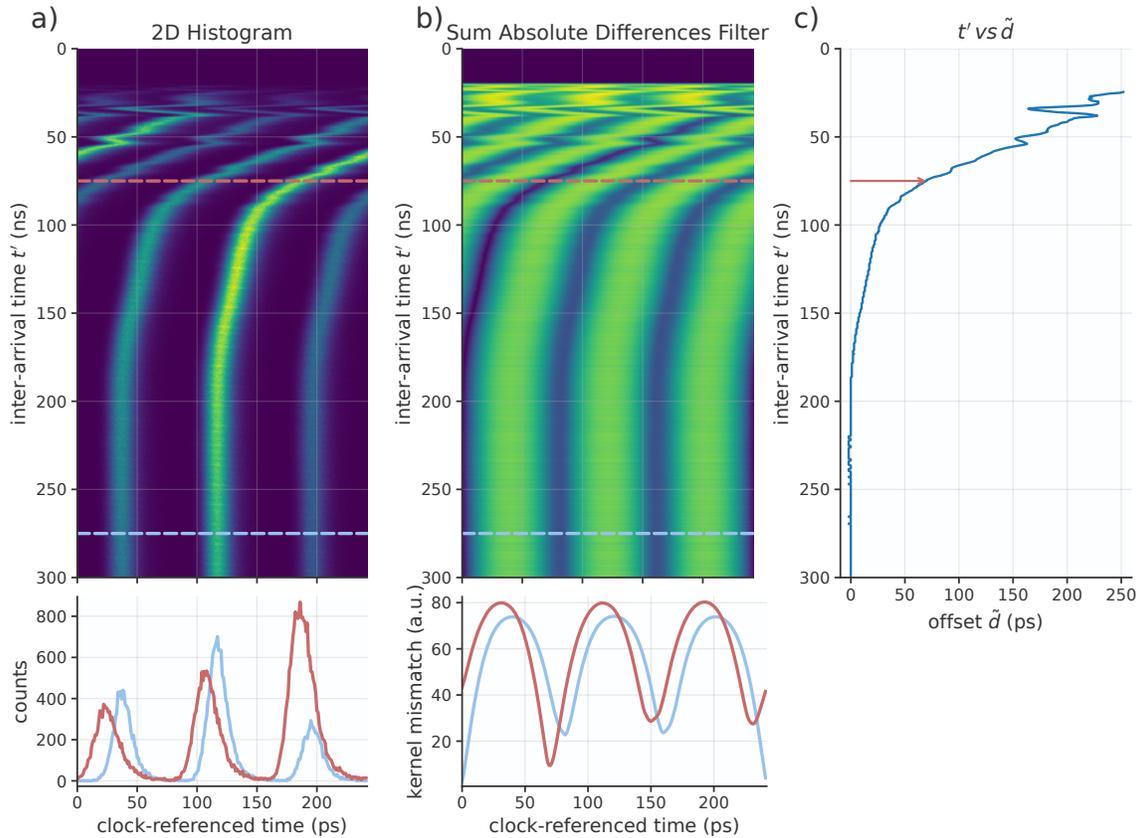


Figure 5.13: **In situ time walk analysis** a) The 2d histogram with clock-referenced histograms on the x-axis and inter-pulse arrival time t' on the y-axis. The effect of time walk is evident in the horizontal translations of the 3-peak structure as t' decreases. Slices of the 2D histogram indicated by the red and blue horizontal line are plotted as regular histograms in the lower figure. b) After applying the Sum Absolute Differences filter to horizontal slices of the 2D histogram. The $t' - vs - \tilde{d}$ delay curve (c) is extracted from this by using the index of each row with minimum mismatch value as the \tilde{d} value for that row.

5.15 Incompatible bases & accidental coincidence rate

An entangled pair can be called 'spectrally compatible' with a given DWDM channel pairing if –given no losses– it would be detected 100% of the time across that channel pair. In the case where signal and idler modes are perfectly spectrally compatible, it has been shown that accidental coincidences still negatively impact visibilities [79]. In this case and assuming negligible dark counts, visibility is reduced as:

$$V = \frac{1}{1 + \mu} V_0$$

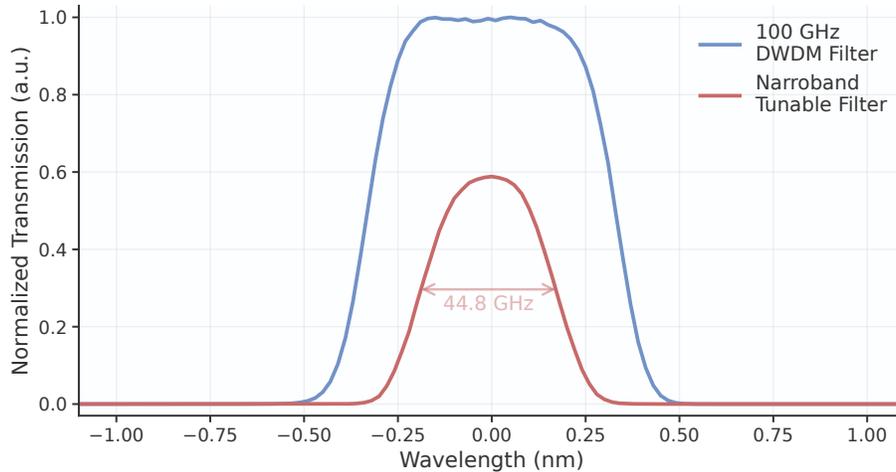


Figure 5.14: **DWDM and tunable narrowband filter bandwidths** Spectrums for a single DWDM channel and narrowband filter, with the center wavelengths set to zero. The narrowband filter is used at Bob with the 16-channel DWDM at Alice to measure coincidence rates in Fig. 5.2b. For the 100 GHz spec. DWDM filters, 100 GHz refers to the filter spacing. The FWHM passband for each is about 82 GHz.

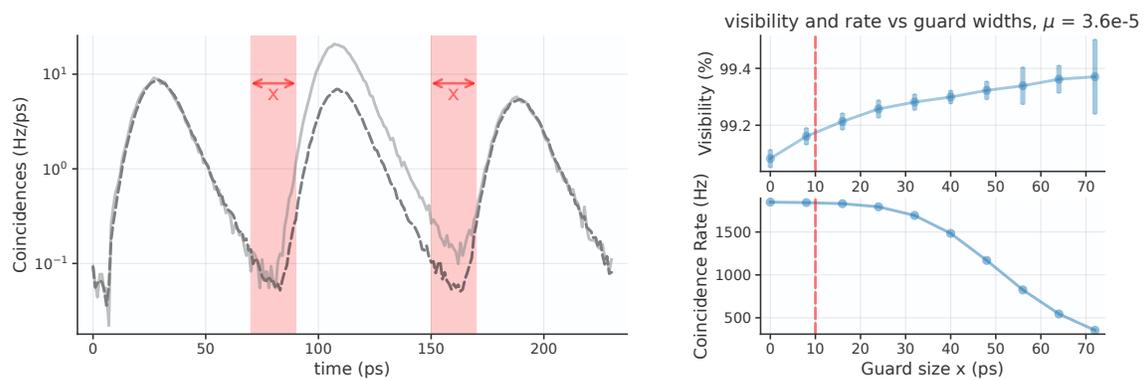


Figure 5.15: **Effect of guard regions on visibilities** Charts on the right show phase basis fidelities and total coincidence rates as a function of width x , where both guard regions stay centered at 80 & 160 ps.

where V_0 is a nominal interferometer-limited visibility [79] and μ is the mean photon number per pulse (classically defined like with 5.5). The accidental coincidence rate C_{Acc} — discussed in section 5.4 — is only partially related to this, as it specifically takes into account only accidental coincidences due to incompatible spectral modes. Such coincidences can arise from two situations, and can be assigned their own coincidence rates

- C_{ee} : two photons both from mutually incompatible spectral regions, like the red regions in Fig. 5.8 c.
- C_{em} and C_{me} : one photon from the central overlapping filter region and one from an incompatible spectral region.

Say one member of a spectrally compatible entangled pair reaches Alice, but not Bob due to loss. The photon received at Alice could form a coincidence with a spectrally incompatible photon that arrives at Bob. These are the C_{em} and C_{me} type coincidences. C_{Acc} in section 5.4 is the sum of C_{ee} , C_{em} and C_{me} :

$$C_{Acc} = C_{ee} + C_{em} + C_{me} \quad (5.11)$$

$$C_{ee}/R = (1 - \delta) \frac{S_A}{R} * (1 - \delta) \frac{S_B}{R} \quad (5.12)$$

$$C_{em}/R = (1 - \delta) \frac{S_A}{R} * \delta(1 - \eta_A) \frac{S_B}{R} \quad (5.13)$$

$$C_{me}/R = (1 - \delta) \frac{S_B}{R} * \delta(1 - \eta_B) \frac{S_A}{R} \quad (5.14)$$

$$(5.15)$$

$$C_{Acc} = \frac{1}{R} (1 - \delta) S_A S_B (\delta(1 - \eta_A) + \delta(1 - \eta_B) + 1 - \delta). \quad (5.16)$$

5.16 Maximum entangled photon source throughput

We observe in the small μ limit that the metrics V , $E_N = C_N/C_{AB}$, $E_I = C_I/C_{AB}$, and $E_S = SKR/C_{AB}$ scale linearly with μ , where E_S is the secret key fraction. Raw coincidence rate is not linear with μ due to the count rate dependent efficiency of the SNSPDs. As count rate increases, the detector spends a larger fraction of time in a partially reset state where photo-detection is less efficient or not possible. We separately collect measurements of detector efficiency versus count rate extending past 10 Mcps, and use this to extrapolate coincidence rate to higher powers. Then, the metrics E_N , E_I , and E_S are multiplied by the extrapolated rate to define extrapolated C_N , C_I , and SKR as shown in Fig. 5.16 b. Maximum values of these metrics are highlighted by colored circular markers.

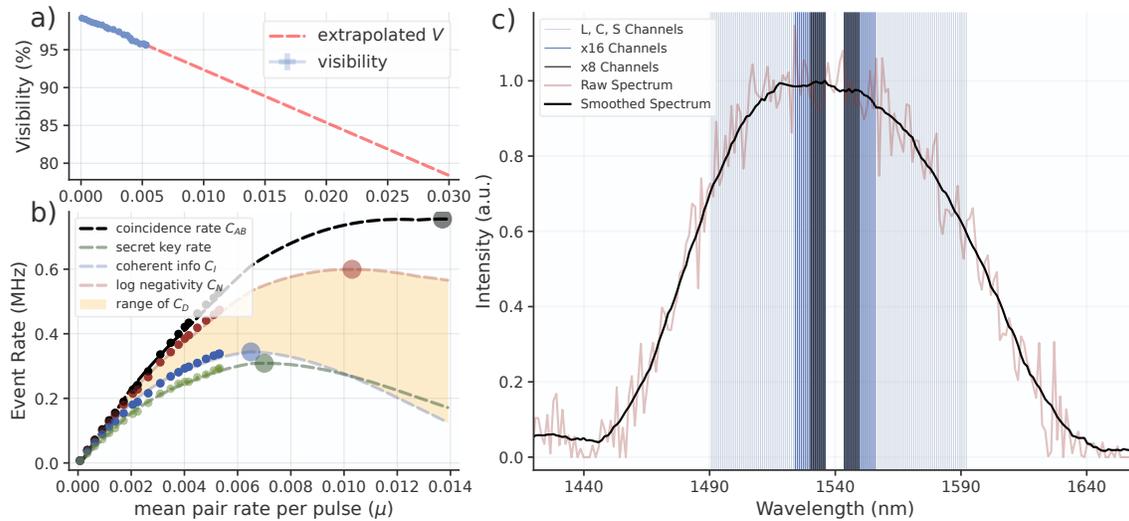


Figure 5.16: **Rates with extrapolated mean photon number** a) and b) include data from Fig. 5.3, and extrapolate it to higher μ . It is notable that C_I and SRK reach their maximum values for only marginally higher pump powers than those used for our measurements. c) Spectrum of entangled photon pairs out of the SPDC, measured with an Anritsu MS9740B spectrum analyzer in High Dynamic Range mode. As the signal was near the instrument noise floor, many repeated spectrum measurements were point-averaged.

In this work we primarily study the capability of 8 DWDM channel pairs, with some analysis of 16-pair performance. However, the spectrum of entangled photon pairs produced by the type-0 SPDC is quite broad, meaning spectral multiplexing across many more channels is possible. In Fig. 5.16 the spectrum of the SPDC is overlaid with sixty 100 GHz DWDM channel pairs spanning the L, C, and S ITU bands [L-29 (1592.1 nm) through C-20 (1543.73) and C-10 (1535.82) through S-1 (1490.76)]. The coincidence rate through these added channels can be estimated from this spectrum and the known performance of the central 8 channel pairs. Table 5.1 specifies estimates for the total rate from the 60 multiplexed spectral channels.

Chapter 6

CONCLUSION

This thesis comprises work on four major projects of somewhat disparate motivations and origins. The low dark count free space coupling project and the PPM project were partially motivated by planned improvements to deep space optical communication systems. The time-walk correction project grew naturally out of issues with SNSPD tagging that were observed in other projects. Finally, the high rate entanglement project resulted from an interest in using the differential single pixel SNSPDs to their full potential in a quantum application.

One prevailing observation from this body of work is that lessons and insights gained from each project have utility beyond the motivations that led to the project itself. These insights can be oddly general and specific at the same time. They do not necessarily align with the delineations usually used to categorize research for one goal versus another. This is how, for example, observations from a project on deep space optical communication can be used to improve the performance of a quantum entanglement source.

Here we state predominant insights gained from the four major projects of this thesis:

1. From the low dark count rate free space coupling project, we learn that the use of free space optics inside a cryogenic environment is not necessarily as unwieldy as one might expect. Optics inside a cryostat cannot be directly aligned without expensive actuators that may or may not function and very low temperatures. But there are ways around this, like by moving all alignment controls outside the fridge and coupling in through windows. Such designs may even have dark count rates comparable or superior to fiber coupled SNSPD systems, as we demonstrate.
2. The time-walk correction project demonstrated how effective SNSPDs continue to be even at high count rates where their RF pulses overlap. Researchers may initially assume that the high count rate behavior of SNSPDs is 'complicated' or 'corrupted,' and that the detectors fail to operate well in this regime. But we have found, with the calibration and correction methodology, that they continue to respond predictably

and with good jitter up to rates where the bias current has insufficient time to recover, thereby reducing the detector efficiency. Depending on the types of amplifiers used, time-walk effects can dramatically reduce jitter before the detector has lost even a few percent of its efficiency due to incomplete bias-current reset. Therefore, time-walk correction can easily lead to 2-3 times higher usable count rates for single detectors, and up to an order of magnitude higher rates in quantum applications that rely on multi-detector coincidences.

3. The PPM project demonstrated the complexity and potential utility of the photon number response in the differential single pixel SNSPDs. For better or worse, the ideal application of these detectors from quantum or classical communication will require nuanced digital processing methods. When not planned for, the PNR effects can be a nuisance. But when properly managed, it makes these detectors into highly effective photon number resolving devices — equivalent to a large array of binary-type SNSPDs. This will be useful for various photon heralding applications, and for commissioning of complex multi-photon states of light. We introduced the GMM method for PPM decoding, based on a general sense that working in a high dimensional space for event attribution will continue to be a fruitful approach for future work. SNSPD readout will only become more complex with the emergence of multiplexed arrays and ultra-high count rate versions. Effects like time-walk the photon number dependent response may be easier to understand and manage if they are thought of as simply modifying how detector data appears when graphed in a high dimensional space.
4. Work on the high rate entanglement system highlighted how important it is to intelligently manage a complex experiment. By transitioning a time-bin entanglement source to a high repetition rate compatible with the differential single pixel detectors, some aspects became simpler (relative to a low-repetition rate system), and others became more complicated. The promise of this project then hinged on managing the complex aspects reliably. One major advantage of the high repetition rate was it allowed us to use small and highly stable interferometers. With lower repetition rate time-bin entanglement sources, precise temperature control of interferometers is needed when their path length delay exceeds multiple nanoseconds [22]. Here we were able to use interferometers with a path length delay of just 80 ps, which varied in

phase by less than a few degrees over multiple hours. On the other hand, the high rate system required time-walk correction for the SNSPDs in order to operate the system at state-of-the-art rates. Enabling this correction method in a full system was a new challenge, and it brought about the much more elegant in-situ calibration method from section 5.12. The improved and mostly automated procedure for cancelling SNSPD time walk added minimal complexity for the system user, and further supported the move towards high repetition rate sources for emerging quantum networks.

6.1 Outlook

To recapitulate the insights derived from the previous chapters, three principal points stand out: 1. With proper mounting and thermalisation techniques, the use of free space optical components inside a cryostat is not prohibitively challenging. 2. Time walk and PNR correction will likely be necessary for high count rate photon number resolving SNSPDs. 3. The new capabilities, as discussed, should be incorporated into a design that does not necessitate substantial complication or discrete calibration endeavors. The key is to develop software supportive of in-situ calibration and event-corruption management.

Our findings can be leveraged in the development of future high-rate heralded SPDC sources. In this context, we see a certain design for such a source, as shown in Fig. 6.1, to be particularly promising.

We propose a design for a future SPDC & SNSPD system that supports high-rate heralding of a range of idler frequencies from a cavity-enhanced SPDC all onto a single SNSPD array. We envision pumping the pair generating crystal in free space and then coupling one arm to an SNSPD array, also in free-space, with the whole setup located inside a cryostat with the detector.

The signal arm is reflected off a diffraction grating, which separates different signal frequencies into different spatial modes imaged onto the SNSPD. This makes for a compact system that should have excellent SPDC - detector coupling efficiency. All the lessons learned about high rate PNR heralding could be incorporated into this array, including time-walk correction as well as accurate simultaneous arrival time and photon number attribution.

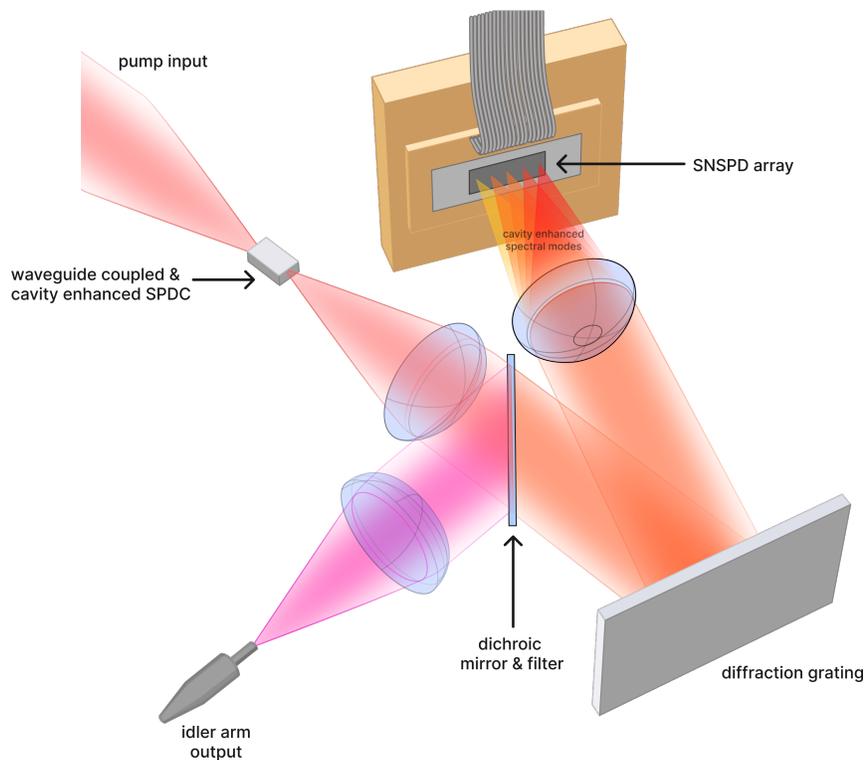


Figure 6.1: **Proposed multiplexed SPDC heralding system** A design for high efficiency heralding of SPDC. A diffraction grating separates spectral modes out of the cavity enhanced SPDC into spatial modes, which are focused onto an SNSPD array in different locations. The idler-arm fiber coupling stands in for whatever type of output coupling is required for the application.

This design could be adapted for use in entanglement-based QKD, for a high-rate single photon source [102]–[104], as part of a heralded EPR/entanglement source [105], or for preparation of non-Gaussian states [106], [107]. For heralded single photon and entangled pair sources, the spectral multiplexed herald design supports certain methods for increasing output rates without sacrificing state purity [108,]. One of the issues facing the development of linear optics quantum computing is the lack of such high-rate high purity sources of non-Gaussian states of light, such a single-photon states. Heralded sources of entanglement are related, and there is a promising path towards demonstrating these at high rate. This is needed because the entanglement distribution system from chapter 5, and all other such

systems, must operate at low pump power and low mean photon number μ in order to minimize the detrimental effects of SPDC multi-pair events on entanglement visibility. A heralded single-pair entanglement source would support drastically higher pair generation rates.

One open question is how to apply both the time-walk correction and the PNR attribution techniques simultaneously. This is important for in-development high-rate SNSPD arrays, successors to the PEACQ [6], which incorporate impedance matching tapers. These will support some degree of photon number resolution simply by spreading out the optical mode over multiple nanowires. But for excellent PNR, single-wire multi and single-photon event discrimination is necessary. For such arrays that must operate at very high rates for emerging quantum networking applications, single wires must support PNR attribution at high count rates as well.

The development of a method for time-walk correction and simultaneous PNR attribution goes beyond the scope of this thesis. However, as discussed in chapter 4, we believe that high-dimensional modelling of the the SNDPD response is useful for overcoming this challenge. Both multi-photon and single-photon events will suffer from time-walk effects for SNSPD pulses that arrive soon after previous pulses. But graphing such data in a high dimensional space spanned by timing measurements from multiple trigger levels and the inter-pulse time t' may show separated $|1\rangle$ and $|2+\rangle$ event groups. This is a promising direction for future research.

SNSPD technology continues an ongoing trend of rapid improvement. This detector technology therefore is well positioned to dictate certain engineering features of emerging quantum communication and computing systems. Perhaps existing problems in quantum transduction and interconnects can be solved through the use of SNSPDs for high-rate high-efficiency bell state measurements.

Certain types of quantum memories, for example, function best when interfaced with low-bandwidth, low-rate channels at wavelengths that are not well supported for long-haul transmission through fiber. This means there may be certain design choices for quantum repeaters and quantum computers that use bandwidth, and frequency conversion processes to interface high rate wide-bandwidth transmission channels with large banks of quantum memories. High rate SNSPDs could be pivotal in such conversion systems, and help bring about a robust system of interconnects between diverse quantum technologies.

Appendix A

APH 138 HOMEWORK ASSIGNMENT

In March of 2022, Matthew Shaw was a guest lecturer for the Quantum Hardware and Techniques course (APH/Ph 138b). The following is a homework assignment I wrote to accompany his series of lectures.

As Matthew Shaw will be giving this series of lectures and using this homework assignment in 2024, the answers have been removed.

1. Free space coupling with low dark counts (50 points)

An experimental apparatus emits a collimated beam of 1550 nm photons with Gaussian beam waist $w_0 = 3$ mm. You wish to focus the beam onto an SNSPD directly through a window in a cryostat.

As we will see later on, a set of filters will be needed between the detector and the window to minimize dark counts. In practice, the set of filters can be quite thick. Say a $f = 100$ mm lens is used right outside the cryostat to focus the beam onto the detector through a set of filters (Fig. A.1 a). The long focal length makes room for a few inches of filters between the external lens and focused spot.

1. (4 pts) If the detector has a circular active area with radius $5 \mu\text{m}$, what ratio of power in the beam can it collect? Assume the detector has unity efficiency across all angles of incidence with respect to the surface normal.

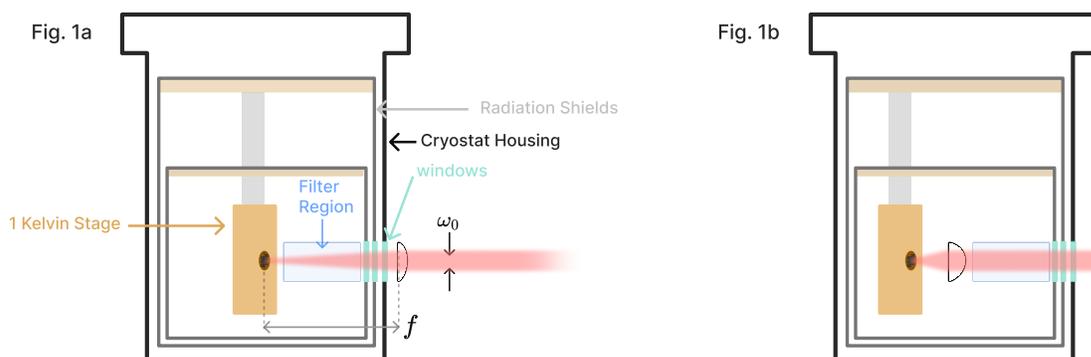


Figure A.1: Cryostat free space coupling options

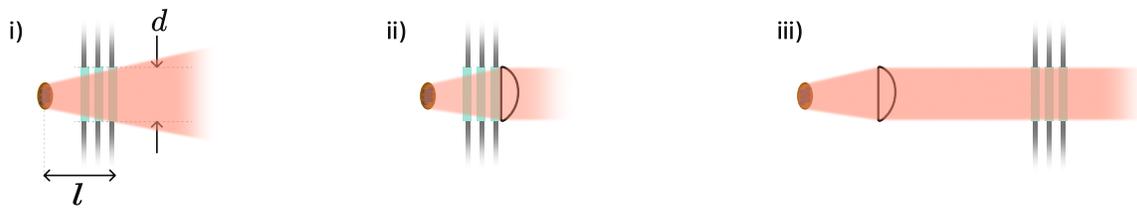


Figure A.2: Three coupling options

2. (4 pts) A faster lens mounted much closer to the detector inside the cryostat focuses to a smaller waist. Consider an $f = 18$ mm lens with the detector at the focal length (Fig. A.1 b). Verify more than 99% of the collimated light will be focused onto the active area of the detector.

Without filtering, the mid-infrared photons coupled to the detector from the room temperature laboratory are a dominant source of dark counts. Think of the environment outside the window as an isotropic blackbody emitter. Consider 3 cases, where the shaded red regions illustrate the light field of thermal radiation that could couple to the detector:

- i) There is no lens; the detector is distance l inside the cryostat, and the first window with diameter d defines an entrance pupil.
 - ii) Same as (i), but a lens with focal length l is placed right outside the first window. The detector is at the focal point.
 - iii) Same as (ii) but the lens is placed inside the cryostat with the detector still at the focal length. Equivalent to Fig. A.1 b above.
3. (6 pts) Does (ii) couple more, less, or equal dark counts to the detector than (i)? What about case (iii)? Why? No calculations should be needed. (Hint: Consider the units of radiance, which characterizes a black body emitter. Etendue or beam parameter product may be useful concepts to consider).
4. (9 pts) Using Planck's law with laboratory temperature T and the geometry of case (i) above, write an expression for spectral radiant flux (photons per unit wavelength) on the active area of a detector with radius r .
5. (6 pts) Consider the configuration in Fig. A.1 b. The detector has an internal quantum efficiency approximated by:

$$\eta(\lambda) = \frac{1}{2}(1 - \text{erf}[\lambda - 3 \mu\text{m}]).$$

λ is measured in μm and $\text{erf}()$ is the error function. Using your conclusions from (1.3) and expression from (1.4), write a formula $N_{\text{photons}}[\lambda]$ for the number of detectable dark counts with respect to λ , then numerically integrate it to find the dark count rate with no filtering. The laboratory temperature T is 293 K, lens focal length l is 18 mm, detector radius r is 5 μm , and the diameter d of all optics is 1 inch. The maximum count rate of this SNSPD is 10 MHz. Is the detector usable or overexposed?

6. (6 pts) A set of shortpass filters can remove the bulk of blackbody radiation. A shortpass filter can be roughly modeled with the formula:

$$F(\lambda, E_t) = \frac{1}{E_t} [(E_t - 1)H(\lambda_c - \lambda) + 1]$$

where H is the Heaviside step function, λ_c is the cutoff wavelength of the filter, and E_t is the extinction ratio of the filter. Use this with $N_{\text{photons}}[\lambda]$ from (d). How many filters with $\lambda_c = 1560 \text{ nm}$ and $E_t = 30 \text{ dB}$ are necessary to suppress the spectral region of detectable dark counts longer than 1560 nm so that it is not the dominant source of dark counts?

7. (7 pts) If a narrow band filter is also inserted with center wavelength 1550 nm and spectral width below $1 - 2 \text{ nm}$, then dark count rate can be approximated as just $N_{\text{photons}}[\lambda = 1550 \text{ nm}]$ times the filter width. Show for this wavelength range you can simplify dark count rate further to a simple exponential function. If the laboratory air conditioner breaks, raising the lab temperature from 293 K to 300 K, how much higher is the dark count rate?

A quantum communication experiment requires time-tagging photons with respect to a 50 GHz clock with 95% fidelity. That is, 95% of the timing measurements of detected photons emitted at the same time with respect to a clock fall within a 20 ps bin. Say the detector and readout electronics have a combined jitter of 10 ps FWHM, and a mode locked laser is used for the experiment that generates transform-limited

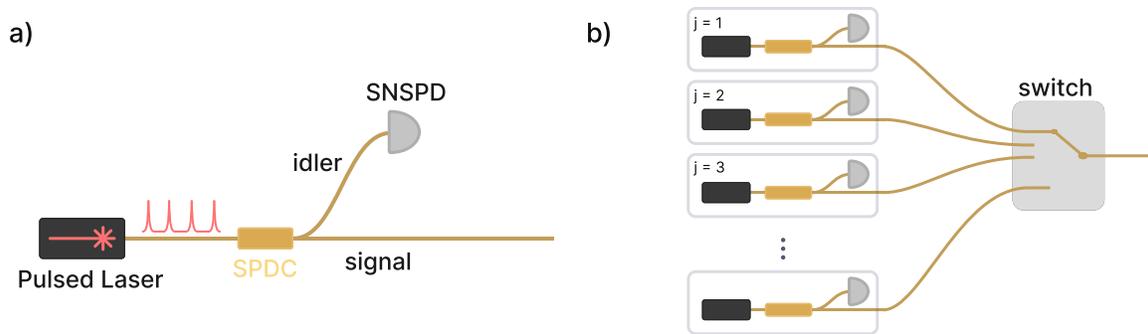


Figure A.3: Heralded single photon source designs

Gaussian pulses. You tune its temporal length to a value for which the total timing uncertainty of time-tagged photons — including system jitter and pulse temporal length — matches the 95 % fidelity at 50 GHz requirement. Assume detector jitter has a Gaussian shape as well.

8. (8 pts) Find the spectral width of a filter that would transmit 95% of the photons from the mode locked laser. What is the dark count rate with this filter, using the expression from (1.7) and $T = 293 \text{ K}$?

2. SPDC coupling and single photon sources (50 points)

A Spontaneous Parametric Down Conversion (SPDC) crystal is known to generate a twin beam squeezed state of the form:

$$|\psi\rangle = \sqrt{1 - \gamma^2} \sum_{n=0}^{\infty} \gamma^n |n_s, n_i\rangle$$

where n_s and n_i are the number of photons corresponding to the signal and idler parts of the wavefunction. Consider Fig. A.3 a, where the crystal is pumped with a pulsed laser, and the signal and idler components that emerge are separated either by polarization or frequency. The idler arm is sent to an SNSPD. This configuration can be used as a heralded single photon source (HSPS). A click on the detector on the idler arm ‘heralds’ a non-vacuum state in the signal arm. High fidelity and probability single photon sources are very useful for various quantum optics experiments and technologies, including linear optical quantum computing.

Most SNSPDs are *binary*-type single photon detectors, meaning they differentiate between zero and one or more photons arriving in a given light pulse. A positive operator value measure (POVM) quantifies how a ‘click’ from a binary SPD updates our knowledge of the incident state:

$$\hat{\Pi}_{\text{binary}} = \sum_{n=0}^{\infty} [1 - (1 - \eta)^n] |n\rangle\langle n|$$

where η is the coupling efficiency between the state of interest and the detector.

1. (6 pts) Find the expectation value of $\hat{\Pi}_{\text{binary}}$ given the SPDC state above. This is the probability $p_{\text{binary}}(\gamma, \eta)$ of getting a binary detector click on the idler arm. For $\gamma \ll 1$, what is p_{binary} up to lowest order in γ , and what fock state of the signal arm is the source of this dominant term?
2. (6 pts) A general form for the density matrix of the signal mode given a herald event is:

$$\rho_s(\gamma, \eta) = \frac{\text{Tr}_i(\hat{\Pi}|\psi\rangle\langle\psi|)}{\langle\psi|\hat{\Pi}|\psi\rangle}.$$

Write down the $|1\rangle\langle 1|$ term of this matrix, and simplify any infinite sums. This is the single photon fidelity $F_{\text{binary}}(\gamma, \eta)$. Why does F_{binary} approach zero for γ approaching 1? What types of states is the SPDC generating in this limit?

An HSPS with high single photon fidelity and probability is most useful, but you see these metrics are maximized for opposite limits of γ . One approach to achieving high probability and fidelity simultaneously is to link multiple SPDC sources and heralding detectors as shown in Fig. A.3 b. A click from the detector j triggers the switch to move to position j and let the heralded state pass through. This way, γ for each source can be kept low to maximize fidelity, while heralding probability increases with the number of sources.

3. (6 pts) If such a multiplexing setup is engineered to have 98% single photon fidelity from each source and 98% heralding probability overall, how many sources and binary SNSPDs are needed? Use an idler arm efficiency η of 80%.

A photon number resolving (PNR) SNSPD is able to discriminate the number of photons in a light pulse*. By heralding the idler mode with a PNR SNSPD, the generation of multi-photon signal pulses can be identified and discarded. There is a POVM for an ideal PNR single photon detector, where i is the number of photons detected:

$$\hat{\Pi}_{PNR}(i) = \sum_{n=i}^{\infty} \binom{n}{i} (1-\eta)^{n-i} \eta^i |n\rangle\langle n|.$$

4. (12 pts) Derive a herald probability p_{PNR} and fidelity F_{PNR} for the PNR POVM, following the steps in the previous sections with i set to 1. You can use symbolic math tools to simplify them if you wish. The probability of successfully heralding states in the signal arm p_{PNR} should now approach zero for γ near one. Why is this?
5. (12 pts) Make a parametric plot for $0 < \gamma < 1$ with F_{PNR} on the x-axis and p_{PNR} on the y-axis. Plot the curve for a few different values of idler arm efficiency $0 < \eta < 1$. All curves should reach the same maximum herald probability. What is it?
6. (8 pts) Consider again the configuration in Fig. A.3 b. Find the number of sources using PNR detectors needed to reach 98% single photon herald probability and fidelity with $\eta = 0.8$. Also find the number of sources for $\eta = 0.95$.

Appendix B

SOFTWARE TOOLS

B.1 Software tools for equipment and experiment control

Much of my time during the phd was spent writing software. While the main product of a phd is papers and the underlying ideas of the experiments carried out, software was often used to rigorously encode these more semantic or ephemeral results. Sometimes, the efficacy of a certain experimental idea depends greatly on the simplicity and reliability of the software used to implement it. If the setup of an initially complex experimental arrangement — for example the synchronization of intensity modulators and arbitrary waveform generator with a mode locked laser — can be made significantly simpler through the use of software, then the idea becomes more practical and more likely to be adopted by other researchers.

For these reasons I include introductions to the software tools on which I spent the most time and gained the most benefit. Perhaps these repositories provide insight that the thesis so far has not.

B.2 Experiment and control software**Sequence generator**

The Sequence Generator repository is for generating AWG sequences that are synchronized with the Pritel OAC fast mode locked laser. This is needed for carving the mode locked laser signal with intensity modulators. This toolkit was useful for my PPM project as well as a concurrent high rate QKD project with slightly different requirements.

The most important feature of this codebase is the ability to determine compatible AWG sample rates and sequence lengths for a given laser repetition rate, while imposing certain requirements, like that the AWG sequence length must be a multiple of 128 samples. The script supports situations where a small integer number of laser pulses does not match in

time with an integer number of AWG samples. The main requirement is that the time for the full AWG sequence to run must be an integer multiple of the laser repetition period, so that the AWG sequence can be repeated indefinitely without drifting out of sync with the laser.

This analysis is performed in the functions `determine_ppm_properties` and `determine_regular_properties` for the PPM and QKD applications, respectively.

Sequence generator repository

Time-walk correction

A repository of tools for performing time-walk calibration and correction on timetag data files. It is set up to use the binary format `.ttbin` from swabian timetagger, but can be easily adapted to other formats.

Time walk correction repository

Bias control user interface

A web-based user interfaces for controlling isolated voltage sources used for SNSPD biasing. Is is an improvement over a previous web interface which is based on the [svelte frontend framework](#) and should be much easier to maintain and extend than the [previous web interface](#).

Svelte bias control repository

Entanglement analysis repositories

This master repository contains submodules for all the repositories used for analyzing data from the high-rate entanglement distribution system. It includes a script for automatically populating each repository with the original raw data stored or figshare.

Entanglement analysis repository

Entanglement control software

Based on an example file shipped with the swabian timetagger, this leverages the swabian python api for collecting entanglement data for the high-rate entanglement distribution system. It incorporates an innovative method for defining long running measurements based on a construct called `Actions`. `Actions` are objects that perform some operation at

one stage in the script's main event loop (e.g., change an interferometer voltage to a specific value), or over multiple event loop iterations (e.g., integrate coincidences). Actions may also contain and run other actions, so that successively more complex measurements can be built from simple reusable components. This is done through an `evaluate` method that all `Action` methods share. The base class for all actions is located in `measurements/measurement_management.py`. When a complex measurement is finished, a highly nested construct of actions may export its internal data to a `.json` file. The high-rate experiment [analysis repositories](#) start with loading and analyzing these `.json` files.

[Entanglement control software repository](#)

Dark count rate through filters simulation

Based on the known lens f-number, aperture size, detector size, and filter transmissions for the dark count minimization project, the rate of dark counts due to transmitted blackbody photons can be estimated. With this simulation we determined that 4 thick custom short-pass filters, and one bandpass filter were ideal for our experiment.

[Dark count rate simulation repository](#)

B.3 SNSPhD

The SNSPhD python package includes a number of utility functions and presets used for managing data and generating figures for this thesis. It is based on the `phd` package from [Griffin Chure](#). Notably, it includes the `vis.phd_style()` function for setting up nice looking matplotlib defaults in my personal style, and the `viz.save_light_dark_all()` function for saving light-mode `svg`, dark-mode `svg`, and `pdf` versions of a figure. The `svgs` are used to populate the [thesis website](#), and the `pdfs` are used for the latex thesis itself. The `layout.bisect` function is also useful for laying out subfigures in a straightforward way.

The package can be installed with:

```
1 pip install snsphd
```

[SNSPhD package repository](#)

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